

# Design for Analog Circuits - Laboratory Report

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Assignment 3

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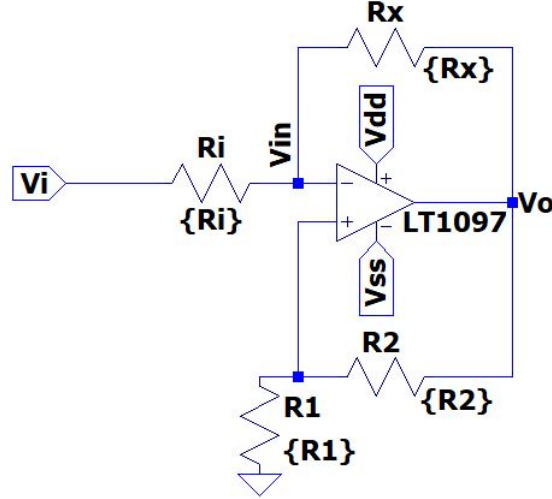
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# 1 Negative Impedance Converter

## 1.1 Aim

To perform DC sweep analysis of the Negative Impedance Converter Circuit provided and observe its performance.

## 1.2 Circuit Diagram



**.param R1=50 R2=10k Ri=400 Rx=20k**

Figure 1: LTSpice Schematic of Negative Impedance Converter

## 1.3 Theory

Assuming ideal op-amp, the voltage at both input nodes of the op-amp is  $V_{in}$ . Writing the KCL equation at the non-inverting terminal of the op-amp, we have:

$$\frac{V_o - V_{in}}{R_2} = \frac{V_{in}}{R_1}$$

or,  $V_o = V_{in}(1 + \frac{R_2}{R_1})$

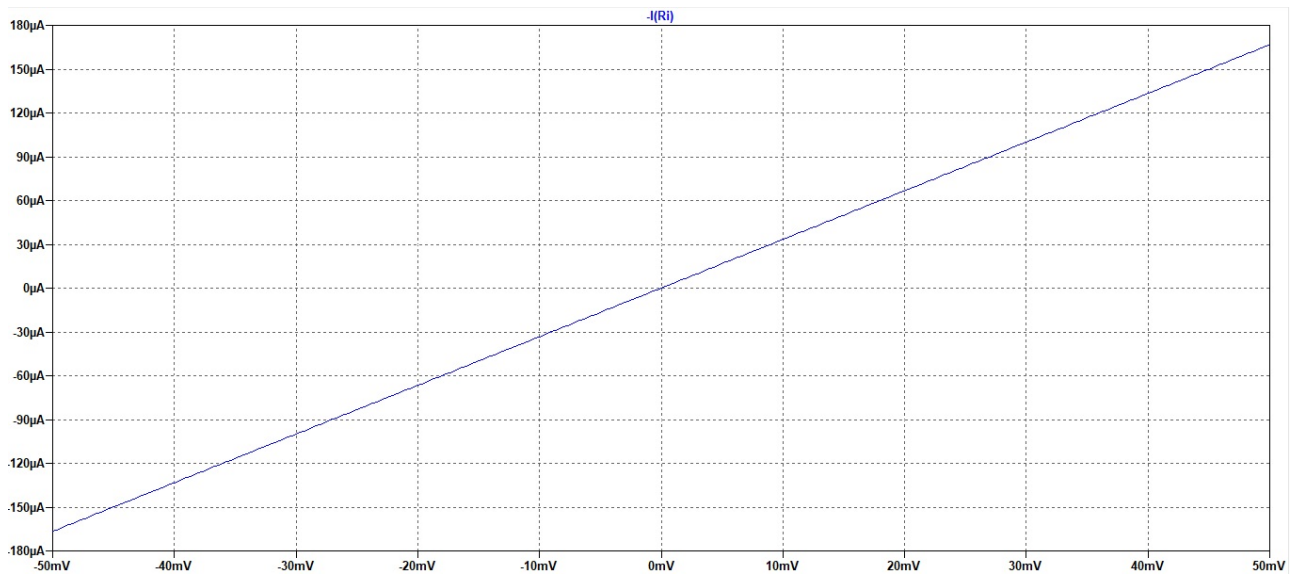
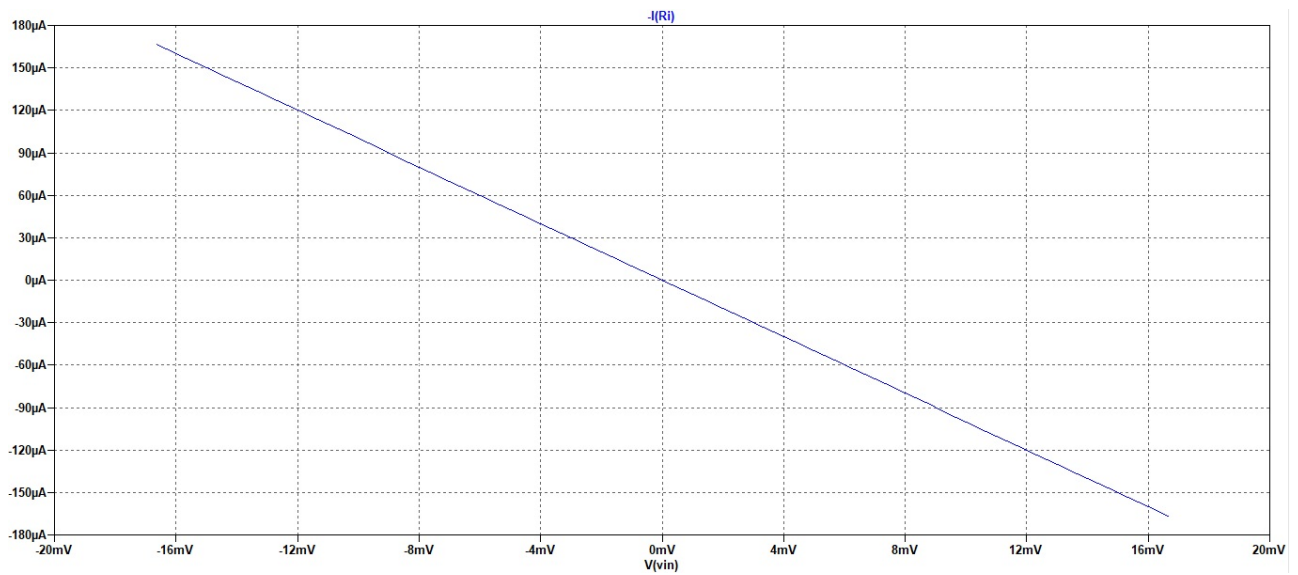
Current through  $R_i$  (and  $R_x$ ) is given by:

$$I_{R_1} = -V_{in}(\frac{R_2}{R_1 R_x})$$

So, looking at node  $V_{in}$  we should see an impedance of  $-R_x R_1 / R_2 = -100\Omega$ .

## 1.4 DC Sweep Simulation Results

The Figures 2 and 3 below show the DC sweep simulation plots of  $I_{R_i}$  versus  $V_i$  and  $V_{in}$  respectively. The slope of  $I_{R_i}$  versus  $V_{in}$  comes out to be  $-99.99\Omega$ .

Figure 2:  $I_{R_i}$  vs  $V_i$  for negative impedance converterFigure 3:  $I_{R_i}$  vs  $V_{in}$  for negative impedance converter

## 2 Instrumentation Amplifier

### 2.1 Aim

To perform transient simulation of the Instrumentation Amplifier circuit provided and observe its differential and common mode response. ‘

### 2.2 Schematic

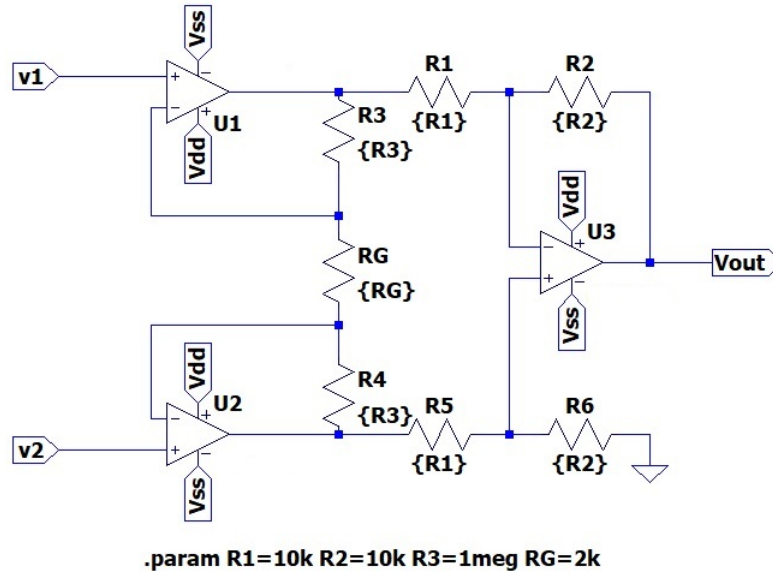


Figure 4: LTSpice Schematic of Instrumentation Amplifier

### 2.3 Theory

The gain of the instrumentation amplifier should be

$$\frac{V_{out}}{V_2 - V_1} = \left(1 + \frac{2R_3}{R_G}\right) \frac{R_2}{R_1}$$

For the parameters provided we get a value of 1001 for the gain.

### 2.4 Transient Simulation Results

The figure 5 shows the transient simulation results of the instrumentation amplifier with a 10 mV 1 kHz sinewave differential input and 5 V DC common mode input. The output sinewave amplitude is 9.95 V and the DC amplitude is  $2 \times 10^{-5}$  V. The differential gain is 995 and the common mode gain is  $4 \times 10^{-6}$ .

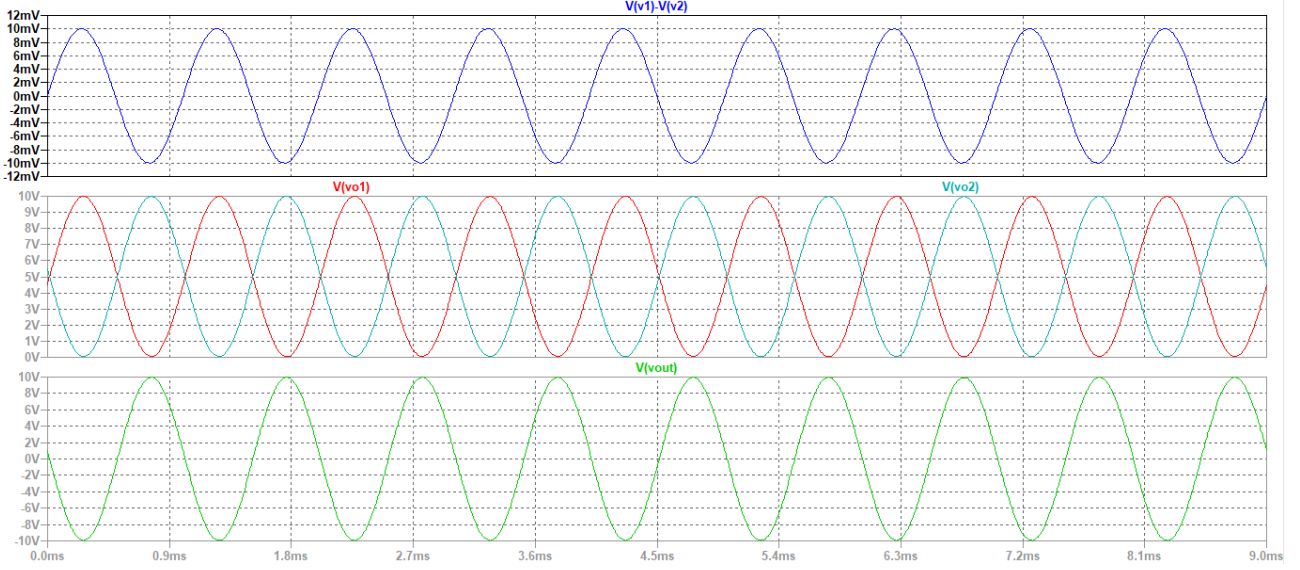


Figure 5: Transient Simulation of Instrumentation amplifier

### 3 Conclusion

1. The negative impedance converter reduces the effective resistance of the voltage source  $V_i$  from  $400\Omega$  to  $300\Omega$ . But the problem with the circuit is that it will not work for values of  $R_i$  below  $100\Omega$ . The reason is as follows:  
The positive and negative feedback factors for the circuit are

$$\text{Positive feedback factor} = \frac{R_1}{R_1 + R_2} \simeq \frac{50}{10000}$$

$$\text{Negative feedback factor} = \frac{R_i}{R_i + R_x} \simeq \frac{200}{10000}$$

If the value of  $R_i$  is less than  $100\Omega$ , the circuit will be in positive feedback and hence will not function as negative impedance converter.

2. The instrumentation amplifier gain is not evenly distributed between the two stages. The input stage has a gain of 1001 whereas the output stage has a gain of 1. In the simulation results referred above the universal op-amp block of LTSpice has been used, and a good gain is obtained ( $\simeq 995$ ); but with a practical op-amp model there will be loss of gain (gain observed with LT 1097 op-amp is  $\simeq 558$ ).