

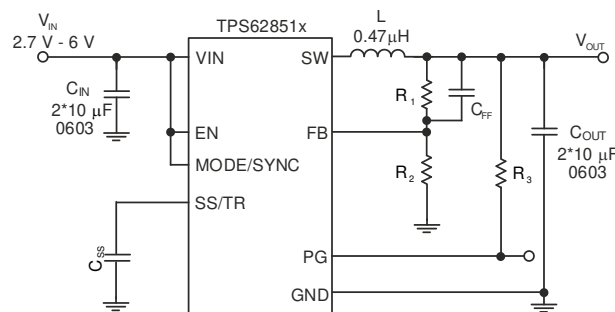
TPS62851x 2.7-V to 6-V, 0.5-A / 1-A / 2-A Step-Down Converter in SOT583 Package

1 Features

- $T_J = -40^{\circ}\text{C}$ to $+150^{\circ}\text{C}$
- Input voltage range: 2.7 V to 6 V
- Quiescent current 15 μA typical
- Output voltage from 0.6 V to 5.5 V
- Output voltage accuracy $\pm 1\%$ (PWM operation)
- Adjustable soft start-up to 10 ms
- Forced PWM or PWM/PFM operation
- Switching frequency in PWM: 2.25 MHz
- Switching Frequency external sync (1.8 MHz to 4 MHz)
- Precise ENABLE input allows:
 - User-defined undervoltage lockout
 - Exact sequencing
- 100% Duty cycle mode
- Active output discharge
- Spread spectrum clocking - optional
- Foldback overcurrent protection - optional
- Power-good output with window comparator

2 Applications

- [Motor drives](#)
- [Factory automation and control](#)
- [Building automation](#)
- [Test and measurement](#)
- [Multi-function printer \(MFP\)](#)
- General purpose POL



Simplified Schematic

3 Description

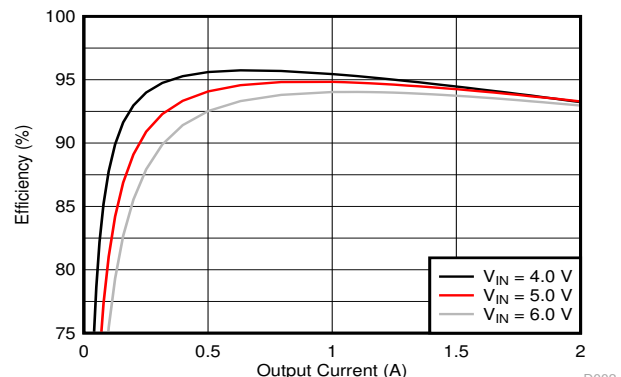
The TPS62851x is a family of pin-to-pin 0.5-A, 1-A, and 2-A high efficiency, easy-to-use, synchronous step-down DC/DC converters. They are based on a peak current mode control topology. Low resistive switches allow up to 2-A continuous output current at high ambient temperature. The switching frequency is internally fixed at 2.25 MHz and can also be synchronized to an external clock in the range from 1.8 MHz to 4 MHz. In PWM/PFM mode, the TPS62851x automatically enters Power Save Mode at light loads to maintain high efficiency across the whole load range. The TPS62851x provide a 1% output voltage accuracy in PWM mode which helps design a power supply with high output voltage accuracy. The SS/TR pin allows setting the start-up time or forming tracking of the output voltage to an external source. This allows external sequencing of different supply rails and limits the inrush current during start-up.

The TPS62851x are available in a SOT583 package.

Device Information

PART NUMBER	PACKAGE ⁽¹⁾	BODY SIZE (NOM)
TPS628510	SOT583	2.1 mm x 1.6 mm (incl pins)
TPS628511	SOT583	2.1 mm x 1.6 mm (incl pins)
TPS628512	SOT583	2.1 mm x 1.6 mm (incl pins)

(1) For all available packages, see the orderable addendum at the end of the data sheet.



Efficiency versus I_{OUT} , $V_{OUT} = 3.3\text{ V}$



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4 Revision History

NOTE: Page numbers for previous revisions may differ from page numbers in the current version.

DATE	REVISION	NOTES
August 2020	*	Initial release

5 Device Comparison Table

DEVICE NUMBER	OUTPUT CURRENT	V _{out} DISCHARGE	FOLDBACK CURRENT LIMIT	SPREAD SPECTRUM CLOCKING (SSC)	SOFT START	OUTPUT VOLTAGE
TPS628510DRLR	0.5 A	ON	OFF	OFF	external cap on SS/TR pin	adjustable
TPS628511DRLR	1 A	ON	OFF	OFF	external cap on SS/TR pin	adjustable
TPS628512DRLR	2 A	ON	OFF	OFF	external cap on SS/TR pin	adjustable

6 Pin Configuration and Functions

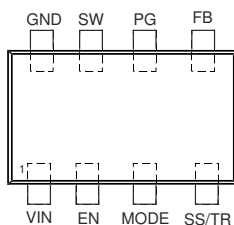


Figure 6-1. 8-Pin SOT583 DRL Package (Top View)

Pin Functions

PIN		I/O	DESCRIPTION
NAME	NO.		
EN	2	I	This is the enable pin of the device. Connect to logic low to disable the device. Pull high to enable the device. Do not leave this pin unconnected.
FB	5	I	Voltage feedback input. Connect the resistive output voltage divider to this pin.
GND	8		Ground pin
MODE/SYNC	3	I	The device runs in PFM/PWM mode when this pin is pulled low. When the pin is pulled high, the device runs in forced PWM mode. Do not leave this pin unconnected. The mode pin can also be used to synchronize the device to an external frequency. See Section 7.5 for the detailed specification for the digital signal applied to this pin for external synchronization.
PG	6	O	Open-drain power-good output
SS/TR	4	I	Soft-Start / Tracking pin. An external capacitor connected from this pin to GND defines the rise time for the internal reference voltage. The pin can also be used as an input for tracking and sequencing - see Section 10.3.2 in this data sheet.
SW	7		This is the switch pin of the converter and is connected to the internal Power MOSFETs.
VIN	1		Power supply input. Make sure the input capacitor is connected as close as possible between pin VIN and GND.

7 Specifications

7.1 Absolute Maximum Ratings

over operating temperature range (unless otherwise noted)⁽¹⁾

		MIN	MAX	UNIT
Pin voltage ⁽²⁾	V _{IN}	– 0.3	6.5	V
Pin voltage ⁽²⁾	SW (DC)	– 0.3	V _{IN} + 0.3	V
Pin voltage ⁽²⁾	SW (AC, less than 10ns) ⁽³⁾	– 3	10	V
Pin voltage ⁽²⁾	FB	– 0.3	4	V
Pin voltage ⁽²⁾	SS/TR, PG	– 0.3	V _{IN} + 0.3	V
Pin voltage ⁽²⁾	EN, MODE/SYNC	– 0.3	6.5	V
T _{stg}	Storage temperature	–65	150	°C

(1) Stresses beyond those listed under *Absolute Maximum Rating* may cause permanent damage to the device. These are stress ratings only, which do not imply functional operation of the device at these or any other conditions beyond those indicated under *Recommended Operating Condition*. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

(2) All voltage values are with respect to the network ground terminal

(3) While switching

7.2 ESD Ratings

			VALUE	UNIT
V _(ESD)	Electrostatic discharge	Human body model (HBM), per ANSI/ESDA/JEDEC JS-001, all pins ⁽¹⁾	±2000	V
		Charged device model (CDM), per JEDEC specification JESD22-C101, all pins ⁽²⁾	±750	

(1) JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.

(2) JEDEC document JEP157 states that 250-V CDM allows safe manufacturing with a standard ESD control process.

7.3 Recommended Operating Conditions

Over operating temperature range (unless otherwise noted)

		MIN	NOM	MAX	UNIT
V _{IN}	Input voltage range	2.7		6	V
V _{OUT}	Output voltage range	0.6		5.5	V
L	Effective inductance	0.32	0.47	1.2	μH
C _{OUT}	Effective output capacitance ⁽¹⁾	8	10	200	μF
C _{IN}	Effective input capacitance ⁽¹⁾	5	10		μF
I _{SINK_PG}	Sink current at PG pin	0		2	mA
T _J	Junction temperature	–40		150	°C

(1) The values given for all the capacitors in the table are effective capacitance, which includes the DC bias effect. Due to the DC bias effect of ceramic capacitors, the effective capacitance is lower than the nominal value when a voltage is applied. Please check the manufacturer's DC bias curves for the effective capacitance vs DC voltage applied. Further restrictions may apply. Please see the feature description for COMP/FSET about the output capacitance vs compensation setting and output voltage.

7.4 Thermal Information

THERMAL METRIC ⁽¹⁾		TPS62851x	TPS62851x	UNIT
		DRL (JEDEC) ⁽²⁾	DRL (EVM)	
		8 PINS	8 PINS	
R _{θJA}	Junction-to-ambient thermal resistance	110	60	°C/W
R _{θJC(top)}	Junction-to-case (top) thermal resistance	41.3	n/a	°C/W
R _{θJB}	Junction-to-board thermal resistance	20	n/a	°C/W

THERMAL METRIC ⁽¹⁾		TPS62851x	TPS62851x	UNIT
		DRL (JEDEC) ⁽²⁾	DRL (EVM)	
		8 PINS	8 PINS	
Ψ_{JT}	Junction-to-top characterization parameter	0.8	n/a	°C/W
Y_{JB}	Junction-to-board characterization parameter	20	n/a	°C/W
$R_{\theta JC(bot)}$	Junction-to-case (bottom) thermal resistance	n/a	n/a	°C/W

(1) For more information about traditional and new thermal metrics, see the [Semiconductor and IC Package Thermal Metrics](#) application report.

(2) JEDEC standard PCB with 4 layers, no thermal vias

7.5 Electrical Characteristics

Over operating junction temperature range ($T_J = -40^{\circ}\text{C}$ to $+150^{\circ}\text{C}$) and $V_{IN} = 2.7\text{ V}$ to 6 V . Typical values at $V_{IN} = 5\text{ V}$ and $T_J = 25^{\circ}\text{C}$. (unless otherwise noted)

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
SUPPLY						
I_Q	Quiescent current	EN = V_{IN} , no load, device not switching, MODE = GND, $V_{OUT} = 0.6\text{ V}$		17	34	μA
I_{SD}	Shutdown current	EN = GND, Nominal value at $T_J = 25^{\circ}\text{C}$, Max value at $T_J = 150^{\circ}\text{C}$		1.5	48	μA
V_{UVLO}	Undervoltage lock out threshold	V_{IN} rising	2.45	2.6	2.7	V
		V_{IN} falling	2.1	2.5	2.6	V
T_{JSD}	Thermal shutdown threshold	T_J rising		170		°C
	Thermal shutdown hysteresis	T_J falling		15		°C
CONTROL and INTERFACE						
$V_{EN,IH}$	Input threshold voltage at EN, rising edge		1.05	1.1	1.15	V
$V_{EN,IL}$	Input threshold voltage at EN, falling edge		0.96	1.0	1.05	V
V_{IH}	High-level input-threshold voltage at MODE/SYNC		1.1			V
$I_{EN,LKG}$	Input leakage current into EN	$V_{IH} = V_{IN}$ or $V_{IL} = \text{GND}$			125	nA
V_{IL}	Low-level input-threshold voltage at MODE/SYNC				0.3	V
I_{LKG}	Input leakage current into MODE/SYNC				100	nA
t_{Delay}	Enable delay time	Time from EN high to device starts switching; V_{IN} applied already	135	200	520	μs
t_{Delay}	Enable delay time	Time from EN high to device starts switching; V_{IN} applied already, $V_{IN} \geq 3.3\text{ V}$			480	μs
t_{Ramp}	Output voltage ramp time	Time from device starts switching to power good; device not in current limit	0.8	1.3	1.8	ms
t_{Ramp}	Output voltage ramp time, SS/TR pin open	Time from device starts switching to power good; device not in current limit	90	150	210	μs
$I_{SS/TR}$	SS/TR source current		2	2.5	2.8	μA
	Tracking gain	$V_{FB} / V_{SS/TR}$		1		
	Tracking offset	V_{FB} when $V_{SS/TR} = 0\text{ V}$		± 1		mV
f_{SYNC}	Frequency range on MODE/SYNC pin for synchronization		1.8		4	MHz
	Duty cycle of synchronization signal at MODE/SYNC		20		80	%
	Time to lock to external frequency			50		μs
V_{TH_PG}	UVP power good threshold voltage; DC level	rising ($\%V_{FB}$)	92	95	98	%
V_{TH_PG}	UVP power good threshold voltage; DC level	falling ($\%V_{FB}$)	87	90	93	%

Over operating junction temperature range ($T_J = -40^{\circ}\text{C}$ to $+150^{\circ}\text{C}$) and $V_{IN} = 2.7\text{ V}$ to 6 V . Typical values at $V_{IN} = 5\text{ V}$ and $T_J = 25^{\circ}\text{C}$. (unless otherwise noted)

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
V_{TH_PG}	OVP power good threshold voltage; DC level	rising ($\%V_{FB}$)	107	110	113	%
	OVP power good threshold voltage; DC level	falling ($\%V_{FB}$)	104	107	111	%
V_{PG_OL}	Low-level output voltage at PG	$I_{SINK_PG} = 2\text{ mA}$		0.07	0.3	V
I_{PG_LKG}	Input leakage current into PG	$V_{PG} = 5\text{ V}$			100	nA
t_{PG}	PG deglitch time	for a high level to low level transition on the power good output		40		μs
OUTPUT						
V_{FB}	Feedback voltage			0.6		V
I_{FB_LKG}	Input leakage current into FB	$V_{FB} = 0.6\text{ V}$		1	70	nA
V_{FB}	Feedback voltage accuracy	PWM, $V_{IN} \geq V_{OUT} + 1\text{ V}$	-1		1	%
V_{FB}	Feedback voltage accuracy	PFM, $V_{IN} \geq V_{OUT} + 1\text{ V}$, $V_{OUT} \geq 1.5\text{ V}$, $C_{O,eff} \geq 10\text{ }\mu\text{F}$, $L = 0.47\text{ }\mu\text{H}$	-1		2	%
V_{FB}	Feedback voltage accuracy	PFM, $V_{IN} \geq V_{OUT} + 1\text{ V}$, $V_{OUT} < 1.5\text{ V}$, $C_{O,eff} \geq 10\text{ }\mu\text{F}$, $L = 0.47\text{ }\mu\text{H}$	-1		3	%
V_{FB}	Feedback voltage accuracy with voltage tracking	$V_{IN} \geq V_{OUT} + 1\text{ V}$, $V_{SS/TR} = 0.3\text{ V}$	-4		4	%
	Load regulation	PWM		0.05		%/A
	Line regulation	PWM, $I_{OUT} = 1\text{ A}$, $V_{IN} \geq V_{OUT} + 1\text{ V}$		0.02		%/V
R_{DIS}	Output discharge resistance				100	Ω
f_{SW}	PWM Switching frequency		2.025	2.25	2.475	MHz
$t_{on,min}$	Minimum on-time of high-side FET	$V_{IN} = 3.3\text{ V}$, $T_J = -40^{\circ}\text{C}$ to 125°C		35	50	ns
$t_{on,min}$	Minimum on-time of low-side FET			10		ns
$R_{DS(ON)}$	High-side FET on-resistance	$V_{IN} \geq 5\text{ V}$		65	120	m Ω
	Low-side FET on-resistance	$V_{IN} \geq 5\text{ V}$		33	70	m Ω
	High-side MOSFET leakage current	$T_J = 85^{\circ}\text{C}$			2.5	μA
	High-side MOSFET leakage current			0.01	44	μA
	Low-side MOSFET leakage current	$T_J = 85^{\circ}\text{C}$			37	μA
	Low-side MOSFET leakage current			0.01	70	μA
	SW leakage	$V(SW) = 0.6\text{ V}$, current into SW pin	-0.05		11	μA
I_{LIMH}	High-side FET switch current limit	DC value, for TPS628512; $V_{IN} = 3\text{ V}$ to 6 V	2.85	3.4	3.9	A
I_{LIMH}	High-side FET switch current limit	DC value, for TPS628511; $V_{IN} = 3\text{ V}$ to 6 V	2.1	2.6	3.0	A
I_{LIMH}	High-side FET switch current limit	DC value, for TPS628510; $V_{IN} = 3\text{ V}$ to 6 V	1.6	2.1	2.5	A
I_{LIMNEG}	Low-side FET negative current limit	DC value		-1.8		A

7.6 Typical Characteristics

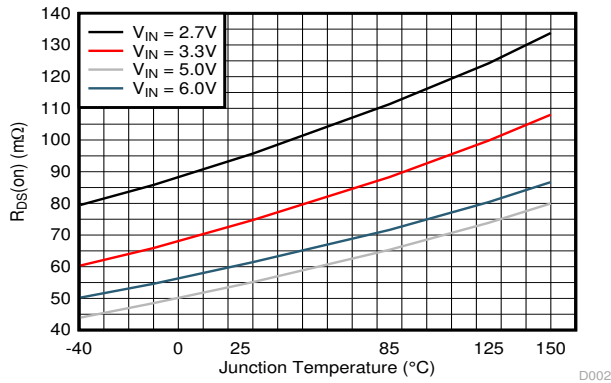


Figure 7-1. $R_{DS(on)}$ of High-side Switch

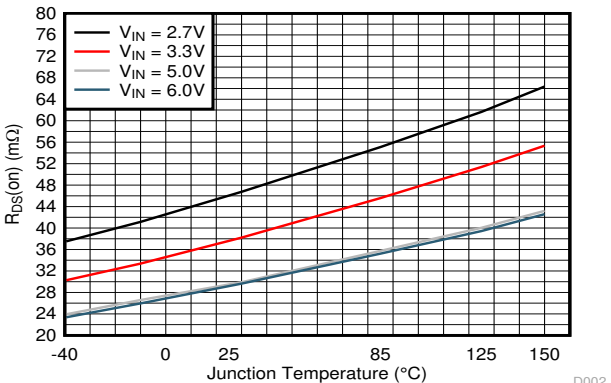


Figure 7-2. $R_{DS(on)}$ of Low-side Switch

8 Parameter Measurement Information

8.1 Schematic

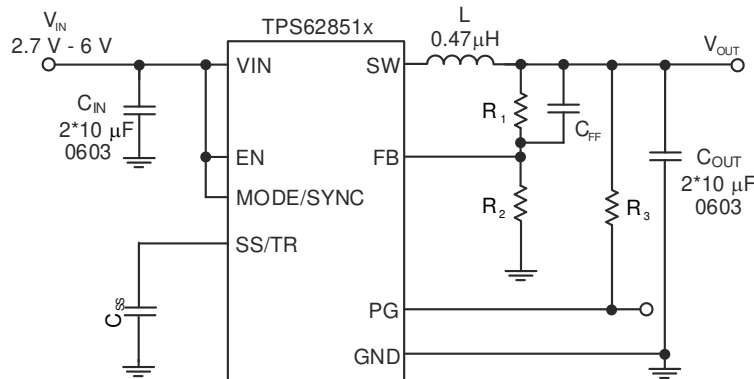


Figure 8-1. Measurement Setup

Table 8-1. List of Components

REFERENCE	DESCRIPTION	MANUFACTURER ⁽¹⁾
IC	TPS628512	Texas Instruments
L	0.47-μH inductor DFE201210U	Murata
C _{IN}	2 x 10 μF / 6.3 V GRM188D70J106MA73	Murata
C _{OUT}	2 x 10 μF / 6.3 V GRM188D70J106MA73 for V _{out} ≥ 1 V	Murata
C _{OUT}	3 x 10 μF / 6.3 V GRM188D70J106MA73 for V _{out} < 1 V	Murata
C _{SS}	4.7 nF (equal to 1-ms start-up ramp); GCM188R72A472KA37	Any
C _{FF}	10 pF	Any
R ₁	Depending on V _{OUT}	Any
R ₂	Depending on V _{OUT}	Any
R ₃	100 kΩ	Any

(1) See the [Section 13.1.1](#).

9 Detailed Description

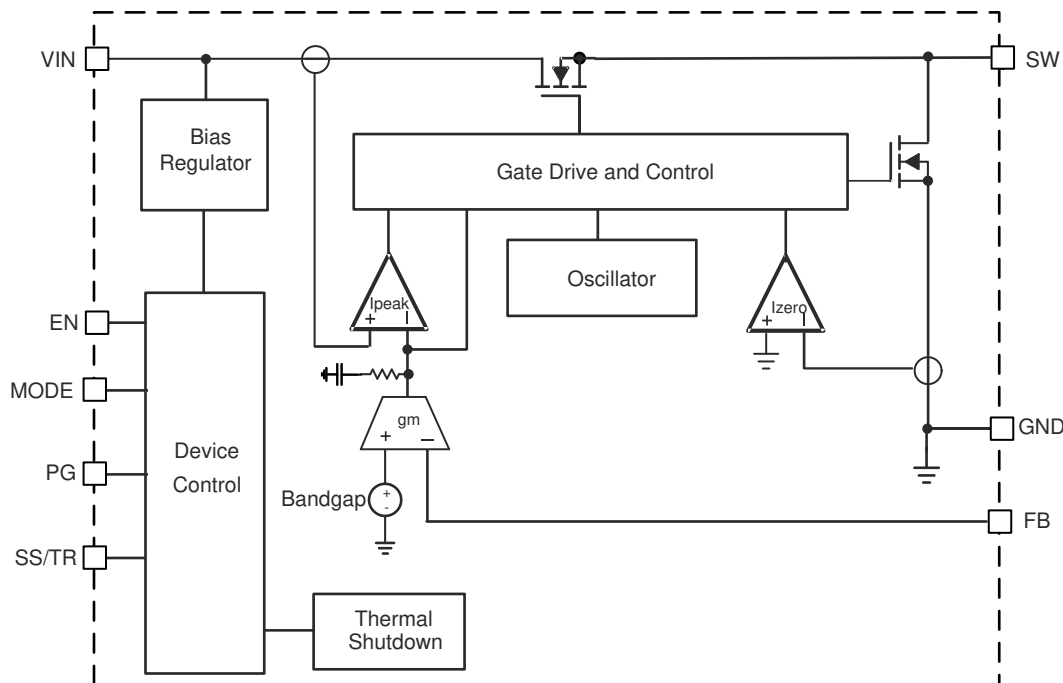
9.1 Overview

The TPS62851x synchronous switch mode power converters are based on a peak current mode control topology. The control loop is internally compensated.

The regulation network achieves fast and stable operation with small external components and low ESR ceramic output capacitors. The devices can be operated without a feedforward capacitor on the output voltage divider, however, using a typically 10-pF feedforward capacitor improves transient response.

The devices support forced fixed frequency PWM operation with the MODE pin tied to a logic high level. The frequency is defined as 2.25 MHz internally fixed. Alternatively, the devices can be synchronized to an external clock signal in a range from 1.8 MHz to 4 MHz, applied to the MODE pin with no need for additional passive components. An internal PLL allows you to change from internal clock to external clock during operation. The synchronization to the external clock is done on a falling edge of the clock applied at MODE to the rising edge on the SW pin. This allows a roughly 180° phase shift when the SW pin is used to generate the synchronization signal for a second converter. When the MODE pin is set to a logic low level, the device operates in power save mode (PFM) at low output current and automatically transfers to fixed frequency PWM mode at higher output current. In PFM mode, the switching frequency decreases linearly based on the load to sustain high efficiency down to very low output current.

9.2 Functional Block Diagram



9.3 Feature Description

9.3.1 Precise Enable (EN)

The voltage applied at the enable pin of the TPS62851x is compared to a fixed threshold of 1.1 V for a rising voltage. This allows you to drive the pin by a slowly changing voltage and enables the use of an external RC network to achieve a power-up delay.

The Precise Enable input provides a user-programmable undervoltage lockout by adding a resistor divider to the input of the Enable pin.

The enable input threshold for a falling edge is typically 100 mV lower than the rising edge threshold. The TPS62851x starts operation when the rising threshold is exceeded. For proper operation, the enable (EN) pin must be terminated and must not be left floating. Pulling the enable pin low forces the device into shutdown, with

a shutdown current of typically 1 μ A. In this mode, the internal high-side and low-side MOSFETs are turned off and the entire internal control circuitry is switched off.

9.3.2 MODE / SYNC

When MODE/SYNC is set low, the device operates in PWM or PFM mode, depending on the output current. The MODE/SYNC pin allows you to force PWM mode when set high. The pin also allows you to apply an external clock in a frequency range from 1.8 MHz to 4 MHz for external synchronization. The specifications for the minimum on-time and minimum off-time have to be observed when setting the external frequency. The external clock must be set to about 2.25 MHz initially and then increased or decreased to the desired frequency. This ensures a low distortion of the output voltage when the external frequency is applied.

9.3.3 Spread Spectrum Clocking (SSC)

The device offers spread spectrum clocking as an option. When SSC is enabled, the switching frequency is randomly changed in PWM mode when the internal clock is used. The frequency variation is typically between the nominal switching frequency and up to 288 kHz above the nominal switching frequency. When the device is externally synchronized by applying a clock signal to the MODE/SYNC pin, the TPS62851x follows the external clock and the internal spread spectrum block is turned off. SSC is also disabled during soft start.

9.3.4 Undervoltage Lockout (UVLO)

If the input voltage drops, the undervoltage lockout prevents misoperation of the device by switching off both the power FETs. When enabled, the device is fully operational for input voltages above the rising UVLO threshold and turns off if the input voltage trips below the threshold for a falling supply voltage.

9.3.5 Power Good Output (PG)

Power good is an open-drain output that requires a pullup resistor to any voltage up to the recommended input voltage level. It is driven by a window comparator. PG is held low when the device is disabled, in undervoltage lockout in thermal shutdown, and not in soft start. When the output voltage is in regulation hence, within the window defined in the electrical characteristics, the output is high impedance.

V_{IN} must remain present for the PG pin to stay low. If the power good output is not used, it is recommended to tie to GND or leave open. The PG indicator features a de-glitch, as specified in the electrical characteristics, for the transition from "high impedance" to "low" of its output.

Table 9-1. PG Status

EN	DEVICE STATUS	PG STATE
X	$V_{IN} < 2\text{ V}$	undefined
low	$V_{IN} \geq 2\text{ V}$	low
high	$2\text{ V} \leq V_{IN} \leq \text{UVLO}$ OR in thermal shutdown OR V_{OUT} not in regulation OR device in soft start	low
high	V_{OUT} in regulation	high impedance

9.3.6 Thermal Shutdown

The junction temperature (T_J) of the device is monitored by an internal temperature sensor. If T_J exceeds 170°C (typ), the device goes into thermal shutdown. Both the high-side and low-side power FETs are turned off and PG goes low. When T_J decreases below the hysteresis amount of typically 15°C, the converter resumes normal operation, beginning with soft start. During a PFM pause, the thermal shutdown is not active. After a PFM pause, the device needs up to 9 μ s to detect a junction temperature that is too high. If the PFM burst is shorter than this delay, the device does not detect a junction temperature that is too high.

9.4 Device Functional Modes

9.4.1 Pulse Width Modulation (PWM) Operation

The TPS62851x has two operating modes: Forced PWM mode is discussed in this section and PWM/PFM as discussed in [Section 9.4.2](#).

With the MODE/SYNC pin set to high, the TPS62851x operates with pulse width modulation in continuous conduction mode (CCM). The switching frequency is 2.25 MHz or defined by an external clock signal applied to the MODE/SYNC pin. With an external clock applied to MODE/SYNC, the TPS62851x follows the frequency applied to the pin. In general, the frequency range in forced PWM mode is 1.8 MHz to 4 MHz. However, the frequency needs to be in a range the TPS62851x can operate at, taking the minimum on-time into account.

9.4.2 Power Save Mode Operation (PWM/PFM)

When the MODE/SYNC pin is low, power save mode is allowed. The device operates in PWM mode as long as the peak inductor current is above the PFM threshold of about 0.8 A. When the peak inductor current drops below the PFM threshold, the device starts to skip switching pulses. In power save mode, the switching frequency decreases with the load current maintaining high efficiency.

9.4.3 100% Duty-Cycle Operation

The duty cycle of a buck converter operated in PWM mode is given as $D = V_{OUT} / V_{IN}$. The duty cycle increases as the input voltage comes close to the output voltage and the off-time gets smaller. When the minimum off-time of typically 10 ns is reached, the TPS62851x skips switching cycles while it approaches 100% mode. In 100% mode, it keeps the high-side switch on continuously. The high-side switch stays turned on as long as the output voltage is below the target. In 100% mode, the low-side switch is turned off. The maximum dropout voltage in 100% mode is the product of the on-resistance of the high-side switch plus the series resistance of the inductor and the load current.

9.4.4 Current Limit and Short Circuit Protection

The TPS62851x is protected against overload and short circuit events. If the inductor current exceeds the current limit I_{LIMH} , the high-side switch is turned off and the low-side switch is turned on to ramp down the inductor current. The high-side switch turns on again only if the current in the low side-switch has decreased below the low side current limit. Due to internal propagation delay, the actual current can exceed the static current limit. The dynamic current limit is given as:

$$I_{peak(typ)} = I_{LIMH} + \frac{V_L}{L} \cdot t_{PD} \quad (1)$$

where

- I_{LIMH} is the static current limit as specified in the electrical characteristics
- L is the effective inductance at the peak current
- V_L is the voltage across the inductor ($V_{IN} - V_{OUT}$)
- t_{PD} is the internal propagation delay of typically 50 ns

The current limit can exceed static values, especially if the input voltage is high and very small inductances are used. The dynamic high-side switch peak current can be calculated as follows:

$$I_{peak(typ)} = I_{LIMH} + \frac{V_{IN} - V_{OUT}}{L} \cdot 50ns \quad (2)$$

9.4.5 Foldback Current Limit and Short Circuit Protection

This is valid for devices where foldback current limit is enabled.

When the device detects current limit for more than 1024 subsequent switching cycles, it reduces the current limit from its nominal value to typically 1.3 A. Foldback current limit is left when the current limit indication goes away. If device operation continues in current limit, it would, after 3072 switching cycles, try again full current limit for again 1024 switching cycles.

9.4.6 Output Discharge

The purpose of the discharge function is to ensure a defined down-ramp of the output voltage when the device is being disabled and to keep the output voltage close to 0 V when the device is off. The output discharge feature is only active once the TPS62851x has been enabled at least once since the supply voltage was applied. The

discharge function is enabled as soon as the device is disabled, in thermal shutdown, or in undervoltage lockout. The minimum supply voltage required for the discharge function to remain active typically is 2 V. Output discharge is not activated during a current limit or foldback current limit event.

9.4.7 Soft Start / Tracking (SS/TR)

The internal soft-start circuitry controls the output voltage slope during start-up. This avoids excessive inrush current and ensures a controlled output voltage rise time. It also prevents unwanted voltage drops from high impedance power sources or batteries. When EN is set high to start operation, the device starts switching after a delay of about 200 μ s then the internal reference and hence V_{OUT} rises with a slope controlled by an external capacitor connected to the SS/TR pin.

Leaving the SS/TR pin un-connected provides the fastest start-up ramp with 160 μ s typically. A capacitor connected from SS/TR to GND is charged with 2.5 μ A by an internal current source during soft start until it reaches the reference voltage of 0.6 V. The capacitance required to set a certain ramp-time (t_{ramp}) therefore is:

$$C_{SS}[nF] = \frac{2.5\mu A \cdot t_{ramp}[ms]}{0.6V} \quad (3)$$

If the device is set to shutdown (EN = GND), undervoltage lockout, or thermal shutdown, an internal resistor pulls the SS/TR pin to GND to ensure a proper low level. Returning from those states causes a new start-up sequence.

A voltage applied at SS/TR can be used to track a master voltage. The output voltage follows this voltage in both directions up and down in forced PWM mode. In PFM mode, the output voltage decreases based on the load current. The SS/TR pin must not be connected to the SS/TR pin of other devices. The maximum value for C_{SS} is 47 nF to ensure proper discharge before the device starts to ramp the output voltage.

9.4.8 Input Overvoltage Protection

When the input voltage exceeds typically 6.8 V, the device is set to PFM mode so it cannot transfer energy from the output to the input.

10 Application and Implementation

Note

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes. Customers should validate and test their design implementation to confirm system functionality.

10.1 Application Information

10.1.1 Programming the Output Voltage

The output voltage of the TPS62851x is adjustable. It can be programmed for output voltages from 0.6 V to 5.5 V, using a resistor divider from VOUT to GND. The voltage at the FB pin is regulated to 600 mV. The value of the output voltage is set by the selection of the resistor divider from [Equation 6](#). It is recommended to choose resistor values which allow a current of at least 2 μ A, meaning the value of R_2 must not exceed 400 k Ω . Lower resistor values are recommended for highest accuracy and most robust design.

$$R_1 = R_2 \cdot \left(\frac{V_{OUT}}{V_{FB}} - 1 \right) \quad (4)$$

10.1.2 External Component Selection

10.1.2.1 Inductor Selection

The TPS62851x is designed for a nominal 0.47- μ H inductor with a switching frequency of typically 2.25 MHz. Larger values can be used to achieve a lower inductor current ripple but they can have a negative impact on efficiency and transient response. Smaller values than 0.47 μ H cause a larger inductor current ripple which causes larger negative inductor current in forced PWM mode at low or no output current. For a higher or lower nominal switching frequency, the inductance should be changed accordingly. See [Section 7.3](#) for details.

The inductor selection is affected by several effects like inductor ripple current, output ripple voltage, PWM-to-PFM transition point, and efficiency. In addition, the inductor selected has to be rated for appropriate saturation current and DC resistance (DCR). [Equation 5](#) calculates the maximum inductor current.

$$I_{L(max)} = I_{OUT(max)} + \frac{\Delta I_{L(max)}}{2} \quad (5)$$

$$\Delta I_{L(max)} = \frac{V_{OUT} \cdot \left(1 - \frac{V_{OUT}}{V_{IN}} \right)}{L_{min}} \cdot \frac{1}{f_{SW}} \quad (6)$$

where

- $I_{L(max)}$ is the maximum inductor current
- $\Delta I_{L(max)}$ is the peak-to-peak inductor ripple current
- L_{min} is the minimum inductance at the operating point

Table 10-1. Typical Inductors

TYPE	INDUCTANCE [μH]	CURRENT [A] (1)	FOR DEVICE	NOMINAL SWITCHING FREQUENCY	DIMENSIONS [LxBxH] mm	MANUFACTURER(2)
DFE201210U-R47M	0.47 μH, ±20%	see data sheet	TPS628510/511 / 512	2.25 MHz	2.0 x 1.2 x 1.0	Murata
DFE201210U-1R0M	1 μH, ±20%	see data sheet	TPS628510/511 / 512	2.25 MHz	2.0x 1.2 x 1.0	Murata
DFE201210U-R68	0.68 μH, ±20%	see data sheet	TPS628510/511 / 512	2.25 MHz	2.0x 1.2 x 1.0	Murata
XEL3515-561ME	0.56 μH, ±20%	4.5	TPS628510/511 / 512	2.25 MHz	3.5 x 3.2 x 1.5	Coilcraft
XFL4015-701ME	0.70 μH, ±20%	3.3	TPS628510/511 / 512	2.25 MHz	4.0 x 4.0 x 1.6	Coilcraft
XFL4015-471ME	0.47 μH, ±20%	3.5	TPS628510/511 / 512	2.25 MHz	4.0 x 4.0 x 1.6	Coilcraft

(1) Lower of I_{RMS} at 20°C rise or I_{SAT} at 20% drop.

(2) See the [Section 13.1.1](#).

Calculating the maximum inductor current using the actual operating conditions gives the minimum saturation current of the inductor needed. A margin of about 20% is recommended to add. A larger inductor value is also useful to get lower ripple current, but increases the transient response time and size as well.

10.1.3 Capacitor Selection

10.1.3.1 Input Capacitor

For most applications, 10-μF nominal is sufficient and is recommended. The input capacitor buffers the input voltage for transient events and also decouples the converter from the supply. A low-ESR multilayer ceramic capacitor (MLCC) is recommended for best filtering and must be placed between VIN and GND as close as possible to those pins.

10.1.3.2 Output Capacitor

The architecture of the TPS62851x allows the use of tiny ceramic output capacitors with low equivalent series resistance (ESR). These capacitors provide low output voltage ripple and are recommended. To keep its low resistance up to high frequencies and to get narrow capacitance variation with temperature, it is recommended to use X7R or X5R dielectric. Using a higher value has advantages like smaller voltage ripple and a tighter DC output accuracy in power save mode.

10.2 Typical Application

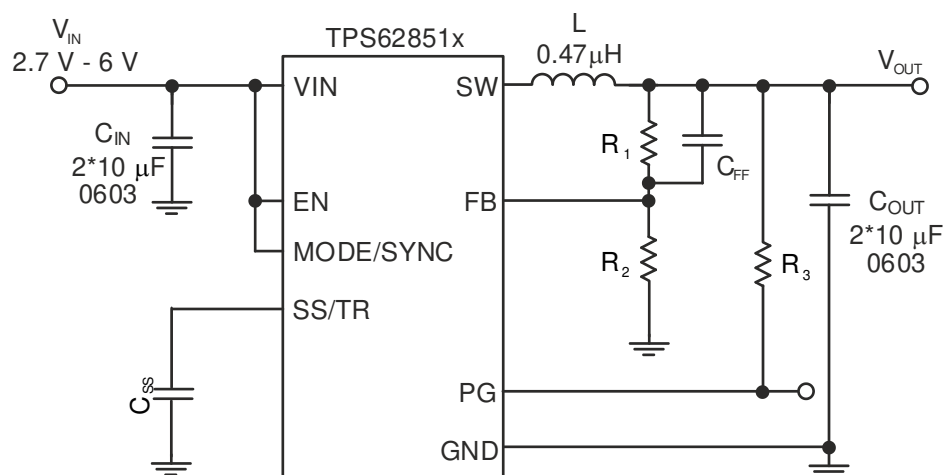


Figure 10-1. Typical Application for Indy

10.2.1 Design Requirements

The design guidelines provide a component selection to operate the device within the recommended operating conditions.

10.2.2 Detailed Design Procedure

$$R_1 = R_2 \cdot \left(\frac{V_{OUT}}{V_{FB}} - 1 \right) \quad (7)$$

With $V_{FB} = 0.6 \text{ V}$:

Table 10-2. Setting the Output Voltage

NOMINAL OUTPUT VOLTAGE V_{OUT}	R_1	R_2	C_{FF}	EXACT OUTPUT VOLTAGE
0.8 V	16.9 k Ω	51 k Ω	10 pF	0.7988 V
1.0 V	20 k Ω	30 k Ω	10 pF	1.0 V
1.1 V	39.2 k Ω	47 k Ω	10 pF	1.101 V
1.2 V	68 k Ω	68 k Ω	10 pF	1.2 V
1.5 V	76.8 k Ω	51 k Ω	10 pF	1.5 V
1.8 V	80.6 k Ω	40.2 k Ω	10 pF	1.803 V
2.5 V	47.5 k Ω	15 k Ω	10 pF	2.5 V
3.3 V	88.7 k Ω	19.6 k Ω	10 pF	3.315 V

10.2.3 Application Curves

All plots have been taken with a nominal switching frequency of 2.25 MHz when set to PWM mode, unless otherwise noted. The BOM is according to [Table 8-1](#).

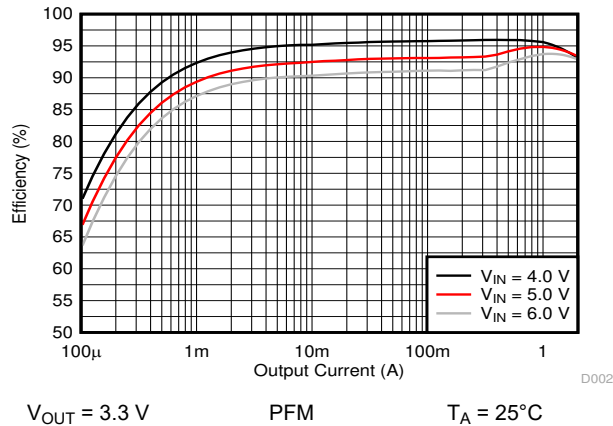


Figure 10-2. Efficiency versus Output Current

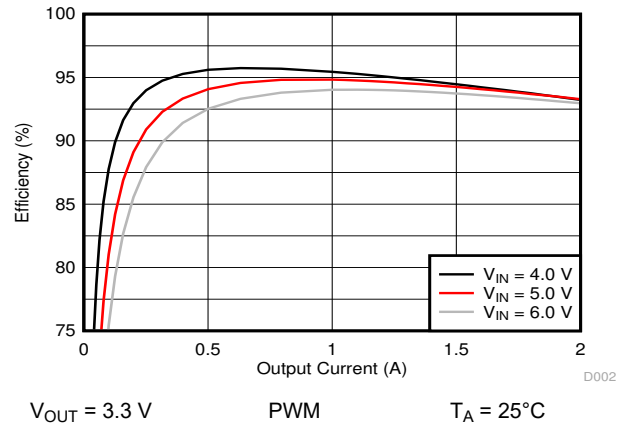


Figure 10-3. Efficiency versus Output Current

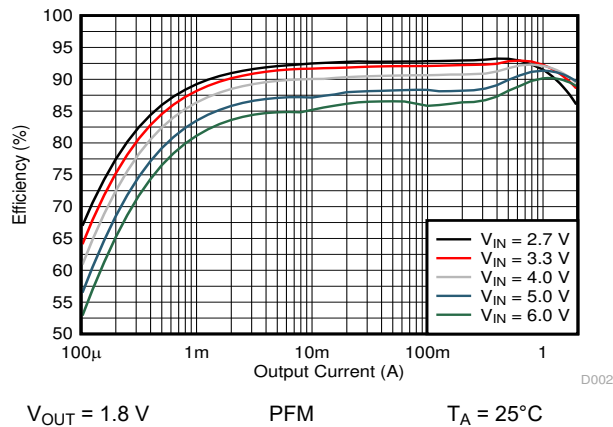


Figure 10-4. Efficiency versus Output Current

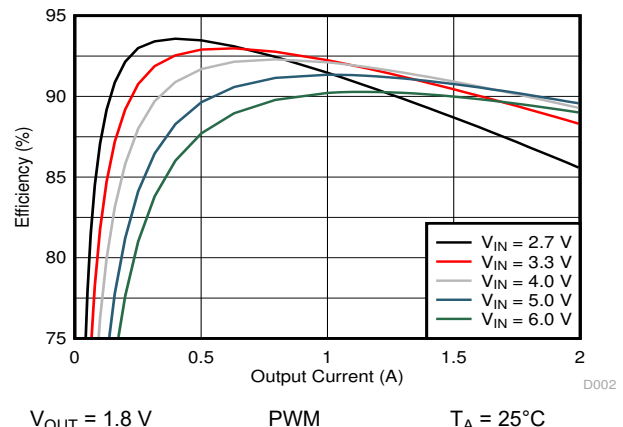


Figure 10-5. Efficiency versus Output Current

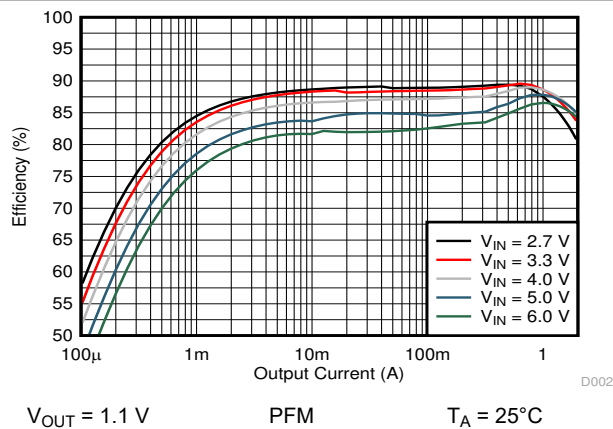


Figure 10-6. Efficiency versus Output Current

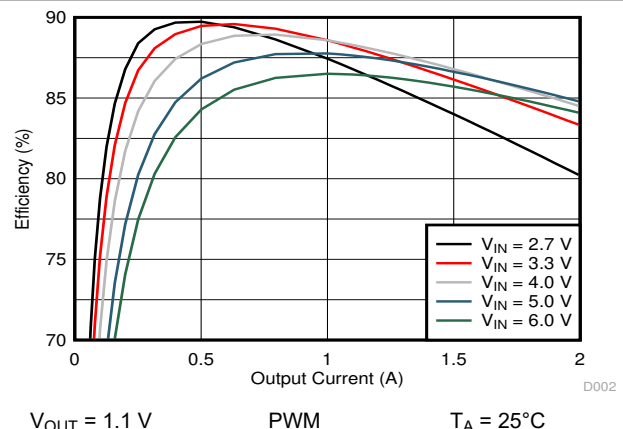


Figure 10-7. Efficiency versus Output Current

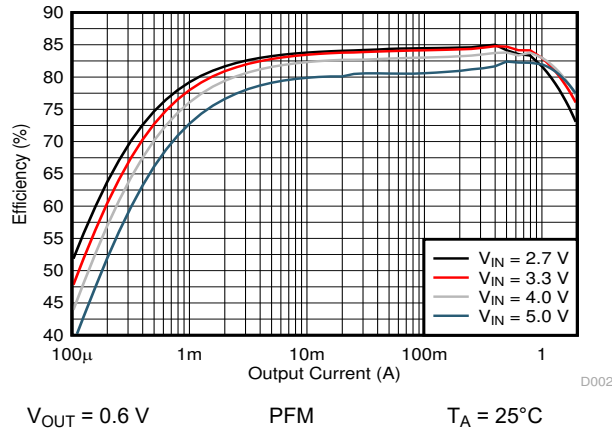


Figure 10-8. Efficiency versus Output Current

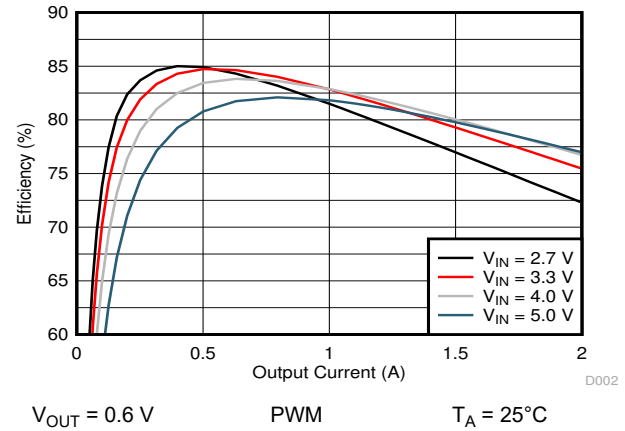


Figure 10-9. Efficiency versus Output Current

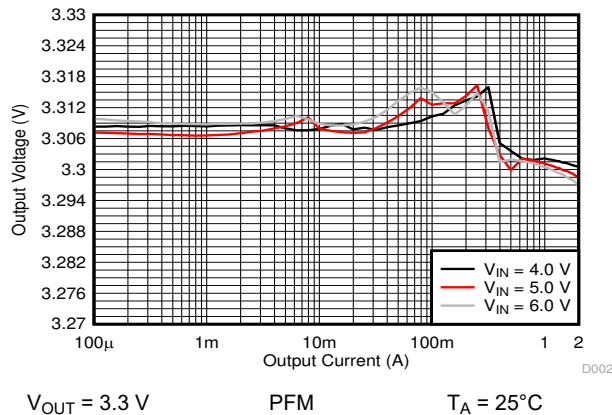


Figure 10-10. Output Voltage versus Output Current

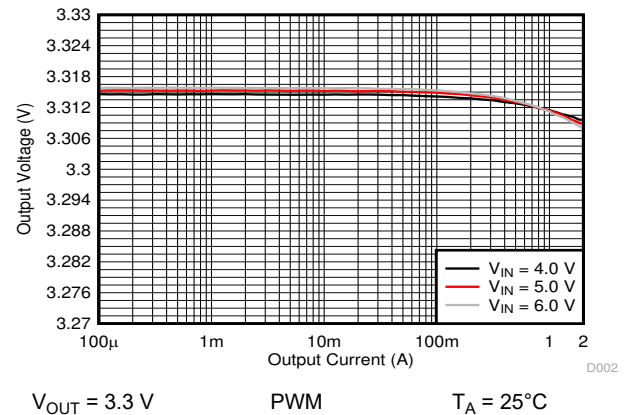


Figure 10-11. Output Voltage versus Output Current

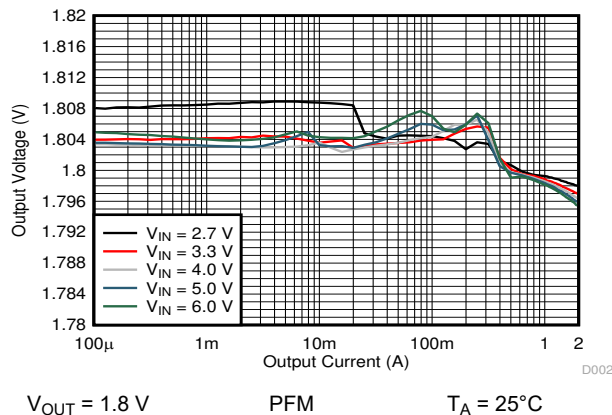


Figure 10-12. Output Voltage versus Output Current

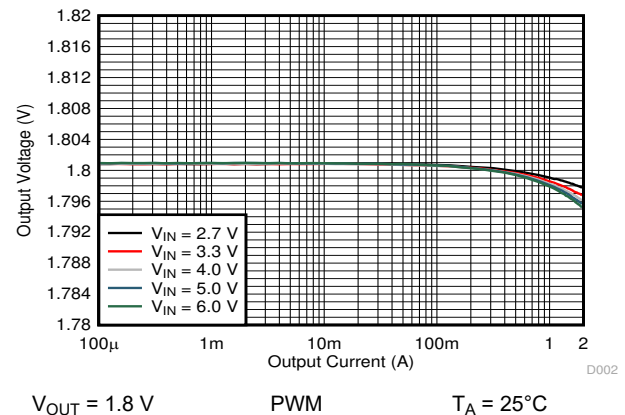


Figure 10-13. Output Voltage versus Output Current

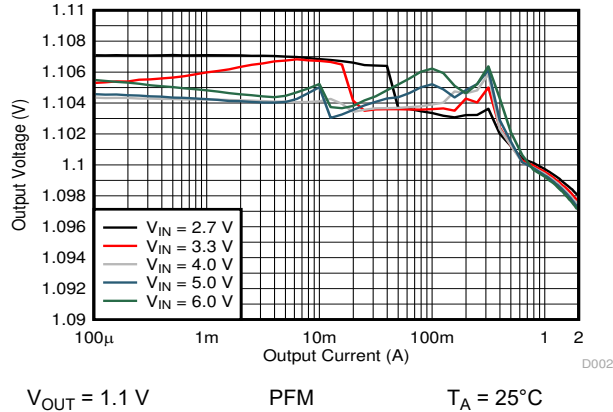


Figure 10-14. Output Voltage versus Output Current

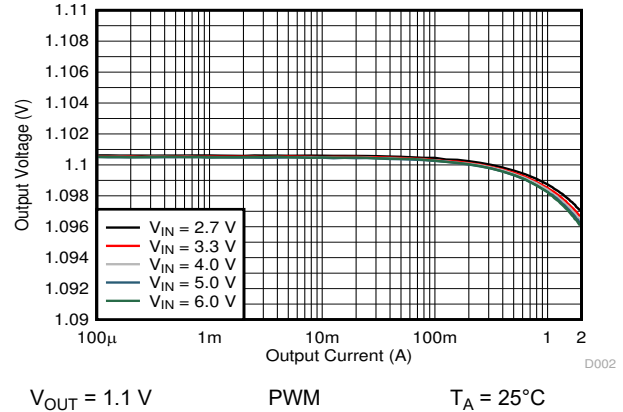


Figure 10-15. Output Voltage versus Output Current

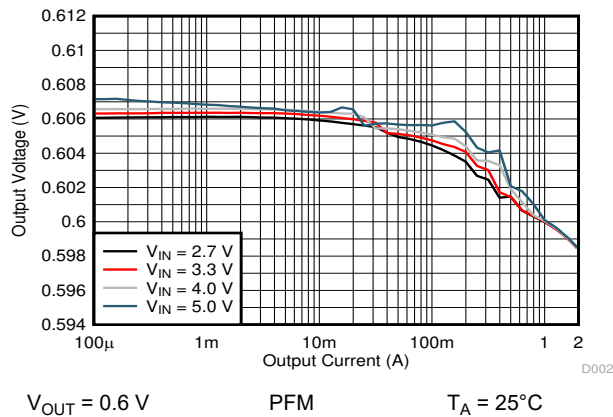


Figure 10-16. Output Voltage versus Output Current

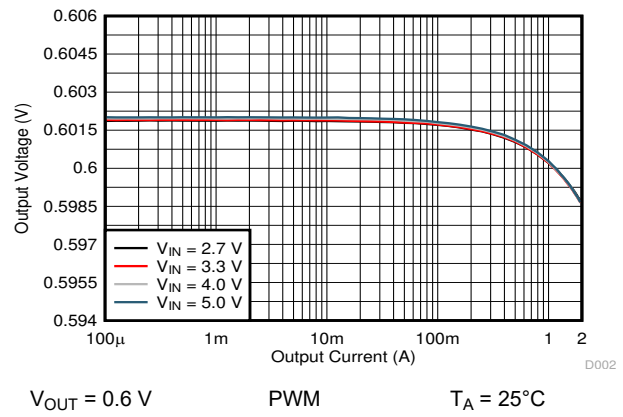
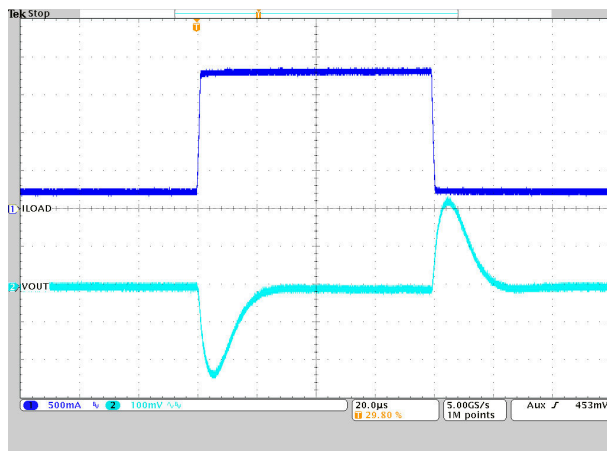
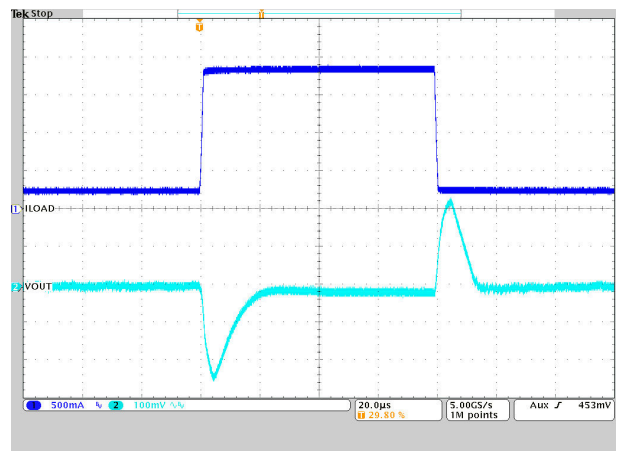


Figure 10-17. Output Voltage versus Output Current



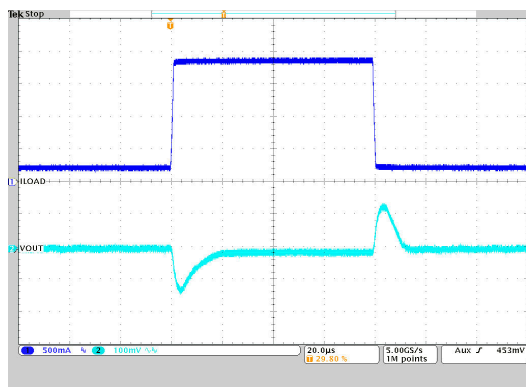
$V_{OUT} = 3.3\text{ V}$ PFM $T_A = 25^\circ\text{C}$
 $V_{IN} = 5.0\text{ V}$ $I_{OUT} = 0.2\text{ A to } 1.8\text{ A to } 0.2\text{ A}$

Figure 10-18. Load Transient Response



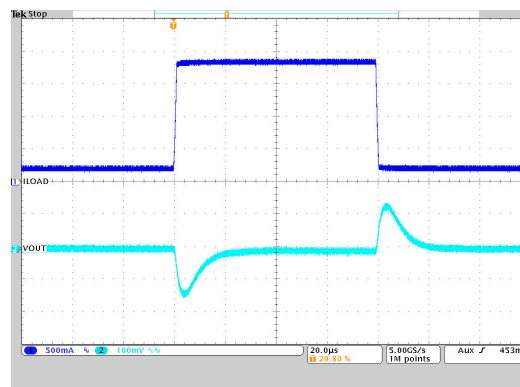
$V_{OUT} = 3.3\text{ V}$ PWM $T_A = 25^\circ\text{C}$
 $V_{IN} = 5.0\text{ V}$ $I_{OUT} = 0.2\text{ A to } 1.8\text{ A to } 0.2\text{ A}$

Figure 10-19. Load Transient Response



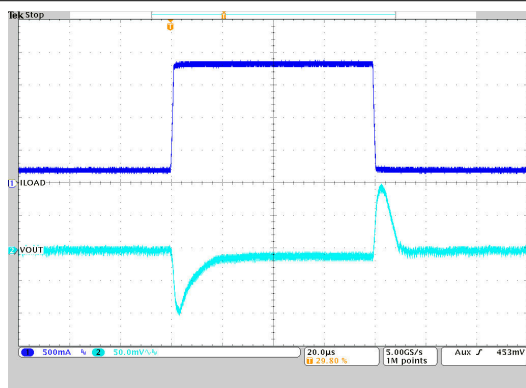
$V_{OUT} = 1.8\text{ V}$ PFM $T_A = 25^\circ\text{C}$
 $V_{IN} = 5.0\text{ V}$ $I_{OUT} = 0.2\text{ A to } 1.8\text{ A to } 0.2\text{ A}$

Figure 10-20. Load Transient Response



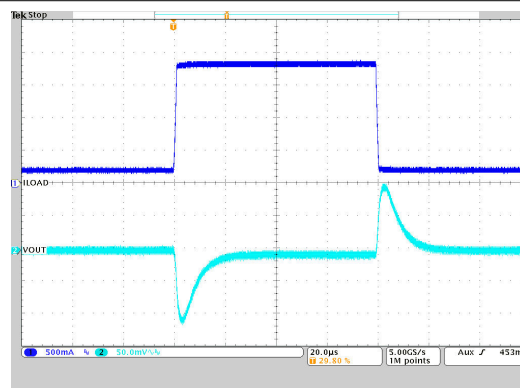
$V_{OUT} = 1.8\text{ V}$ PWM $T_A = 25^\circ\text{C}$
 $V_{IN} = 5.0\text{ V}$ $I_{OUT} = 0.2\text{ A to } 1.8\text{ A to } 0.2\text{ A}$

Figure 10-21. Load Transient Response



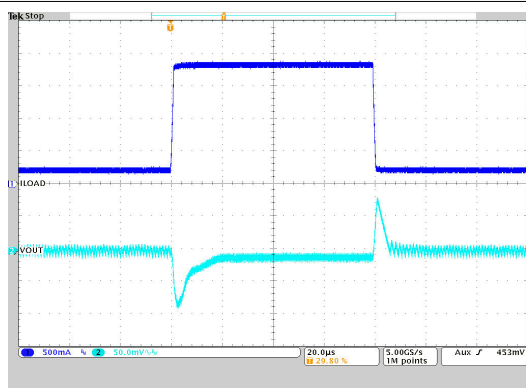
$V_{OUT} = 1.2\text{ V}$ PFM $T_A = 25^\circ\text{C}$
 $V_{IN} = 5.0\text{ V}$ $I_{OUT} = 0.2\text{ A to } 1.8\text{ A to } 0.2\text{ A}$

Figure 10-22. Load Transient Response



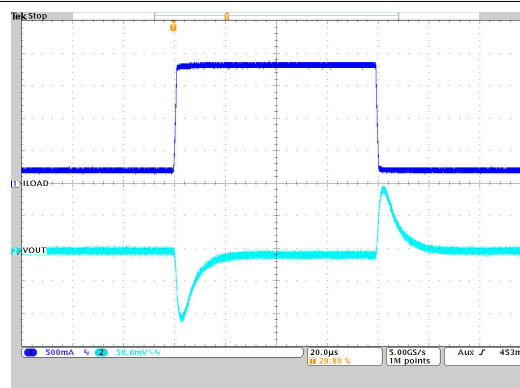
$V_{OUT} = 1.2\text{ V}$ PWM $T_A = 25^\circ\text{C}$
 $V_{IN} = 5.0\text{ V}$ $I_{OUT} = 0.2\text{ A to } 1.8\text{ A to } 0.2\text{ A}$

Figure 10-23. Load Transient Response



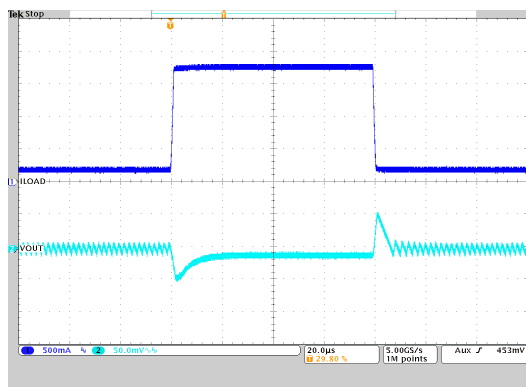
$V_{OUT} = 1.0\text{ V}$ PFM $T_A = 25^\circ\text{C}$
 $V_{IN} = 5.0\text{ V}$ $I_{OUT} = 0.2\text{ A to } 1.8\text{ A to } 0.2\text{ A}$

Figure 10-24. Load Transient Response



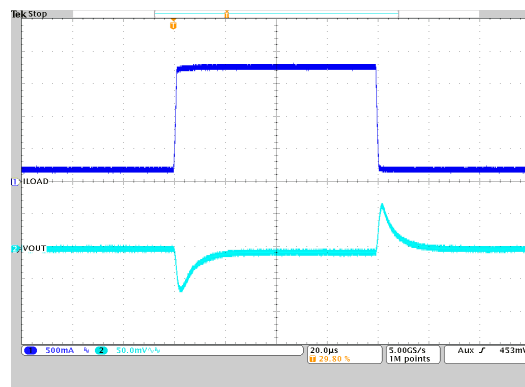
$V_{OUT} = 1.0\text{ V}$ PWM $T_A = 25^\circ\text{C}$
 $V_{IN} = 5.0\text{ V}$ $I_{OUT} = 0.2\text{ A to } 1.8\text{ A to } 0.2\text{ A}$

Figure 10-25. Load Transient Response



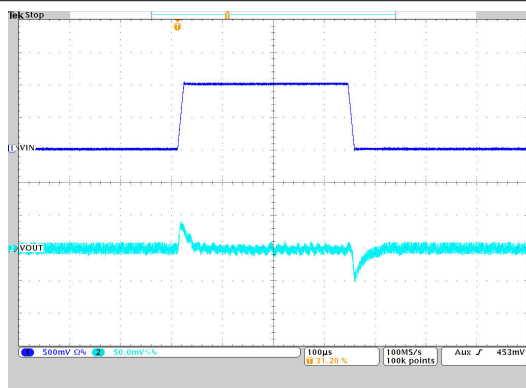
$V_{OUT} = 0.6\text{ V}$ PFM $T_A = 25^\circ\text{C}$
 $V_{IN} = 3.3\text{ V}$ $I_{OUT} = 0.2\text{ A to } 1.8\text{ A to } 0.2\text{ A}$

Figure 10-26. Load Transient Response



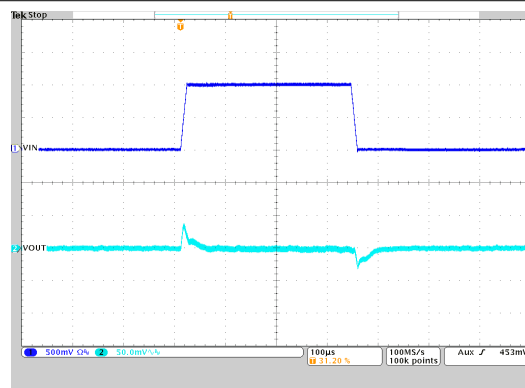
$V_{OUT} = 0.6\text{ V}$ PWM $T_A = 25^\circ\text{C}$
 $V_{IN} = 3.3\text{ V}$ $I_{OUT} = 0.2\text{ A to } 1.8\text{ A to } 0.2\text{ A}$

Figure 10-27. Load Transient Response



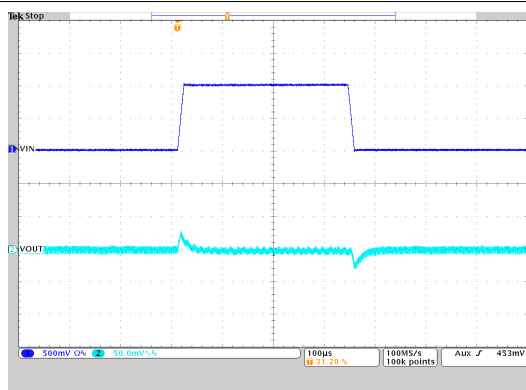
$V_{OUT} = 3.3\text{ V}$ PFM $T_A = 25^\circ\text{C}$
 $I_{OUT} = 0.2\text{ A}$ $V_{IN} = 4.5\text{ V to } 5.5\text{ V to } 4.5\text{ V}$

Figure 10-28. Line Transient Response



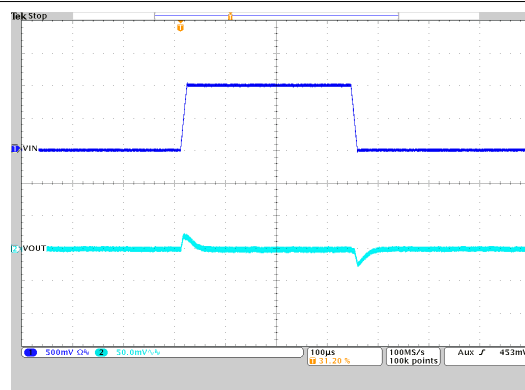
$V_{OUT} = 3.3\text{ V}$ PWM $T_A = 25^\circ\text{C}$
 $I_{OUT} = 2\text{ A}$ $V_{IN} = 4.5\text{ V to } 5.5\text{ V to } 4.5\text{ V}$

Figure 10-29. Line Transient Response



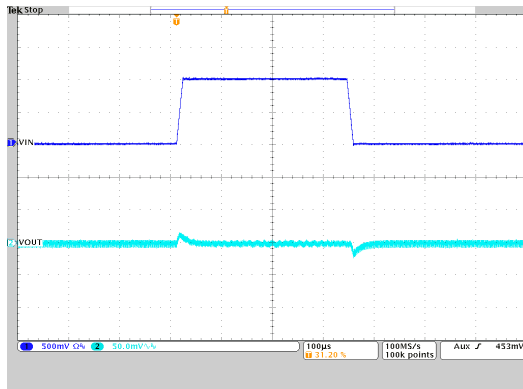
$V_{OUT} = 1.8\text{ V}$ PFM $T_A = 25^\circ\text{C}$
 $I_{OUT} = 0.2\text{ A}$ $V_{IN} = 4.5\text{ V to } 5.5\text{ V to } 4.5\text{ V}$

Figure 10-30. Line Transient Response



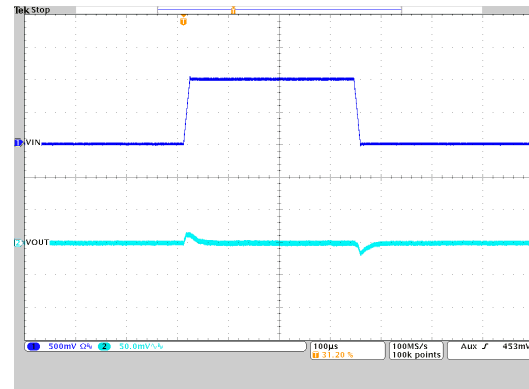
$V_{OUT} = 1.8\text{ V}$ PWM $T_A = 25^\circ\text{C}$
 $I_{OUT} = 2\text{ A}$ $V_{IN} = 4.5\text{ V to } 5.5\text{ V to } 4.5\text{ V}$

Figure 10-31. Line Transient Response



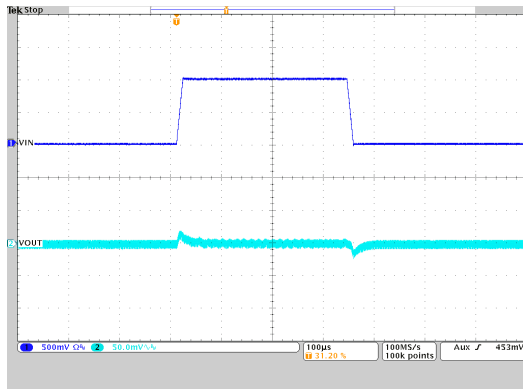
$V_{OUT} = 1.2\text{ V}$ PFM $T_A = 25^\circ\text{C}$
 $I_{OUT} = 0.2\text{ A}$ $V_{IN} = 4.5\text{ V to } 5.5\text{ V to } 4.5\text{ V}$

Figure 10-32. Line Transient Response



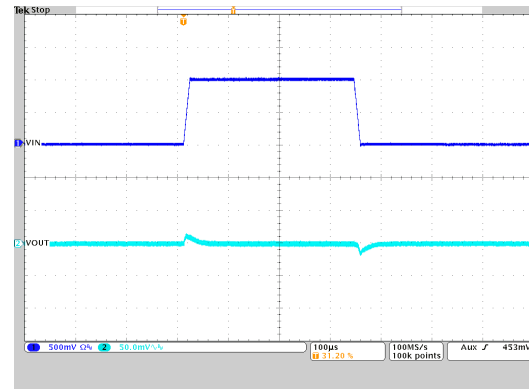
$V_{OUT} = 1.2\text{ V}$ PWM $T_A = 25^\circ\text{C}$
 $I_{OUT} = 2\text{ A}$ $V_{IN} = 4.5\text{ V to } 5.5\text{ V to } 4.5\text{ V}$

Figure 10-33. Line Transient Response



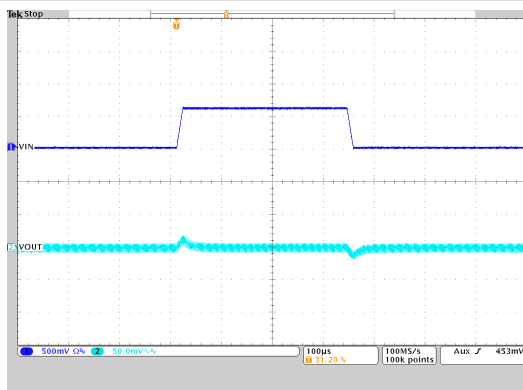
$V_{OUT} = 1.0\text{ V}$ PFM $T_A = 25^\circ\text{C}$
 $I_{OUT} = 0.2\text{ A}$ $V_{IN} = 4.5\text{ V to } 5.5\text{ V to } 4.5\text{ V}$

Figure 10-34. Line Transient Response



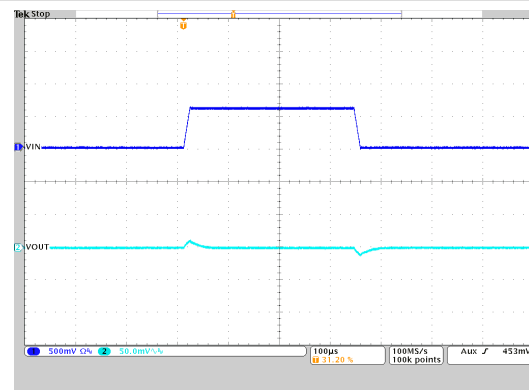
$V_{OUT} = 1.0\text{ V}$ PWM $T_A = 25^\circ\text{C}$
 $I_{OUT} = 2\text{ A}$ $V_{IN} = 4.5\text{ V to } 5.5\text{ V to } 4.5\text{ V}$

Figure 10-35. Line Transient Response



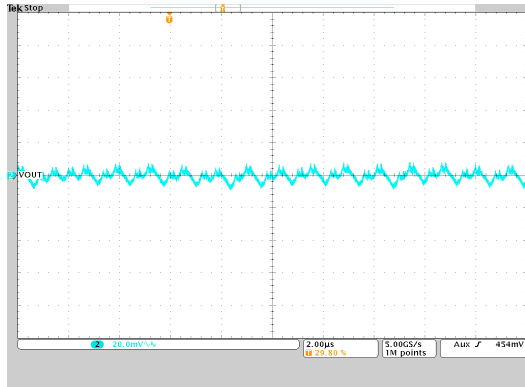
$V_{OUT} = 0.6\text{ V}$ PFM $T_A = 25^\circ\text{C}$
 $I_{OUT} = 0.2\text{ A}$ $V_{IN} = 3.0\text{ V to } 3.6\text{ V to } 3.0\text{ V}$

Figure 10-36. Line Transient Response



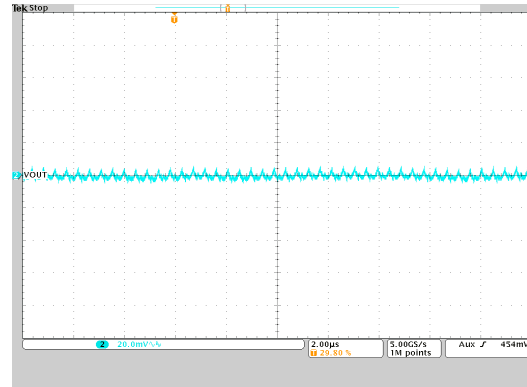
$V_{OUT} = 0.6\text{ V}$ PWM $T_A = 25^\circ\text{C}$
 $I_{OUT} = 2\text{ A}$ $V_{IN} = 3.0\text{ V to } 3.6\text{ V to } 3.0\text{ V}$

Figure 10-37. Line Transient Response



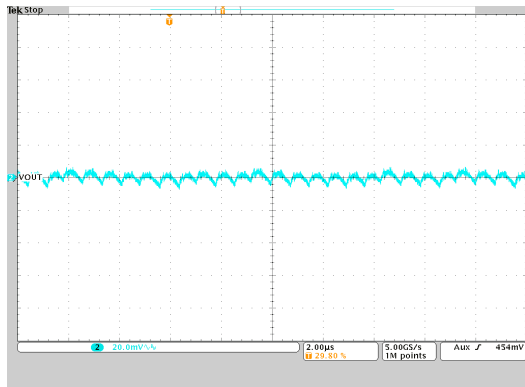
$V_{OUT} = 3.3\text{ V}$ PFM $T_A = 25^\circ\text{C}$
 $V_{IN} = 5\text{ V}$ $I_{OUT} = 0.2\text{ A}$

Figure 10-38. Output Voltage Ripple



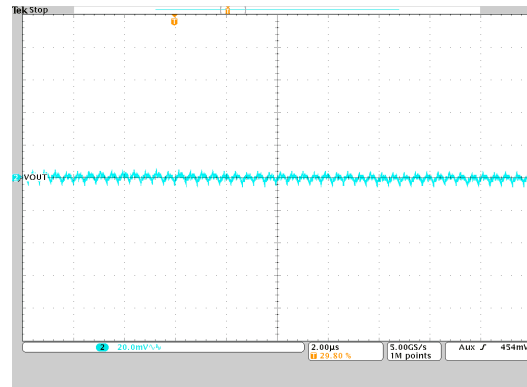
$V_{OUT} = 3.3\text{ V}$ PWM $T_A = 25^\circ\text{C}$
 $V_{IN} = 5\text{ V}$ $I_{OUT} = 2\text{ A}$

Figure 10-39. Output Voltage Ripple



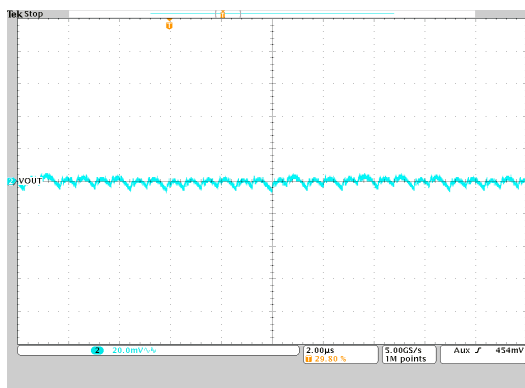
$V_{OUT} = 1.8\text{ V}$ PFM $T_A = 25^\circ\text{C}$
 $V_{IN} = 5\text{ V}$ $I_{OUT} = 0.2\text{ A}$

Figure 10-40. Output Voltage Ripple



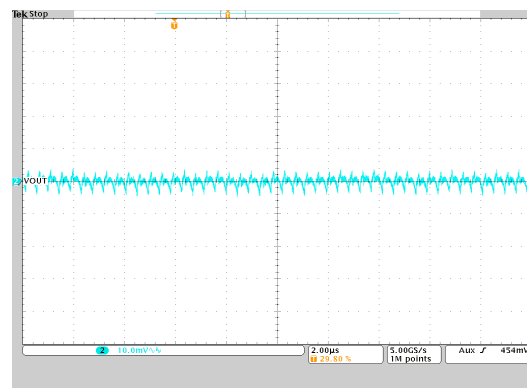
$V_{OUT} = 1.8\text{ V}$ PWM $T_A = 25^\circ\text{C}$
 $V_{IN} = 5\text{ V}$ $I_{OUT} = 2\text{ A}$

Figure 10-41. Output Voltage Ripple



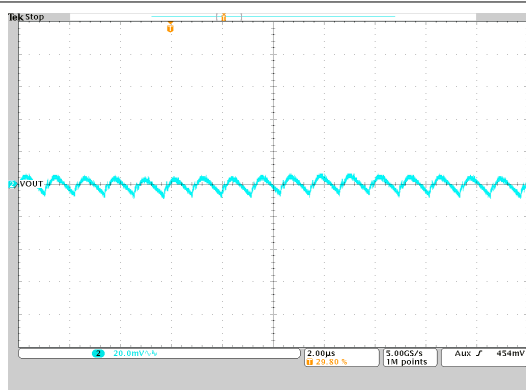
$V_{OUT} = 1.2\text{ V}$ PFM $T_A = 25^\circ\text{C}$
 $V_{IN} = 5\text{ V}$ $I_{OUT} = 0.2\text{ A}$

Figure 10-42. Output Voltage Ripple



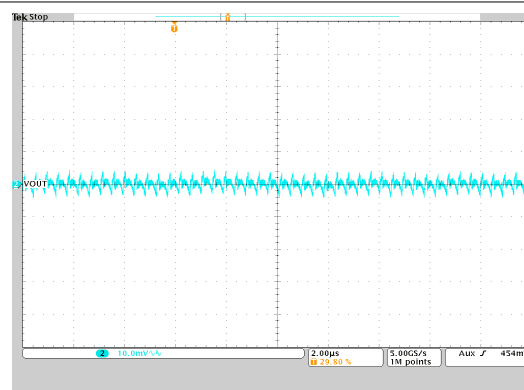
$V_{OUT} = 1.2\text{ V}$ PWM $T_A = 25^\circ\text{C}$
 $V_{IN} = 5\text{ V}$ $I_{OUT} = 2\text{ A}$

Figure 10-43. Output Voltage Ripple



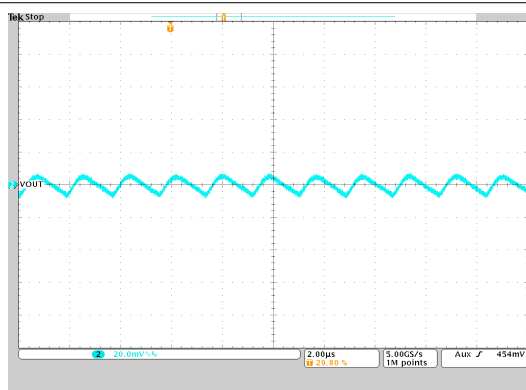
$V_{OUT} = 1.0\text{ V}$ PFM $T_A = 25^\circ\text{C}$
 $V_{IN} = 5\text{ V}$ $I_{OUT} = 0.2\text{ A}$

Figure 10-44. Output Voltage Ripple



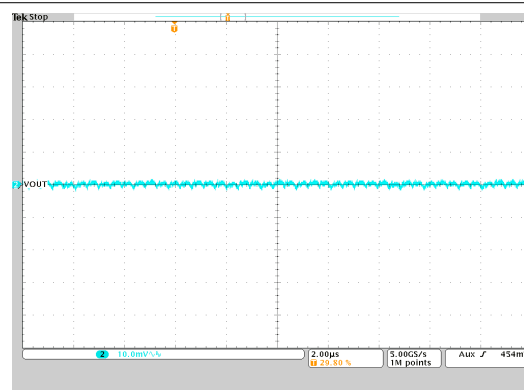
$V_{OUT} = 1.0\text{ V}$ PWM $T_A = 25^\circ\text{C}$
 $V_{IN} = 5\text{ V}$ $I_{OUT} = 2\text{ A}$

Figure 10-45. Output Voltage Ripple



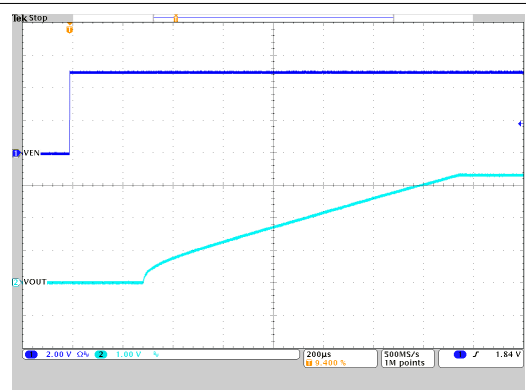
$V_{OUT} = 0.6\text{ V}$ PFM $T_A = 25^\circ\text{C}$
 $V_{IN} = 3.3\text{ V}$ $I_{OUT} = 0.2\text{ A}$

Figure 10-46. Output Voltage Ripple



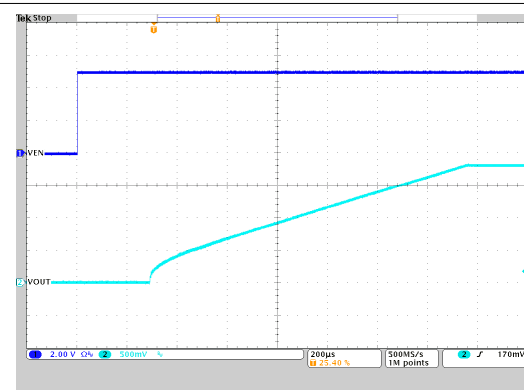
$V_{OUT} = 0.6\text{ V}$ PWM $T_A = 25^\circ\text{C}$
 $V_{IN} = 3.3\text{ V}$ $I_{OUT} = 2\text{ A}$

Figure 10-47. Output Voltage Ripple



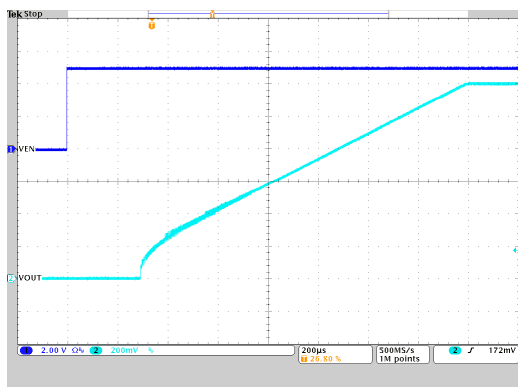
$V_{OUT} = 3.3\text{ V}$ PWM or PFM $T_A = 25^\circ\text{C}$
 $V_{IN} = 5\text{ V}$ $C_{SS} = 4.7\text{ nF}$ $I_{OUT} = 2\text{ A}$

Figure 10-48. Start-Up Timing



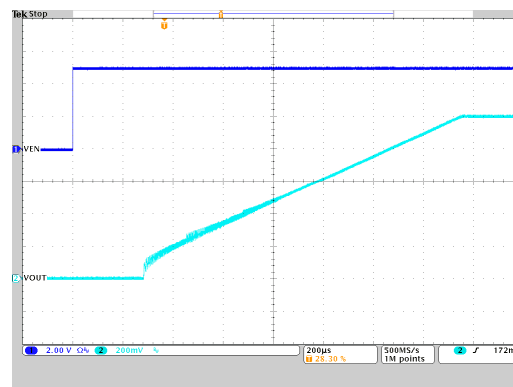
$V_{OUT} = 1.8\text{ V}$ PWM or PFM $T_A = 25^\circ\text{C}$
 $V_{IN} = 5\text{ V}$ $C_{SS} = 4.7\text{ nF}$ $I_{OUT} = 2\text{ A}$

Figure 10-49. Start-Up Timing



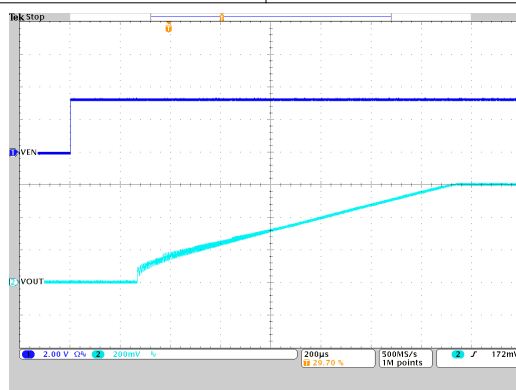
$V_{OUT} = 1.2\text{ V}$ PWM or PFM $T_A = 25^\circ\text{C}$
 $V_{IN} = 5\text{ V}$ $C_{SS} = 4.7\text{ nF}$ $I_{OUT} = 2\text{ A}$

Figure 10-50. Start-Up Timing



$V_{OUT} = 1.0\text{ V}$ PWM or PFM $T_A = 25^\circ\text{C}$
 $V_{IN} = 5\text{ V}$ $C_{SS} = 4.7\text{ nF}$ $I_{OUT} = 2\text{ A}$

Figure 10-51. Start-Up Timing



$V_{OUT} = 0.6\text{ V}$ PWM or PFM $T_A = 25^\circ\text{C}$
 $V_{IN} = 3.3\text{ V}$ $C_{SS} = 4.7\text{ nF}$ $I_{OUT} = 2\text{ A}$

Figure 10-52. Start-Up Timing

10.3 System Examples

10.3.1 Fixed Output Voltage Versions

Versions with an internally fixed output voltage allow you to remove the external feedback voltage divider. This not only allows you to reduce the total solution size but also provides higher accuracy as there is no additional error caused by the external resistor divider. The FB pin needs to be tied to the output voltage directly as shown in [Figure 10-53](#). The application runs with an internally defined switching frequency of 2.25 MHz.

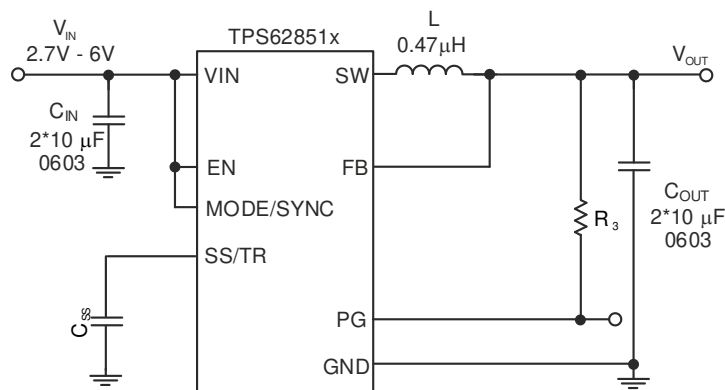


Figure 10-53. Schematic for Fixed Output Voltage Versions

10.3.2 Voltage Tracking

The TPS62851x follows the voltage applied to the SS/TR pin. A voltage ramp on SS/TR to 0.6 V ramps the output voltage according to the 0.6-V feedback voltage.

Tracking the 3.3 V of device 1, so that both rails reach their target voltage at the same time, requires a resistor divider on SS/TR of device 2 equal to the output voltage divider of device 1. The output current of 2.5 μ A on the SS/TR pin causes an offset voltage on the resistor divider formed by R_5 and R_6 . The equivalent resistance of $R_5 // R_6$ must be kept below 15 k Ω . The current from SS/TR causes a slightly higher voltage across R_6 than 0.6 V, which is desired because device 2 switches to its internal reference as soon as the voltage at SS/TR is higher than 0.6 V.

In case both devices need to run in forced PWM mode, it is recommended to tie the MODE pin of device 2 to the output voltage or the power good signal of device 1, the master device. The TPS6281x does have a duty cycle limitation defined by the minimum on-time. For tracking down to low output voltages, device 2 cannot follow once the minimum duty cycle is reached. Enabling PFM mode while tracking is in progress allows you to ramp down the output voltage close to 0 V.

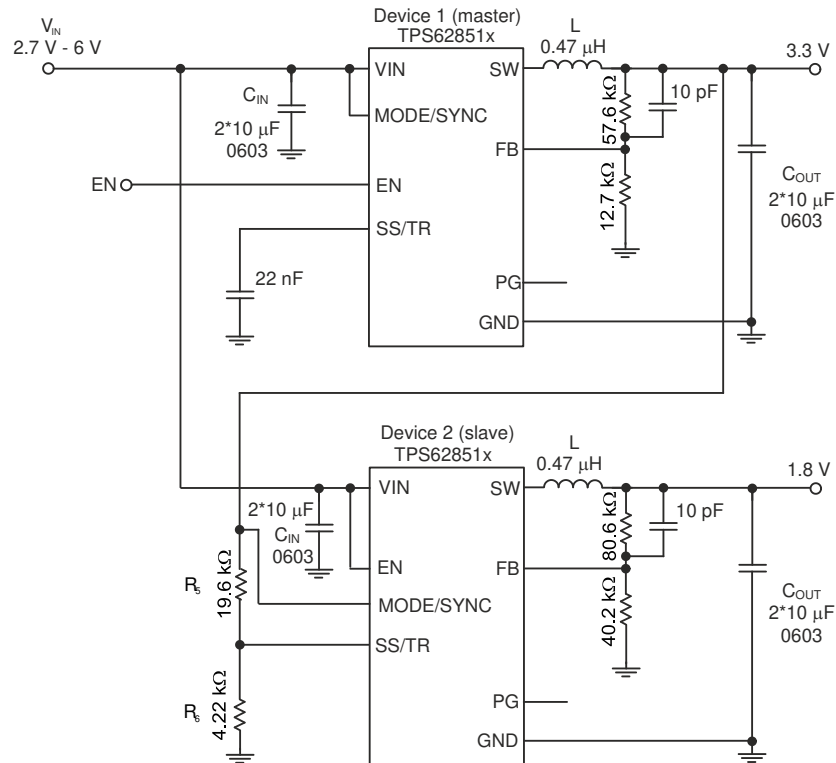


Figure 10-54. Schematic for Output Voltage Tracking

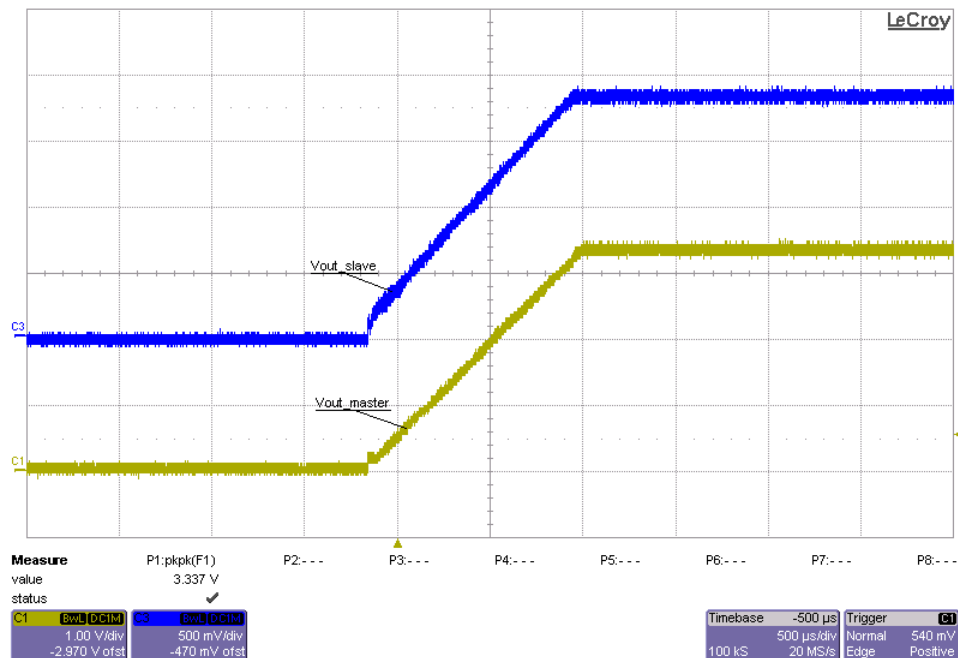


Figure 10-55. Scope Plot for Output Voltage Tracking

10.3.3 Synchronizing to an External Clock

The TPS62851x can be externally synchronized by applying an external clock on the MODE/SYNC pin. There is no need for any additional circuitry as long as the input signal meets the requirements given in the electrical specifications. The clock can be applied / removed during operation, allowing you to switch from an externally defined fixed frequency to power-save mode or to internal fixed frequency operation.

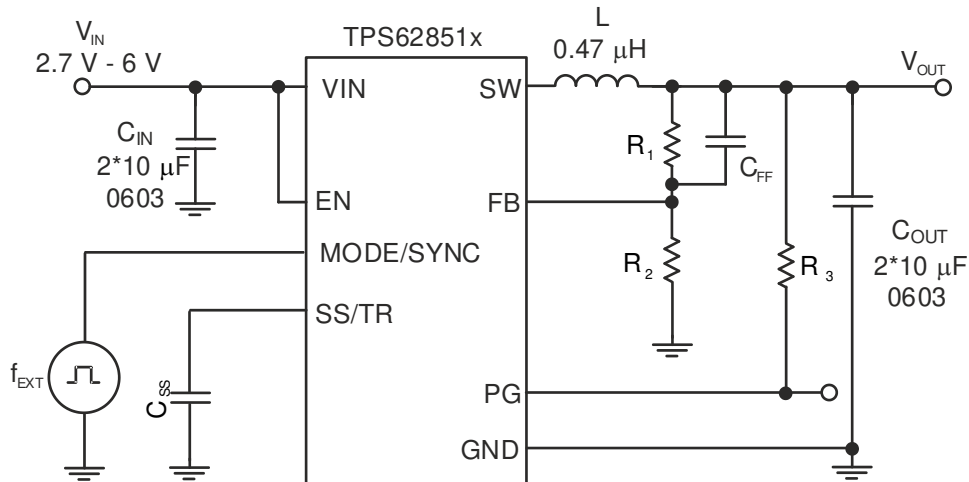


Figure 10-56. Schematic using External Synchronization

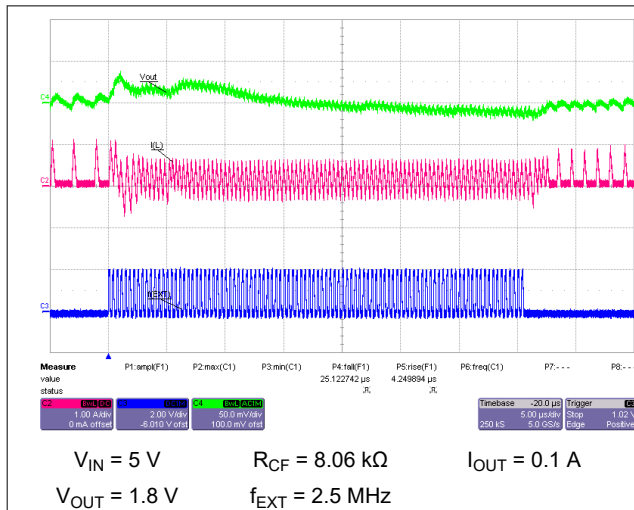


Figure 10-57. Switching from External Synchronization to Power-Save Mode (PFM)

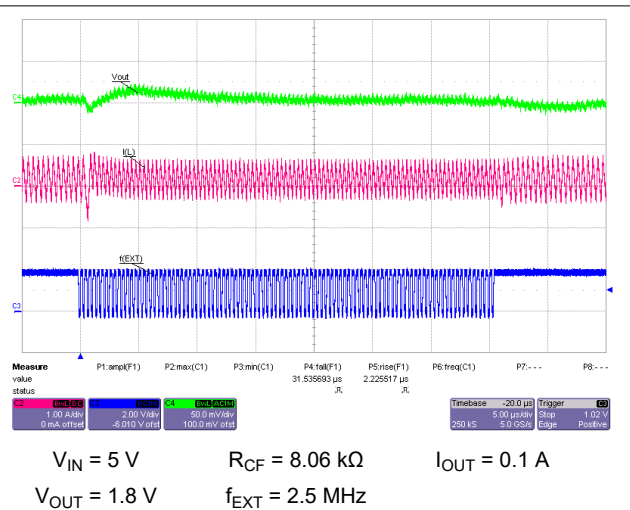


Figure 10-58. Switching from External Synchronization to Internal Fixed Frequency

11 Power Supply Recommendations

The TPS62851x device family does not have special requirements for its input power supply. The output current of the input power supply needs to be rated according to the supply voltage, output voltage, and output current of the TPS62851x.

12 Layout

12.1 Layout Guidelines

A proper layout is critical for the operation of a switched mode power supply, even more at high switching frequencies. Therefore, the PCB layout of the TPS62851x demands careful attention to ensure operation and to get the performance specified. A poor layout can lead to issues like poor regulation (both in [Section 12.2](#) and load), stability and accuracy weaknesses, increased EMI radiation, and noise sensitivity.

See [Figure 12-1](#) for the recommended layout of the TPS62851x, which is designed for common external ground connections. The input capacitor must be placed as close as possible between the VIN and GND pin.

Provide low inductive and resistive paths for loops with high di/dt . Therefore, paths conducting the switched load current must be as short and wide as possible. Provide low capacitive paths (with respect to all other nodes) for wires with high dv/dt . Therefore, the input and output capacitance must be placed as close as possible to the IC pins and parallel wiring over long distances and narrow traces must be avoided. Loops which conduct an alternating current should outline an area as small as possible, as this area is proportional to the energy radiated.

Sensitive nodes like FB need to be connected with short wires and not nearby high dv/dt signals (for example, SW). As they carry information about the output voltage, they must be connected as close as possible to the actual output voltage (at the output capacitor). The capacitor on the SS/TR pin as well as the FB resistors, R_1 and R_2 , must be kept close to the IC and be connected directly to the pin and the system ground plane.

The package uses the pins for power dissipation. Thermal vias on the VIN and GND pins help to spread the heat into the pcb.

The recommended layout is implemented on the EVM and shown in the [TPS62851xEVM-139 Evaluation Module User's Guide](#).

12.2 Layout Example

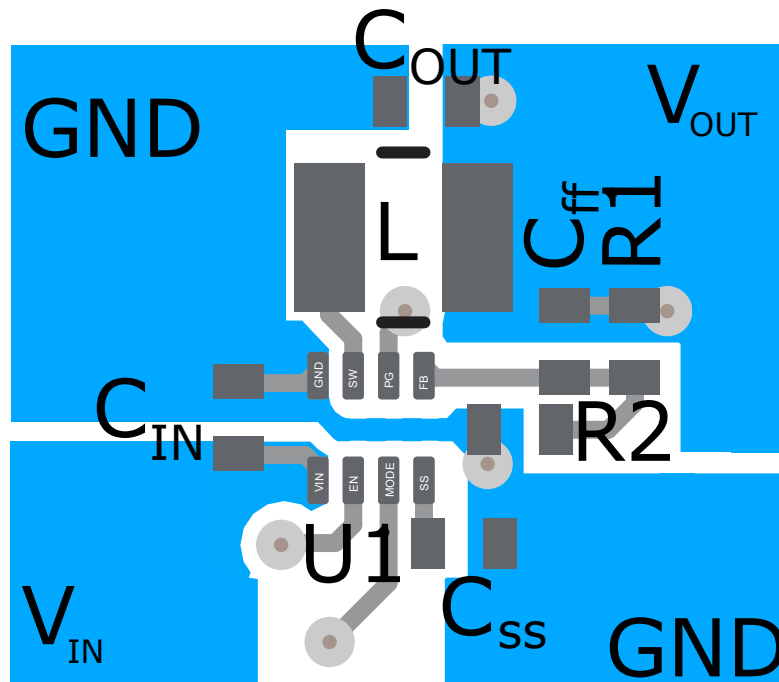


Figure 12-1. Example Layout

13 Device and Documentation Support

13.1 Device Support

13.1.1 Third-Party Products Disclaimer

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13.2 Receiving Notification of Documentation Updates

To receive notification of documentation updates, navigate to the device product folder on ti.com. Click on *Subscribe to updates* to register and receive a weekly digest of any product information that has changed. For change details, review the revision history included in any revised document.

13.3 Support Resources

[TI E2E™ support forums](#) are an engineer's go-to source for fast, verified answers and design help — straight from the experts. Search existing answers or ask your own question to get the quick design help you need.

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13.5 Electrostatic Discharge Caution



This integrated circuit can be damaged by ESD. Texas Instruments recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

13.6 Glossary

[TI Glossary](#)

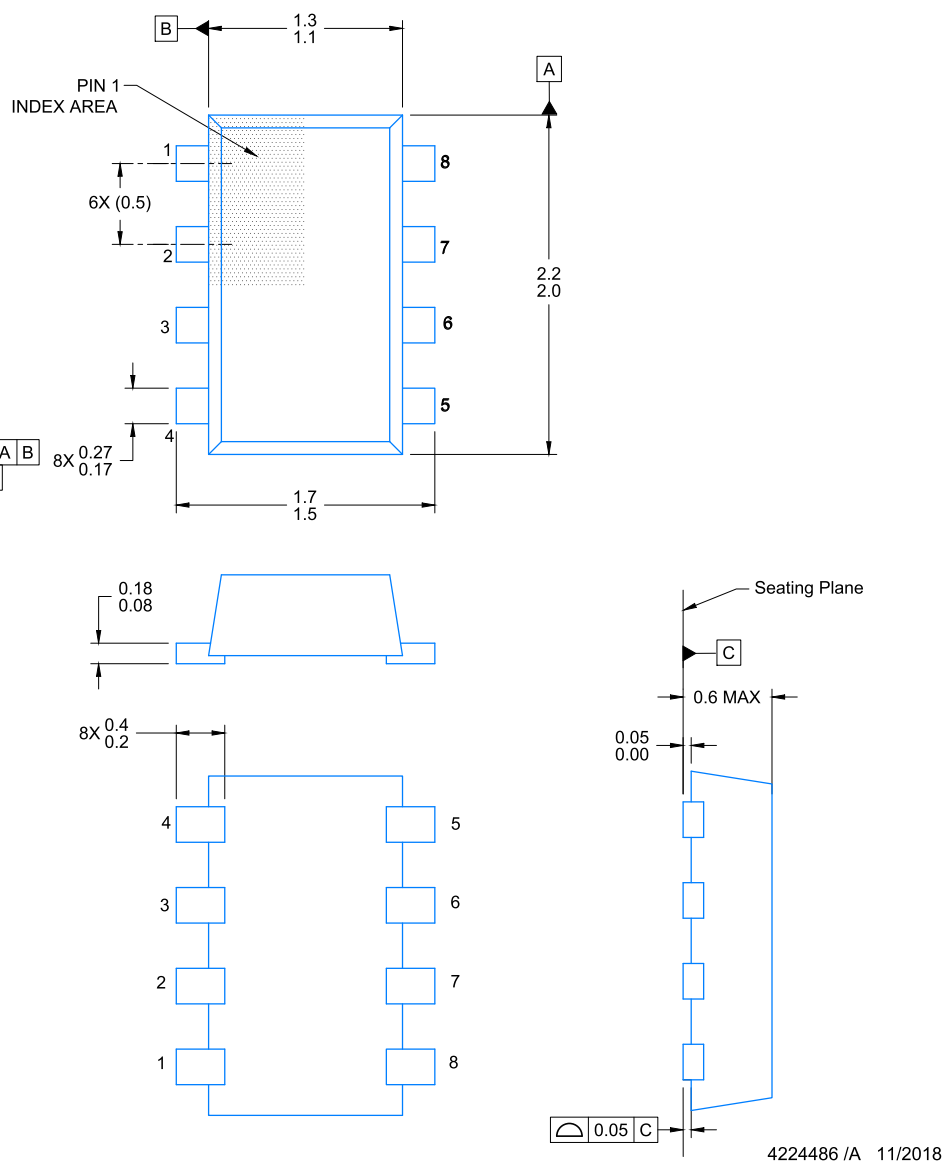
This glossary lists and explains terms, acronyms, and definitions.

14 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.

PACKAGE OUTLINE**DRL0008A****FCSOT - 0.6 mm max height**

FLIPCHIP SOT

**NOTES:**

1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
2. This drawing is subject to change without notice.
3. Body dimensions do not include mold flash, protrusions or gate burrs. Mold flash, interlead flash, protrusions or gate burrs shall not exceed 0.15 per end or side.
4. Reference JEDEC registration TO-236, except minimum foot length.

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EXAMPLE BOARD LAYOUT**DRL0008A****FCSOT - 0.6 mm max height**

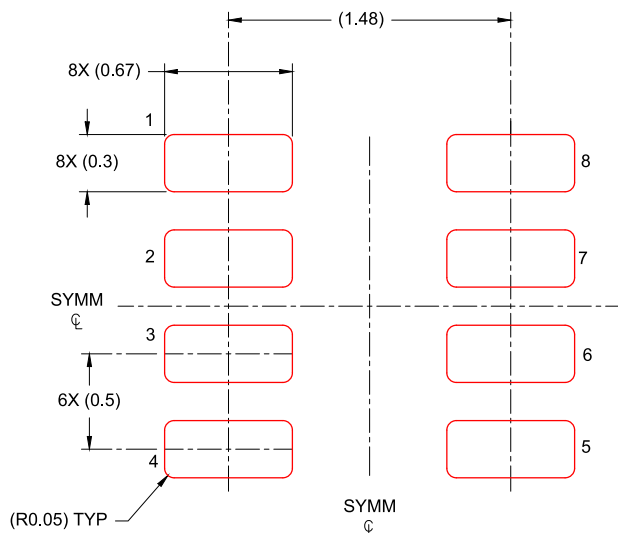
FLIPCHIP SOT

EXAMPLE STENCIL DESIGN

DRL0008A

FCSOT - 0.6 mm max height

FLIPCHIP SOT



SOLDER PASTE EXAMPLE
BASED ON 0.125 mm THICK STENCIL
SCALE: 30X

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NOTES: (continued)

7. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
8. Board assembly site may have different recommendations for stencil design.

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ADVANCE INFORMATION

PACKAGING INFORMATION

Orderable Device	Status (1)	Package Type	Package Drawing	Pins	Package Qty	Eco Plan (2)	Lead finish/ Ball material (6)	MSL Peak Temp (3)	Op Temp (°C)	Device Marking (4/5)	Samples
TPS628510DRLR	PREVIEW	SOT-5X3	DRL	8	4000	RoHS (In work) & Non-Green	Call TI	Call TI	-40 to 150		
TPS628511DRLR	PREVIEW	SOT-5X3	DRL	8	4000	RoHS (In work) & Non-Green	Call TI	Call TI	-40 to 150		
TPS628512DRLR	PREVIEW	SOT-5X3	DRL	8	4000	RoHS (In work) & Non-Green	Call TI	Call TI	-40 to 150		
XPS628510DRLR	ACTIVE	SOT-5X3	DRL	8	4000	RoHS (In work) & Non-Green	Call TI	Call TI	-40 to 150		Samples
XPS628511DRLR	ACTIVE	SOT-5X3	DRL	8	4000	RoHS (In work) & Non-Green	Call TI	Call TI	-40 to 150		Samples
XPS628512DRLR	ACTIVE	SOT-5X3	DRL	8	4000	RoHS (In work) & Non-Green	Call TI	Call TI	-40 to 150		Samples

(1) The marketing status values are defined as follows:

ACTIVE: Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

PREVIEW: Device has been announced but is not in production. Samples may or may not be available.

OBSOLETE: TI has discontinued the production of the device.

(2) **RoHS:** TI defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements for all 10 RoHS substances, including the requirement that RoHS substance do not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, "RoHS" products are suitable for use in specified lead-free processes. TI may reference these types of products as "Pb-Free".

RoHS Exempt: TI defines "RoHS Exempt" to mean products that contain lead but are compliant with EU RoHS pursuant to a specific EU RoHS exemption.

Green: TI defines "Green" to mean the content of Chlorine (Cl) and Bromine (Br) based flame retardants meet JS709B low halogen requirements of <=1000ppm threshold. Antimony trioxide based flame retardants must also meet the <=1000ppm threshold requirement.

(3) MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

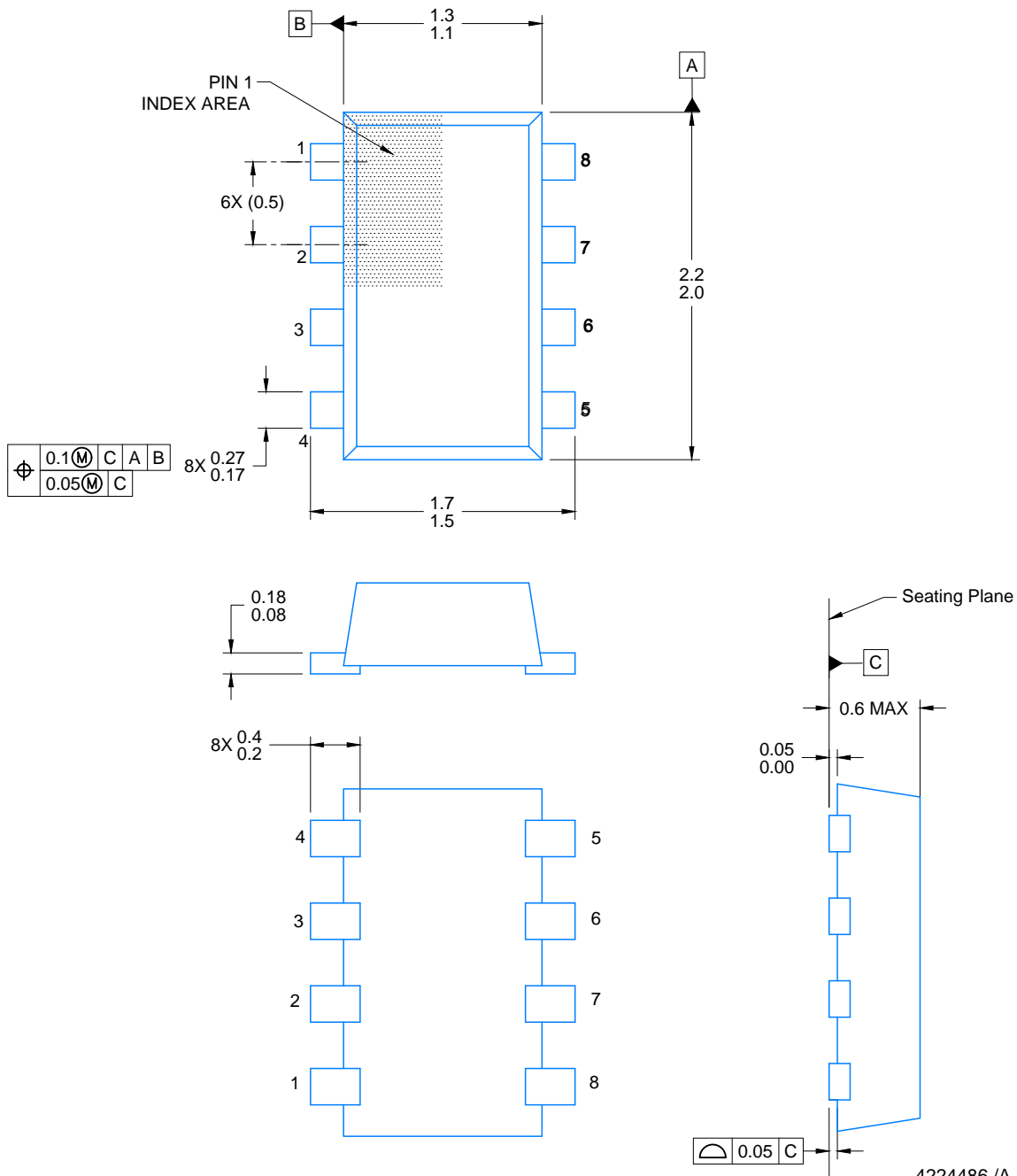
(4) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

(5) Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

⁽⁶⁾ Lead finish/Ball material - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

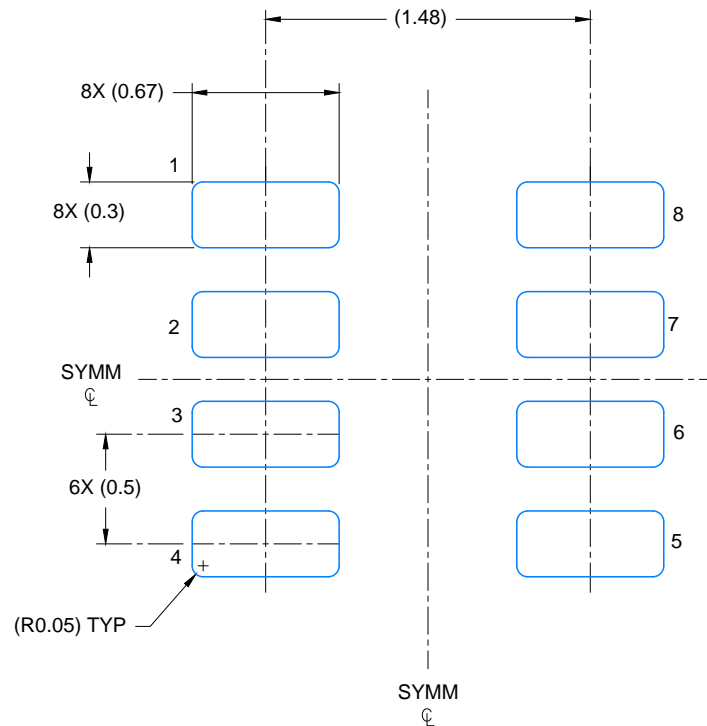
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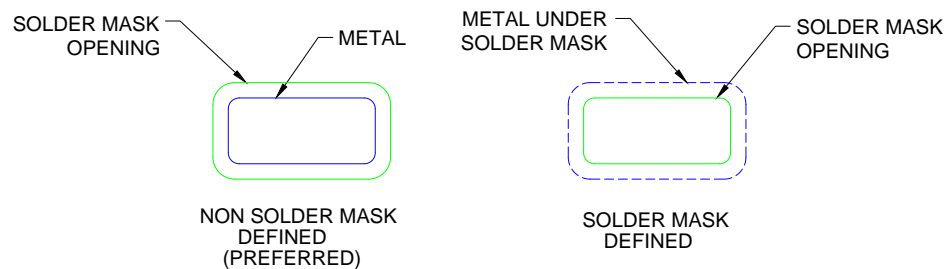


NOTES:

1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
2. This drawing is subject to change without notice.
3. Body dimensions do not include mold flash, protrusions or gate burrs.
Mold flash, interlead flash, protrusions or gate burrs shall not exceed 0.15 per end or side
4. Reference JEDEC registration TO-236, except minimum foot length.



LAND PATTERN EXAMPLE
EXPOSED METAL SHOWN
SCALE: 30X

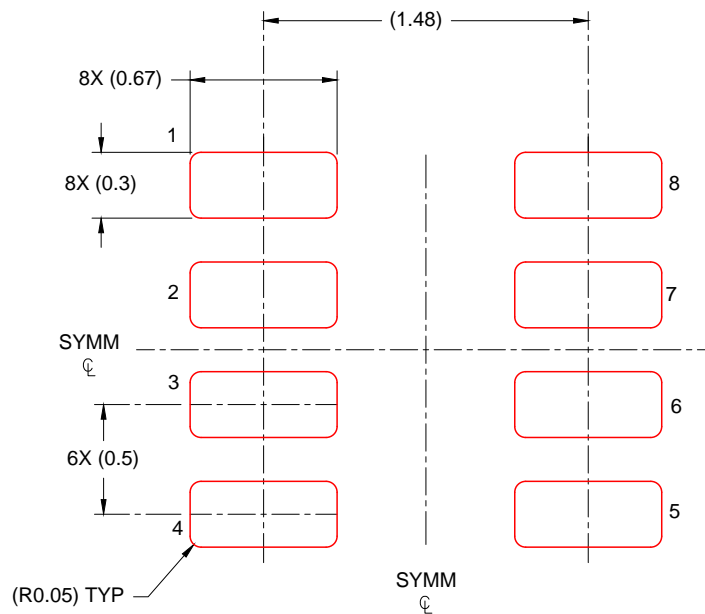


SOLDER MASK DETAILS

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NOTES: (continued)

5. Publication IPC-7351 may have alternate designs.
6. Solder mask tolerances between and around signal pads can vary based on board fabrication site.



SOLDER PASTE EXAMPLE
 BASED ON 0.125 mm THICK STENCIL
 SCALE: 30X

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NOTES: (continued)

7. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
8. Board assembly site may have different recommendations for stencil design.

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