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C*****
C****
C**** SIMULATION OF TWO-PHASE OIL-WATER FLOW IN A HORIZONTAL
C**** ONE-DIMENSIONAL SYSTEM USING THE IMPES FORMULATION AND
C**** GAUSSIAN ELIMINATION
C****
C**** MAXIMUM NUMBER OF GRID BLOCKS IS CURRENTLY SET AT 100
C*****
PROGRAM OW

C
C-----DECLARATIONS
C
INTEGER EN,I,J,K,N,NULL
REAL*8 LAMOM,LAMOP,LAMWM,LAMWP
REAL*8 PERM(100),PHI(100),DX(100),X(100)
REAL*8 SWT(100),KROT(100),KRWT(100),PCT(100)
REAL*8 KRO(100),KRW(100),PCOW(100),DPCOW(100)
REAL*8 PT(100),BOT(100),BWT(100),MUOT(100),MUWT(100)
REAL*8 BO(100),BW(100),DBO(100),DBW(100),MUO(100),MUW(100)
REAL*8 SW(100),PO(100),PONEW(100),PW(100),LAMO(100),LAMW(100)
REAL*8 TXOP(100),TXOM(100),TXWP(100),TXWM(100)
REAL*8 CPOO(100),CPOW(100),CSWO(100),CSWW(100)
REAL*8 A(100),B(100),C(100),D(100)
REAL*8 AREA,SWI,CR,T,DT,TMAX,PINIT,PR,PL,QWI,ALFA

C
CHARACTER*8 PHEAD(103)
DATA PHEAD/" TIME ","PL ","
*"P( 1) ","P( 2) ","P( 3) ","
*"P( 4) ","P( 5) ","P( 6) ","P( 7) ","P( 8) ","
*"P( 9) ","P(10) ","P(11) ","P(12) ","P(13) ","
*"P(14) ","P(15) ","P(16) ","P(17) ","P(18) ","
*"P(19) ","P(20) ","P(21) ","P(22) ","P(23) ","
*"P(24) ","P(25) ","P(26) ","P(27) ","P(28) ","
*"P(29) ","P(30) ","P(31) ","P(32) ","P(33) ","
*"P(34) ","P(35) ","P(36) ","P(37) ","P(38) ","
*"P(39) ","P(40) ","P(41) ","P(42) ","P(44) ","
*"P(44) ","P(45) ","P(46) ","P(47) ","P(48) ","
*"P(49) ","P(50) ","P(51) ","P(52) ","P(55) ","
*"P(54) ","P(55) ","P(56) ","P(57) ","P(58) ","
*"P(59) ","P(60) ","P(61) ","P(62) ","P(66) ","
*"P(64) ","P(65) ","P(66) ","P(67) ","P(68) ","
*"P(69) ","P(70) ","P(71) ","P(72) ","P(77) ","
*"P(74) ","P(75) ","P(76) ","P(77) ","P(78) ","
*"P(79) ","P(80) ","P(81) ","P(82) ","P(88) ","
*"P(84) ","P(85) ","P(86) ","P(87) ","P(88) ","
*"P(89) ","P(90) ","P(91) ","P(92) ","P(99) ","
*"P(94) ","P(95) ","P(96) ","P(97) ","P(98) ","
*"P(99) ","P(100) ","PR "/"

C
CHARACTER*8 SHEAD(101)
DATA SHEAD/" TIME ","SW( 1) ","SW( 2) ","SW( 3) ","
*"SW( 4) ","SW( 5) ","SW( 6) ","SW( 7) ","SW( 8) ","
*"SW( 9) ","SW(10) ","SW(11) ","SW(12) ","SW(13) ","
*"SW(14) ","SW(15) ","SW(16) ","SW(17) ","SW(18) ","
*"SW(19) ","SW(20) ","SW(21) ","SW(22) ","SW(23) ","
*"SW(24) ","SW(25) ","SW(26) ","SW(27) ","SW(28) ","
*"SW(29) ","SW(30) ","SW(31) ","SW(32) ","SW(33) ","
*"SW(34) ","SW(35) ","SW(36) ","SW(37) ","SW(38) ","
*"SW(39) ","SW(40) ","SW(41) ","SW(42) ","SW(44) ","
*"SW(44) ","SW(45) ","SW(46) ","SW(47) ","SW(48) ","
*"SW(49) ","SW(50) ","SW(51) ","SW(52) ","SW(55) ","
*"SW(54) ","SW(55) ","SW(56) ","SW(57) ","SW(58) "

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      *"SW(59)  ", "SW(60)  ", "SW(61)  ", "SW(62)  ", "SW(66)  ",
      *"SW(64)  ", "SW(65)  ", "SW(66)  ", "SW(67)  ", "SW(68)  ",
      *"SW(69)  ", "SW(70)  ", "SW(71)  ", "SW(72)  ", "SW(77)  ",
      *"SW(74)  ", "SW(75)  ", "SW(76)  ", "SW(77)  ", "SW(78)  ",
      *"SW(79)  ", "SW(80)  ", "SW(81)  ", "SW(82)  ", "SW(88)  ",
      *"SW(84)  ", "SW(85)  ", "SW(86)  ", "SW(87)  ", "SW(88)  ",
      *"SW(89)  ", "SW(90)  ", "SW(91)  ", "SW(92)  ", "SW(99)  ",
      *"SW(94)  ", "SW(95)  ", "SW(96)  ", "SW(97)  ", "SW(98)  ",
      *"SW(99)  ", "SW(100)  "/"

C
      EN=1
      NULL=0

C
C----READ SYSTEM DATA FROM FILE SYST.DAT
C
      OPEN(12,FILE='SYST.DAT')
      READ(12,*)
C----USO AND USW ARE UPSTREAM WEIGHTING FACTORS FOR OIL AND WATER
C-----1.0 IS UPSTREAM
C-----0.0 OS DOWNSTREAM
C-----SHOULD BE A VALUE BETWEEN 0.0 AND 1.0 (STANDARD IS 1.0)
      READ(12,*)USO,USW
      READ(12,*)AREA
      READ(12,*)N
      READ(12,*)(DX(I),I=1,N)
      READ(12,*)(PHI(I),I=1,N)
      READ(12,*)(PERM(I),I=1,N)
      READ(12,*)SWI
      READ(12,*)CR
      READ(12,*)DT
      READ(12,*)TMAX
      READ(12,*)PINIT
      READ(12,*)PR
      READ(12,*)PL
      READ(12,*)QWI
      CLOSE(12)

C
C----GENERATE X-POSITIONS
C
      X(1)=DX(1)/2.
      DO 9 I=2,N
        9 X(I)=X(I-1)+(DX(I-1)+DX(I))/2.

C
C----DETERMINE WHICH LEFT SIDE BOUNDARY CONDIION TO BE USED
C----IF CONSTANT INJECTION RATE, IBC=2
C----IF CONSTANT LEFT SIDE PRESSURE, IBC=1
C
      IF(PL.NE.0.)THEN
        QWI=0.
        IBC=1
      ELSE
        IBC=2
      ENDIF

C
      QOP=0.
      WC=0.

C
      PHEAD(N+3)="PR      "

C
C----READ TABLES FOR RELATIVE PERMEABILITIES AND CAPILLARY PRESSURES
C----FROM INPUT DATA FILE DATA FILE SAT.DAT
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        OPEN(10,FILE='SAT.DAT')
        READ(10,*)NSAT,PCMULT
        READ(10,*)
        DO 10 J=1,NSAT
        READ(10,*)SWT(J),KROT(J),KRWT(J),PCT(J)
10    CONTINUE
        CLOSE(10)
C
        DO 11 J=1,NSAT
        11    PCT(J)=PCT(J)*PCMULT
C-----READ PVT DATA FROM INPUT DATA FILE PVT.DAT
C
        OPEN(11,FILE='PVT.DAT')
        READ(11,*)NPVT
        READ(11,*)
        DO 20 J=1,NPVT
        READ(11,*)PT(J),BOT(J),BWT(J),MUOT(J),MUWT(J)
C
C-----CONVERT BO AND BW TO 1/BO OG 1/BW
C
        BOT(J)=1./BOT(J)
        BWT(J)=1./BWT(J)
        20    CONTINUE
        CLOSE(11)
C
C-----OPEN FILES FOR PRINTOUT AND WRITE HEADINGS
C----- (PO.OUT FOR OIL PRESSURES, SW.OUT FOR WATER SATURATIONS
C----- AND WELLS.OUT FOR PRODUCTION/INJECTION RESULTS)
C
        OPEN(13,FILE='PO.OUT')
        WRITE(13,2001)(PHEAD(I),I=1,N+3)
        WRITE(13,2007)(X(I),I=1,N)
        2001    FORMAT(' TIME, RATES AND OIL PRESSURES',/,2X,100A8)
        OPEN(14,FILE='SW.OUT')
        WRITE(14,2002)(SHEAD(I),I=1,N+1)
        WRITE(14,2007)(X(I),I=1,N)
        2002    FORMAT(' TIME AND WATER SATURATIONS',/,2X,100A8)
        OPEN(15,FILE='WELLS.OUT')
        WRITE(15,2003)
        2003    FORMAT(' PRODUCTION/INJECTION RESULTS',/,
        * ' TIME PL QWI PR QOP QWP WC')
        2007    FORMAT(5X," X=",100F8.2)
C
C-----INITIALIZATION
C
        T=0.
        DO 30 I=1,N
        PO(I)=PINIT
        SW(I)=SWI
        30    CONTINUE
        IF(IBC.EQ.2)PL=PO(1)
C
C-----TIME LOOP
C
        DO 1000 J=1,1000
C
C-----PRINTOUT OF TIME, PRESSURES, SATURATIONS AND PROD/INJ
C
        WRITE (13,2004)T,PL,(PO(I),I=1,N),PR
        2004    FORMAT(103F8.2)
        WRITE (14,2005)T,(SW(I),I=1,N)
        2005    FORMAT(F8.2,101F8.4)

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        WRITE (15,2006)T,PL,QWI,PR,QOP,QWP,WC
2006  FORMAT(7F8.2)
C
        T=T+DT
C
C-----END OF RUN ?
C
        IF(T.GT.TMAX)GO TO 1001
C
C-----INTERPOLATE IN INPUT DATA TABLES
C-----FOR SATURATION DEPENDENT PROPERTIES (KRO, KRW, PCOW)
C-----AND PRESSURE DEPENDENT PROPERTIES (BO, BW, MUO, MUW)
C
        DO 100 I=1,N
C
C-----FIND REL. PERM. FOR OIL
C
        CALL INTERP(SW(I),KRO(I),DUMMY,NULL,NSAT,SWT,KROT)
C
C-----FIND REL. PERM. FOR WATER
C
        CALL INTERP(SW(I),KRW(I),DUMMY,NULL,NSAT,SWT,KRWT)
C
C-----FIND PC AND ITS DERIVATIVE
C
        CALL INTERP(SW(I),PCOW(I),DPCOW(I),EN,NSAT,SWT,PCT)
C
C-----FIND (1/BO) AND ITS DERIVATIVE
C
        CALL INTERP(PO(I),BO(I),DBO(I),EN,NPVT,PT,BOT)
C
C-----FIND (1/BW) AND ITS DERIVATIVE
C
        PW(I)=PO(I)-PCOW(I)
        CALL INTERP(PW(I),BW(I),DBW(I),EN,NPVT,PT,BWT)
C
C-----FIND OIL VISCOSITY
C
        CALL INTERP(PO(I),MUO(I),DUMMY,NULL,NPVT,PT,MUOT)
C
C-----FIND WATER VISCOSITY
C
        CALL INTERP(PW(I),MUW(I),DUMMY,NULL,NPVT,PT,MUWT)
C
C-----COMPUTE MOBILITY TERMS
C
        LAMO(I)=KRO(I)*BO(I)/MUO(I)
        LAMW(I)=KRW(I)*BW(I)/MUW(I)
100  CONTINUE
C
C-----LOOP FOR GRID BLOCKS
C
        DO 200 I=1,N
C
        IF(I.NE.1)THEN
            LAMOM=LAMO(I-1)*USO+LAMO(I)*(1.-USO)
            LAMWM=LAMW(I-1)*USW+LAMW(I)*(1.-USW)
            IF (PO(I-1).LT.PO(I)) LAMOM=LAMO(I)*USO+LAMO(I-1)*(1.-USO)
            IF (PW(I-1).LT.PW(I)) LAMWM=LAMW(I)*USW+LAMW(I-1)*(1.-USW)
        ELSE
            LAMOM=LAMO(I)
            LAMWM=LAMW(I)

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ENDIF
IF(I.NE.N)THEN
    LAMOP=LAMO(I)*USO+LAMO(I+1)*(1.-USO)
    LAMWP=LAMW(I)*USW+LAMW(I+1)*(1.-USW)
    IF(PO(I+1).GT.PO(I))LAMOP=LAMO(I+1)*USO+LAMO(I)*(1.-USO)
    IF(PW(I+1).GT.PW(I))LAMWP=LAMW(I+1)*USW+LAMW(I)*(1.-USW)
ELSE
    LAMOP=LAMO(I)
    LAMWP=LAMW(I)
ENDIF
C-----TRANSMISSIBILITIES
IF(I.NE.1)THEN
    TXOM(I)=2.*LAMOM/(DX(I)/PERM(I)+DX(I-1)/PERM(I-1))/DX(I)
    TXWM(I)=2.*LAMWM/(DX(I)/PERM(I)+DX(I-1)/PERM(I-1))/DX(I)
ELSE
    TXOM(I)=2.*LAMOM/DX(I)*PERM(I)/DX(I)
    TXWM(I)=2.*LAMWM/DX(I)*PERM(I)/DX(I)
C-----INJECTION OF WATER AT LEFT SIDE
C-----REQUIRES SUM OF TRANSMISSIBILITIES
    TXWM(I)=TXWM(I)+TXOM(I)
ENDIF
C
IF(I.NE.N)THEN
    TXWP(I)=2.*LAMWP/(DX(I+1)/PERM(I+1)+DX(I)/PERM(I))/DX(I)
    TXOP(I)=2.*LAMOP/(DX(I+1)/PERM(I+1)+DX(I)/PERM(I))/DX(I)
ELSE
    TXOP(I)=2.*LAMOP/DX(I)*PERM(I)/DX(I)
    TXWP(I)=2.*LAMWP/DX(I)*PERM(I)/DX(I)
ENDIF
C-----STORAGE COEFFICIENTS
CPOO(I)=(1.-SW(I))*PHI(I)*(CR*BO(I)+DBO(I))/DT
CSWO(I)=-PHI(I)*BO(I)/DT
CPOW(I)=SW(I)*PHI(I)*(CR*BW(I)+DBW(I))/DT
CSWW(I)=PHI(I)*BW(I)/DT-CPOW(I)*DPCOW(I)
C-----MATRIX COEFFICIENTS
ALFA=-CSWO(I)/CSWW(I)
A(I)=TXOM(I)+ALFA*TXWM(I)
C(I)=TXOP(I)+ALFA*TXWP(I)
IF(I.NE.1)THEN
    B(I)=-(TXOP(I)+TXOM(I)+CPOO(I))
*    -(TXWP(I)+TXWM(I)+CPOW(I))*ALFA
ENDIF
IF(I.NE.N.AND.I.NE.1)THEN
    D(I)=-(CPOO(I)+ALFA*CPOW(I))*PO(I)
*    +ALFA*(TXWP(I)*(PCOW(I+1)-PCOW(I))
*    +TXWM(I)*(PCOW(I-1)-PCOW(I)))
ENDIF
IF(I.EQ.1.AND.IBC.EQ.2)THEN
    D(I)=-(CPOO(I)+ALFA*CPOW(I))*PO(I)
*    +ALFA*(TXWP(I)*(PCOW(I+1)-PCOW(I))+QWI/DX(I)/AREA)
    B(I)=-(TXOP(I)+CPOO(I))
*    -(TXWP(I)+CPOW(I))*ALFA
ENDIF
IF(I.EQ.1.AND.IBC.EQ.1)THEN
    D(I)=-(CPOO(I)+ALFA*CPOW(I))*PO(I)
*    +ALFA*(TXWP(I)*(PCOW(I+1)-PCOW(I))+TXWM(I)*(PL+PCOW(1)))
    B(I)=-(TXOP(I)+CPOO(I))
*    -(TXWP(I)+TXWM(I)+CPOW(I))*ALFA
ENDIF
IF(I.EQ.N)THEN
    D(I)=-(CPOO(I)+ALFA*CPOW(I))*PO(I)

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      *      -(TXOP(I)+ALFA*TXWP(I))*PR
      *      +ALFA*TXWM(I)*(PCOW(I-1)-PCOW(I))
      ENDIF
200  CONTINUE
C
C----PRESSURE SOLUTION
C
      CALL TRIDIA(N,A,B,C,D,PONEW)
C
C----SATURATION SOLUTION
C
      DO 300 I=1,N
      IF(I.NE.N.AND.I.NE.1)SW(I)=SW(I)+(TXOP(I)*(PONEW(I+1)-PONEW(I))
      *      +TXOM(I)*(PONEW(I-1)-PONEW(I))
      *      -CPOO(I)*(PONEW(I)-PO(I)))/CSWO(I)
      IF(I.EQ.N)SW(I)=SW(I)+(TXOP(I)*(PR-PONEW(I))
      *      +TXOM(I)*(PONEW(I-1)-PONEW(I))
      *      -CPOO(I)*(PONEW(I)-PO(I)))/CSWO(I)
      IF(I.EQ.1)SW(I)=SW(I)+(TXOP(I)*(PONEW(I+1)-PONEW(I))
      *      -CPOO(I)*(PONEW(I)-PO(I)))/CSWO(I)
300  CONTINUE
C
C----UPDATE PRESSURES
C
      DO 400 I=1,N
      PO(I)=PONEW(I)
400  CONTINUE
C
C----COMPUTE PL IF IBC=2
C
      IF(IBC.EQ.2)PL=PO(1)-PCOW(1)-QWI/DX(1)/AREA/TXWM(1)
C
C----COMPUTE QWI IF IBC=1
C
      IF(IBC.EQ.1)QWI=(PO(1)-PCOW(1)-PL)*DX(1)*AREA*TXWM(1)
C
C----COMPUTE QOP, QWP AND WC
C
      QOP=-(PR-PO(N))*DX(N)*AREA*TXOP(N)
      QWP=-(PR-PO(N)+PCOW(N))*DX(N)*AREA*TXWP(N)
      WC=QWP/(QWP+QOP)
C
1000 CONTINUE
1001 CONTINUE
      END
C
C----SUBROUTINE FOR INTERPOLATION OF DATA FROM INPUT TABLE
C
      SUBROUTINE INTERP(X,Y,DY,ISW,N,XT,YT)
C
C-----
C      THE ROUTINE SEARCHES IN THE TABLE AND CONDUCTS LINEAR INTERPO-
C      LATION IN ORDER TO DETERMINE Y IN POINT X, AND ITS DERIVATIVE
C      IF ISW.NE.0
C      IF THE ARGUMENT (X) IS OUTSIDE THE TABLE, ENPOINTS ARE USED
C
C      X=ARGUMENT
C      Y=INTERPOLATED VALUE
C      DY=COMPUDED DERIVATIVE OF Y
C      ISW=0 IF DERIVATIVE IS NOT TO BE COMPUTED
C      N=NUMBER OF ENTRIES IN TABLE
C      XT=INDEPENDENT TABLE VARIABLE

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C      YT=DEPENDENT TABLE VARIABLE
C-----
C
C      IMPLICIT REAL*8(A-H,O-Z)
C      REAL*8 X,Y,DY,XT(100),YT(100)
C
C-----IF X IS GREATER THAN LARGEST TABLE VALUE
C
C      IF(X.LT.XT(N)) GOTO 10
C      Y=YT(N)
C      IF(ISW.NE.0)DY=(YT(N)-YT(N-1))/(XT(N)-XT(N-1))
C      RETURN
C
C-----IF X IS LESS THAN THE SMALLEST TABLE VALUE
C
C      10 IF(X.GT.XT(1)) GOTO 11
C      Y=YT(1)
C      IF(ISW.NE.0)DY=(YT(2)-YT(1))/(XT(2)-XT(1))
C      RETURN
C
C-----IN GENERAL
C
C      11 DO 20 I=2,N
C      IF(X.GE.XT(I)) GO TO 20
C      Y=YT(I-1) +(X-XT(I-1))*(YT(I)-YT(I-1))/(XT(I)-XT(I-1))
C      IF(ISW.NE.0)DY=(YT(I)-YT(I-1))/(XT(I)-XT(I-1))
C      RETURN
C      20 CONTINUE
C      RETURN
C      END
C
C-----SUBROUTINE FOR GAUSSIAN ELIMINATION
C
C      SUBROUTINE TRIDIA(N,A,B,C,D,P)
C-----
C      THE SUBROUTINE USES GAUSSIAN ELIMINATION FOR SOLUTION OF THE
C      SET OF EQUATIONS
C
C      
$$A(I)*P(I-1) + B(I)*P(I) + C(I)*P(I+1) = D(I)$$

C
C      A(I),B(I),C(I),D(I)=MATRIX COEFFICIENTS
C      P=PRESSURE
C      N=NUMBER OF EQUATIONS
C-----
C
C      REAL*8 A(100),B(100),C(100),D(100),P(100),BB(100),DD(100),X
C      BB(1)=B(1)
C      DD(1)=D(1)
C      DO 60 I=2,N
C      X=A(I)/BB(I-1)
C      BB(I)=B(I)-X*C(I-1)
C      60 DD(I)=D(I)-X*DD(I-1)
C      P(N)=DD(N)/BB(N)
C      DO 70 K=2,N
C      I=N-K+1
C      70 P(I)=(DD(I)-C(I)*P(I+1))/BB(I)
C      RETURN
C      END

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