



INDIAN INSTITUTE OF SCIENCE, BENGALURU

DEPARTMENT OF ELECTRONIC SYSTEMS
ENGINEERING

DESIGN FOR ANALOG CIRCUITS
LABORATORY REPORT

ASSIGNMENT 7
ACTIVE FILTERS

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Contents

| | | |
|----------|-------------------------------|----------|
| 1 | Low Pass Filter | 1 |
| 1.1 | Aim | 1 |
| 1.2 | Schematic | 1 |
| 1.3 | Component Selection | 1 |
| 1.4 | Frequency Response | 1 |
| 1.5 | Transient Response | 2 |
| 2 | High Pass Filter | 3 |
| 2.1 | Aim | 3 |
| 2.2 | Schematic | 3 |
| 2.3 | Component Selection | 3 |
| 2.4 | Frequency Response | 3 |
| 2.5 | Transient Response | 4 |
| 3 | Band Pass Filter | 5 |
| 3.1 | Aim | 5 |
| 3.2 | Schematic | 5 |
| 3.3 | Component Selection | 5 |
| 3.4 | Frequency Response | 5 |
| 3.5 | Transient Response | 6 |
| 4 | Band Reject Filter | 7 |
| 4.1 | Aim | 7 |
| 4.2 | Schematic | 7 |
| 4.3 | Component Selection | 7 |
| 4.4 | Frequency Response | 7 |
| 4.5 | Transient Response | 8 |
| 5 | Conclusion | 8 |

List of Figures

| | | |
|----|--|---|
| 1 | LTSpice Schematic of Low Pass Filter | 1 |
| 2 | Frequency response of Low Pass Filter | 1 |
| 3 | Transient response of Low Pass Filter | 2 |
| 4 | LTSpice Schematic of High Pass Filter | 3 |
| 5 | Frequency response of High Pass Filter | 3 |
| 6 | Transient response of High Pass Filter | 4 |
| 7 | LTSpice Schematic of Band Pass Filter | 5 |
| 8 | Frequency response of Band Pass Filter | 5 |
| 9 | Transient response of Band Pass Filter | 6 |
| 10 | LTSpice Schematic of Band Reject Filter | 7 |
| 11 | Frequency response of Band Reject Filter | 7 |
| 12 | Transient response of Band Reject Filter | 8 |

1 Low Pass Filter

1.1 Aim

To perform transient and frequency domain simulations of active low pass filter.

1.2 Schematic

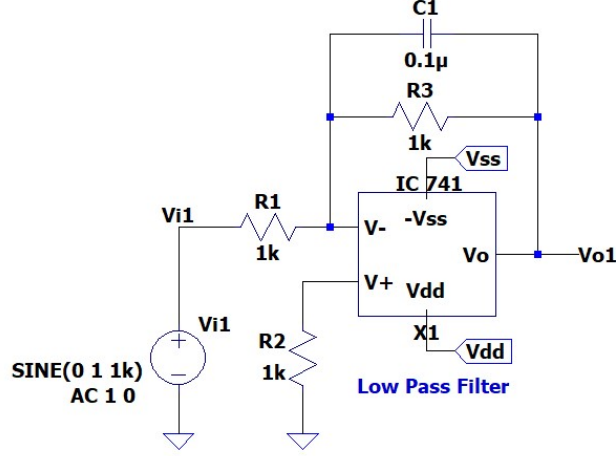


Figure 1: LTSpice Schematic of Low Pass Filter

1.3 Component Selection

The transfer function of the filter (assuming ideal op-amp) is given by

$$\frac{V_{o1}(s)}{V_{i1}(s)} = -\frac{R_3}{R_1} \frac{1}{1 + sR_3C_1} \quad (1)$$

The -3 dB cutoff frequency of the filter is $f_L = \frac{1}{2\pi R_3 C_1}$. For obtaining a cutoff frequency of 1.59 kHz=10 krad/s, we choose $R_1 = R_2 = R_3 = 1k\Omega$ and $C_1 = 0.1\mu F$.

1.4 Frequency Response

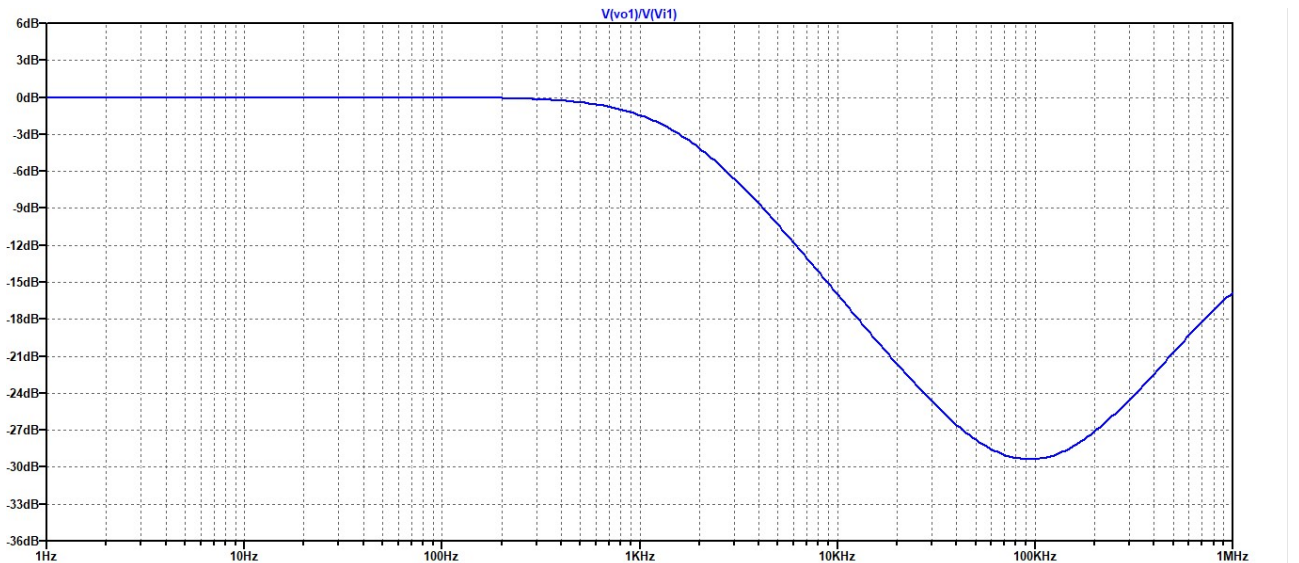


Figure 2: Frequency response of Low Pass Filter

The figure 2 above shows the frequency response of the low pass filter circuit. The -3 dB cutoff frequency obtained is 1589.89 Hz from LTSpice measurement.

1.5 Transient Response

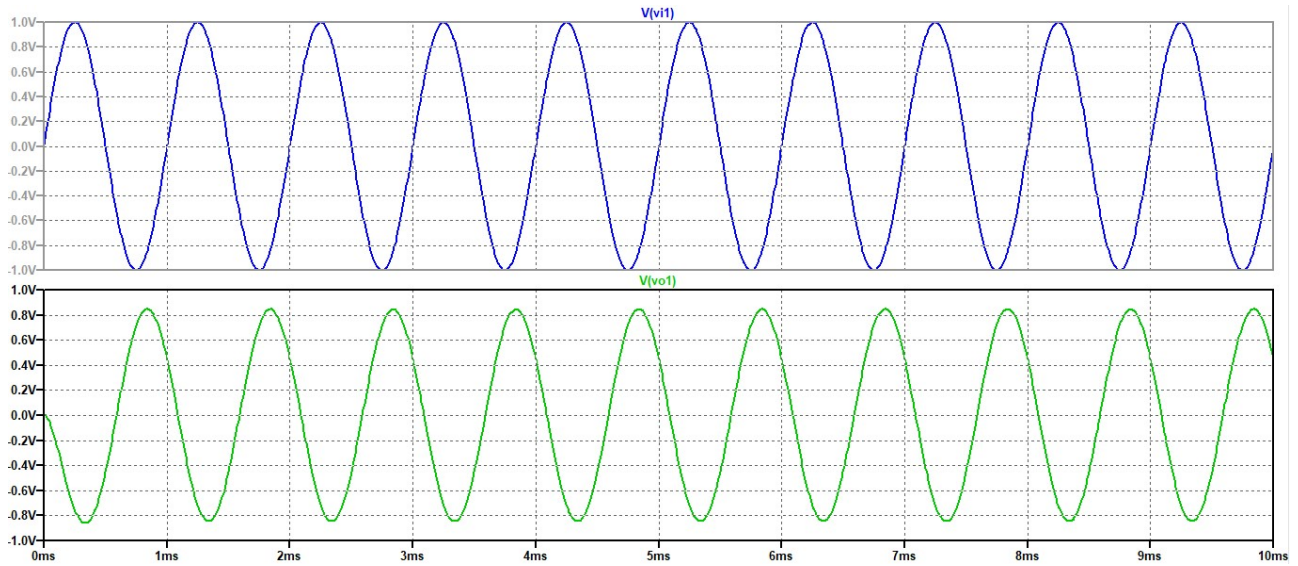


Figure 3: Transient response of Low Pass Filter

The figure 3 above shows the transient simulation results with $1V, 1kHz$ sinewave input. An output voltage of $0.846V$ is obtained.

2 High Pass Filter

2.1 Aim

To perform transient and frequency domain simulations of active high pass filter.

2.2 Schematic

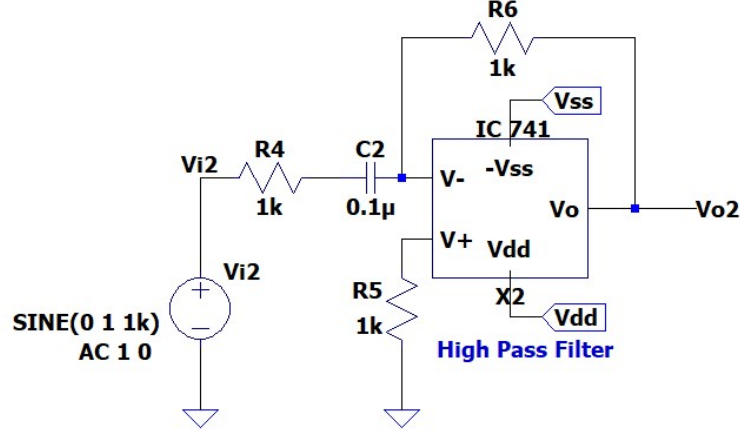


Figure 4: LTSpice Schematic of High Pass Filter

2.3 Component Selection

The transfer function of the filter (assuming ideal op-amp) is given by

$$\frac{V_{o2}(s)}{V_{i2}(s)} = -\frac{R_6}{R_4} \frac{sC_2R_4}{1 + sC_2R_4} \quad (2)$$

The -3 dB cutoff frequency of the filter is $f_L = \frac{1}{2\pi R_4 C_2}$. For obtaining $f_L = 1.59kHz = 10krad/s$, we choose $R_4 = R_5 = R_6 = 1k\Omega$ and $C_2 = 0.1\mu F$.

2.4 Frequency Response

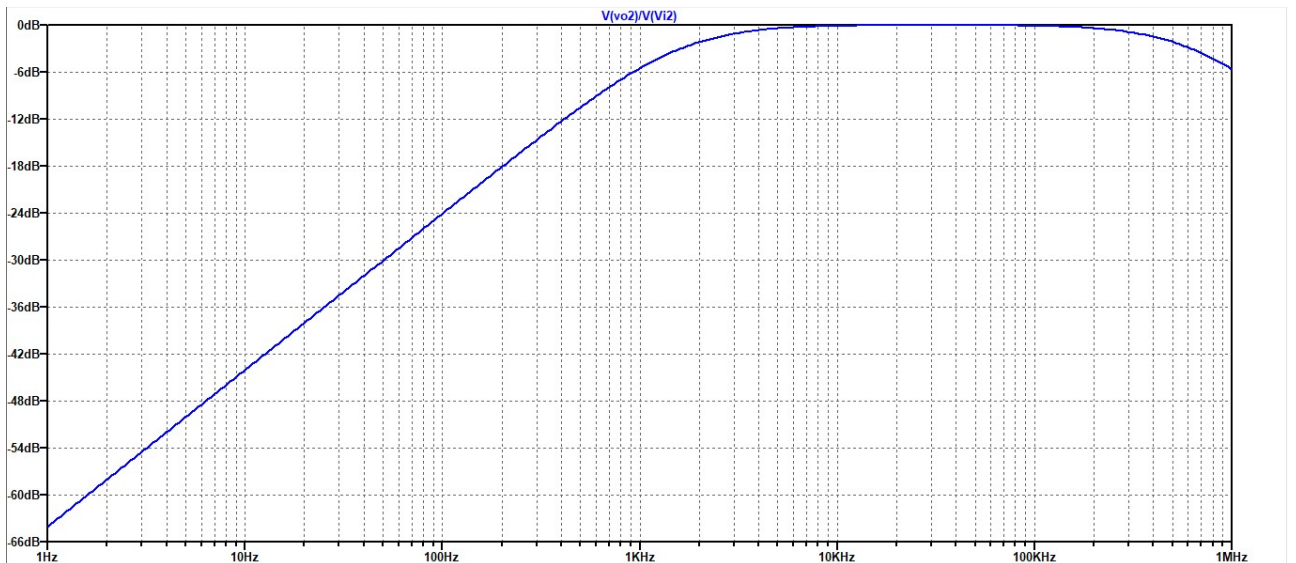


Figure 5: Frequency response of High Pass Filter

The figure 5 above shows the frequency response of the high pass filter circuit. The -3 dB cutoff frequency obtained is 1588.59 Hz.

2.5 Transient Response

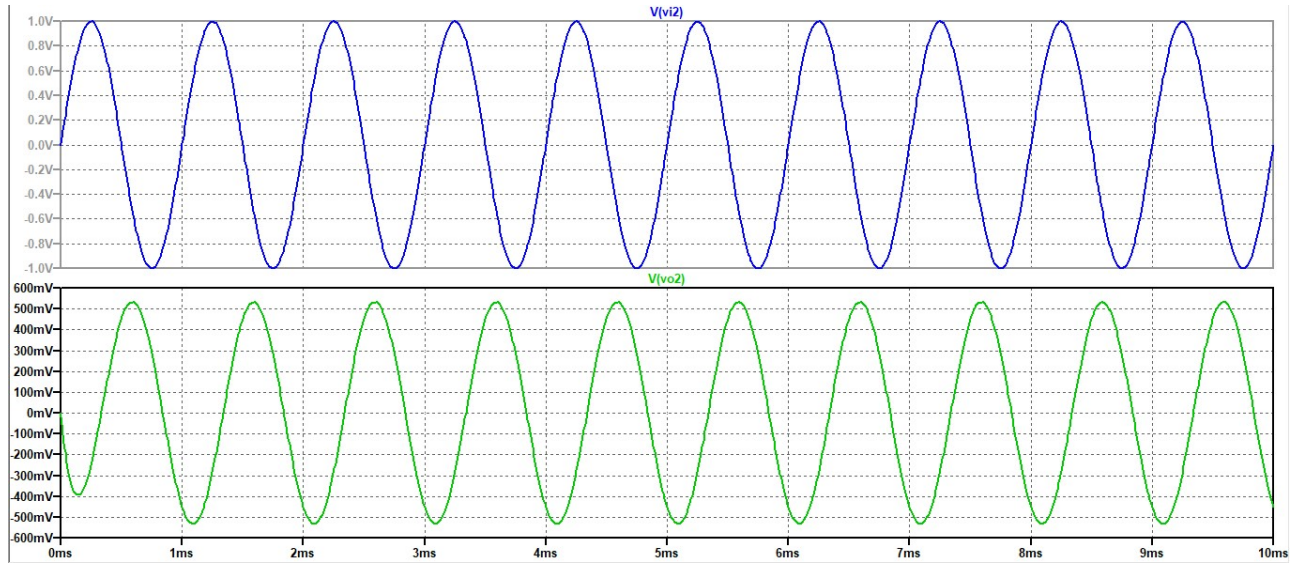


Figure 6: Transient response of High Pass Filter

The figure 6 above shows the transient simulation results with $1V, 1kHz$ sinewave input. An output voltage of $0.532V$ is obtained.

3 Band Pass Filter

3.1 Aim

To perform transient and frequency domain simulations of active band pass filter.

3.2 Schematic

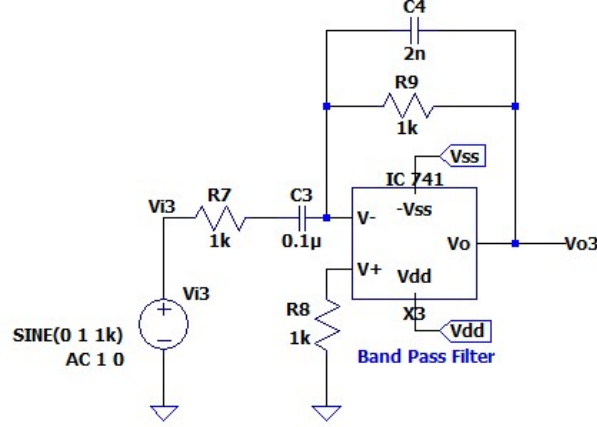


Figure 7: LTSpice Schematic of Band Pass Filter

3.3 Component Selection

The transfer function of the filter circuit (assuming ideal op-amp) is given by

$$\frac{V_{o3}(s)}{V_{i3}(s)} = -\frac{R_9}{R_7} \frac{1}{1 + sR_9C_4} \frac{sC_3R_7}{1 + sC_3R_7} \quad (3)$$

The -3 dB cutoff frequencies of the filter are $f_H = \frac{1}{2\pi R_9C_4}$ and $f_L = \frac{1}{2\pi R_7C_3}$, f_L and f_H being the lower and upper cutoff frequencies respectively. For obtaining $f_L = 1.59kHz = 10krad/s$ and $f_H = 80kHz = 502.7krad/s$, we choose $R_7 = R_8 = R_9 = 1k\Omega$, $C_3 = 0.1\mu F$ and $C_4 = 2nF$.

3.4 Frequency Response

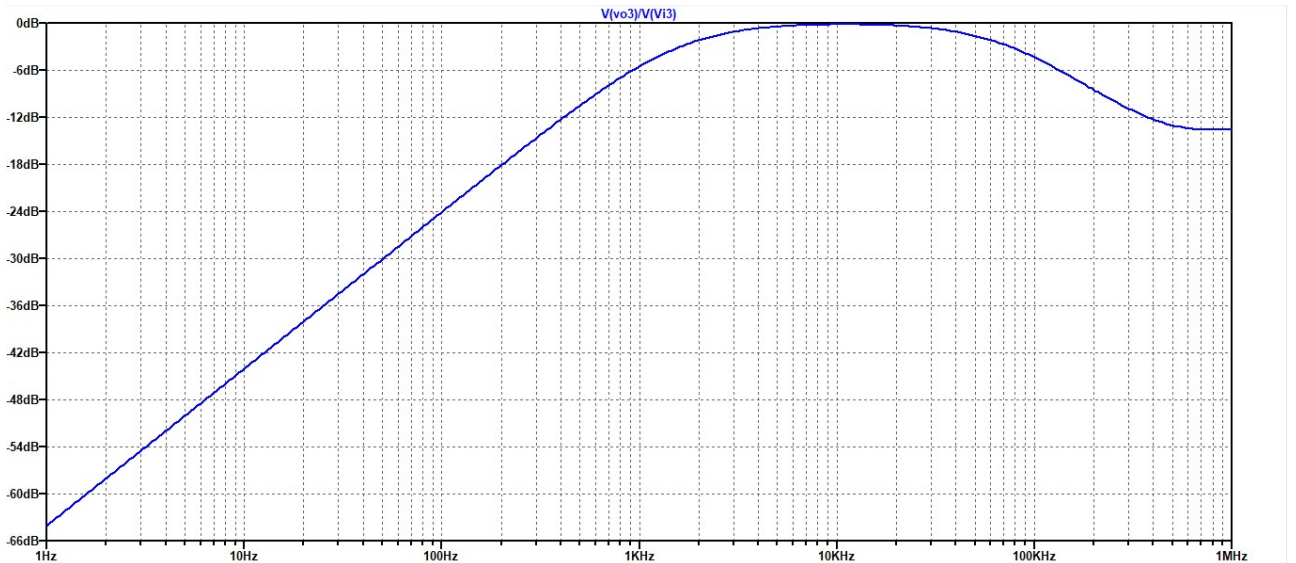


Figure 8: Frequency response of Band Pass Filter

The figure 8 above shows the frequency response of the band pass filter circuit. The -3 dB cutoff frequencies obtained are 1589.25 Hz and 75.393 kHz respectively.

3.5 Transient Response

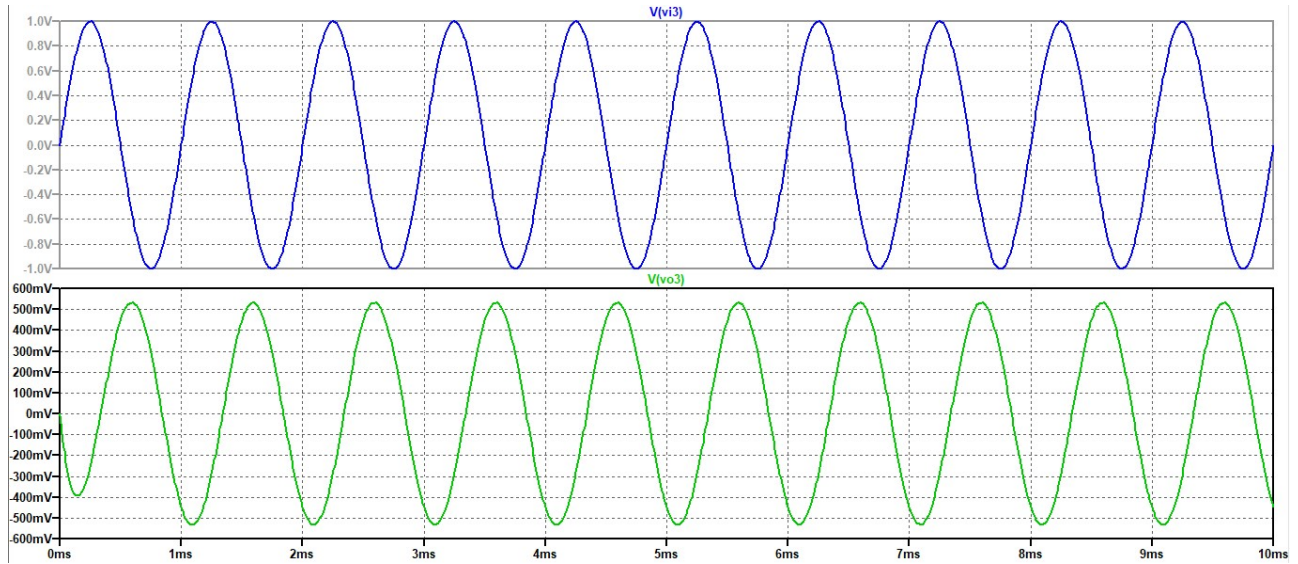


Figure 9: Transient response of Band Pass Filter

The figure 9 above shows the transient simulation results with 1V, 1kHz sinewave input. An output voltage of 0.532V is obtained.

4 Band Reject Filter

4.1 Aim

To perform transient and frequency domain simulations of active band reject filter.

4.2 Schematic

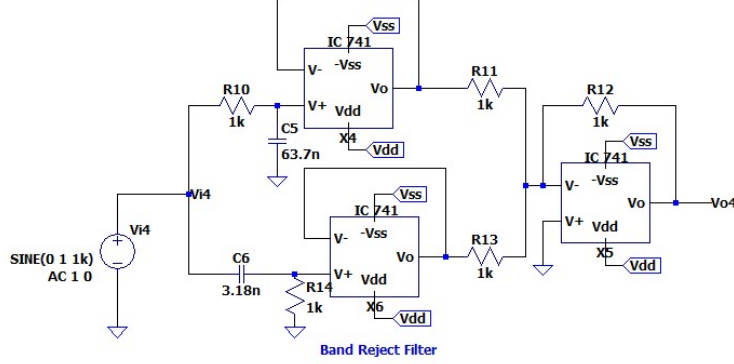


Figure 10: LTSpice Schematic of Band Reject Filter

4.3 Component Selection

The transfer function of the filter (assuming ideal op-amp and $R_{11} = R_{13}$) is given by

$$\frac{V_{o4}(s)}{V_{i4}(s)} = -\frac{R_{12}}{R_{11}} \left(\frac{1}{1 + sR_{10}C_5} + \frac{sR_{14}C_6}{1 + sR_{14}C_6} \right) \quad (4)$$

The -3 dB cutoff frequencies of the filter are $f_H = \frac{1}{2\pi R_{14}C_6}$ and $f_L = \frac{1}{2\pi R_{10}C_5}$, f_L and f_H being the lower and upper cutoff frequencies respectively. For obtaining $f_L = 2.5kHz = 15.71krad/s$ and $f_H = 50kHz = 314.16krad/s$, we choose $R_{10} = R_{11} = R_{12} = R_{13} = R_{14} = 1k\Omega$, $C_5 = 63.7nF$ and $C_6 = 3.18nF$.

4.4 Frequency Response

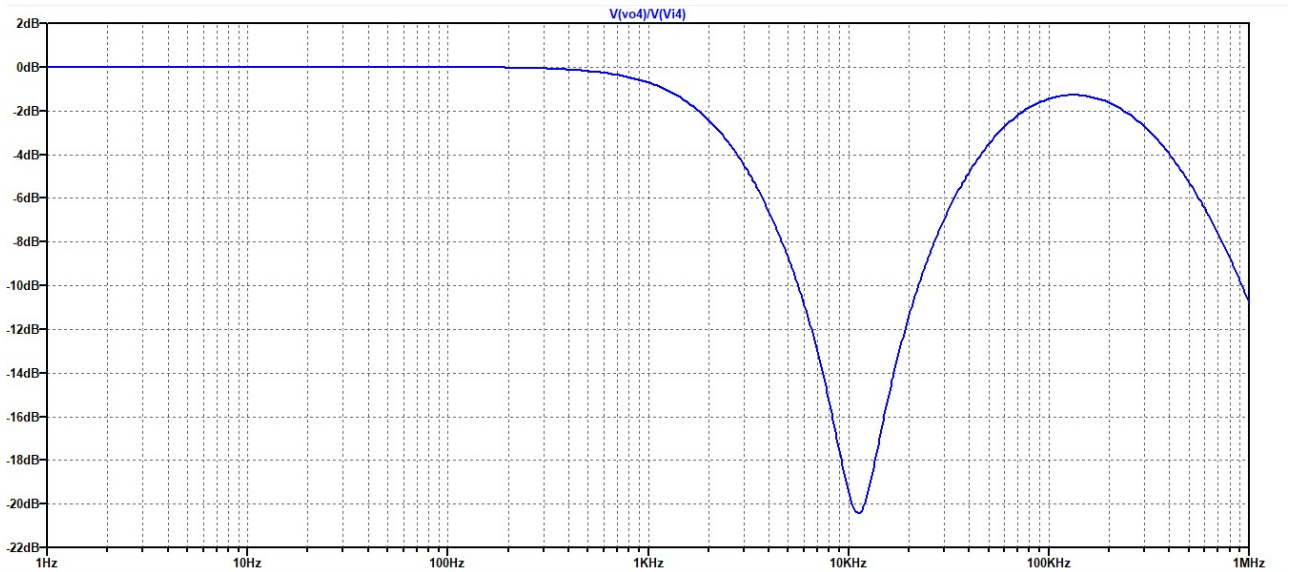


Figure 11: Frequency response of Band Reject Filter

The figure 11 above shows the frequency response of the band reject filter circuit. The -3 dB cutoff frequencies obtained are 2289.85 Hz and 55.823 kHz respectively.

4.5 Transient Response

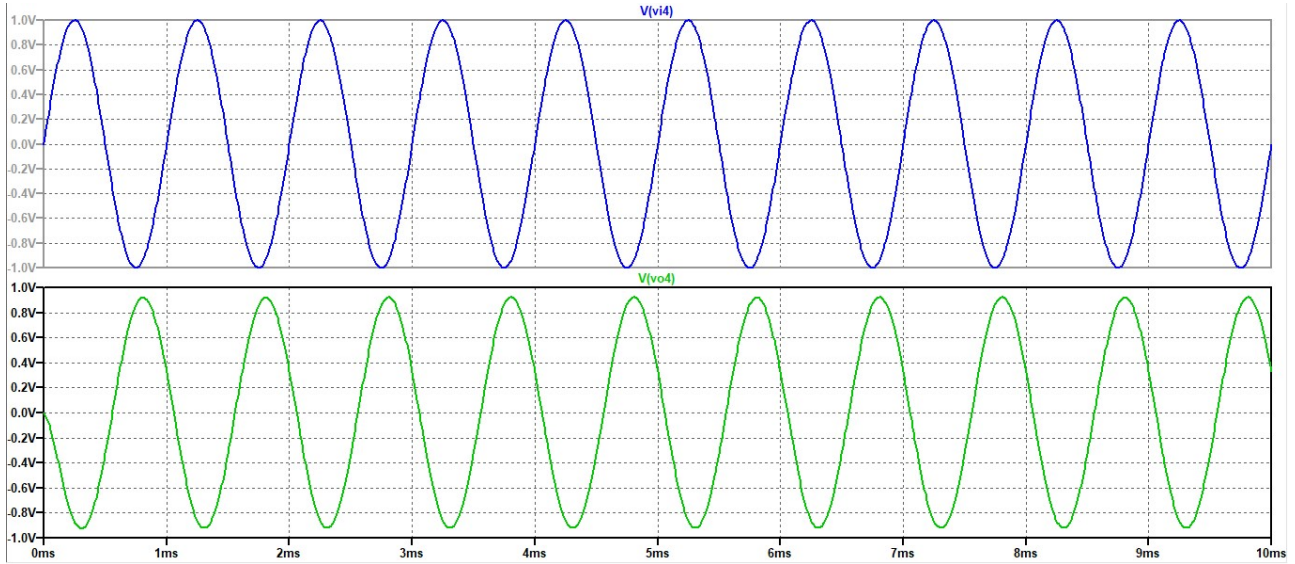


Figure 12: Transient response of Band Reject Filter

The figure 12 above shows the transient simulation results with 1V, 1kHz sinewave input. An output voltage of 0.922V is obtained.

5 Conclusion

- a The op-amp is a vital component of active filters. As a result, the performance of the filter depends largely on the op-amp parameters. Due to high frequency limitations of the op-amp the high-frequency response obtained is often not desirable (as evident from figures 5 and 11 respectively). The IC741 op-amp having an unity gain bandwidth of 1 MHz, its gain at frequencies higher than 10kHz is not good enough for the ideal op-amp approximations used to derive the transfer functions.
- b A very important advantage of active filters is that it can provide gain to the output signal, which is not possible with passive filters.
- c The active filter also eliminates usage of inductors, reducing the weight and footprint of the circuit.
- d Due to the high frequency limitations active filters cannot be used in RF applications. Also, the input and output voltage range is limited by the op-amp supply voltage levels.