

Name \rightarrow Spandan Bharadwaj

Roll no \rightarrow 230102108

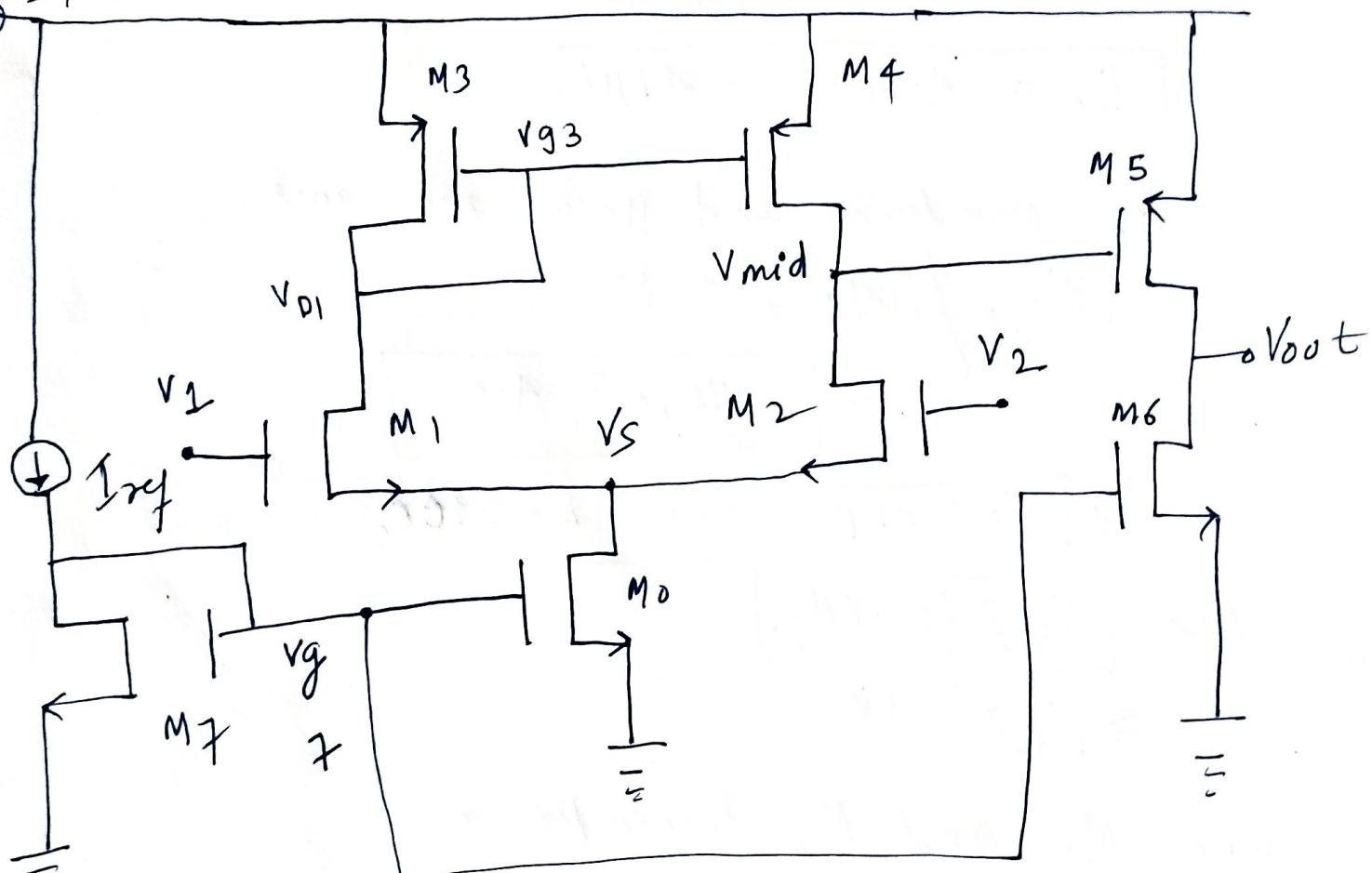
* EE-206 \rightarrow

OTA - Assignment \rightarrow

* Circuit diagram \rightarrow

$$V_{DD} = 1.8V$$

* Open-loop \rightarrow



* Calculations \rightarrow
 $V_2 =$ AC signal of $0.1mV$ amplitude and $0.9V$ dc
 $V_1 = 0.9V$ dc \rightarrow (for maximum swing)

* For M7 transistor \rightarrow

Assuming $0.1V$ overdrive for M_7 we get,

I_{ref} choosing as $4.6 \mu A$

$$\Rightarrow I_{ref} = \frac{H_n L_{ox}}{2} \left(\frac{\omega}{L} \right)_7 (V_{gs} - V_{th})^2$$

$$\Rightarrow 4 \cdot 6 \text{ mA} = \frac{230}{2} \left(\frac{w}{L} \right)_T (0.1)^2$$

$$\Rightarrow \left(\frac{w}{L} \right)_T = 4$$

$$\Rightarrow \begin{cases} L = 900 \text{n} \\ w_T = 3.6 \mu \end{cases}$$

* For M₀ transistor \Rightarrow

The tail current is 10 times that of ~~overdrive~~ current mirror.

$$I_0 = 4.6 \text{ mA} \times 10 = 46 \text{ mA}$$

As overdrive and $\mu_n w_X$ are same

$$\left(\frac{w}{L} \right)_0 / \left(\frac{w}{L} \right)_T = 10$$

$$\Rightarrow \left(\frac{w}{L} \right)_0 = 40$$

$$\Rightarrow w_0 = 36 \mu \text{ and } L_0 = 900 \text{n}$$

Now, $V_s > (V_{gs} - V_{th})_0$

$$\Rightarrow V_s > 0.1 \text{ V}$$

For M₁ and M₂ transistors \Rightarrow

$$I_1 = I_2 = 46/2 \text{ mA} = 23 \text{ mA}$$

Choosing its overdrive also to be 0.1 V
we get,

$$\left(\frac{w}{L} \right)_1 / \left(\frac{w}{L} \right)_0 = \frac{1}{2} \quad \text{as } I_1 = I_2 = \frac{I_0}{2}$$

$$\Rightarrow \left(\frac{w}{L} \right)_1 = \left(\frac{w}{L} \right)_2 = 20$$

$$\Rightarrow w_1 = w_2 = 18 \mu$$

$$L_1 = L_2 = 900 \text{n}$$

and other parameters except $(\frac{w}{L})_0$
is same

$$\text{Now, } V_{g_1} - V_{th_1} = 0.1 \text{ V}$$

$$\Rightarrow 0.9V - Vs = 0.37V = 0.1V$$

$$V_s = 0.9V - 0.37 - 0.1V$$

$$\Rightarrow V_s = 0.43 \text{ V} > 0.1 \text{ V}$$

So, Mo is in saturation (proneal).

$$\text{Now, } V_{D1} > (V_{GS} - V_{TH})_1$$

$$\Rightarrow V_{D1} > 0.1V$$

* For M_3 and M_4 transistor :-

$$I_3 = I_4 = 23 \text{ mA}$$

$$\text{Now, } I_3 = \frac{HPLox}{\omega_L} (\omega_L)_3 \left(V_{sg} - V_{th} \right)^2$$

$$\Rightarrow \frac{23\text{ HA}}{\text{EDH}}^2 = (\omega_L)_3 (V_{sg} - V_{th})_3$$

taking $(\omega/l)_3 = 4$

$$\Rightarrow \boxed{(V_{sg} - V_{th})_3 = 0.339V}$$

$$\text{From here } (V_{sg} - V_{th})_3 = (V_{sg} - V_{tp})_4 = 0.339 V$$

$$\text{and } w_3 \text{ and } w_4 \quad \text{and } l_3 = l_4 = 90^\circ$$

$\begin{matrix} \parallel \\ 3.6V \end{matrix}$ $\begin{matrix} \parallel \\ 3.6V \end{matrix}$

Now, for M_3 to be on, $\sqrt{V_{sg}} > |V_{tp}|$

$$\Rightarrow |.8V - V_{tp}| > V_g$$

$$\Rightarrow 1.8V - 0.39V > V_g$$

$$\Rightarrow 1 \cdot 41v > v_{01}$$

Now we get

$$(V_{sg} - V_{th})_3 = 0.339$$

$$\Rightarrow 1.8V = 0.339 + V_{D1} + 0.39$$

$$\Rightarrow V_{D1} = 1.071V$$

It satisfies as $V_{D1} > 0.1V$ and $V_{D1} > 1.41V$
So, M_3, M_4 and M_1 and M_2
are in saturation

Practically, due to body effect and due
to finite load impedance of M_0 ,

$$(\frac{W}{L})_7 = \frac{3.450}{0.90} \quad \text{but all other parameters are same.}$$

So, $\begin{cases} \text{gain due to first stage} = g_m_2 (\infty || 100\Omega) \\ (\text{taken from log file attached at end}) \\ = -3.95 \times 10^{-4} \times [258397.9328] \\ = -102.06 \end{cases}$

Practically coming, gain of first
stage as $= -101.0204$
 $\boxed{\text{Error} = -1.021}$

Practically,

$$V_{DI} = V_{mid} = 0.922 \text{ V}$$

due to body effect V_{th} varies

* For M_6 transistor \rightarrow

choosing $I_6 = 23 \mu A$

$$\text{as } V_{g7} = V_{g6}$$

$$\text{so, } (V_{gs} - V_{th})_6 = 0.1 \text{ V}$$

$$\Rightarrow 23 \mu A = 115 \times \left(\frac{w}{l}\right)_6 (0.1)^2$$

$$\Rightarrow \left(\frac{w}{l}\right)_6 = 20$$

$$\Rightarrow L_6 = 900 \text{ m} \quad w_6 = 18 \text{ } \mu \text{m}$$

$$\text{Practically } w_6 = 16.65 \text{ } \mu \text{m and } L_6 = 900 \text{ } \mu \text{m}$$

as finite τ_{ON} so, variations are arising.

I_6 also practically

coming up as $22.9 \mu A$.

$$V_{out} > (V_{gs} - V_{th})_6$$

$$V_{out} > 0.1 \text{ V}$$

* For M5 transistor \Rightarrow

$$(V_{sg} - V_{th})_5 = V_s - V_{mid} - V_{th}$$

$$= 1.8 - 1.071 - 0.39$$

$$= 0.339V$$

$$I_5 = 23HA$$

$$\Rightarrow 23HA = \frac{H_p C_{ox}}{2} \left(\frac{w}{l} \right)_5 (0.339)^2$$

$$\Rightarrow \left(\frac{w}{l} \right)_5 = 4$$

and it satisfied
 $|V_{SD}| > V_{sg} - V_{th}$

$$\Rightarrow \boxed{\frac{w_5}{L_5} = 3.60}$$

$$\boxed{V_{out} = 0.94V}$$

So, M5 ~~is~~ in
and M6 saturation

Gain for Second stage \Rightarrow

(taken from log file) $g_m 5 \times (\tau_{op5} || \tau_{op6})$

$$= 9.14 \times 10^{-5} \times (279329.608)$$

$$= 25.53^{\circ}$$

Practically open loop gain of OTA
got is 2366.199.

and first stage practically
is 101.0204

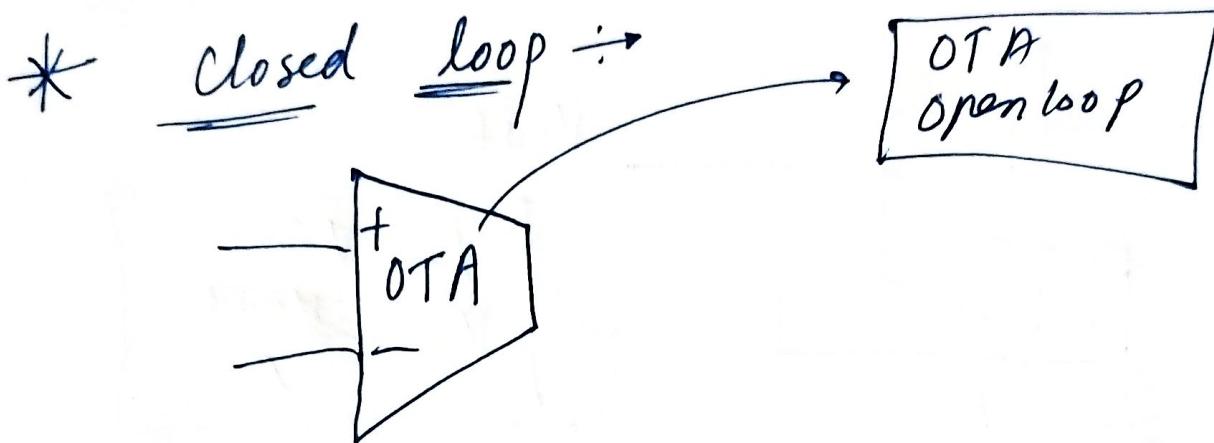
So, gain for
second practically is
Stage 23.4229.

Error = -8.25%.

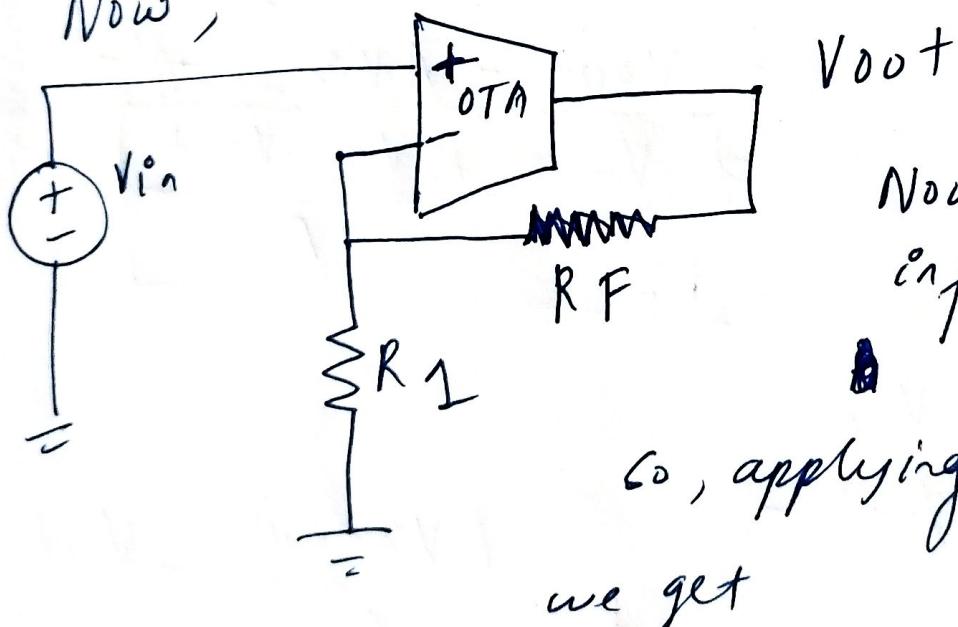
Theoretically
total gain is (-102.06×-25.53)
 $= 2605.5918$

but practical gain = 2366.199

so, error of -9.18 %



Now,



V_{out}

Now considering
infinite Amplification
 $\blacksquare V_+ = V_- \Rightarrow V_{in}$

\therefore , applying KCL at V_-

we get

$$\frac{V_- - V_{out}}{R_F} + \frac{V_-}{R_1} = 0$$

$$\Rightarrow \boxed{\frac{V_{out}}{V_-} = \frac{R_1 + R_F}{R_1}}$$

$$\Rightarrow \boxed{\frac{V_{out}}{V_-} = 1 + \frac{R_F}{R_1}}$$

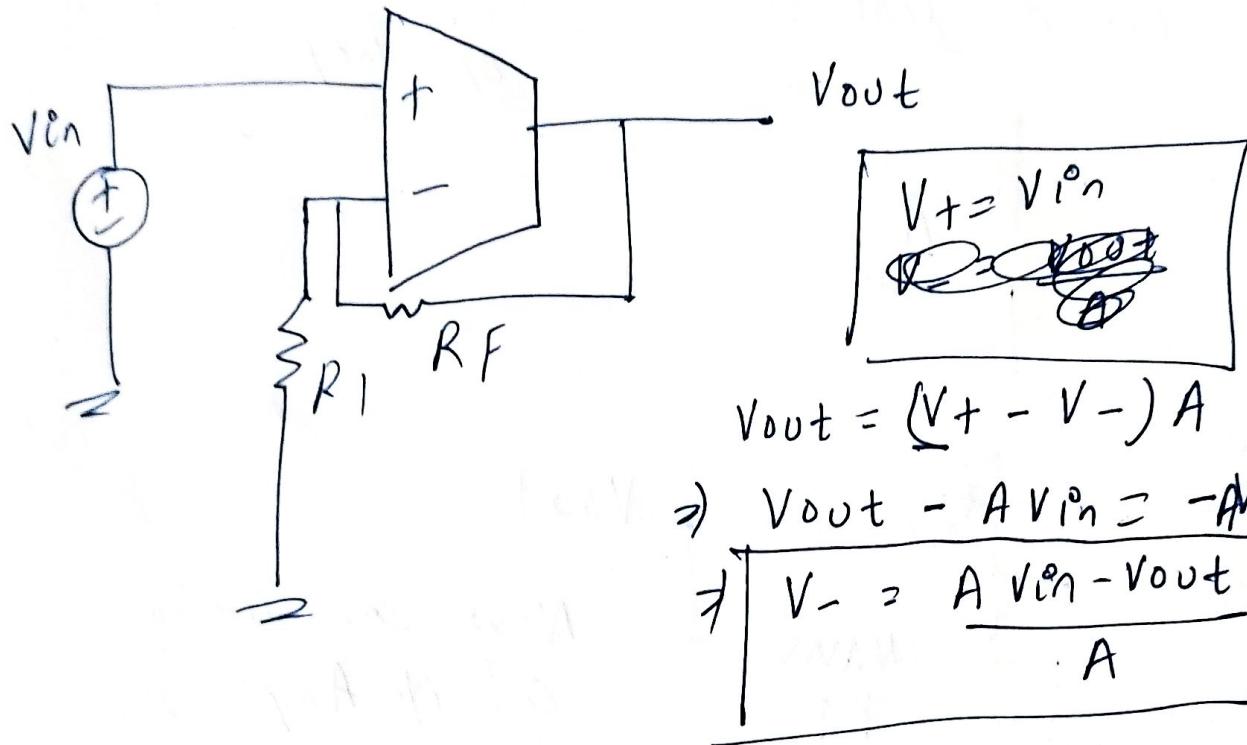
So, if $R_F = R_1$

we get a

$$\text{So, } R_F = R_1 = 20K$$

but the OTA we have designed has a finite

A i.e.
2366.199



So, KCL at V_- ,

$$\left[\frac{A V_{in} - V_{out}}{A} \right] + \left[\frac{A V_{in} - V_{out}}{A} - V_{out} \right] = 0$$

$\frac{1}{R_1} + \frac{1}{RF} + \frac{1}{AR_F^2}$

$$\Rightarrow \frac{V_{in}}{R_1} + \frac{V_{in}}{RF} = V_{out} \left[\frac{1}{AR_1} + \frac{1}{RF} + \frac{1}{AR_F^2} \right]$$

$$\Rightarrow V_{in} \left[\frac{R_1 + RF}{R_1 RF} \right] = V_{out} \left[\frac{1}{AR_1 (A+1)} \right]$$

$$\Rightarrow V_{in} \left[\frac{R_1 + RF}{R_1 RF} \right] = V_{out} \left[\frac{RF + AR_1 + R_1}{AR_1 RF} \right]$$

$$\Rightarrow \left[\frac{V_{out}}{V_{in}} \right] = \left[\frac{A(R_1 + RF)}{(AR_1)R_1 + RF} \right]$$

$$\Rightarrow \frac{V_{out}}{V_{in}} = \left[1 + \frac{RF}{R_1} \right] \left[\frac{A}{(AR_1) + \frac{RF}{R_1}} \right]$$

this  causing the discrepancy

so, chosen $R_F = 21k$ and $R_1 = 20k$

and $A = 2366.199$

$$\Rightarrow \left[\frac{V_{out}}{V_{in}} \right] = \left[1 + \frac{21}{20} \right] \left[\frac{2366.199}{2367.199 + \frac{21}{20}} \right]$$

$$\Rightarrow \frac{V_{out}}{V_{in}} = 2.048$$

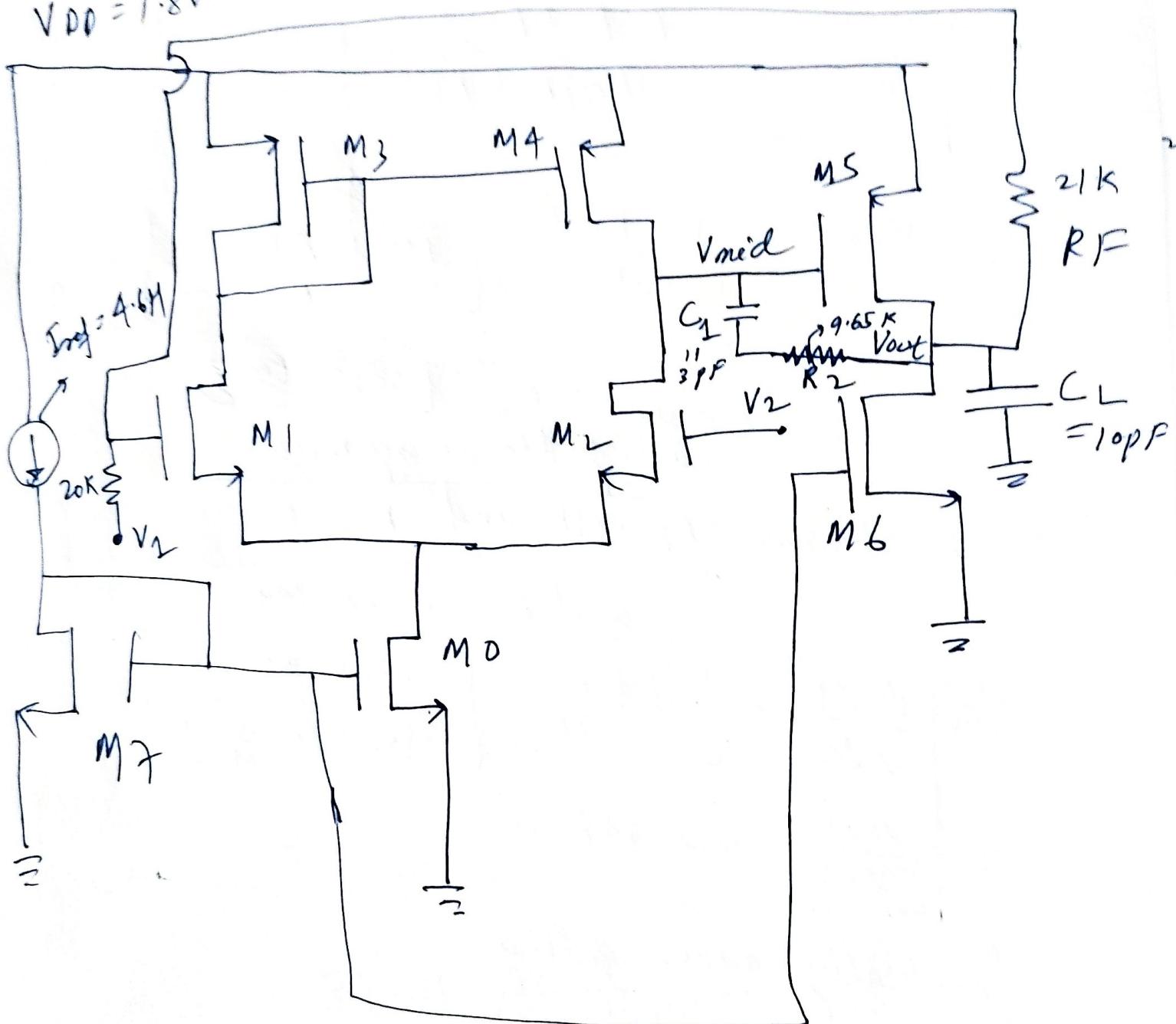
Practically again getting

$$\left[\frac{V_{out}}{V_{in}} \right] = \frac{\cancel{2.035}}{2.03675}$$

$$\text{error \%} = -0.5493$$

Closed-loop circuit diagram

$$V_{DD} = 1.8V$$



$V_1 = 0.9V \text{ dc}$ $V_2 = 0.9V \text{ dc with } 0.1m \text{ amplitude sine wave}$

Taken $C_1 = 3 \mu F$ and $C_2 = 10 \mu F$ poles are for approx

Now, bode plot had zero in the middle, which was compromising my phase margin

So, I put a R_2 in series with C_2 to shift my zero and get the required P.M.

First I approximated R_2 as $\frac{1}{9m_5}$

$$\left(\begin{array}{l} \text{taken from} \\ \text{log file} \end{array} \right) = \frac{10^5}{9 \cdot 13} \\ = 10 \cdot 952 \text{ k}$$

but I got a P.M of $\cancel{103}$.

So, I meddled and adjusted and at $R_2 = \cancel{9.65} \text{ k}$ 9.65 k

I got P.M of 60° (approx)

Bandwidth (3db) = 13.070498 MHz
(approx)

Location of dominant pole →

$$= \frac{1}{A C_1 (r_{0P5} || r_{0N6})}$$

freq of second stage

$$= \frac{10^{12}}{(3 \times 23.4229 \times 279329.60)}$$

$$= \cancel{50.947} \cancel{\times} \cancel{10^3} \text{ rad/sec}$$

$$= 50.947 \times 10^3 \text{ rad/sec}$$

Theoretical →

$(\omega/L)_7$	$3.6v/0.9v = 4$
----------------	-----------------

$(\omega/L)_0$	$36v/9v = 40$
----------------	---------------

$(\omega/L)_1$	$18v/9v = 20$
----------------	---------------

$(\omega/L)_2$	$18v/9v = 20$
----------------	---------------

$(\omega/L)_3$	$3.6v/0.9v = 4$
----------------	-----------------

$(\omega/L)_4$	$3.6v/0.9v = 4$
----------------	-----------------

$(\omega/L)_5$	$3.6v/0.9v = 4$
----------------	-----------------

$(\omega/L)_6$	$18v/0.9v = 20$
----------------	-----------------

Gain of first stage	-102.06
---------------------	-----------

gm ₂	$3.95 \times 10^{-4} \rightarrow \log \text{ file}$
-----------------	---

Gain of second stage	$23.4229 - 25.530$
----------------------	--------------------

gm ₅	$9.14 \times 10^{-4} \rightarrow \log \text{ file}$
-----------------	---

Overall gain	2605.5918
--------------	-------------

Practical \rightarrow

(w/L)7	$3.45/0.90 = 3.83$
(w/L)0	$36/90 = 40$
(w/L)1	$18/90 = 20$
(w/L)2	$18/90 = 20$
(w/L)3	$3.6/0.90 = 4$
(w/L)4	$3.6/0.90 = 4$
(w/L)5	$3.6/0.90 = 4$
(w/L)6	$16.65/0.90 = 18.5$
gain of first stage	101.0204
error in first stage (wrt theoretical)	8.25% - 1.02.1.
gain of second stage	23.4229
error in second stage (wrt theoretical)	- 8.25.1.
overall gain	2366.199
error in overall gain (wrt theoretical)	- 9.18.1.
C1	3PF
C_L	10PF
R2	9.65K
P.M	60° (approx)
Location of dominant pole	$50 \cdot 947 \times 10^3$ rad/sec
Power dissipation	$(4.6 + 46 + 23) HA \times 1.8 V$ $= 1.3248 \times 10^{-4} W = 0.13248 mW$

Closed-loop \rightarrow

theoretical \rightarrow

gain of overall circuit $\rightarrow 2$

practical \rightarrow

calculated (with finite A_o) = 2.048

found in LTSpice = 2.03675

error = -0.5493%

Log file attached with

- this pdf

in teams