

Propulsion System.

1st Stage - SRM → Isp.

2nd Stage - LRMI → Just modification of proportion project.
Isp.

Step 1 → we should know the total DV required to reach
Daily load - 50 kg max

we should know the
→ 2nd Stage perfect altitude. → ?

CEA

→ 1st Stage

Oxidizer - Ammonium Nitrate \rightarrow less performing → it's hydroscopicity → keeps attracting water. → which makes it difficult to handle.

Binder - HTPB. → this is the only composition that we know how to use.

Fuel - Aluminum. → nano sized

→ X not selected.

Problem during storage

Potassium Nitrate → it cheap → but very less performing.

during Combustion → it contains metal particles of Potassium.

→ inefficient combustion.

from the existing model → Vega
→ Rocket mode

→ Isp ≈ 120.061 sec.

CC pressure = 70 bar.

$$C^* = \underline{\underline{1788.63 \text{ m/s}}}$$

the max
that we have
obtained.

from CEA

for the Stage - 2

→

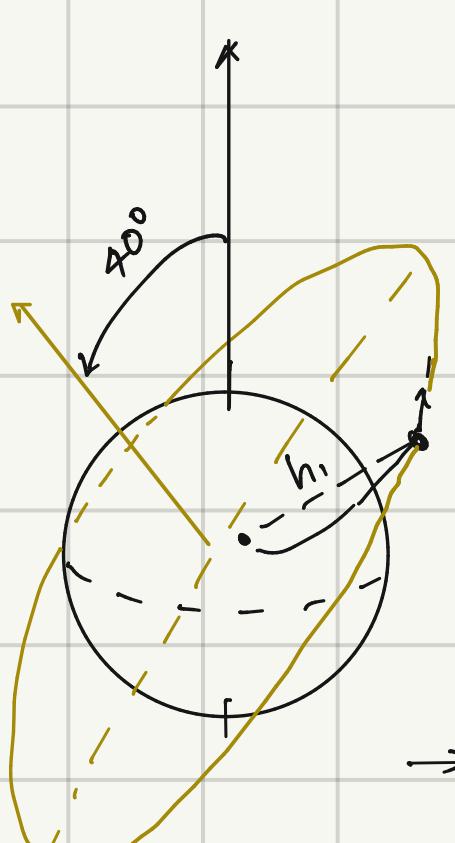
All are
Hypergolic.

3 - diff fuel/oxid minfare. →

→ 1. fuel $C_2H_5OH(l)$ 100%; oxidizer $H_2O_2(l)$ 100%.

→ 2. fuel $C_2H_8N_2(l)$ - UMH 50%; $N_2H_4(l)$ 50%, oxidizer $N_2O_4(l)$ 100%.

→ 3. fuel: $C_2H_8N_2(l)$ - UMH 50%; $N_2H_4(l)$ 50%; oxidizer $N_2O_4(l)$ 97% & NO 3%.



Mixture

Corrosivity

1

No

2

Yes

3

No

I*

Unknown

Unknown

Tabulated.

Performance is dependent on the propellant choice.

Hypergolic \rightarrow reduce overall complexity.
lower mass for S/C.

from CEA

$$\hookrightarrow I_{sp} \approx 315.25 \text{ sec.}$$
$$C.C \text{ pressure} = 15 \text{ bar.}$$
$$C^* = \underline{\underline{1679.48 \text{ m/s}}}$$

} the max
that we have
obtained.

there is no major
change in the
values for
16.5 - 20 bar

was the best out of 7
of ratio $\rightarrow \underline{\underline{2}} \rightarrow [1, 1.5, 2, 2.5 \dots 5.5]$

Trial - 1

L H₂

B.P $\rightarrow -253^\circ\text{C}$

f.P $\rightarrow -259^\circ\text{C}$

L O₂

B.P $\rightarrow -183^\circ\text{C}$

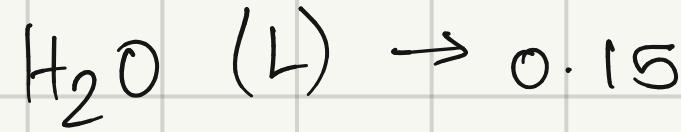
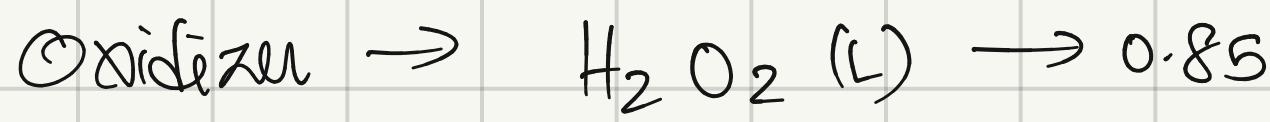
F.P $\rightarrow -219$

7/11/2020.

Final Results → for Propulsion.

for LRM.

Option - 1



$$P_c = 90 \text{ bar}$$

$A_e/A_t \rightarrow A_{\text{area}}$ →

(Bar) Pe →

(Sec) I_{sp}

(Sec) I_{sp}

	15	25	45
0.66061	0.337 - 0.334		0.15628
275.93	287.14	310.73	
275.93	287.23	310.6	

Sea level

many consider for outside atm.
 $A_e/A_t \geq 45$

→ Equilibrium

→ frozen

Option-2



$$P_c = 120 \text{ bar}$$

$A_e/A_t \rightarrow A_{\text{area}}$ →

(Bar) Pe →

(Sec) I_{sp}

(Sec) I_{sp}

	25	75
0.45375 - 0.41329		0.10515 - 0.09411
421.44	464.84	
414.465	453.84	

sea level.

many consider for outside atm
 $A_e/A_t \geq 75$

→ Equilibrium

→ frozen

→ λ^* is still unknown. → ?

for SRM

Oxidiser — $\text{NH}_4\text{NO}_3(\text{IV})$ — wt 68 $T = 300\text{K}$

Fuel — Al (C₈) — 18

Binder — HTPB — 12

↳ C_4H_6

↳ $h = -51.8 \text{ KJ/mol.}$

$$P_c = 70 \text{ bar}$$

$A_e/A_t \rightarrow$

10

15

20

25

$P_e (\text{bar}) \rightarrow$

0.899

0.522

0.357

0.2666

$I_{sp} (\text{Sec}) \rightarrow$

250.3

260.153

266.3

285.08

Sea level

Vaccum.