

Observability Analysis: Rotary-Wing UAV with Aerodynamic Drag

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System Parameters

Inertia, Mass, and Gravity

In this version of the dynamics, we consider a body frame (B) and inertial frame (W). Without loss of generality, we assume the body frame is the principal axes such that the inertia tensor is diagonal.

```
In[1158]:=
j = {jx, jy, jz}; (* Measured a priori,
either using CAD or something more complicated *)
jmat = DiagonalMatrix[j]
jmatInv = Inverse[jmat];
```

```
Out[1159]=
{{jx, 0, 0}, {0, jy, 0}, {0, 0, jz}}
```

```
In[1161]:=
m; g; (* Measured a priori *)
```

Motor Coefficients

```
In[1162]:=
τm; (* first order time constant of the motor response *)
```

Propeller Coefficients

```
In[1163]:=
kη; (* Thrust coefficient *)
km; (* Yaw moment coefficient *)
kd; (* Rotor drag coefficient *)
kz; (* Loss of thrust due to inflow, inflow coefficient *)
kh; (* Translational lift coefficient *)
```

Propeller Position Vectors

These vectors are written in the body frame (note the B in front of each vector). Since we choose the body frame, we can assume that these values can be easily measured in CAD and therefore known.

Without loss of generality, we consider a planar symmetric configuration.

```
In[1168]:=
  l; d;

In[1169]:=

BpBR1 = {1, 0, d};
BpBR2 = {0, 1, d};
BpBR3 = {-1, 0, d};
BpBR4 = {0, -1, d};
```

Propeller Rotation Directions

These reflect the direction of each motor, observability result should be invariant to these but it's here for completeness. These results should hold without loss of generality.

```
In[1173]:=
  e = {1, -1, 1, -1};
```

IMU Position Vector and Rotation

The position and rotation of the IMU frame with respect to the body frame. Without loss of generality, choose identity with zero offset from CoM.

```
In[1174]:=
  BpBI = {0, 0, 0}; (* xyz position of the IMU w.r.t. the body axes,
  in which case we assume to be known *)
  psiI = 0; (* Yaw angle of IMU frame from body axes *)
  IRB = {{Cos[psiI], -Sin[psiI], 0}, {Sin[psiI], Cos[psiI], 0}, {0, 0, 1}}
  (* Recall that we assume that IMU z axis and principal z axis are parallel *)

Out[1176]=
  {{1, 0, 0}, {0, 1, 0}, {0, 0, 1}}
```

IMU biases

Typically these biases can be calibrated at the beginning of the flight.

```
In[1177]:=
  ba = {bax, bay, baz};
  bg = {bgx, bgy, bgz};
```

System States

Inertial Position

```
In[1179]:=
  Wpos = {xpos, ypos, zpos};
```

Body Attitude (Represented with Euler Angles)

The body attitude is represented using Euler angles.

```
In[1180]:=
 $\theta$ ; (* Pitch angle about the y axis *)
 $\psi$ ; (* Yaw angle about the z axis *)
 $\phi$ ; (* Roll angle about the x axis *)
 $\Theta = \{\phi, \theta, \psi\};$ 
```

Construct the elementary rotation matrices

```
In[1184]:=
 $R\phi = \{\{1, 0, 0\}, \{0, \cos[\phi], -\sin[\phi]\}, \{0, \sin[\phi], \cos[\phi]\}\};$ 
```

```
In[1185]:=
 $R\theta = \{\{\cos[\theta], 0, \sin[\theta]\}, \{0, 1, 0\}, \{-\sin[\theta], 0, \cos[\theta]\}\};$ 
```

```
In[1186]:=
 $R\psi = \{\{\cos[\psi], -\sin[\psi], 0\}, \{\sin[\psi], \cos[\psi], 0\}, \{0, 0, 1\}\};$ 
```

Now construct the rotation from the inertial frame (W) to the body frame (B). This is a ZYX rotation.

```
In[1187]:=
 $WRB = R\psi.R\theta.R\phi; \text{MatrixForm}[WRB]$ 
```

```
Out[1187]//MatrixForm=

$$\begin{pmatrix} \cos[\theta] \cos[\psi] \cos[\phi] \sin[\theta] \sin[\phi] - \cos[\phi] \sin[\psi] & \cos[\phi] \cos[\psi] \sin[\theta] + \sin[\phi] \sin[\psi] \\ \cos[\theta] \sin[\psi] \cos[\phi] \sin[\theta] \sin[\phi] + \sin[\theta] \sin[\phi] \sin[\psi] & -\cos[\psi] \sin[\phi] + \cos[\phi] \sin[\theta] \sin[\psi] \\ -\sin[\theta] & \cos[\theta] \sin[\phi] \end{pmatrix}$$

```

And get the inverse, which rotates a vector in the inertial frame (W) to the body frame (B)

```
In[1188]:=
 $BRW = \text{Transpose}[WRB]; \text{MatrixForm}[BRW]$ 
```

```
Out[1188]//MatrixForm=

$$\begin{pmatrix} \cos[\theta] \cos[\psi] & \cos[\theta] \sin[\psi] & -\sin[\theta] \\ \cos[\psi] \sin[\theta] \sin[\phi] - \cos[\phi] \sin[\psi] & \cos[\phi] \cos[\psi] + \sin[\theta] \sin[\phi] \sin[\psi] & \cos[\theta] \sin[\phi] \\ \cos[\phi] \cos[\psi] \sin[\theta] + \sin[\phi] \sin[\psi] & -\cos[\psi] \sin[\phi] + \cos[\phi] \sin[\theta] \sin[\psi] & \cos[\theta] \cos[\phi] \end{pmatrix}$$

```

Velocity (in both frames)

```
In[1189]:=
 $Wvel = \{xdot, ydot, zdot\};$ 
 $Bvel = \{Bxdot, Bydot, Bzdot\};$ 
```

```
In[1191]:=
 $\Omega = \{p, q, r\}; (* \text{The rates expressed in the Body Frame!!} *)$ 
```

Wind Vector (in both frames)

```
In[1192]:=
 $Wwind = \{wx, wy, wz\};$ 
 $Bwind = \{Bwx, Bwy, Bwz\};$ 
```

Motor Speeds

```
In[1194]:=
 $\eta = \{\eta_1, \eta_2, \eta_3, \eta_4\};$ 
```

Control Forces and Moments

Commanded Motor Speeds

```
In[1195]:=
 $u = \{u_1, u_2, u_3, u_4\};$ 
```

Rotor Thrusts

```
In[1196]:=
 $\text{thrusts} = k\eta * (\eta^2)$ 
```

```
Out[1196]=
 $\{k\eta \eta_1^2, k\eta \eta_2^2, k\eta \eta_3^2, k\eta \eta_4^2\}$ 
```

```
In[1197]:=
BTR1 = {0, 0, thrusts[[1]]};
(* These are the individual thrust vectors in the body frame coordinates *)
BTR2 = {0, 0, thrusts[[2]]};
BTR3 = {0, 0, thrusts[[3]]};
BTR4 = {0, 0, thrusts[[4]]};
```

Rotor Yaw Moments

```
In[1201]:=
 $\text{dragmoment} = \epsilon * k_m * (\eta^2)$ 
```

```
Out[1201]=
 $\{k_m \eta_1^2, -k_m \eta_2^2, k_m \eta_3^2, -k_m \eta_4^2\}$ 
```

```
In[1202]:=
ByawmomentR1 = {0, 0, dragmoment[[1]]};
(* These are the drag moments in the body frame coordinates *)
ByawmomentR2 = {0, 0, dragmoment[[2]]};
ByawmomentR3 = {0, 0, dragmoment[[3]]};
ByawmomentR4 = {0, 0, dragmoment[[4]]};
```

Control Wrench

The total moments cause by each rotor is the drag moment + the moment arm

```
In[1206]:=
BcontrolmomentR1 = BpBR1 * BTR1 + ByawmomentR1;
BcontrolmomentR2 = BpBR2 * BTR2 + ByawmomentR2;
BcontrolmomentR3 = BpBR3 * BTR3 + ByawmomentR3;
BcontrolmomentR4 = BpBR4 * BTR4 + ByawmomentR4;
```

```
In[1210]:=
Btotcontrolmoment =
  BcontrolmomentR1 + BcontrolmomentR2 + BcontrolmomentR3 + BcontrolmomentR4 ;
(* This is the total moment expressed in the body frame! *)
Btotcontrolforce = {0, 0, Total[thrusts]};
```

Aerodynamic Forces and Moments

Aerodynamic forces consist of rotor drag, loss of thrust due to inflow, and parasitic (frame) drag. These are all defined in the body frame. Note that we are assuming that each propulsive unit sees the same airspeed (i.e. small body rates) and that they have the same describing coefficients (rotor drag, blade flapping, etc.). This enables us to compute the rotor drag faster.

Airspeed Calculation

```
In[1212]:=
Wva = Wvel - Wwind;
Bva = Bvel - Bwind;
airspeed = (Bva[[1]]^2 + Bva[[2]]^2 + Bva[[3]]^2)^(1/2);
vh2 = Bva[[1]]^2 + Bva[[2]]^2

Out[1215]=
(-Bwx + Bxdot)^2 + (-Bwy + Bydot)^2
```

Rotor Drag

```
In[1216]:=
BrotordragR1 = -η1 * DiagonalMatrix[{kd, kd, kz}].Bva;
BrotordragR2 = -η2 * DiagonalMatrix[{kd, kd, kz}].Bva;
BrotordragR3 = -η3 * DiagonalMatrix[{kd, kd, kz}].Bva;
BrotordragR4 = -η4 * DiagonalMatrix[{kd, kd, kz}].Bva;

In[1220]:=
BH = BrotordragR1 + BrotordragR2 + BrotordragR3 + BrotordragR4;
```

Moment Due to Rotor Drag

```
In[1221]:=
BrotordragmomentR1 = BpBR1 * BrotordragR1;
BrotordragmomentR2 = BpBR2 * BrotordragR2;
BrotordragmomentR3 = BpBR3 * BrotordragR3;
BrotordragmomentR4 = BpBR4 * BrotordragR4;

Btotrotordragmoment =
  BrotordragmomentR1 + BrotordragmomentR2 + BrotordragmomentR3 + BrotordragmomentR4;
```

Translational Lift

```
In[1226]:=
  BTL = {0, 0, 4 * kh * vh2};
```

Total Aerodynamic Wrench

```
In[1227]:=
  Btotaeroforce = BH + BTL;
  Btotaeromoment = Btotrotordragmoment;
```

Total Forces and Moments

Compute the total forces and moments in the body frame

```
In[1229]:=
  Btotforce = Btotcontrolforce + Btotaeroforce;
  Wtotforce = WRB.Btotforce;

In[1231]:=
  Btotmoment = Btotcontrolmoment + Btotaeromoment;
```

Filter States

```
In[1232]:=
  constants = {k $\eta$ , km, kd, kz, kflap,  $\tau$ m};

In[1233]:=
  x = Join[Bvel,  $\theta$ ,  $\Omega$ ,  $\eta$ , Bwind]

Out[1233]=
  {Bxdot, Bydot, Bzdot,  $\phi$ ,  $\theta$ ,  $\psi$ , p, q, r,  $\eta$ 1,  $\eta$ 2,  $\eta$ 3,  $\eta$ 4, Bwx, Bwy, Bwz}

In[1234]:=

In[1235]:=
  n = Length[x]

Out[1235]=
  16

In[1236]:=
  statevec = x;
  inputvec = u;
```

Process Model

Kinematics

```
In[1238]:=
Wposdot = Wvel;
MatrixForm[Wposdot];

In[1240]:=
 $\theta\dot{} = \{ \{1, \sin[\phi] * \tan[\theta], \cos[\phi] * \tan[\theta]\}, \{0, \cos[\phi], -\sin[\phi]\}, \{0, \sin[\phi] * \sec[\theta], \cos[\phi] * \sec[\theta]\} \} . \Omega;$ 
MatrixForm[ $\theta\dot{}]$ ;
```

Rotational Dynamics

```
In[1242]:=
 $\Omega\dot{} = \text{jmatInv.}(\text{Btotmoment} - \text{Cross}[\Omega, \text{jmat.}\Omega]);$ 
MatrixForm[ $\Omega\dot{}]$ ;
```

Translational Dynamics

```
In[1244]:=
Wvelldot = (1/m) * (Wtotforce + {0, 0, -m*g});
MatrixForm[Wvelldot];

In[1246]:=
Bvelldot = (1/m) * (Btotforce + BRW.{0, 0, -m*g}) - Cross[ $\Omega$ , Bvel];
MatrixForm[Bvelldot];
```

Motor Dynamics

```
In[1248]:=
 $\eta\dot{} = (1/\tau m) * (u - \eta);$ 
MatrixForm[ $\eta\dot{}]$ ;
```

Wind Dynamics

```
In[1250]:=
Wwinddot = ConstantArray[0, 3];
Bwinddot = ConstantArray[0, 3];
MatrixForm[Bwinddot];
```

Parameter Dynamics

Assume that the parameters do not change over time.

```
In[1253]:=
f = Join[Bvelldot,  $\theta\dot{}$ ,  $\Omega\dot{}$ ,  $\eta\dot{}$ , Bwinddot];

In[1254]:=
(*For[i=0,i<Length[x],i++,Print[f[[i]]]*)
```

```
In[1255]:=
  (*For[i=0, i≤Length[x], i++,Print[Grad[f,x][i]]]*)

In[1256]:=
  vecfield = f;
```

Measurement Model

The measurement model includes the gyro and accelerometer measurements.

```
In[1257]:=
  aAct = (1/m) * Btotforce;

In[1258]:=
  hAcc = IRB.aAct;
  hGyro = IRB.Ω;
  hVel = Bvel;
  hPos = Wpos;
  hAttitude = Θ;
  hMotor = η;

In[1264]:=
  h = Join[hAcc, hGyro, hVel, hAttitude, hMotor];

In[1265]:=
  outputvec = h;

In[1266]:=
  (*For[i=0,i≤15,i++,Print[h[i]]]*)

In[1267]:=
  (*For[i=0, i≤Length[h], i++,Print[Grad[h,x][i]]]*)
```

Observability Analysis

Automated Analysis

```
In[1268]:=
  lieseq = {{}, {0}, {1}, {2}, {3}, {4}};
  (* Which Lie derivatives to take. Empty set is the output function itself *)

In[1269]:=
  rule0 = Table[inputvec[[i]] → 0, {i, 1, Length[inputvec]}];

In[1270]:=
  vecfield0 = vecfield /. rule0;

In[1271]:=
  rules = Table[Table[inputvec[[j]] → KroneckerDelta[i, j], {j, 1, Length[inputvec]}],
    {i, 1, Length[inputvec]}];

In[1272]:=
  cavecfields = Table[vecfield - vecfield0 /. rules[[i]], {i, 1, Length[inputvec]}];

In[1273]:=
  vecfields = Join[{vecfield0}, cavecfields];
```



```

In[1274]:=
  LieIterate[h_, i_] := Grad[h, statevec].vecfields[[i + 1]];

In[1275]:=
  LieDerivative[h_, seq_] := Fold[LieIterate, h, seq];

In[1276]:=
  lies = Table[LieDerivative[outputvec, lieseq[[i]]], {i, 1, Length[lieseq]};

In[1277]:=
  obsvec = DeleteCases[Flatten[lies], 0]; MatrixForm[obsvec];

In[1278]:=
  obsmat = Grad[obsvec, statevec];

In[1279]:=
  params = statevec;

In[1280]:=
  psub = Table[i, {i, 1, Length[params]}];

In[1281]:=
  psubrules = Table[params[[i]] → psub[[i]], {i, 1, Length[params]}];

In[1282]:=
  obsmateval = obsmat /. psubrules;

In[1283]:=
  (*NullSpace[obsmateval];*)

In[1284]:=
  MatrixRank[obsmateval]

Out[1284]=
  16

In[1285]:=
  Length[statevec]

Out[1285]=
  16

```