

Instructor's Supplement Problems

Chapter 11

- Given the unity-feedback system of Figure P11.1 in the text problems with

$$G(s) = \frac{K(s+10)(s+15)}{s(s+2)(s+5)(s+20)}$$

do the following: [Section: 11.2]

- Use frequency response methods to determine the value of gain, K , to yield a step response with a 20% overshoot. Make any required second-order approximations.
 - Use MATLAB or any other computer program to test your second-order approximation by simulating the system for your designed value of K . ML
- Given the unity-feedback system of Figure P11.1 in the text problems with

$$G(s) = \frac{K(s+10)(s+11)}{s(s+3)(s+6)(s+9)}$$

do the following: [Section: 11.3]

- Use frequency response methods to design a lag compensator to yield $K_v = 1000$ and 15%-overshoot for the step response. Make any required second-order approximations.
 - Use MATLAB or any other computer program to test your second-order approximation by simulating the system for your designed value of K and lag compensator. ML
- Design a lag compensator so that the system of Figure P11.1 in the text problems where

$$G(s) = \frac{K(s+4)}{(s+2)(s+6)(s+8)}$$

operates with a 45° phase margin and a static error constant of 100. [Section: 11.3]

- For the system of Problem 2 above, do the following: [Section: 11.3]
 - Use frequency response methods to find the gain, K , required to yield about 15%-overshoot. Make any required second-order approximations.

- Use frequency response methods to design a PI compensator to yield zero steady-state error for a ramp input without appreciably changing the transient response characteristics designed in Part a.

- Use MATLAB or any other computer program to test your second-order approximation by simulating the system for your designed value of K and PI compensator. ML

- Repeat the design of Example 11.3 in the text using a PD controller. [Section: 11.4]
- Repeat Problem 12 in the text problems for a PD controller. ML
- The model for a specific linearized TCP/IP computer network queue, working under a random early detection (RED) algorithm, has been modeled using the block diagram of Figure P11.1 in the text problems, where $G(s) = M(s)P(s)$, with

$$M(s) = \frac{0.005L}{s + 0.005}$$

and

$$P(s) = \frac{140,625e^{-0.1s}}{(s+2.67)(s+10)}$$

Also, L is a parameter to be varied (Hollot, 2001).

- Adjust L to obtain a 15%-overshoot in the transient response for step inputs.
 - Verify Part a with a Simulink unit-step response simulation. SL
- Active front steering is used in front-steering four-wheel cars to control the yaw rate of the vehicle as a function of changes in wheel-steering commands. For a certain car, and under certain conditions, it has been shown that the transfer function from steering wheel angle to yaw rate is given by (Zhang, 2008):

$$P(s) = \frac{28.4s + 119.7}{s^2 + 7.15s + 14.7}$$

The system is controlled in a unity-feedback configuration.

2 Instructor's Supplement Problems

- a. Use the Nichols chart and follow the procedure of Example 11.5 to design a lag-lead compensator such that the system has zero steady-state error for a step input. The bandwidth of the closed-loop system must be $\omega_B = 10$ rad/s. Let the open-loop magnitude response peak be less than 1 dB and the steady-state error constant $K_v = 20$.
 - b. Relax the bandwidth requirement to $\omega_B \geq 10$ rad/s. Design the system for a steady-state error of zero for a step input. Let the open-loop magnitude response peak be less than 1 dB and $K_v = 20$ using only a lead compensator.
 - c. Simulate the step response of both designs using MATLAB. ML
9. The amount of leftover moisture in a grain drying conveyor process can be controlled by varying the conveyor's motor speed (*Mansor, 2011*). Although the

process is highly variable, the transfer function at one of the operating points has been found to be

$$G(s) = \frac{0.0169s + 0.03558}{3.368s^3 + 3.762s^2 + 32.19s + 1} e^{-27s}$$

A unity-feedback system will be built around this plant such as the one shown in Figure P11.1 in the text problems to maintain grain moisture at specified levels. The specifications are: $e_{ss} = 0$ for a unit-step input; e_{ss} is half that of the uncompensated system for a ramp input; settling time = 500 seconds, and %OS = 13%.

Since the system is Type 0, it must be augmented to a Type 1 using an integrator in order to achieve $e_{ss} = 0$ for a step input. In addition, a phase lead-lag compensator will be required to achieve the specifications. Simulate your design using a computer program.

Bibliography

- Hollot, C. V., Misra, V., Towsley, D., and Gong, W. A Control Theoretic Analysis of RED. Proceedings of IEEE INFOCOM, 2001, pp. 1510–1519.
- Mansor, H., Noor, S. B. M., Ahmad, R. K. R., and Taip, F. S. Online Quantitative feedback theory (QFT)-based self-tuning controller for grain drying process. *Scientific Research and Essays*, vol. 6, no. 31, December 16, 2011, pp. 6520–6534.
- Zhang, J.-Y., Kim, J.-W., Lee, K.-B., and Kim, Y.-B. Development of an Active Front Steering (AFS) System With QFT Control. *International Journal of Automotive Technology*, vol. 9, no. 6, 2008, pp. 695–702.