

APPENDIX E: User Defined Solution Control

You can control the I/O, monitor the energies and other solution norms of interest, and shut down the problem whenever you please with user subroutine ucctrl1 in dyn21.F. The arguments are defined in the listing provided below. This subroutine is called each time step and does not need any control card to operate.

```

subroutine ucctrl1 (numnp,ndof,time,dt1,dt2,prtc,pltc,frci,prto,
. plto,frc0,vt,vr,at,ar,ut,ur,xmst,xmsr,irbody,rbdyn,usrhv,
. messag,totalm,cycle,idrint,mtype,lrb,nrba,rbcor,x,rbv,nrbn,
. nrb,xrb,yrb,zrb,axrb,ayrb,azrb,dtx,nmmat,rba,fvalnew,fvalold,
. fvalmid,fvalnxr)

c
c*****Livermore Software Technology Corporation (LSTC)*****
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c
c   user subroutine for solution control. It is called at the
c   beginning of time step n+1.
c
c
c   note: ls-dyna uses an internal numbering system to
c         accommodate arbitrary node numbering. to access
c         information for user node n, address array location m,
c         m = lqf8(n,1). to obtain user node number, n,
c         corresponding to array address m, set n = lqfinv(m,1)
c
c   arguments:
c       numnp = number of nodal points
c       ndof = number of degrees of freedom per node
c       time = current solution time at n+1
c       dt1 = time step size between time n-1 and n
c       dt2 = time step size between time n and n+1
c       prtc = output interval for taurus time history data
c       pltc = output interval for taurus state data
c       frci = output interval for taurus interface force data
c       prto = output time for time history file
c       plto = output time for state data
c       frco = output time for force data
c       vt(3,numnp) = nodal translational velocity vector
c       vr(3,numnp) = nodal rotational velocity vector. this
c                     array is defined if and only if ndof = 6
c       at(3,numnp) = nodal translational acceleration vector
c       ar(3,numnp) = nodal rotational acceleration vector. this
c                     array is defined if and only if ndof = 6
c       ut(3,numnp) = nodal translational displacement vector
c       ur(3,numnp) = nodal rotational displacement vector. this
c                     array is defined if and only if ndof = 6
c       xmst(numnp) = reciprocal of nodal translational masses
c       xmsr(numnp) = reciprocal of nodal rotational masses. this
c                     array is defined if and only if ndof = 6

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c          fvalold      = array for storing load curve values at time n
c          fvalnew      = array for setting load curve values at time n+1
c          only load curves with 0 input points may be user
c          defined. When the load curve is user set, the
c          value at time n must be stored in array fvalold.
c          fvalmid      = array for predicting load curve values at time n+3/2
c          fvalnxt      = array for predicting load curve values at time n+2
c          for some applications it is necessary to predict the
c          load curve values at time n+2, a time that is not known,
c          this for instance for boundary prescribed motion. In
c          this case the load curve values at time n+3/2 need to
c          be predicted in fvalmid, and fvalold should be set to
c          fvalnew and fvalnew should be set to fvalnxt. See
c          coding below.
c
c          irbody       = 0 if no rigid bodies
c          rbdyn(numnp) =flag for rigid body nodal points
c                         if deformable node then set to 1.0
c                         if rigid body node then set to 0.0
c                         defined if and only if rigid bodies are present
c                         i.e., irbody.ne.0 if no rigid bodies are
c                         present
c          usrvh(lenhv)=user defined history variables that are stored
c                         in the restart file. lenhv = 100+7*nummat where
c                         nummat is the # of materials in the problem.
c                         array usrvh is updated only in this subroutine.
c          messag       = flag for dyna3d which may be set to:
c                         'sw1.' ls-dyna3d terminates with restart file
c                         'sw3.' ls-dyna3d writes a restart file
c                         'sw4.' ls-dyna3d writes a plot state
c          totalm       = total mass in problem
c          cycle        = cycle number
c          idrint      = flag for dynamic relaxation phase
c                         .ne.0: dynamic relaxation in progress
c                         .eq.0: solution phase
c          mtype(*)     = material type for each part in the model
c          lrb(*)       = lead rigid body for each rigid body
c                         If part n is rigid and is a lead or has not
c                         been merged then lrb(n)==n.
c          nrba(*)      = starting index in nrb(*) of the nodes for each
c                         rigid body
c          rbcor(3,*)   = rigid body cg coordinates
c          x(3,*)       = Node coordinate array
c          rbv(6,*)    = rigid body cg velocity
c          nrbn(*)     = # nodes in each rigid body
c          nrb(*)      = List of all rigid body nodes
c          xrb(*)      = RB scratch array as long as longest nrbn() value
c          yrb(*)      = RB scratch array as long as longest nrbn() value
c          zrb(*)      = RB scratch array as long as longest nrbn() value
c          axrb(*)     = RB scratch array as long as longest nrbn() value
c          ayrb(*)     = RB scratch array as long as longest nrbn() value
c          azrb(*)     = RB scratch array as long as longest nrbn() value
c          dtx          = (dt1+dt2)*0.5 except at time 0 when it is = dt2
c          nmmat        = number of parts in the model
c          rba(6,*)    = rigid body cg acceleration
c          fvalnew      = array for setting load curve values at time n+1
c          only load curves with 0 input points may be user
c          defined. When the load curve is user set, the
c          value at time n must be stored in array fvalold.
c          fvalold      = array for storing load curve values at time n
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c      fvalmid      = array for predicting load curve values at time n+3/2
c      fvalnxt      = array for predicting load curve values at time n+2
c          for some applications it is necessary to predict the
c          load curve values at time n+2, a time that is not known,
c          this for instance for boundary prescribed motion. In
c          this case the load curve values at time n+3/2 need to
c          be predicted in fvalmid, and fvalold should be set to
c          fvalnew and fvalnew should be set to fvalnxt. See
c          coding below.
c
c      include 'ptimes.inc'
c
c      prtims(1-37)=output intervals for ascii files
c
c      ascii files:
c          ( 1)-cross section forces
c          ( 2)-rigid wall forces
c          ( 3)-nodal data
c          ( 4)-element data
c          ( 5)-global data
c          ( 6)-discrete elements
c          ( 7)-material energies
c          ( 8)-noda interface forces
c          ( 9)-resultant interface forces
c          (10)-smug animator
c          (11)-spc reaction forces
c          (12)-nodal constraint resultant forces
c          (13)-airbag statistics
c          (14)-avs database
c          (15)-nodal force groups
c          (16)-output intervals for nodal boundary conditions
c          (17)-(32) unused at this time
c          (37)-auto tiebreak damage output
c
c      prtlst(32)=output times for ascii files above. when solution time
c          exceeds the output time a print state is dumped.
c
c      common/rbkeng/enrbdy,rbdyx,rbdyy,rbdyz
c
c      total rigid body energies and momentums:
c          enrbdy = rigid body kinetic energy
c          rbdyx = rigid body x-momentum
c          rbdyy = rigid body y-momentum
c          rbdyz = rigid body z-momentum
c
c      common/swmke/swxmom,swymom,swzmmom,swkeng
c
c      total stonewall energies and momentums:
c          swxmmom = stonewall x-momentum
c          swymom = stonewall y-momentum
c          swzmmom = stonewall z-momentum
c          swkeng = stonewall kinetic energy
c
c      common/deengs/deeng
c
c          deeng = total discrete element energy
c
c      common/bk28/summss,xke,xpe,tt,xte0,erodeke,erodeie,selie,selke,
c          . erodehg
c
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c      xpe = total internal energy in the finite elements
c
c      common/sprengs/spreng
c
c      spreng = total spr energy
c
c      character*(*) messag
c      integer cycle
c      real*8 x
c      dimension vt(3,*),vr(3,*),at(3,*),ar(3,*),
c     . xmst(*),xmsr(*),rbdyn(*),usrhv(*),mtype(*),lrb(*),nrba(*),
c     . rbcor(3,1),x(*),rbv(6,*),nrbn(*),nrb(*),xrb(*),yrb(*),
c     . zrb(*),axrb(*),ayrb(*),azrb(*),rba(6,*),fvalnew(*),
c     . fvalold(*),fvalmid(*),fvalnxt(*)
c      real*8 ut(3,*),ur(3,*)
c
c      sample momentum and kinetic energy calculations
c
c      remove all comments in column 1 below to activate
c      i = 1
c      if (i.eq.1) return
c      return
cc
cc
cc      initialize kinetic energy, xke, and x,y,z momentums.
cc
c      xke = 2.*swkeng+2.*enrbdy
c      xm = swxmom+rbdyx
c      ym = swymom+rbdyy
c      zm = swzmom+rbdyz
cc
c      numnp2 = numnp
c      if (ndof.eq.6) then
c          numnp2 = numnp+numnp
c      endif
c      write(iotty,*) ndof
cc
cc
cc      no rigid bodies present
cc
c      if (irbody.eq.0) then
cc          note in blank comment vr follows vt.  this fact is used below.
c          do 10 n = 1,numnp2
c              xmsn = 1./xmst(n)
c              vn1 = vt(1,n)
c              vn2 = vt(2,n)
c              vn3 = vt(3,n)
c              xm = xm+xmsn*vn1
c              ym = ym+xmsn*vn2
c              zm = zm+xmsn*vn3
c              xke = xke+xmsn*(vn1*vn1+vn2*vn2+vn3*vn3)
c 10      continue
cc
cc
cc      rigid bodies present
cc
c      else
cc          nodal accerations for rigid bodies
cc
c          do 12 n = 1,nmmat
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```
c      if (mtype(n).ne.20.or.lrb(n).ne.n) go to 12
c      lrbn = nrba(n)
c      call stvlut(rbcor(1,n),x,vt,at,ar,vr,rbv(1,n),dt2,
c      .    nrbn(n),nrb(lrbn),xrb,yrb,zrb,axrb,ayrb,azrb,dtx)
c
c      rigid body nodal accelerations
c
c      if (ndof.eq.6) then
c          call rbnacc(nrbn(n),nrb(lrbn),rba(4,n),ar)
c      endif
c
c 12    continue
cc
c      do 20 n = 1,numnp
c      xmsn = 1./xmst(n)
c      vn1 = rbdyn(n)*vt(1,n)
c      vn2 = rbdyn(n)*vt(2,n)
c      vn3 = rbdyn(n)*vt(3,n)
c      xm = xm+xmsn*vn1
c      ym = ym+xmsn*vn2
c      zm = zm+xmsn*vn3
c      xke = xke+xmsn*(vn1*vn1+vn2*vn2+vn3*vn3)
c 20    continue
c      if (ndof.eq.6) then
c          do 30 n = 1,numnp
c          xmsn = 1./xmsr(n)
c          vn1 = rbdyn(n)*vr(1,n)
c          vn2 = rbdyn(n)*vr(2,n)
c          vn3 = rbdyn(n)*vr(3,n)
c          xm = xm+xmsn*vn1
c          ym = ym+xmsn*vn2
c          zm = zm+xmsn*vn3
c          xke = xke+xmsn*(vn1*vn1+vn2*vn2+vn3*vn3)
c 30    continue
c      endif
c      endif
cc
cc      total kinetic energy
c      xke=.5*xke
cc      total internal energy
c      xie = xpe+deeng+spreng
cc      total energy
c      xte = xke+xpe+deeng+spreng
cc      total x-rigid body velocity
c      xrbv = xm/totalm
cc      total y-rigid body velocity
c      yrbv = ym/totalm
cc      total z-rigid body velocity
c      zrbv = zm/totalm
      return
end
```

