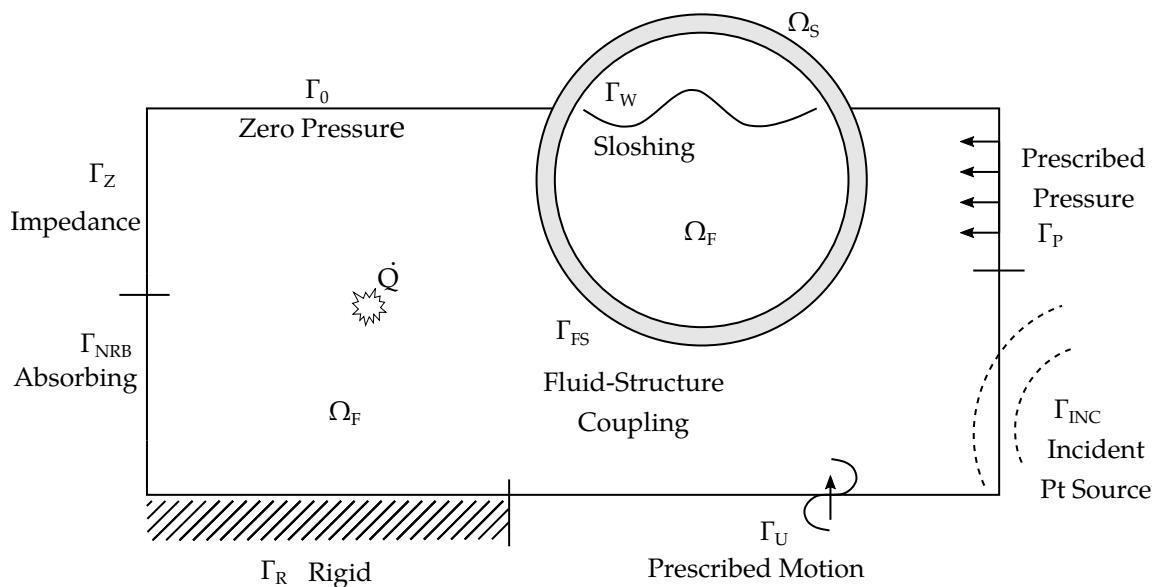


# Appendix W:

## Acoustic Volume Element and Spectral Element Solvers



**Figure 74-1.** Sketch of the structural-acoustic system

### Explicit Transient Acoustic Iso-parametric Element Solutions

The longstanding and default solution path for transient acoustic solutions in LS-DYNA uses low-order iso-parametric finite elements. It is capable of treating shock-induced cavitation and uses the displacement potential as the fundamental nodal unknown. This is the approach used if neither \*CONTROL\_IMPLIPLICIT\_SSD\_DIRECT nor \*CONTROL\_ACOUSTIC\_SPECTRAL is used.

Boundary condition treatment is summarized in [Table 74-1](#). This solution path uses an inverted boundary condition strategy that may be confusing to analysts familiar with potential formulations. Kinematic boundary conditions are interpreted as if the formulation were a Lagrangian, displacement-based model like \*MAT\_ELASTIC. Thus, fluid faces that are constrained with nodal displacement constraints are rigid, sliding faces. Fluid faces that are left free are pressure release or zero pressure faces. And fluid faces that are merged with structural nodes are coupled faces. Structural coupling when there is fluid on both sides of a shell element requires \*BOUNDARY\_ACOUSTIC\_COUPLING or \*BOUNDARY\_ACOUSTIC\_COUPLING\_MISMATCH. Non-reflecting and absorbing boundaries use either \*BOUNDARY\_NON\_REFLECTING or the perfectly matched layer of \*MAT\_PML\_ACOUSTIC.

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Model Parameters	Keywords
Material Properties, $\Omega_F$	*MAT_ACOUSTIC
Structural Coupling, $\Gamma_{FS}$	Merge fluid and structural nodes on one side *BOUNDARY_ACOUSTIC_COUPLING *BOUNDARY_ACOUSTIC_COUPLING_-MISMATCH
Prescribed Boundary Motion, $\Gamma_U$	No support
Prescribed Boundary Pressure, $\Gamma_P$	*LOAD_SEGMENT_SET
Rigid Boundary, $\Gamma_R$	*BOUNDARY_SPC
Impedance Boundary, $\Gamma_Z$	*BOUNDARY_ACOUSTIC_IMPEDANCE
Absorbing Boundary, $\Gamma_{NRB}$	*BOUNDARY_NON_REFLECTING *MAT_PML_ACOUSTIC
Zero Pressure Boundary, $\Gamma_{NRB}$	Leave these nodes unconstrained
Small Amplitude Wave Boundary, $\Gamma_W$	No support
Internal Point Source, $\dot{Q}$	No support

**Table 74-1.** Keywords for explicit transient acoustic iso-parametric finite element solutions

### Explicit Transient Acoustic Spectral Element Solutions

The spectral acoustic elements in LS-DYNA invoked with \*CONTROL\_ACOUSTIC\_SPECTRAL use higher-order interpolants based on Legendre polynomials. The elements converge exponentially and support integration orders from 2 to 15. They are especially recommended for ultrasonic wave propagation. These elements have internal degrees-of-freedom (invisible to users). These degrees-of-freedom are generated automatically based on the integration order chosen. You may change the integration order and accuracy of the solution without remeshing.

For the explicit solution to the transient, fluid-structure interaction problem with acoustic spectral elements, the following nonsymmetric system is solved at every time step:

$$\begin{bmatrix} M_{ss} & 0 \\ -\rho c^2 T_{fs}^T & M_{ff} \end{bmatrix} \begin{bmatrix} \ddot{u} \\ \ddot{p} \end{bmatrix} + \begin{bmatrix} W_{ss} & 0 \\ 0 & W_{ff} \end{bmatrix} \begin{bmatrix} \dot{u} \\ \dot{p} \end{bmatrix} + \begin{bmatrix} K_{ss} & T_{fs} \\ 0 & K_{ff} \end{bmatrix} \begin{bmatrix} u \\ p \end{bmatrix} = \begin{bmatrix} r_s \\ r_f \end{bmatrix}$$

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Here  $M_{ss}$ ,  $W_{ss}$ , and  $K_{ss}$  are the structural mass, damping and stiffness.  $M_{ff}$ ,  $W_{ff}$ , and  $K_{ff}$  are the equivalent matrices for the fluid.  $T_{fs}$  is the fluid-structure coupling matrix. Vector  $u$  is the structural displacements, and  $p$  is the pressure. The time step used is the smallest stable time step in either of the acoustic or structural domains. The applicable keywords are summarized by [Table 74-2](#).

Model Parameters	Keywords
Material Properties, $\Omega_F$	*MAT_ACOUSTIC *MAT_ACOUSTIC_DAMP
Structural Coupling, $\Gamma_{FS}$	*BOUNDARY_ACOUSTIC_COUPLING_- SPECTRAL
Weak Structural Coupling, $\Gamma_{FS}$	*INTERFACE_ACOUSTIC *BOUNDARY_ACOUSTIC_INTERFACE
Prescribed Boundary Motion, $\Gamma_U$	*BOUNDARY_ACOUSTIC_PRESCRIBED_- MOTION
Prescribed Boundary Pressure, $\Gamma_P$	*BOUNDARY_ACOUSTIC_PRESSURE_- SPECTRAL
Rigid Boundary, $\Gamma_R$	This is a natural condition
Impedance Boundary, $\Gamma_Z$	*BOUNDARY_ACOUSTIC_IMPEDANCE
Absorbing Boundary, $\Gamma_{NRB}$	*BOUNDARY_ACOUSTIC_NON_RE- FLECTING
Zero Pressure Boundary, $\Gamma_{NRB}$	*BOUNDARY_ACOUSTIC_FREE_SURFACE
Small Amplitude Wave Boundary, $\Gamma_W$	*BOUNDARY_ACOUSTIC_FREE_SURFACE
Internal Point Source, $\dot{Q}$	*LOAD_ACOUSTIC_SOURCE

**Table 74-2.** Keywords for explicit transient acoustic spectral element solutions

The perfectly matched layer of \*MAT\_ACOUSTIC\_PML is not currently supported in spectral acoustic element solutions.

For post-processing, pressure-time histories are written with \*DATABASE\_ACE-OUT and \*DATABASE\_HISTORY\_ACOUSTIC. Plot states for the user's mesh are written to the D3PLOT file. The integration point used for those plot states is derived from the closest spectral pressure degree-of-freedom.

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## Implicit Direct Steady State Acoustic FE Solutions

For the direct solution to the forced vibration problem with acoustic fluid coupling, a complex symmetric system of equations is solved. This starts with

$$\begin{bmatrix} M_{ss} & 0 \\ 0 & M_{ff} \end{bmatrix} \begin{bmatrix} \ddot{u} \\ \dot{q} \end{bmatrix} + \begin{bmatrix} W_{ss} & T_{fs} \\ T_{fs}^T & W_{ff} \end{bmatrix} \begin{bmatrix} \dot{u} \\ \dot{q} \end{bmatrix} + \begin{bmatrix} K_{ss} & 0 \\ 0 & K_{ff} \end{bmatrix} \begin{bmatrix} u \\ q \end{bmatrix} = \begin{bmatrix} r_s \\ r_f \end{bmatrix}$$

Here  $M_{ss}$ ,  $W_{ss}$ , and  $K_{ss}$  are the structural mass, damping and stiffness.  $M_{ff}$ ,  $W_{ff}$ , and  $K_{ff}$  are the equivalent matrices for the fluid.  $T_{fs}$  is the fluid-structure coupling matrix. Vector  $u$  contains the displacements of structural nodes. Vector  $q$  contains the integral of the pressure, that is, the fluid nodal pressure equals  $\dot{q}$ .

Assuming  $u = \bar{U}_s e^{i\omega t}$ ,  $q = \bar{\Phi}_f e^{i\omega t}$ , and  $r_{f/s} = \bar{F}_{f/s} e^{i\omega t}$ , the assembled system of equations becomes complex

$$\begin{bmatrix} -\omega^2 M_{ss} + i\omega W_{ss} + \bar{K}_{ss} & i\omega T_{fs} \\ i\omega T_{fs}^T & -\omega^2 \bar{M}_{ff} + i\omega \bar{W}_{ff} + \bar{K}_{ff} \end{bmatrix} \begin{bmatrix} \bar{U}_s \\ \bar{\Phi}_f \end{bmatrix} = \begin{bmatrix} \bar{F}_s \\ F_f \end{bmatrix}$$

Submatrices  $K_{ss}$ ,  $M_{ff}$ ,  $W_{ff}$ , and  $K_{ff}$  may also be complex and may be frequency dependent. This is the system that is solved for every forcing frequency with \*CONTROL\_IMPLICIT\_SSD\_DIRECT.

Model Parameters	Keywords
Material Properties, $\Omega_F$	*MAT_ACOUSTIC *MAT_ACOUSTIC_DAMP *MAT_ACOUSTIC_COMPLEX *MAT_ACOUSTIC_POROUS_DB
Structural Coupling, $\Gamma_{FS}$	*BOUNDARY_ACOUSTIC_COUPLING_- MISMATCH
Weak Structural Coupling, $\Gamma_{FS}$	*INTERFACE_ACOUSTIC *BOUNDARY_ACOUSTIC_INTERFACE
Prescribed Boundary Motion, $\Gamma_U$	*BOUNDARY_ACOUSTIC_PRESCRIBED_- MOTION
Rigid Boundary, $\Gamma_R$	This is a natural condition
Impedance Boundary, $\Gamma_Z$	*BOUNDARY_ACOUSTIC_IMPEDANCE *BOUNDARY_ACOUSTIC_COMPLEX

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Model Parameters	Keywords
Absorbing Boundary, $\Gamma_{NRB}$	*BOUNDARY_ACOUSTIC_MECHANICAL
Zero Pressure Boundary, $\Gamma_{NRB}$	*BOUNDARY_ACOUSTIC_NON_REFLECTING
Small Amplitude Wave Boundary, $\Gamma_W$	*BOUNDARY_ACOUSTIC_FREE_SURFACE
Internal Point Source, $\dot{Q}$	*LOAD_ACOUSTIC_SOURCE
Incident Wave Point Source, $\Gamma_{INC}$	*LOAD_ACOUSTIC_SOURCE

**Table 74-3.** Keywords for implicit, direct steady state acoustic finite element solutions

For post-processing, real and imaginary nodal response is written with \*DATABASE\_ACEOUT and \*DATABASE\_HISTORY\_ACOUSTIC.

