

Elemento Viga – Generalizado

Esfuerzo Axial

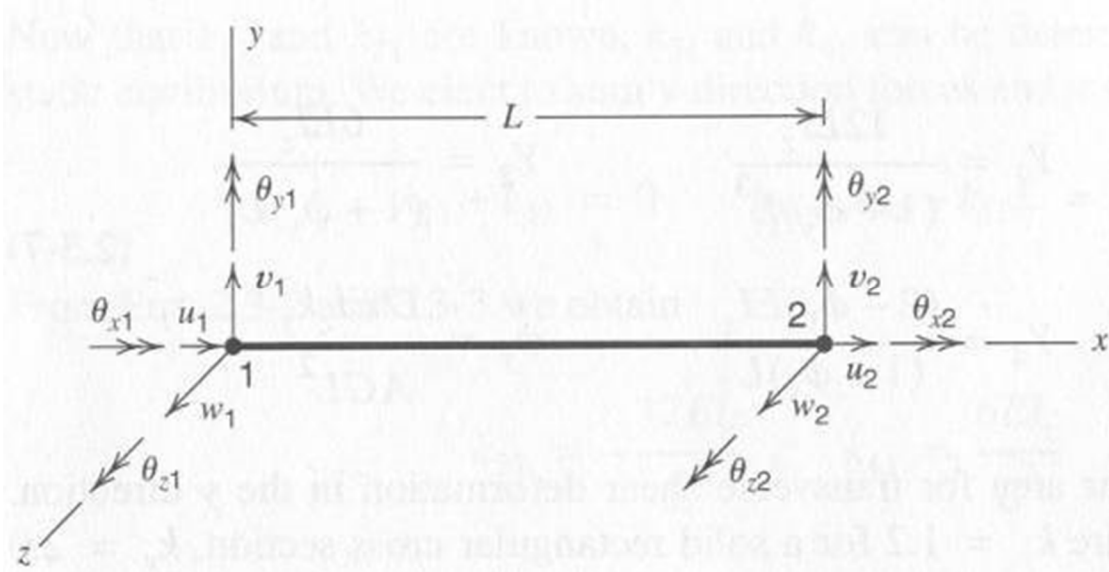
$$[K]_{axial} = \begin{bmatrix} X & -X \\ -X & X \end{bmatrix} \begin{matrix} u_1 \\ u_2 \end{matrix} ; X = \frac{AE}{L}$$

Flexión Plano Z

$$[K] = \begin{bmatrix} Y_1 & Y_2 & -Y_1 & Y_2 \\ Y_2 & Y_3 & -Y_2 & Y_4 \\ -Y_1 & -Y_2 & Y_1 & -Y_2 \\ Y_2 & Y_4 & -Y_2 & Y_3 \end{bmatrix} \begin{matrix} v_1 \\ \theta_{z1} \\ v_2 \\ \theta_{z2} \end{matrix}$$

$$Y_1 = 12 \frac{EI_z}{L^3}; \quad Y_2 = 6 \frac{EI_z}{L^2};$$

$$Y_3 = 4 \frac{EI_z}{L}; \quad Y_4 = 2 \frac{EI_z}{L}$$



$$[k] = \left[\begin{array}{cccccc|cccccc} X & 0 & 0 & 0 & 0 & 0 & -X & 0 & 0 & 0 & 0 & 0 \\ & Y_1 & 0 & 0 & 0 & Y_2 & 0 & -Y_1 & 0 & 0 & 0 & Y_2 \\ & & Z_1 & 0 & -Z_2 & 0 & 0 & 0 & -Z_1 & 0 & -Z_2 & 0 \\ & & & S & 0 & 0 & 0 & 0 & 0 & -S & 0 & 0 \\ & & & & Z_3 & 0 & 0 & 0 & Z_2 & 0 & Z_4 & 0 \\ & & & & & Y_3 & 0 & -Y_2 & 0 & 0 & 0 & Y_4 \\ \hline & & & & & & X & 0 & 0 & 0 & 0 & 0 \\ & & & & & & & Y_1 & 0 & 0 & 0 & -Y_2 \\ & & & & & & & & Z_1 & 0 & Z_2 & 0 \\ & & & & & & & & & S & 0 & 0 \\ & & & & & & & & & & Z_3 & 0 \\ & & & & & & & & & & & Y_3 \end{array} \right] \begin{matrix} u_1 \\ v_1 \\ w_1 \\ \theta_{x1} \\ \theta_{y1} \\ \theta_{z1} \\ \hline u_2 \\ v_2 \\ w_2 \\ \theta_{x2} \\ \theta_{y2} \\ \theta_{z2} \end{matrix}$$

symmetric

Elemento Viga – Generalizado

Esfuerzo Torsor

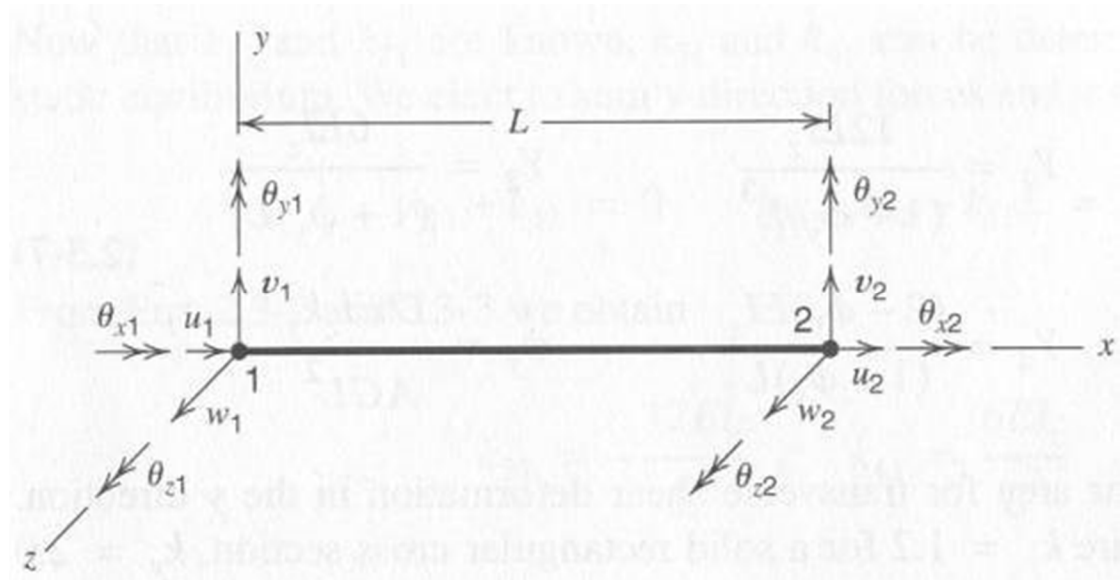
$$[K]_{\text{Torsor}} = \begin{bmatrix} S & -S \\ -S & S \end{bmatrix} \begin{matrix} \theta_{x1} \\ \theta_{x2} \end{matrix} ; S = \frac{GK}{L}$$

Flexión Plano Y

$$[K] = \begin{bmatrix} Z_1 & Z_2 & -Z_1 & Z_2 \\ Z_2 & Z_3 & -Z_2 & Z_4 \\ -Z_1 & -Z_2 & Z_1 & -Z_2 \\ Z_2 & Z_4 & -Z_2 & Z_3 \end{bmatrix} \begin{matrix} w_1 \\ \theta_{y1} \\ w_2 \\ \theta_{y2} \end{matrix}$$

$$Z_1 = 12 \frac{EI_y}{L^3}; \quad Z_2 = 6 \frac{EI_y}{L^2};$$

$$Z_3 = 4 \frac{EI_y}{L}; \quad Z_4 = 2 \frac{EI_y}{L}$$



$$[k] = \left[\begin{array}{cccccc|cccccc} X & 0 & 0 & 0 & 0 & 0 & -X & 0 & 0 & 0 & 0 & 0 \\ & Y_1 & 0 & 0 & 0 & Y_2 & 0 & -Y_1 & 0 & 0 & 0 & Y_2 \\ & & Z_1 & 0 & -Z_2 & 0 & 0 & 0 & -Z_1 & 0 & -Z_2 & 0 \\ & & & S & 0 & 0 & 0 & 0 & 0 & -S & 0 & 0 \\ & & & & Z_3 & 0 & 0 & 0 & Z_2 & 0 & Z_4 & 0 \\ & & & & & Y_3 & 0 & -Y_2 & 0 & 0 & 0 & Y_4 \\ \hline & & & & & & X & 0 & 0 & 0 & 0 & 0 \\ & & & & & & & Y_1 & 0 & 0 & 0 & -Y_2 \\ & & & & & & & & Z_1 & 0 & Z_2 & 0 \\ & & & & & & & & & S & 0 & 0 \\ & & & & & & & & & & Z_3 & 0 \\ & & & & & & & & & & & Y_3 \end{array} \right] \begin{matrix} u_1 \\ v_1 \\ w_1 \\ \theta_{x1} \\ \theta_{y1} \\ \theta_{z1} \\ \hline u_2 \\ v_2 \\ w_2 \\ \theta_{x2} \\ \theta_{y2} \\ \theta_{z2} \end{matrix}$$

symmetric

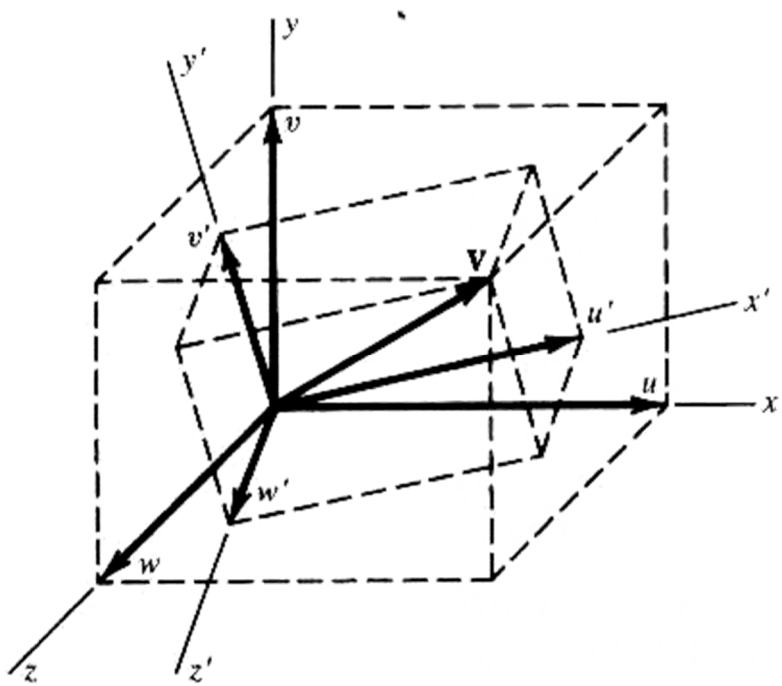
Elemento Viga – Rotación

$$\{d'\} = [T]\{d\} \rightarrow \begin{cases} u'_1 = l_1u_1 + m_1v_1 + n_1w_1 \\ v'_1 = l_2u_1 + m_2v_1 + n_2w_1 \\ w'_1 = l_3u_1 + m_3v_1 + n_3w_1 \end{cases}$$

$$\begin{Bmatrix} u'_1 \\ v'_1 \\ w'_1 \end{Bmatrix} = \begin{bmatrix} l_1 & m_1 & n_1 \\ l_2 & m_2 & n_2 \\ l_3 & m_3 & n_3 \end{bmatrix} \begin{Bmatrix} u_1 \\ v_1 \\ w_1 \end{Bmatrix} ; [\Lambda] = \begin{bmatrix} l_1 & m_1 & n_1 \\ l_2 & m_2 & n_2 \\ l_3 & m_3 & n_3 \end{bmatrix}$$

$$\begin{aligned} \theta'_{x1} &= l_1\theta_{x1} + m_1\theta_{y1} + n_1\theta_{z1} \\ \theta'_{y1} &= l_2\theta_{x1} + m_2\theta_{y1} + n_2\theta_{z1} \\ \theta'_{z1} &= l_3\theta_{x1} + m_3\theta_{y1} + n_3\theta_{z1} \end{aligned}$$

$$\begin{Bmatrix} \theta'_{x1} \\ \theta'_{y1} \\ \theta'_{z1} \end{Bmatrix} = \begin{bmatrix} l_1 & m_1 & n_1 \\ l_2 & m_2 & n_2 \\ l_3 & m_3 & n_3 \end{bmatrix} \begin{Bmatrix} \theta_{x1} \\ \theta_{y1} \\ \theta_{z1} \end{Bmatrix} ; [\Lambda] = \begin{bmatrix} l_1 & m_1 & n_1 \\ l_2 & m_2 & n_2 \\ l_3 & m_3 & n_3 \end{bmatrix}$$



Direction cosines between axes:

	x	y	z
x'	l_1	m_1	n_1
y'	l_2	m_2	n_2
z'	l_3	m_3	n_3

$$[T] = \begin{bmatrix} \Lambda & 0 & 0 & 0 \\ 0 & \Lambda & 0 & 0 \\ 0 & 0 & \Lambda & 0 \\ 0 & 0 & 0 & \Lambda \end{bmatrix}$$

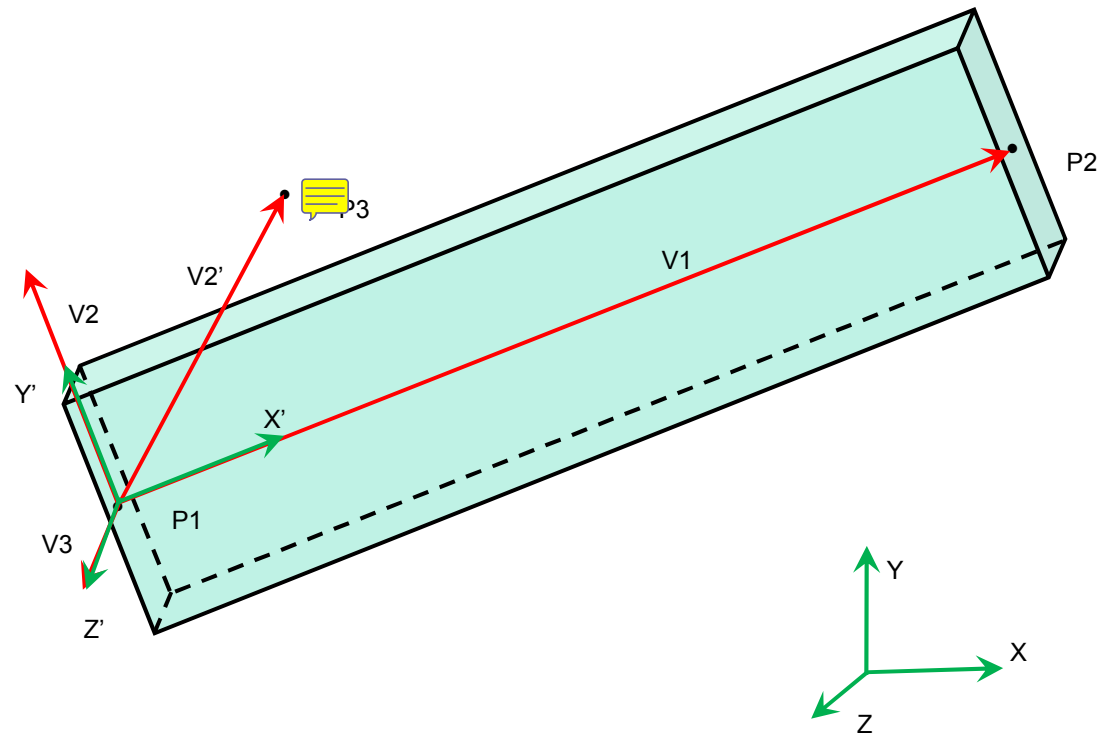
Elemento Viga – Ejemplo

$$\frac{P2 - P1}{|P2 - P1|} = V1 = \begin{Bmatrix} -0.3536 \\ 0.7071 \\ 0.6124 \end{Bmatrix}$$

$$P3 - P1 = V2'$$

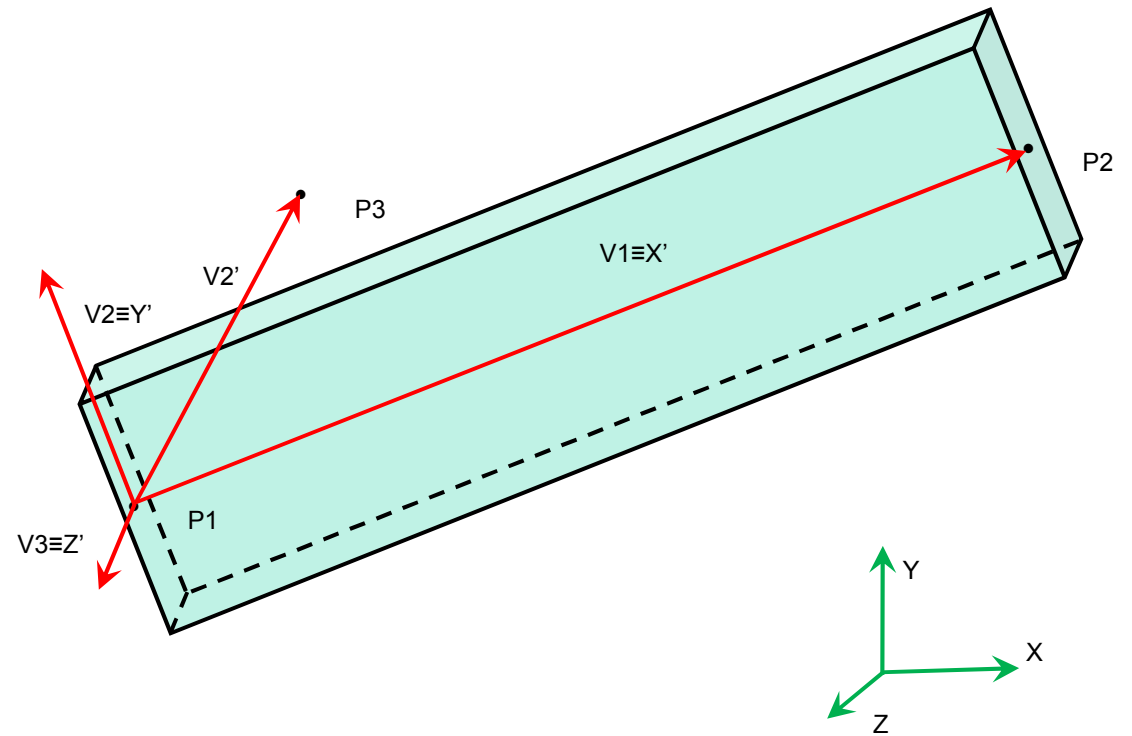
$$\frac{V1 \times V2'}{|V1 \times V2'|} = V3 = \begin{Bmatrix} 0.8660 \\ 0.0 \\ 0.5 \end{Bmatrix}$$

$$V3 \times V1 = V2 = \begin{Bmatrix} -0.3536 \\ -0.7071 \\ 0.6124 \end{Bmatrix}$$



$$\begin{Bmatrix} x' \\ y' \\ z' \end{Bmatrix} = \begin{bmatrix} -0.3536 & 0.7071 & 0.6124 \\ -0.3536 & -0.7071 & 0.6124 \\ 0.8660 & 0.0 & 0.5 \end{bmatrix} \begin{Bmatrix} x \\ y \\ z \end{Bmatrix}$$

Elemento Viga – Ejemplo



$$\text{Sección} \begin{cases} a = 20 \\ b = 10 \end{cases} \Rightarrow \begin{aligned} K &= \beta ab^3 = 0.229 \cdot 20000 = 4580 & I_{Z'} &= \frac{ba^3}{12} = 6666 \\ A &= ab = 200 & I_{Y'} &= \frac{ab^3}{12} = 1666 \end{aligned}$$



Desplazamientos Rígidos

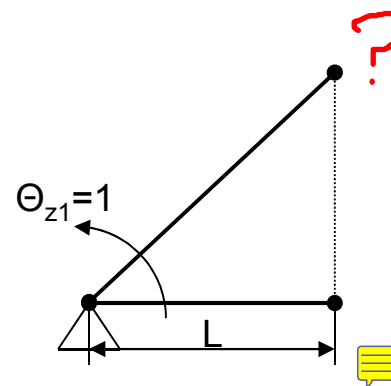
Valores Nodales

$$[K]\{D\} = \{R\}$$

$$\begin{bmatrix} 12 \frac{EI_z}{L^3} & 6 \frac{EI_z}{L^2} & -12 \frac{EI_z}{L^3} & 6 \frac{EI_z}{L^2} \\ 6 \frac{EI_z}{L^2} & 4 \frac{EI_z}{L} & -6 \frac{EI_z}{L^2} & 2 \frac{EI_z}{L} \\ -12 \frac{EI_z}{L^3} & -6 \frac{EI_z}{L^2} & 12 \frac{EI_z}{L^3} & -6 \frac{EI_z}{L^2} \\ 6 \frac{EI_z}{L^2} & 2 \frac{EI_z}{L} & -6 \frac{EI_z}{L^2} & 4 \frac{EI_z}{L} \end{bmatrix} \begin{Bmatrix} 0 \\ 1 \\ v_2 \\ \theta_{z2} \end{Bmatrix} = \begin{Bmatrix} F_1 \\ M_1 \\ 0 \\ 0 \end{Bmatrix}$$

$$\begin{bmatrix} -6 \frac{EI_z}{L^2} \\ 2 \frac{EI_z}{L} \end{bmatrix} + \begin{bmatrix} 12 \frac{EI_z}{L^3} & -6 \frac{EI_z}{L^2} \\ -6 \frac{EI_z}{L^2} & 4 \frac{EI_z}{L} \end{bmatrix} \begin{Bmatrix} v_2 \\ \theta_{z2} \end{Bmatrix} = \begin{Bmatrix} 0 \\ 0 \end{Bmatrix}$$

$$\begin{Bmatrix} v_2 \\ \theta_{z2} \end{Bmatrix} = \frac{L^4}{12} \begin{bmatrix} \frac{4}{L} & \frac{6}{L^2} \\ \frac{6}{L^2} & \frac{12}{L^3} \end{bmatrix} \begin{Bmatrix} \frac{6}{L^2} \\ -2 \end{Bmatrix} = \frac{L^4}{12} \begin{Bmatrix} \frac{4}{L} \frac{6}{L^2} + \frac{6}{L^2} \frac{-2}{L} \\ \frac{6}{L^2} \frac{6}{L^2} + \frac{12}{L^3} \frac{-2}{L} \end{Bmatrix} = \begin{Bmatrix} L \\ 1 \end{Bmatrix}$$



Deformada

$$v(x) = [N] \begin{Bmatrix} v_2 \\ \theta_{z2} \\ v_3 \\ \theta_{z3} \end{Bmatrix} = \begin{bmatrix} 1 - \frac{3x^2}{L^2} + \frac{2x^3}{L^3} \\ x - \frac{2x^2}{L} + \frac{x^3}{L^2} \\ \frac{3x^2}{L^2} - \frac{2x^3}{L^3} \\ -\frac{x^2}{L} + \frac{x^3}{L^2} \end{bmatrix}^T \begin{Bmatrix} 0 \\ 1 \\ L \\ 1 \end{Bmatrix}$$

$$v(x) = x - \frac{2x^2}{L} + \frac{x^3}{L^2} + L \left(\frac{3x^2}{L^2} - \frac{2x^3}{L^3} \right) - \frac{x^2}{L} + \frac{x^3}{L^2} = x$$

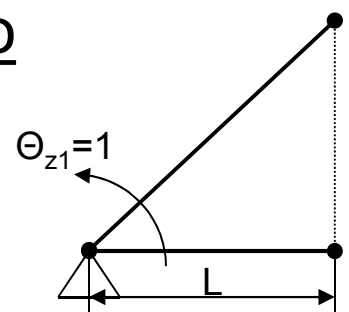
Reacciones

$$\{R\} = \begin{Bmatrix} 0 \\ 0 \\ 0 \\ 0 \end{Bmatrix}$$

Condiciones de Borde – Desplazamiento

$$[K]\{D\} = \{R\}$$

$$\begin{bmatrix} 12\frac{EI_z}{L^3} & 6\frac{EI_z}{L^2} & -12\frac{EI_z}{L^3} & 6\frac{EI_z}{L^2} \\ 6\frac{EI_z}{L^2} & 4\frac{EI_z}{L} & -6\frac{EI_z}{L^2} & 2\frac{EI_z}{L} \\ -12\frac{EI_z}{L^3} & -6\frac{EI_z}{L^2} & 12\frac{EI_z}{L^3} & -6\frac{EI_z}{L^2} \\ 6\frac{EI_z}{L^2} & 2\frac{EI_z}{L} & -6\frac{EI_z}{L^2} & 4\frac{EI_z}{L} \end{bmatrix} \begin{Bmatrix} 0 \\ 1 \\ v_2 \\ \theta_{z2} \end{Bmatrix} = \begin{Bmatrix} F_1 \\ M_1 \\ 0 \\ 0 \end{Bmatrix}$$



$$\{D_x\} = [K_{xx}]^{-1} (\{R_c\} - [K_{xc}]\{D_c\})$$

$$\begin{Bmatrix} v_2 \\ \theta_{z2} \end{Bmatrix} = \begin{bmatrix} 12\frac{EI_z}{L^3} & -6\frac{EI_z}{L^2} \\ -6\frac{EI_z}{L^2} & 4\frac{EI_z}{L} \end{bmatrix}^{-1} \left(\begin{Bmatrix} 0 \\ 0 \end{Bmatrix} - \begin{bmatrix} -12\frac{EI_z}{L^3} & -6\frac{EI_z}{L^2} \\ 6\frac{EI_z}{L^2} & 2\frac{EI_z}{L} \end{bmatrix} \begin{Bmatrix} 0 \\ 1 \end{Bmatrix} \right) = \begin{Bmatrix} L \\ 1 \end{Bmatrix}$$

$$\{R_x\} = [K_{cc}]\{D_c\} + [K_{cx}]\{D_x\}$$

$$\begin{Bmatrix} F_1 \\ M_1 \end{Bmatrix} = \begin{bmatrix} 12\frac{EI_z}{L^3} & 6\frac{EI_z}{L^2} \\ 6\frac{EI_z}{L^2} & 4\frac{EI_z}{L} \end{bmatrix} \begin{Bmatrix} 0 \\ 1 \end{Bmatrix} + \begin{bmatrix} -12\frac{EI_z}{L^3} & 6\frac{EI_z}{L^2} \\ -6\frac{EI_z}{L^2} & 2\frac{EI_z}{L} \end{bmatrix} \begin{Bmatrix} L \\ 1 \end{Bmatrix} = \begin{Bmatrix} 0 \\ 0 \end{Bmatrix}$$

Modelado Matemático

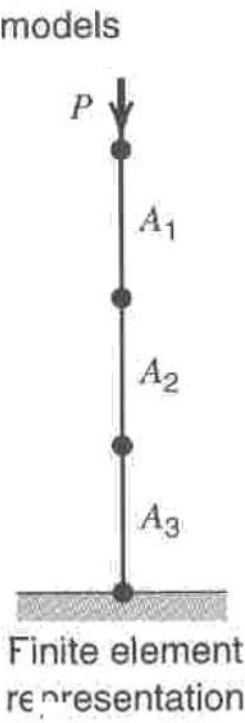
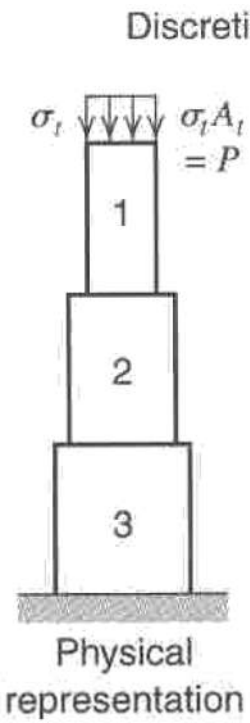
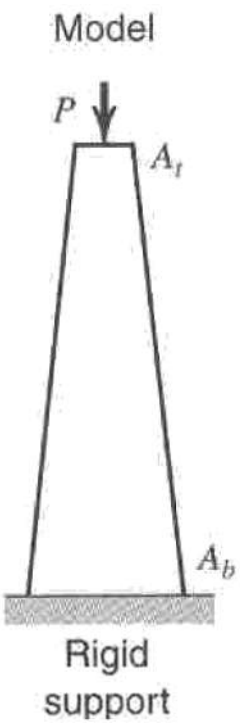
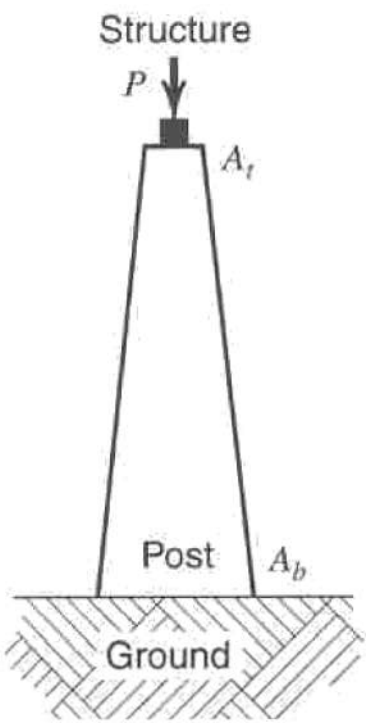
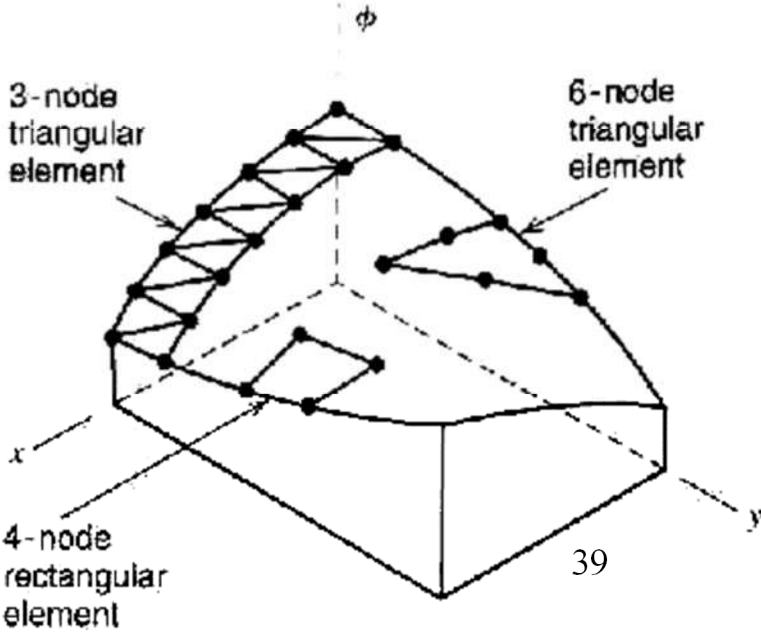
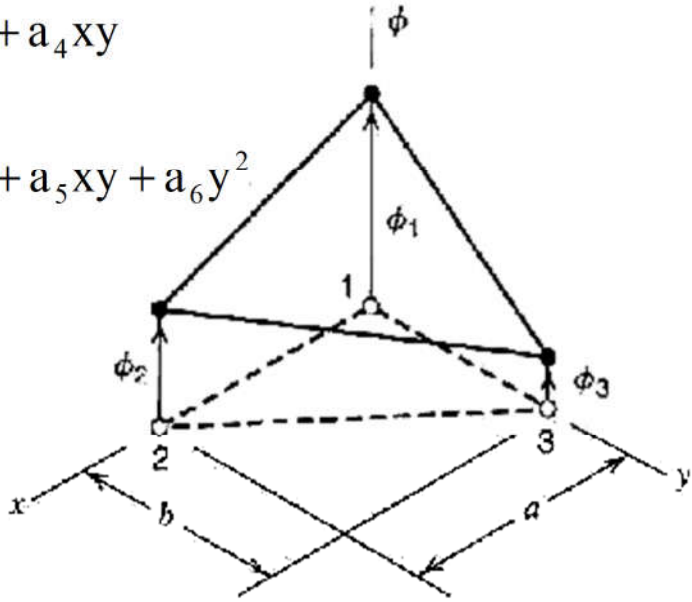
Pasos

- Problema Físico
- Modelo Matemático
- Modelo Numérico

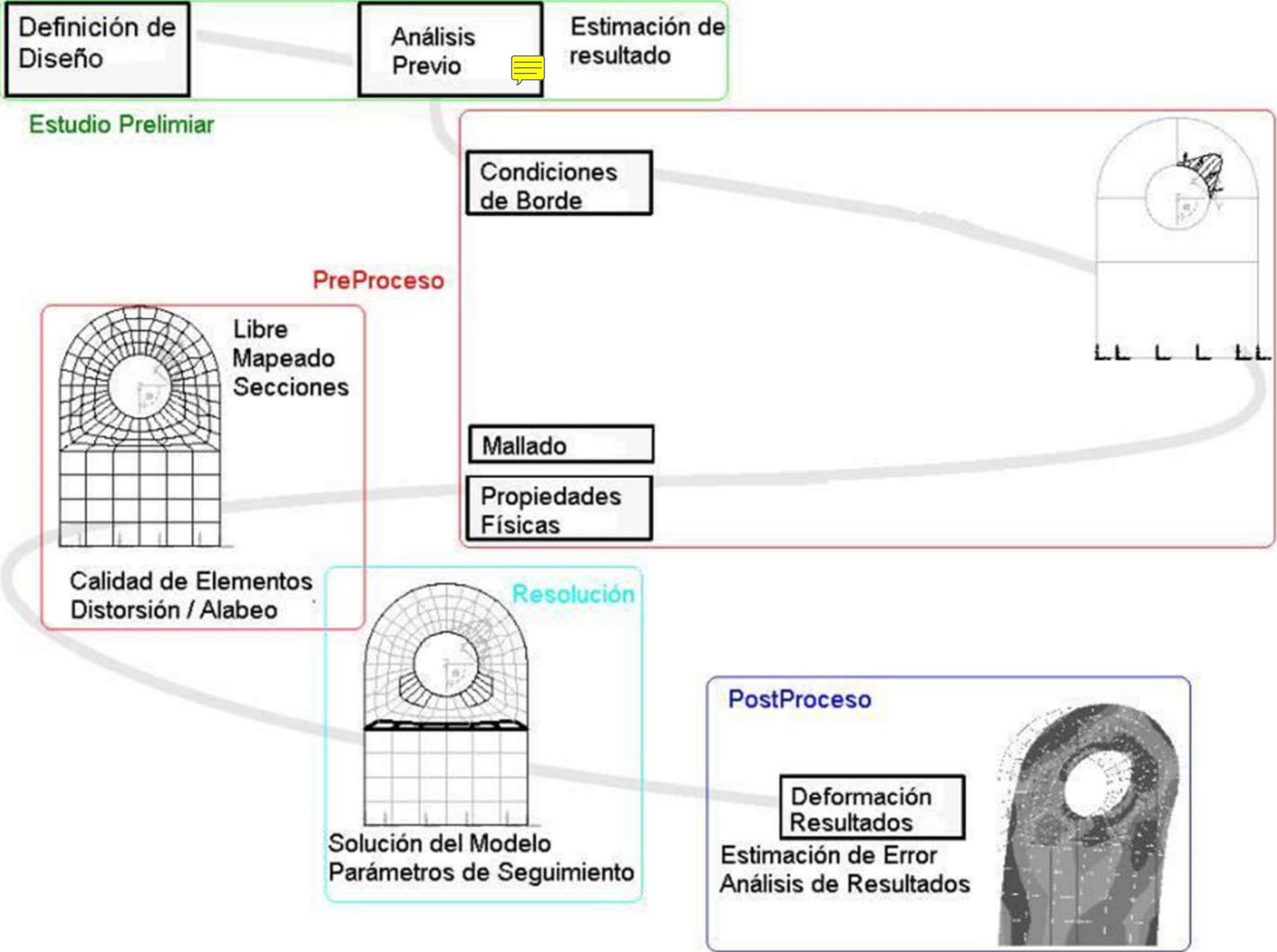


Funciones de Interpolación

$$\phi = \begin{cases} a_1 + a_2x + a_3y \\ a_1 + a_2x + a_3y + a_4xy \\ \vdots \\ a_1 + a_2x + a_3y + a_4x^2 + a_5xy + a_6y^2 \end{cases}$$

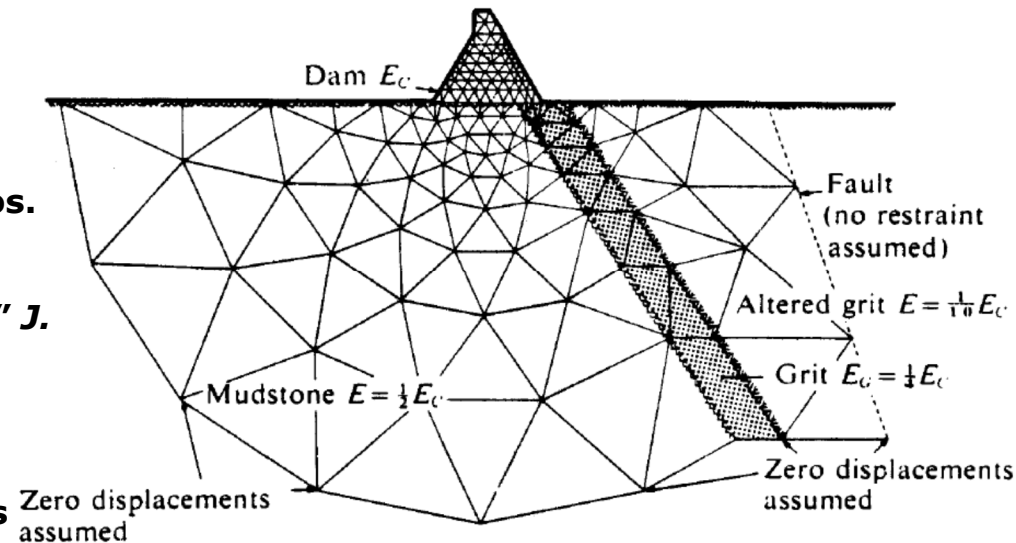


Modelado por Elementos Finitos



Historia del Método

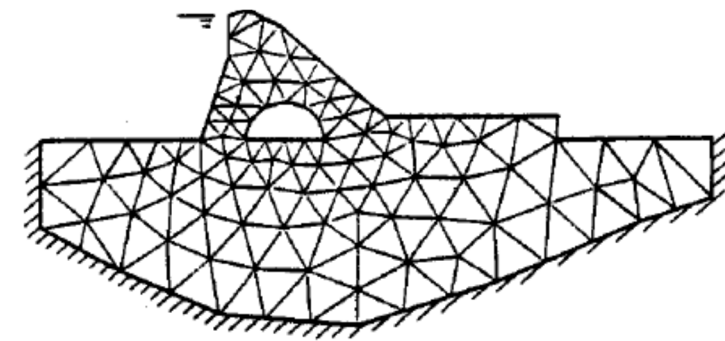
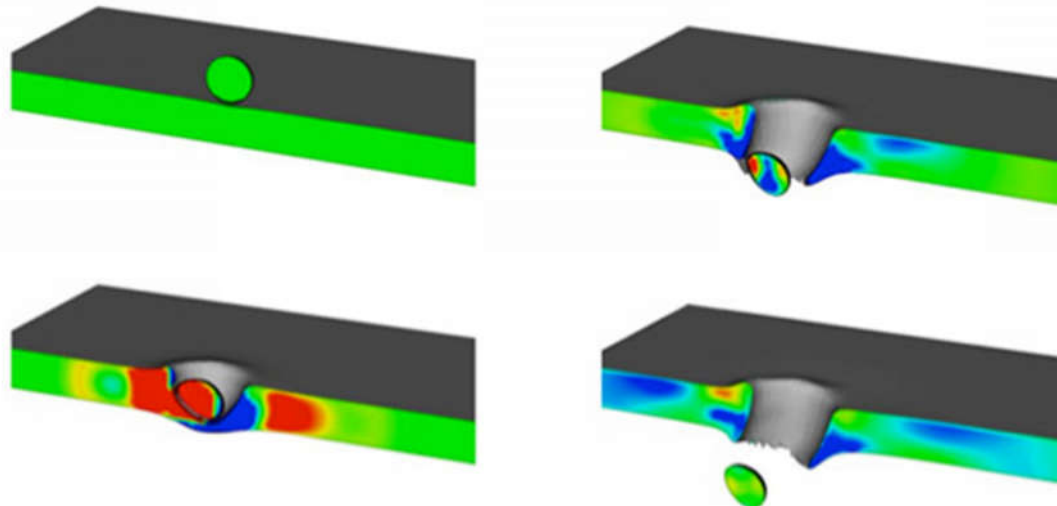
- 1943: Uso de elementos triangulares para problema de Torsión (St. Venant).
R. Courant, "Variational Methods for the Solutions of Problems of Equilibrium and Vibrations," *Bull. Am. Math.*, 1943.
- 1954 – 60: Solución computacional de problemas lineales de análisis estructural
J. H. Argyris, "Energy Theorems and Structural Analysis," *Aircraft Eng.*, 1954.
J. H. Argyris, "Energy Theorems and Structural Analysis," *Aircraft Eng.*, 1955.
J. H. Argyris, "The Matrix Theory of Statics" , *Ingenieur Archiv*, 1957.
J. H. Argyris, "The Analysis of Fuselages of Arbitrary Cross-Section and Taper," *Aircraft Eng.*, 1959.
J. H. Argyris and S. Kelsey, *Energy Theorems and Structural Analysis*, Butter-worth, 1960.
- 1953: IBM Crea la primer computadora de propósitos generales.
- 1954: Nace Fortran.
- 1956: Método directo para desarrollo de elementos finitos. Boeing.
•M. J. Turner, R. W. Clough, H. C. Martin, and L. C. Topp, "Stiffness and Deflection Analysis of Complex Structures," *J. Aeronaut. Sci.*, 1956.
- 1960: Estudios de elasticidad plana. Nombre "Elemento Finito".
•R. W. Clough, "The Finite Element Method in Plane Stress Analysis," *Proceedings of 2nd ASCE Conf. on Elect. Comp.*, 1960.
- 1964: Control Data Corporation desarrolla el primer software
- 1965: Formulación variacional. Aplicación a problemas de campo.
•O. C. Zienkiewicz and Y. K. Cheung, "Finite Elements in the Solution of Field Problems," *Engineer*, 1965.



Zienkiewicz, O. C. "Origins, milestones and directions of the finite element method— A personal view", Archives of Computational Methods in Engineering Volume 2, Issue 1 , pp 1-48

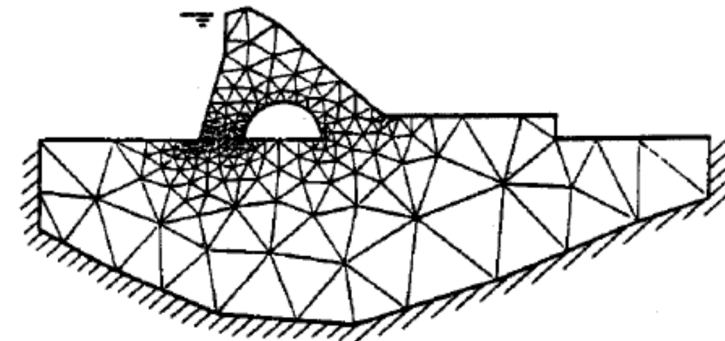
Historia del Método

- 1964: NASA solicita desarrollo de software para análisis de estructuras. Nace NASA STRucture ANalysis (1968)
- 1971: NASTRAN liberado al público. Se expanden las aplicaciones
- 1972: Patch Test (Irons and Razzaque 1972)
- 1978: Estimación del error. (Babuška and Rheinboldt 1978,79)
- 1980's: Desarrollo de workstations y software comercial.
- 1987: Adaptividad (Zienkiewicz and Zhu 1987, 89)
- 1990's: Computación personal.
- 2000's: Multiproceso, Multifísica, Multiescala, Multi...
- 2010's: Límites experimentales. The further development of a general Optimal Uncertainty Quantification (OUQ) framework (cf. H. Owhadi, C. Scovel, T. J. Sullivan, M. McKerns, and M. Ortiz, "Optimal uncertainty quantification," arXiv:1009.0679, 2010).



MESH 1 (728 D.O.F.)

$\eta = 16.5\%$



MESH 2 (1764 D.O.F.)

$\eta = 4.88\%$

Zienkiewicz, O. C. "Origins, milestones and directions of the finite element method— A personal view", Archives of Computational Methods in Engineering Volume 2, Issue 1 , pp 1-48

Simulated 3-D oblique impact of a 440C steel spherical projectile on an Al-6061 plate

<http://www.psaap.caltech.edu/>