Cálculo de Fuerzas

$$\left\{r_{e}\right\} = \int_{v_{e}} [N]^{T} [F] dv_{e} + \int_{s_{e}} [N]^{T} [\Phi] ds_{e} + \int_{v_{e}} [B]^{T} [E] [\epsilon_{0}] dv_{e} - \int_{v_{e}} [B]^{T} [\sigma_{0}] dv_{e}$$

Cálculo de Fuerzas de Volumen

$$\{r_e\}_F = \int_{\Omega} [N]^T [N] dV \{f\}$$

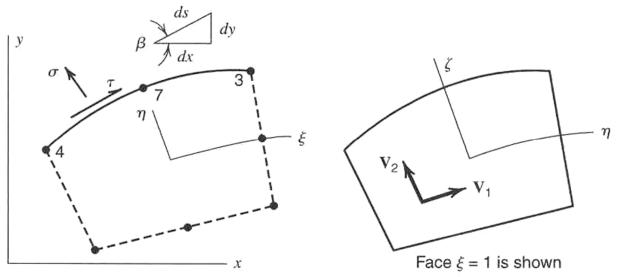
$$\{r_e\}_F = \int_{-1-1}^{1} \begin{bmatrix} N_1 & 0 & \dots & 0 \\ 0 & N_1 & \dots & N_n \end{bmatrix}^T \begin{bmatrix} N_1 & 0 & \dots & 0 \\ 0 & N_1 & \dots & N_n \end{bmatrix} J | t d \eta d \xi \begin{cases} f_{1_x} \\ f_{1_y} \\ \vdots \\ f_{n_y} \end{cases}$$

Cálculo de Fuerzas de Superficie

Las direcciones de los versores isoparamétricos depende de la numeración de nodos.

$${r_e} = \int_{4-7-3} [N(\xi, \eta = 1)]^T {\Phi_x \atop \Phi_y} tds$$

$$\begin{cases} \Phi_{x} \\ \Phi_{y} \end{cases} t ds = \begin{cases} \tau dx - \sigma dy \\ \sigma dx + \tau dy \end{cases} t$$



Los puntos de gauss en J11 y J12 estan evaluados sobre el arco!!!!!!

$$dx = \frac{\partial x}{\partial \xi} d\xi = J_{11}(\xi, \eta = 1) d\xi$$

$$dy = \frac{\partial y}{\partial \xi} d\xi = J_{12}(\xi, \eta = 1) d\xi$$

$$\tau = N_{k} \tau_{k}$$

$$\sigma = N_{k} \sigma_{k}$$

$$\sigma = N_{k} \sigma_{k}$$

$$\frac{\{r_{xi}\}}{\{r_{yi}\}} = \begin{cases} \int_{-1}^{1} N_{i} (\tau J_{11} - \sigma J_{12}) t d\xi \\ \int_{-1}^{1} N_{i} (\sigma J_{11} + \tau J_{12}) t d\xi \end{cases}$$

$$= \begin{cases} \int_{-1}^{1} N_{i} (\tau J_{11} - \sigma J_{12}) t d\xi \\ \int_{-1}^{1} N_{i} (\tau J_{11} - \tau J_{12}) t d\xi \end{cases} = \begin{cases} \int_{-1}^{1} N_{i} (\tau J_{11} - \tau J_{12}) t d\xi \\ \int_{-1}^{1} N_{i} (\tau J_{11} - \tau J_{12}) t d\xi \end{cases} = \begin{cases} \int_{-1}^{1} N_{i} (\tau J_{11} - \tau J_{12}) t d\xi \\ \int_{-1}^{1} N_{i} (\tau J_{11} - \tau J_{12}) t d\xi \end{cases} = \begin{cases} \int_{-1}^{1} N_{i} (\tau J_{11} - \tau J_{12}) t d\xi \\ \int_{-1}^{1} N_{i} (\tau J_{11} - \tau J_{12}) t d\xi \end{cases} = \begin{cases} \int_{-1}^{1} N_{i} (\tau J_{11} - \tau J_{12}) t d\xi \\ \int_{-1}^{1} N_{i} (\tau J_{11} - \tau J_{12}) t d\xi \end{cases} = \begin{cases} \int_{-1}^{1} N_{i} (\tau J_{11} - \tau J_{12}) t d\xi \\ \int_{-1}^{1} N_{i} (\tau J_{11} - \tau J_{12}) t d\xi \end{cases} = \begin{cases} \int_{-1}^{1} N_{i} (\tau J_{11} - \tau J_{12}) t d\xi \\ \int_{-1}^{1} N_{i} (\tau J_{11} - \tau J_{12}) t d\xi \end{cases} = \begin{cases} \int_{-1}^{1} N_{i} (\tau J_{11} - \tau J_{12}) t d\xi \\ \int_{-1}^{1} N_{i} (\tau J_{11} - \tau J_{12}) t d\xi \end{cases}$$

Cálculo de Fuerzas

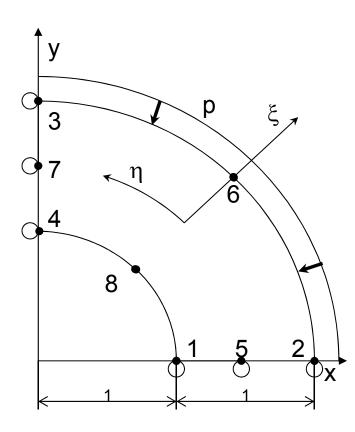
Ejemplo Q8:

$$\tau = 0$$
; $\sigma = -10$; $t = 1$

$$\begin{split} N_2(1,\eta) &= \frac{1}{4}(1+\xi)(1-\eta) - \frac{1}{2}(N_5 + N_6) = \frac{\eta^2 - \eta}{2} \\ N_3(1,\eta) &= \frac{1}{4}(1+\xi)(1+\eta) - \frac{1}{2}(N_7 + N_6) = \frac{\eta^2 + \eta}{2} \\ N_6(1,\eta) &= \frac{1}{2}(1+\xi)(1-\eta^2) = 1 - \eta^2 \end{split}$$

$$dx = \frac{\partial x}{\partial \eta} d\eta = J_{21} d\eta \quad ; \quad dy = \frac{\partial y}{\partial \eta} d\eta = J_{22} d\eta$$

$$\begin{split} J_{21} &= \frac{\partial \sum_{\text{nnod}} N_i (l, \eta) x_i}{\partial \eta} = \frac{\partial N_2}{\partial \eta} x_2 + \frac{\partial N_3}{\partial \eta} x_3 + \frac{\partial N_6}{\partial \eta} x_6 = 2\eta - 1 - \eta \sqrt{8} \\ J_{22} &= \frac{\partial \sum_{\text{nnod}} N_i (l, \eta) y_i}{\partial \eta} = \frac{\partial N_2}{\partial \eta} y_2 + \frac{\partial N_3}{\partial \eta} y_3 + \frac{\partial N_6}{\partial \eta} y_6 = 2\eta + 1 - \eta \sqrt{8} \end{split}$$



Cálculo de Fuerzas

Ejemplo Q8:

$$r_{2x} = \int_{-1}^{1} -N_{2}(1,\eta)\sigma J_{22}d\eta = \int_{-1}^{1} \left(\frac{\eta^{2} - \eta}{2}\right) \sigma \left(2\eta + 1 - \eta\sqrt{8}\right) d\eta = -6.095$$

$$r_{2y} = \int_{-1}^{1} N_{2}(1,\eta)\sigma J_{21}d\eta = \int_{-1}^{1} \left(\frac{\eta^{2} - \eta}{2}\right) \sigma \left(2\eta - 1 - \eta\sqrt{8}\right) d\eta = -0.572$$

$$r_{6x} = \int_{-1}^{1} -N_{6}(1,\eta)\sigma J_{22}d\eta = \int_{-1}^{1} (1 - \eta^{2})\sigma \left(2\eta + 1 - \eta\sqrt{8}\right) d\eta = -13.333$$

$$r_{6y} = \int_{-1}^{1} N_{6}(1,\eta)\sigma J_{21}d\eta = \int_{-1}^{1} (1 - \eta^{2})\sigma \left(2\eta - 1 - \eta\sqrt{8}\right) d\eta = -13.333$$

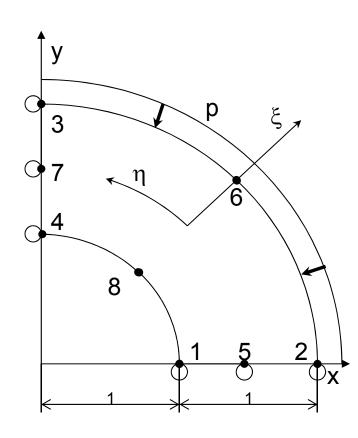
$$r_{3x} = \int_{-1}^{1} -N_{3}(1,\eta)\sigma J_{21}d\eta = \int_{-1}^{1} \left(\frac{\eta^{2} + \eta}{2}\right)\sigma \left(2\eta + 1 - \eta\sqrt{8}\right) d\eta = -0.572$$

$$r_{3y} = \int_{-1}^{1} N_{3}(1,\eta)\sigma J_{21}d\eta = \int_{-1}^{1} \left(\frac{\eta^{2} + \eta}{2}\right)\sigma \left(2\eta - 1 - \eta\sqrt{8}\right) d\eta = -6.095$$

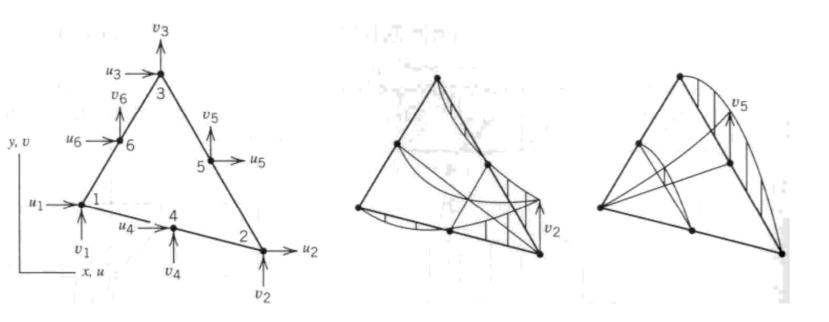
Integración por Gauss:

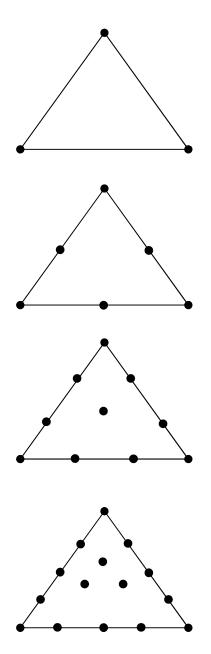
$$r_{6x} = (1 - \eta_1^2)\sigma(2\eta_1 + 1 - \eta_1\sqrt{8}) + (1 - \eta_2^2)\sigma(2\eta_2 + 1 - \eta_2\sqrt{8}) = -13.333$$

$$r_{6y} = (1 - \eta_1^2)\sigma(2\eta_1 - 1 - \eta_1\sqrt{8}) + (1 - \eta_2^2)\sigma(2\eta_2 - 1 - \eta_2\sqrt{8}) = -13.333$$



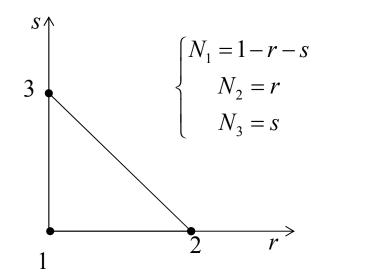
Elementos Triangulares





Formulación Isoparamétrica

$$I = \int_{A} \phi(r, s) dr ds \cong \sum_{i=1}^{n} W_{i} \phi(r_{i}, s_{i}) \frac{1}{2} |J_{i}|$$



$$J(r,s) = \begin{bmatrix} x_{,r} & y_{,r} \\ x_{,s} & y_{,s} \end{bmatrix} = \begin{bmatrix} \sum_{k} N_k(r,s)_{,r} x_k & \sum_{k} N_k(r,s)_{,r} y_k \\ \sum_{k} N_k(r,s)_{,s} x_k & \sum_{k} N_k(r,s)_{,s} y_k \end{bmatrix}$$

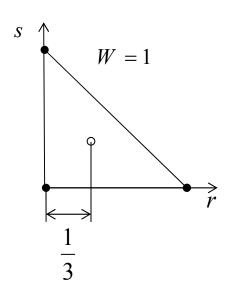
Precisión

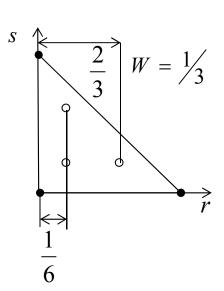
$$pg = 1 \qquad O = 1$$

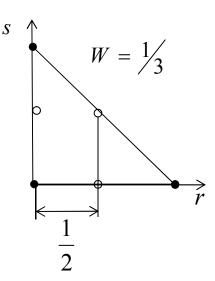
$$pg = 3 \qquad \rightarrow O = 2$$

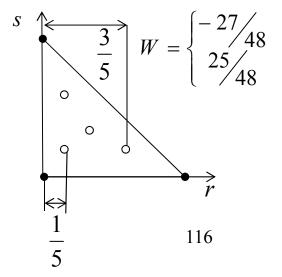
$$pg = 3 \qquad O = 2$$

$$pg = 4 \qquad O = 3$$







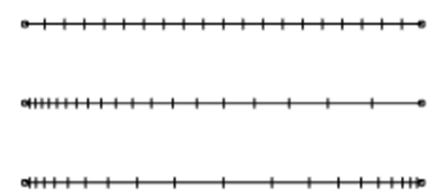


Mallados

Subdivisión

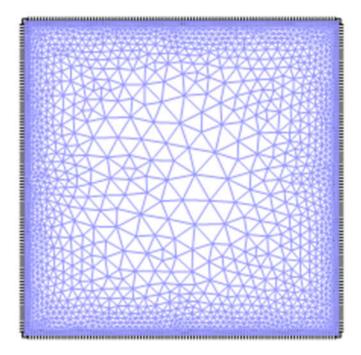
- Tamaño de elemento

• Biasing
Cualquier espacio se puede rellenar con tetrahedros y cualquier área con trigulos, no así con cubos y rectángulos respectivamente.



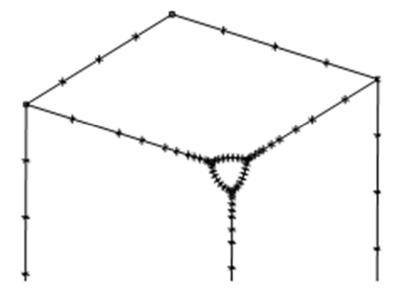
Control de tamaño de elementos

De menor dimensión a mayor



Primero se malla todo parejo, se calcula y se remalla (biasing) donde se encuentren las mayores tensiones.

No conviene hacer un salto muy grande en el tamaño de los elementos ya que rigidiza la solución, no da un buen resultado. La energía es una función suave, así tendrá que ser el resultado.



INVESTIGAR GRIFFITHS

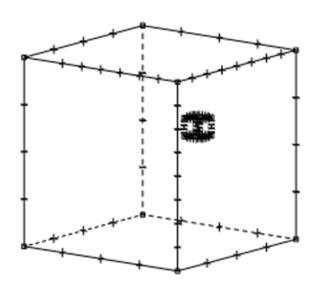
Conviene llenar las areas comprometidas con mallas ordenadas 117 ya que es más facil evaluar tensiones. El resto puede estar desordenado con tetrahedros.

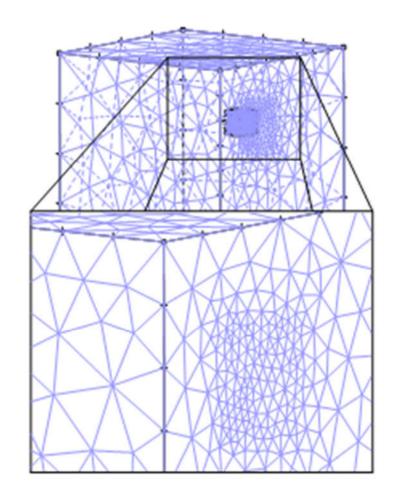
Siempre mallar los más chico primero y dejar que crezca hacia lo grande.

<u>Mallados</u>

Control de tamaño de elementos – Sudbominios

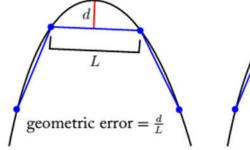
Mallar de más refinado a menos refinado

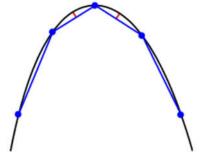




Geometría

Control por Curvatura



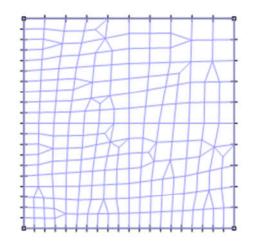


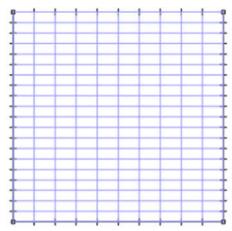
<u>Mallados</u>

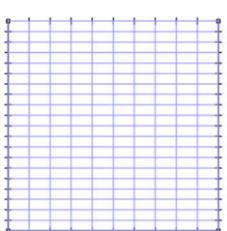
Arranco ordenado con elementos Q donde claramente hay concentración de tensiones, que el programa rellene el resto.

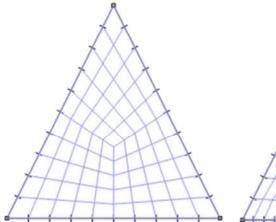
Mallado de superficies y volúmenes

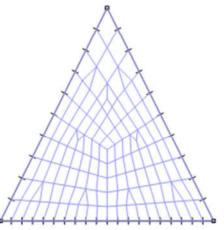
- Mapeado o estructurado
- Libre
- Tipos de elementos ¿Combinar?



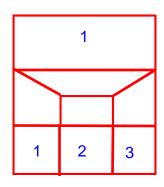


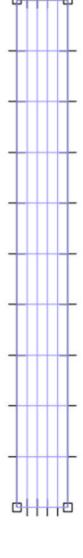


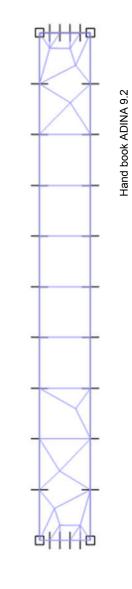


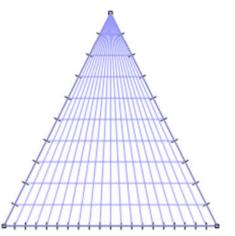


Truco para pasar de 1 a 3





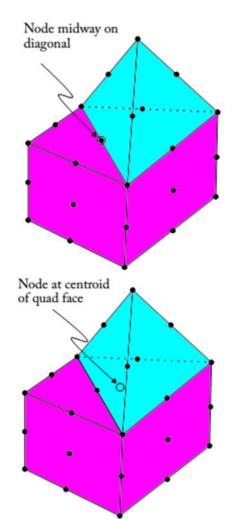


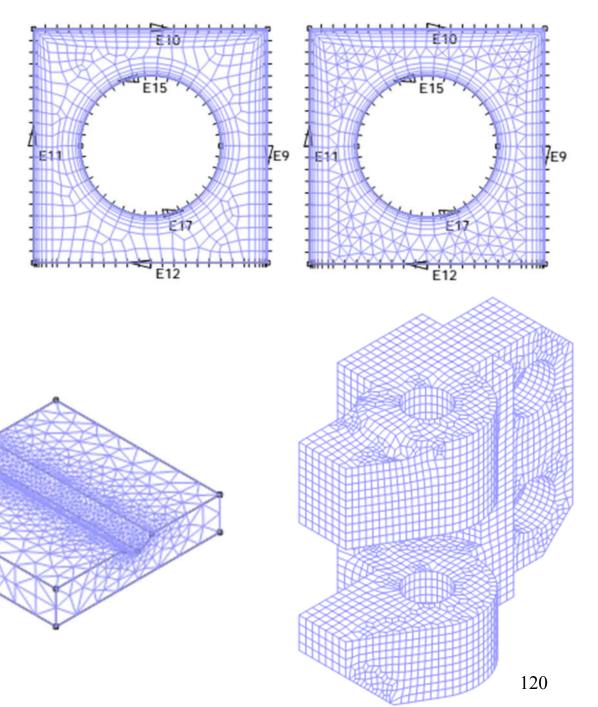


<u>Mallados</u>

Transiciones

- Nodos libres
- Tetraedros
- Hexaedros





Mallados 3D

- Regularidad
- Extrusión

