Bachelor of Engineering Electronic Engineering (HONS)

Headphone Amplifier Design



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Contents

1	Sim	aple transistor circuit	4
	1.1	Transistor basic property	4
	1.2	Relationship between Base voltage(V_{be}) and Collector current(I_c)	5
	1.3	Limit current gain	5
	1.4	Add voltage divider	7
2	Neg	gative Feedback	8
	2.1	Simple Negative Feedback system	8
	2.2	Implement Using Op-amp	8
	2.3	Implement Using transistor	10
3	Cur	crent Source	12
	3.1	Single current source circuit	12
	3.2	Use current source to replace output resistor	13
4	Out	eput Stage	14
	4.1	Class A Output Stage	14
	4.2	Class AB Output Stage	15

List of Tables

1 1	DC operating	point	analysis	result											ļ
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List of Figures

1.1	Single transistor circuit	4
1.2	V_{be} and I_c curve	5
1.3	Basic transistor circuit with R_c and R_e	6
1.4	Output of the circuit in Figure 1.3	6
1.5	Add voltage divider and capacitors	7
2.1	simple negative feedback system	8
2.2	Implement negative feedback circuit with Op-amp	9
2.3	Op-amp feedback simulation result curve	9
2.4	Implement negative feedback circuit with transistor	10
2.5	transistor feedback circuit simulation result	11
3.1	single current source circuit	12
3.2	single current source circuit simulation result	13
3.3	the circuit after adding current source	13
4.1	Class A output stage	14
4.2	Class A output stage simulation result	15
4.3	Class A DC operating current simulation data	15
4.4	Class AB output stage	16
4.5	Class AV output stage simulation resut	16
4.6	Class AB output stage DC operating current	17

Simple transistor circuit

1.1 Transistor basic property

Figure 1.1 shows the basic NPN bipolar junction transistor circuit.

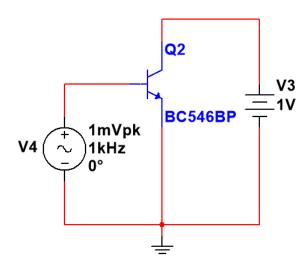


Figure 1.1: Single transistor circuit

We can get transistor operating state from simulation result as Table 1.1. It's obvious that I_C and I_E is proximately 200 times greater than I_B which is the main function of transistor.

Equation 1.1 defines β which is the most important parameter of transistor.

$$\beta = \frac{I_C}{I_B} \tag{1.1}$$

I_B	9.09789μ
I_C	2.02293m
I_E	-2.03003m

Table 1.1: DC operating point analysis result

1.2 Relationship between Base voltage (V_{be}) and Collector current (I_c)

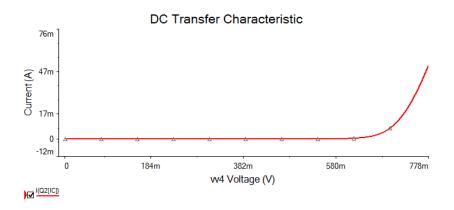


Figure 1.2: V_{be} and I_c curve

After running DC sweep command on V4 in circuit of Figure 1.1, We can get the curve of Figure 1.2. This illustrate that when $V_{be} < 0.65V$, I_c is very small and when $V_{be} > 0.65V$, I_c is increase significantly. Therefore, We can simply consider that when $V_{be} > 0.65V$, transistor is on.

1.3 Limit current gain

Generally, we need a method to control the current gain as we want. Figure 1.3 is a simply solution by adding transistor R_C and R_E .

We can derive voltage gain A_V with Equation 1.2. And in circuit in Figure 1.3, A_V is approximate 5 theoretically.

$$A_V \triangleq \frac{V_{out}}{V_{in}} \approx -\frac{R_C}{R_E} \tag{1.2}$$

From simulation result in Figure 1.4, the practical $A_V = \frac{7.6486m}{2m} = 3.8243$ which is close to theoretic value.

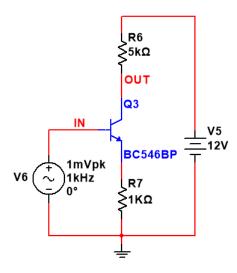


Figure 1.3: Basic transistor circuit with R_c and R_e

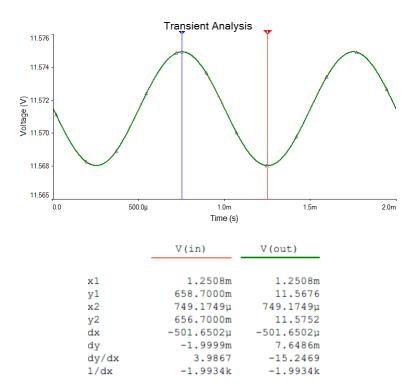


Figure 1.4: Output of the circuit in Figure 1.3

1.4 Add voltage divider

As we know, we need make sure $V_{be} > 0.65V$ for transistor operating correctly. But in practical application, it's hard to keep input signal always meeting this requirement. So we can add capacitor and voltage divider solve this problem like Figure 1.5. In which, capacitor block the original DC voltage of input signal and voltage divider add the DC voltage which we require to signal. Finally, we use another capacitor for outputting pure AC signal form our circuit.

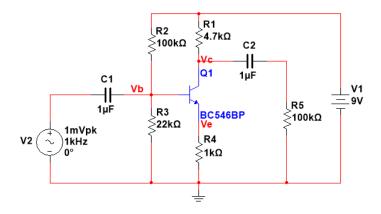


Figure 1.5: Add voltage divider and capacitors

Negative Feedback

2.1 Simple Negative Feedback system

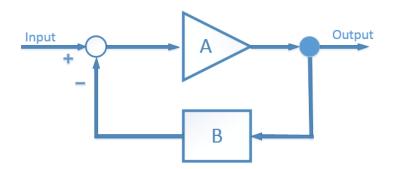


Figure 2.1: simple negative feedback system

Figure 2.1 show a simple negative feedback system in which A is ideal amplifier and B is feedback network.

$$\frac{V_{out}}{V_{in}} = B$$

2.2 Implement Using Op-amp

In Figure 2.2, an Op-amp 741 is used to implement the negative feedback circuit in Figure 2.1.

741 is part A while R1 and R2 form feedback network.

$$\frac{V_{out}}{V_{in}} = B = \frac{R1 + R2}{R2} = \frac{10K + 1K}{1K} = 11$$

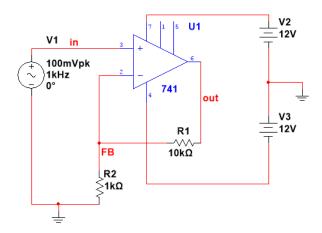


Figure 2.2: Implement negative feedback circuit with Op-amp

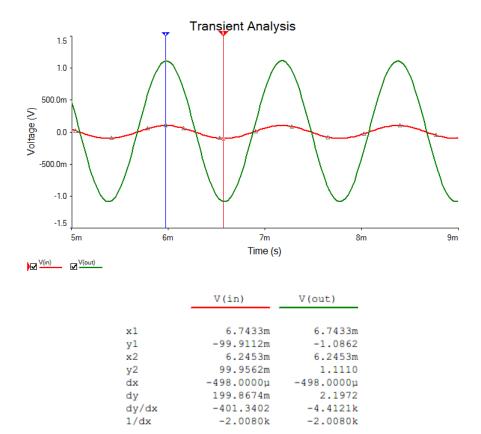


Figure 2.3: Op-amp feedback simulation result curve

From simulation result in Figure 2.3,

$$B = \frac{\Delta V_{out}}{\Delta V_{in}} = \frac{2.1972}{199.8674m} = 10.99328$$

Obviously, the simulation result is very close to our estimation.

2.3 Implement Using transistor

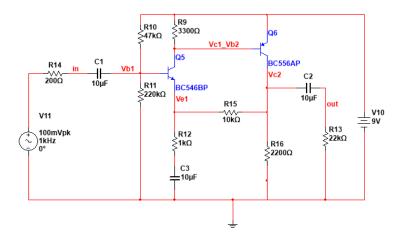
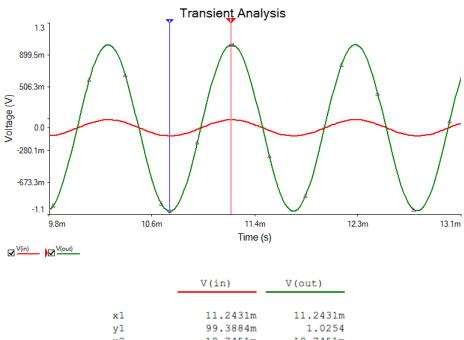


Figure 2.4: Implement negative feedback circuit with transistor

In Figure 2.4 circuit, Op-amp replaced by circuit in Figure 1.5. R12 and R15 make up feedback network which $B = \frac{R15 + R12}{R12} = 11$. As we see in Figure 2.3, the output is reverse to input. Therefore, we add another transistor Q6 to eliminate the phase difference of signal.

Apparently, there's no phase difference between input and output signal. The voltage gain of circuit in Figure 2.4 is $Gain = \frac{\Delta V_{out}}{\Delta V_{in}} = \frac{2.0534}{198.8221m} = 10.3707$. It's also very close to theory result.



x1 11.2431m 11.2431m y1 99.3884m 1.0254 x2 10.7451m 10.7451m y2 -99.4337m -1.0281 dx -498.0000μ -498.0000μ dy -198.8221m -2.0534 dy/dx 399.2412 4.1234k 1/dx -2.0080k -2.0080k

Figure 2.5: transistor feedback circuit simulation result

Current Source

3.1 Single current source circuit

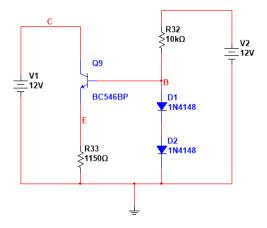


Figure 3.1: single current source circuit

Generally, we need a constant current source in circuit and the most classic one shows in Figure 3.1.

As we know the forward voltage cross a diode is about 0.65V which is approximately equal to V_{be} of transistor.

$$V_B = 2 \times V_{diode} = V_{be} + V_{R_{33}}$$

Therefore:

$$V_{R_{33}} = V_{diode} = 0.65V$$

$$I_e = \frac{V_{R_{33}}}{R_{33}} = \frac{0.65V}{1150\Omega} = 565.217\mu A$$

DC Operating Point Analysis

	Variable	Operating point value
1	@qq9[ic]	503.27881 u
2	@qq9[ie]	-505.07050 u

Figure 3.2: single current source circuit simulation result

From Figure 3.2, we can see simulation result is close to the value we calculated. This simple circuit are able to supply constant current.

3.2 Use current source to replace output resistor

Now we can use current source to replace the R_{16} in circuit of Figure 2.4. Current source can supply stable current output. Till this step, we have finished the voltage amplifier part circuit but current of output is still enough to drive a headphone.

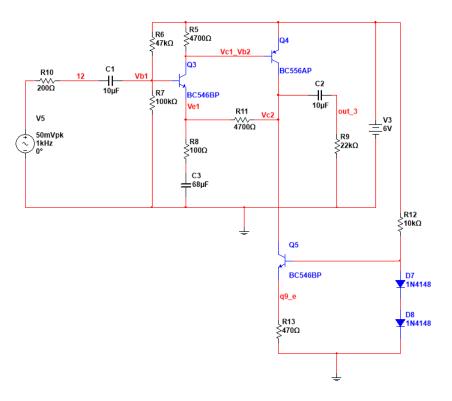


Figure 3.3: the circuit after adding current source

Output Stage

4.1 Class A Output Stage

In Figure 4.1, transistor Q2 and resistor R1 made up of Class A output stage.

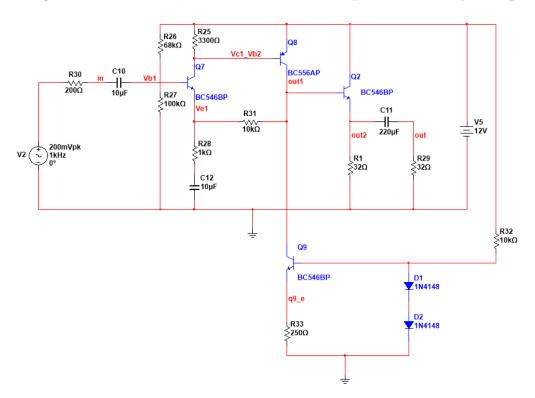


Figure 4.1: Class A output stage

As we can see in Figure 4.2, output signal of class A output stage is good enough to follow the input signal.

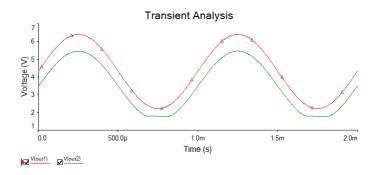


Figure 4.2: Class A output stage simulation result

DC Operating Point Analysis						
Variable	Operating point value					
1 I(Q2[IE])	-109.82711 m					

Figure 4.3: Class A DC operating current simulation data

But from DC operating simulation result in Figure 4.3 we know Class A will consume a lot of current from battery and resistor R1 also waste a lot of power. It's can't acceptable because the final circuit is powered by battery.

4.2 Class AB Output Stage

For better efficiency, we tried Class AB output stage which showed in Figure 4.4. Transistor Q4 and Q5 are used for amplifying upper and lower part of input signal. Resistor R10 and R11 and transistor Q7 are made up of V_{be} multiplier. In this case, it generate $2V_{be}$ cross between collector and emitter of Q7 which eliminates the crossover distortion caused by V_{be} of Q4 and Q5.

Finally, we can see from Figure 4.5 there is almost no distortion in output signal.

In Figure 4.6, we know that DC operating current of Class AB output stage is much smaller than Class A. Therefore, Class AB output stage much more efficient and meet our requirement.

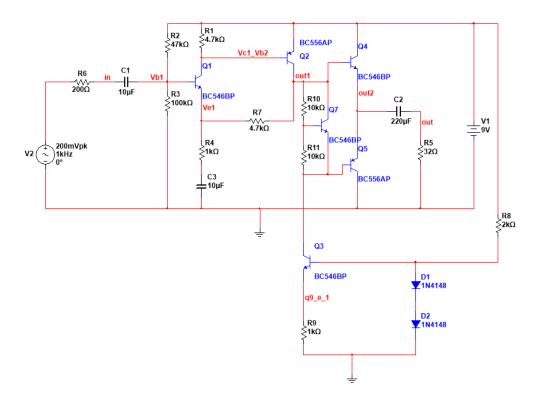


Figure 4.4: Class AB output stage

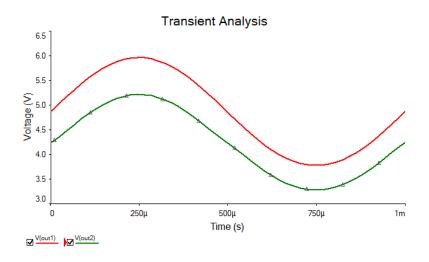


Figure 4.5: Class AV output stage simulation resut

DC Operating Point Analysis

	Variable	Operating point value
1	I(Q4[IE])	-809.46708 u
2	I(Q5[IC])	804.62548 u

Figure 4.6: Class AB output stage DC operating current