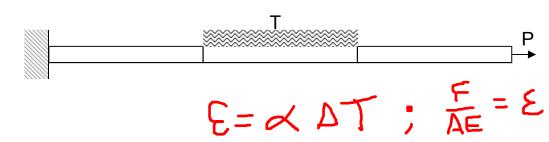
Carga Térmica

Análisis



1) Elemento completamente restringido

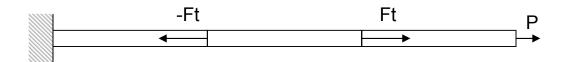


$$F_t = \alpha A E \Delta T \qquad \sigma_0 = -\alpha E \Delta T$$

$$\sigma_0 = -\alpha E \Delta T$$



2) Armar estructura



3) Resolver
$$\frac{AE}{L} \begin{bmatrix} 1 & -1 & 0 & 0 \\ -1 & 2 & -1 & 0 \\ 0 & -1 & 2 & -1 \\ 0 & 0 & -1 & 1 \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \\ u_3 \\ u_4 \end{bmatrix} = \begin{cases} F_1 \\ -F_t \\ F_t \\ P \end{cases} ; \qquad \{D\} = \begin{cases} u_1 \\ u_2 \\ u_3 \\ u_4 \end{cases} \qquad \sigma = E \, \varepsilon = E \, B \, D$$

$$\{D\} = \begin{cases} u_1 \\ u_2 \\ u_3 \\ u_4 \end{cases}$$

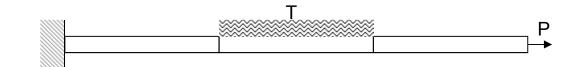
$$\sigma = E \varepsilon = E B D$$

4) Superponer tensiones

$$\sigma = E \,\varepsilon + \sigma_0$$

Carga Térmica

Resolución



Planteo de sistema

$$\frac{AE}{L} \begin{bmatrix} 1 & -1 & 0 & 0 \\ -1 & 2 & -1 & 0 \\ 0 & -1 & 2 & -1 \\ 0 & 0 & -1 & 1 \end{bmatrix} \begin{bmatrix} 0 \\ u_2 \\ u_3 \\ u_4 \end{bmatrix} = \begin{bmatrix} R \\ -F_t \\ F_t \\ P \end{bmatrix}$$

Resolución

$$\begin{cases}
 u_{2} \\
 u_{3} \\
 u_{4}
 \end{cases} =
 \begin{cases}
 \frac{LP}{AE} \\
 L\alpha\Delta T + \frac{2LP}{AE} \\
 L\alpha\Delta T + \frac{3LP}{AE}
 \end{cases}$$

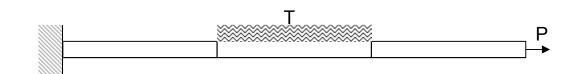
Aplicación Restricciones

$$\frac{AE}{L} \begin{bmatrix} 2 & -1 & 0 \\ -1 & 2 & -1 \\ 0 & -1 & 1 \end{bmatrix} \begin{bmatrix} u_2 \\ u_3 \\ u_4 \end{bmatrix} = \begin{bmatrix} -\alpha AE\Delta T \\ \alpha AE\Delta T \\ P \end{bmatrix}$$



Carga Térmica

Resolución



$$\sigma = E BD + \frac{\sigma_0}{\sigma_0}$$

Paso a Tensiones
$$\sigma = E BD + \sigma_0$$
 $B = \begin{bmatrix} -\frac{1}{L} & \frac{1}{L} \end{bmatrix}$

$$\sigma_1 = E \begin{bmatrix} -\frac{1}{L} & \frac{1}{L} \end{bmatrix} \begin{cases} 0 & \frac{LP}{AE} \end{cases} = \frac{P}{A}$$

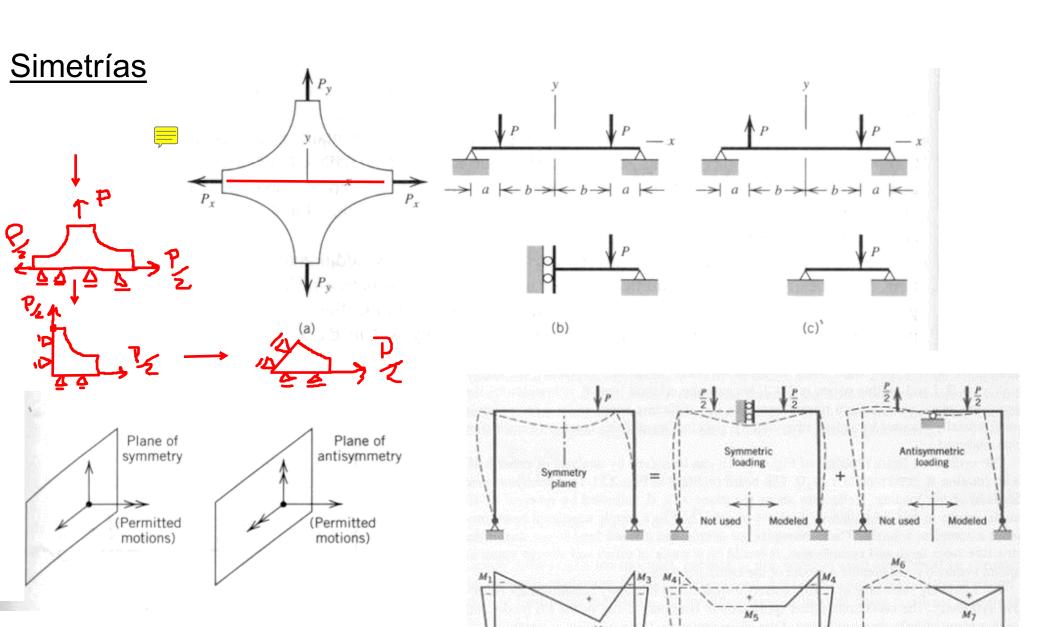
$$\sigma_2 = E \left[-\frac{1}{L} \quad \frac{1}{L} \right] \left\{ \frac{LP}{AE} \quad L\alpha\Delta T + \frac{2LP}{AE} \right\} = -\frac{P}{A} + E\alpha\Delta T + \frac{2P}{A} = E\alpha\Delta T + \frac{P}{A}$$

$$\sigma_3 = E \left[-\frac{1}{L} \quad \frac{1}{L} \right] = \left\{ L\alpha\Delta T \right\} \frac{2LP}{AE} \left(L\alpha\Delta T \right) + \frac{3LP}{AE} \right\} = \frac{P}{A}$$

Resultado:

Compensación de tensión térmica $\sigma = \sigma_2 + \sigma_0 = \frac{P}{A}$ con tensión estructura.

$$\sigma = \sigma_2 + \sigma_0 = \frac{P}{A}$$



Net bending moment

 $M_6 = -M_7$ Antisymmetric component

(c)

Symmetric component

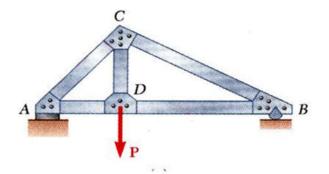
Casos de Estructuras

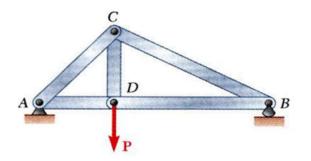




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Casos de Estructuras



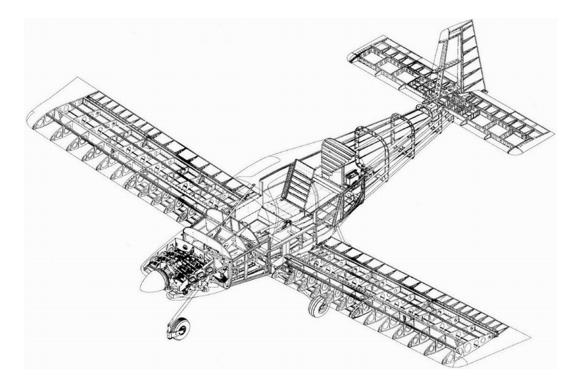




Casos de Estructuras







Mecanismos

