

An Introduction to Risk and Reliability Analysis in Coastal Engineering Designs

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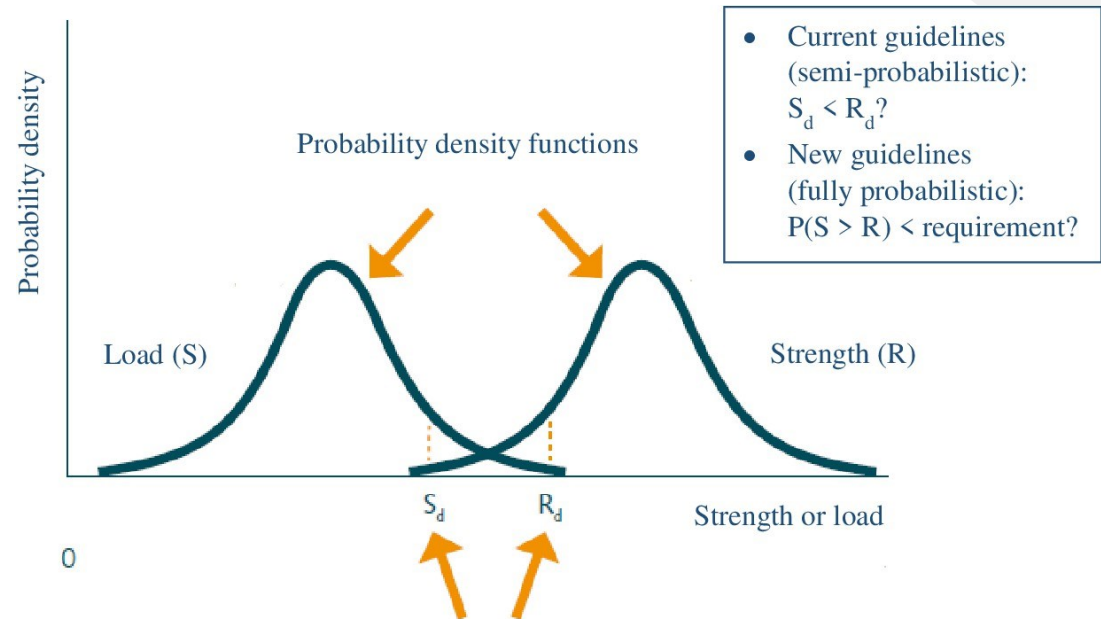
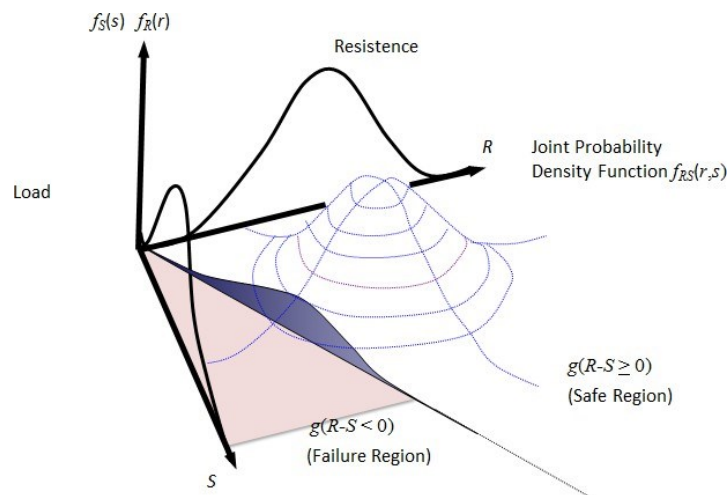
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References:

- Jonkman, S. N., Steenbergen, R. D. J. M., Morales-Nápoles, O., Vrouwenvelder, A. C. W. M., & Vrijling, J. K. (2015). **Probabilistic design: risk and reliability analysis in civil engineering**. Delft university of technology, Lecture notes CIE4130.
- Moustapha, M., Marelli, S., & Sudret, B. (2019). **UQLab user manual–Reliability-based design optimization**. Technical report, Chair of Risk, Safety & Uncertainty Quantification, ETH Zurich. Report# UQLab-V1. 2-114.
- Li, L. (2012). **Sequential Design of Experiments to Estimate a Probability of Failure** (Doctoral dissertation, Supélec).

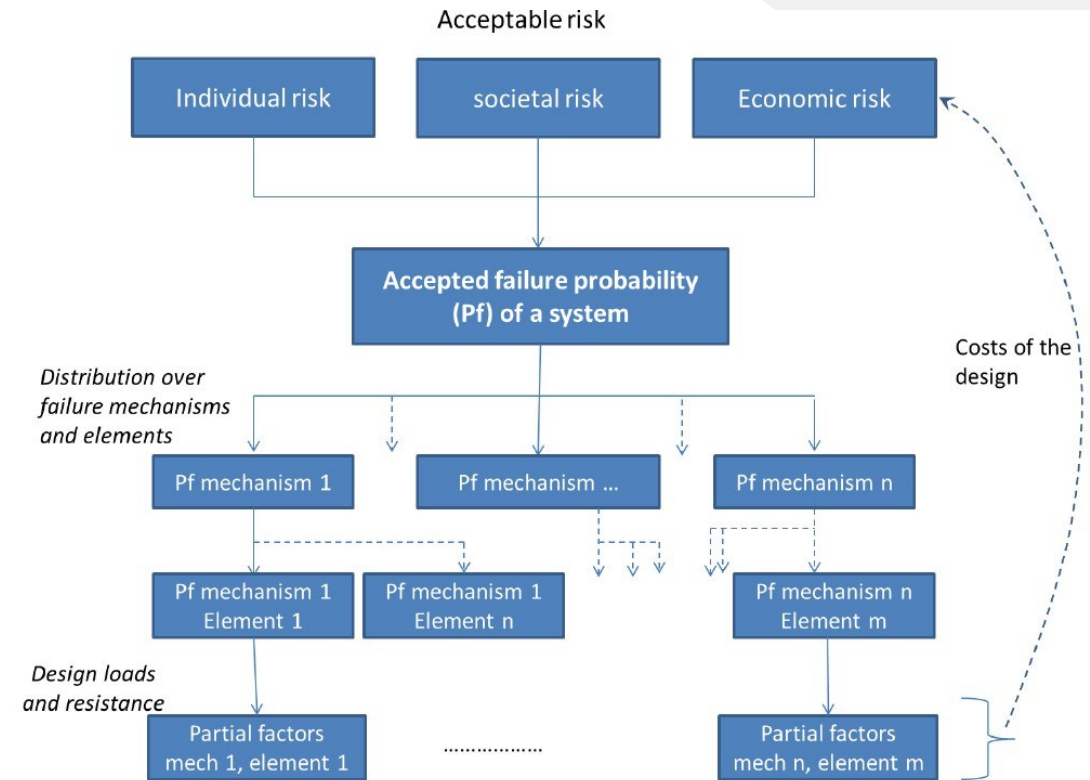
Risk

- Risk refers to the combination of **probability** and **consequences** of undesired events.
- Almost all activities in life are characterized by some level of risk.

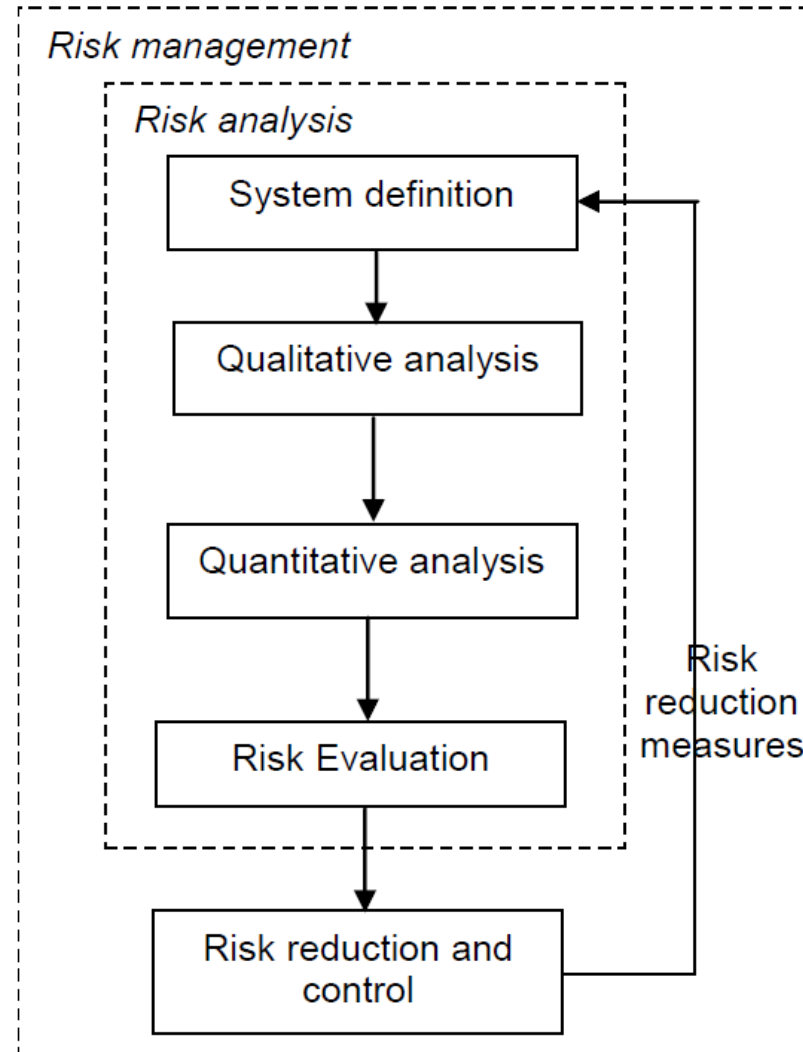


Probabilistic design

- **General definition:** the relationship between safety standards and engineering design.
- **Overall objective:** to design (and maintain) systems with an acceptable risk level in an optimal way.



Schematic view of steps in risk assessment and risk management



Qualitative analysis

- **Goal:** gain insight, as complete as possible, into all possible undesired events and their consequences.
- **Failure:** when a system or part of it no longer fulfils one or more desired functions.
- **Limit state:** a condition of a structure beyond which it no longer fulfils the relevant design criteria.
- **Ultimate limit state (ULS):** if exceeded, failure or collapse of a system or structure occurs.
- **Serviceability limit state (SLS):** if exceeded, leads to temporary and/or partial failure.

Quantitative analysis

- The **probabilities** and **consequences** of the defined undesired events are determined in this step.
- Limit state **Z** (by considering the resistance **R** and the loads **S**):

$$Z = R - S$$

- Failure occurs when $R < S$, so when $Z < 0$.
- **Failure probability:**

$$P(Z < 0) = P(S > R)$$

- There are several techniques for computing the probability of failure.

Formulation for limit state design

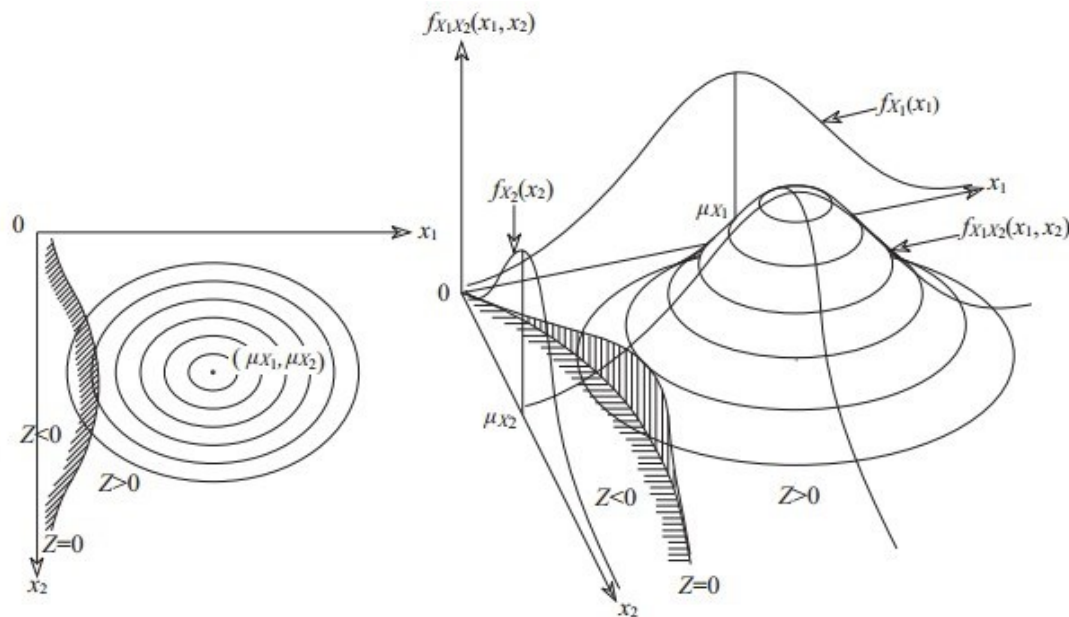
- General formulation:

$$g(\underline{X}) = Z = 0$$

- where the vector \underline{X} consists of n basic variables such as:
 - material properties
 - actions (loads)
 - geometrical properties
 - model uncertainties.
- For all basic variables one has to consider an appropriate **probabilistic** model.
- Negligible variation in time or space: one can consider that variable as **deterministic**.

Failure probability

$$P_f = \Pr[G < 0] = \iint_{D_f} f_{x_1, x_2}(x_1, x_2) dx_1 dx_2 \Rightarrow \boxed{P_f = \Phi(-\beta)}$$



- β : reliability index
- The probability of survival (or the reliability) is defined as:

$$P_s = 1 - P_f$$

Reliability methods

Level 0 methods:

- Deterministic design

Level I methods (semi-probabilistic design):

- The uncertain parameters are modelled by **one characteristic value** for load and resistance.
- for example in codes based on the **partial coefficients (γ 's)** concept.

Reliability methods

Level II methods (approximation):

- The uncertain parameters are modelled by the **mean** values and the **standard deviations**, and by the **correlation coefficients** between the stochastic variables.
- The stochastic variables are implicitly assumed to be **normally distributed**.

Level III methods (numerical):

- The uncertain quantities are modelled by their **joint distribution** functions.
- The probability of failure calculated exactly, e.g. by numerical integration.

Reliability methods

Level IV methods (risk-based):

- In these methods the consequences (cost) of failure are also taken into account and the **risk (consequence multiplied by the probability of failure)** is used as a measure of the reliability.
- In this way different designs can be compared on an economic basis taking into account **uncertainty, costs** and **benefits**.

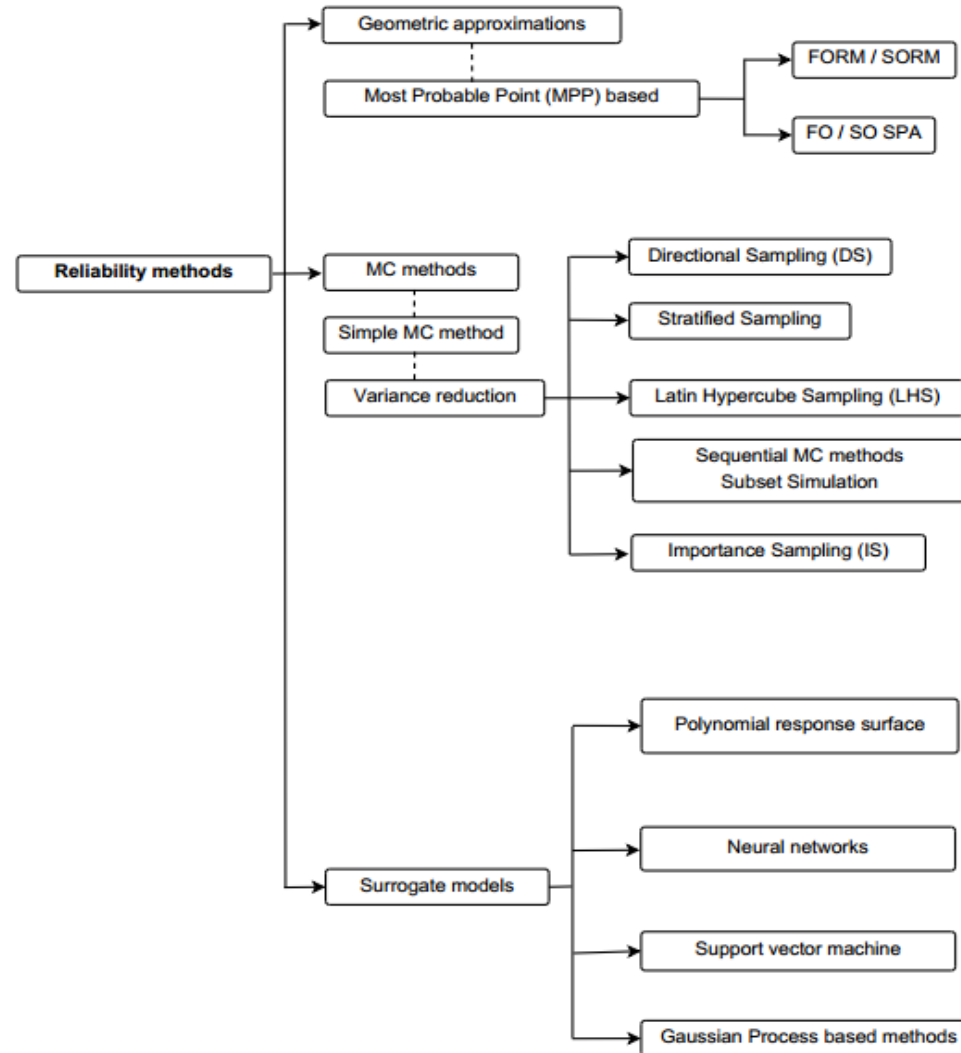
Level III Methods

- Methods of level III evaluate the following integral **explicitly**:

$$P_f = \int_{g(\underline{X}) < 0} f_{\underline{X}}(\underline{x}) d\underline{x}$$

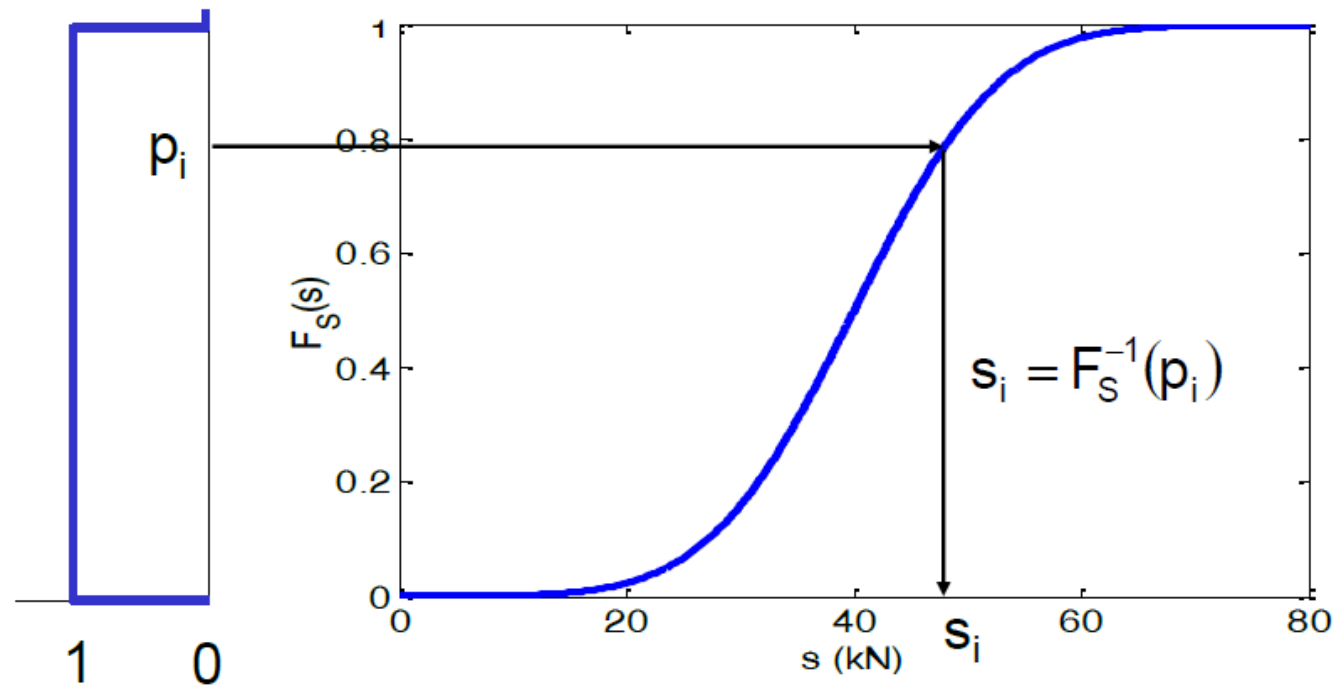
- Direct calculation of this integral is rather difficult in $n > 2$.
- In these case, we use simulation-based techniques, like Monte-Carlo Simulation (MCS)

Reliability methods



Monte-Carlo Simulation (MCS)

- Drawing random numbers from a uniform probability density function between zero and one.



Monte-Carlo Simulation (MCS)

- Drawing samples from joint probability distribution function:

$$F_{\vec{X}}(\vec{X}) = F_{X_1}(X_1)F_{X_2|X_1}(X_2 | X_1) \dots F_{X_m|X_1, X_2, \dots, X_{m-1}}(X_m | X_1, X_2, \dots, X_{m-1})$$

$$X_1 = F_{X_1}^{-1}(X_{u_1})$$

$$X_2 = F_{X_2|X_1}^{-1}(X_{u_2} | X_1)$$

.

.

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$$X_m = F_{X_m|X_1, X_2, \dots, X_{m-1}}^{-1}(X_{u_m} | X_1, X_2, \dots, X_{m-1})$$

Independent variables:

$$X_i = F_{X_i}^{-1}(X_{u_i})$$

Monte-Carlo Simulation (MCS)

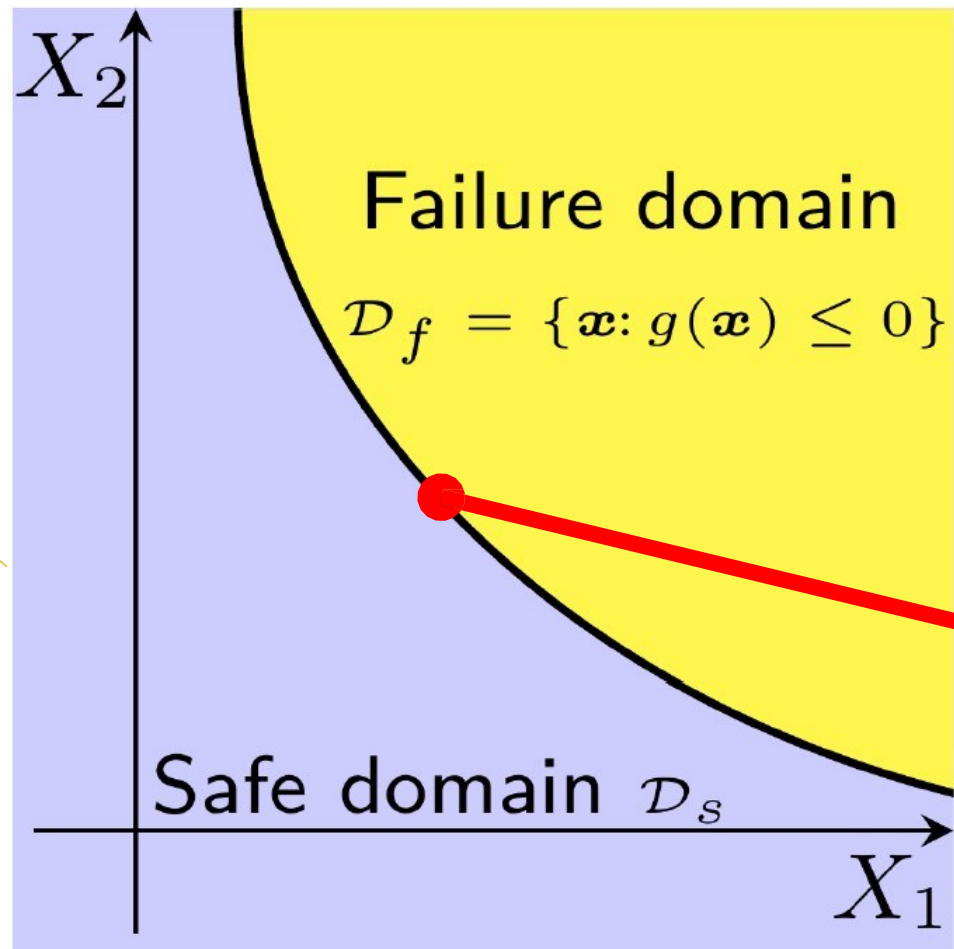
$$P_f = \frac{N_f}{N}$$

- N_f number of failure ($g < 0$)
- N number of simulations
- In case $N \rightarrow \infty$ one obtains the failure probability P_f .
- Criterion for the proper selection of N :

$$N \cong \frac{1}{\delta^2 P_f} \quad \delta = \sqrt{\frac{1 - P_f}{N P_f}}$$

- δ is the target coefficient of variation (relative error)

Level II Methods

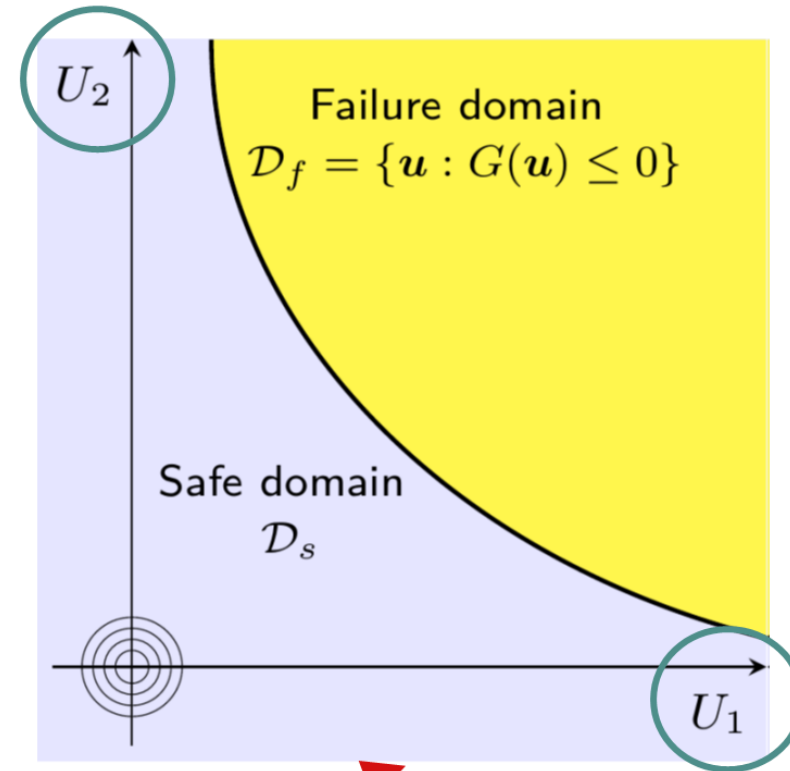
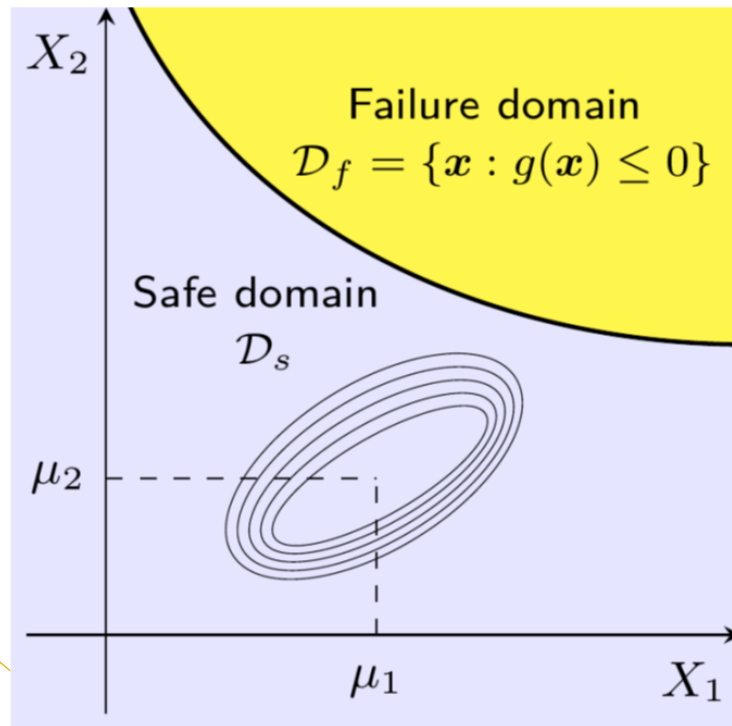


$$P_f = \mathbb{P}(g(X) \leq 0)$$

$$g(x) = 0$$

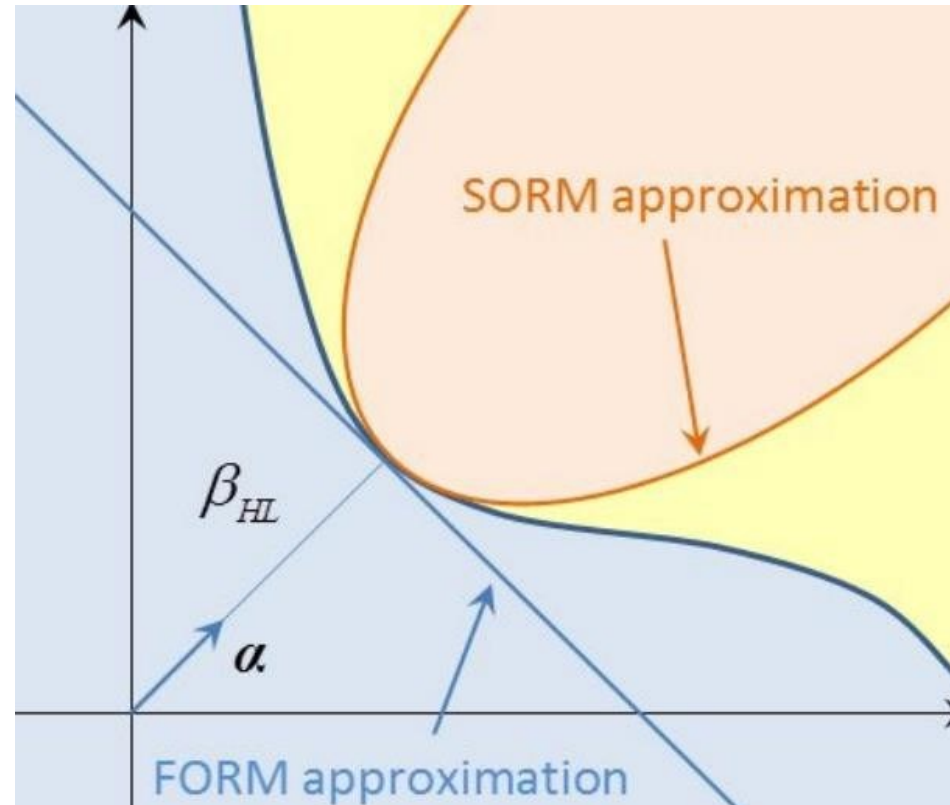
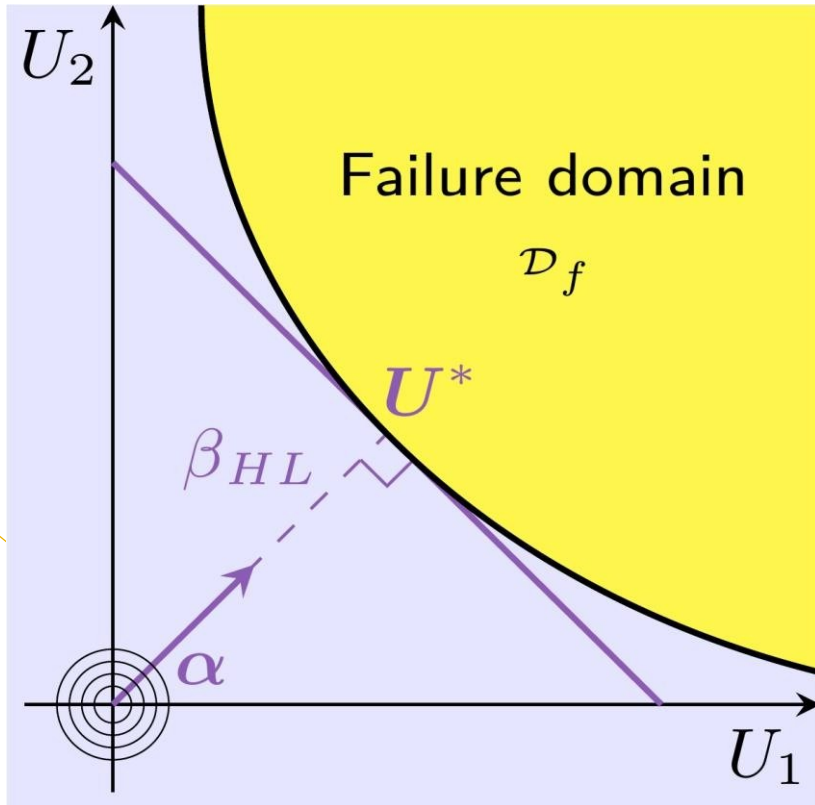
Level II Methods

FORM method



Level II Methods

FORM method



Level II Methods

Reliability Index According to Hasofer-Lind

- Proposed by Hasofer and Lind (1974)
- Consider uncorrelated normally distributed variables
- First, normalize the basic variables X_i using:

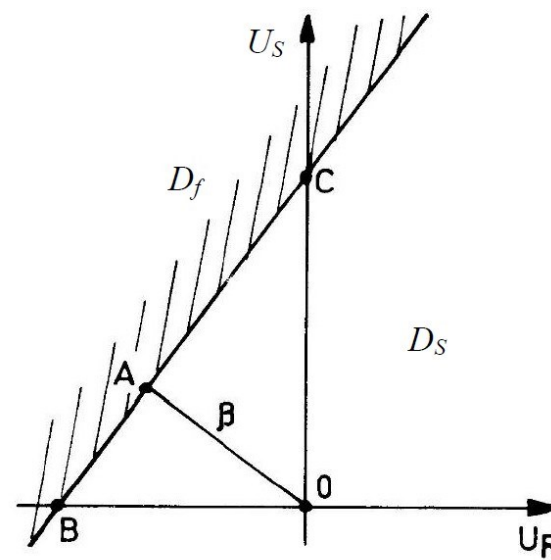
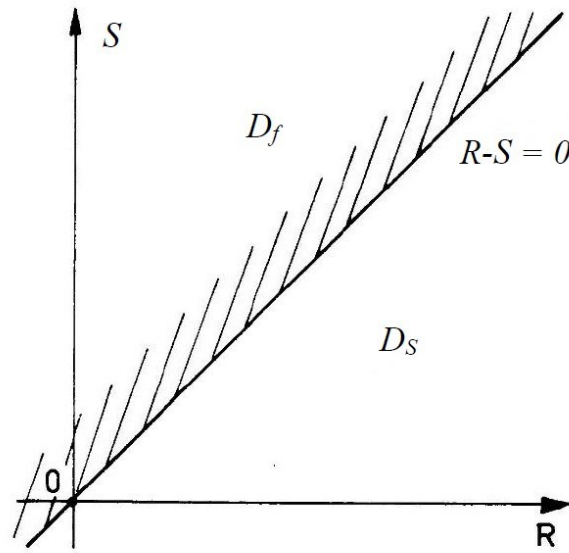
$$U_i = \frac{X_i - \mu_i}{\sigma_i} \quad \mu_i = E[X_i] \text{ and } \sigma_i^2 = \text{Var}[X_i]$$

- In case of normalized basic variables U_i it holds that $E[U_i] = 0$, and $\text{Var}[U_i] = 1$.
- The limit state equation becomes $g(\underline{U}) = 0$ in the n-dimensional U-space.

Level II Methods

Reliability Index According to Hasofer-Lind

- The reliability index β is equal to the **shortest distance** from the **origin** to the **surface described by $g(\underline{U}) = 0$** in the space of the normalized basic variables.

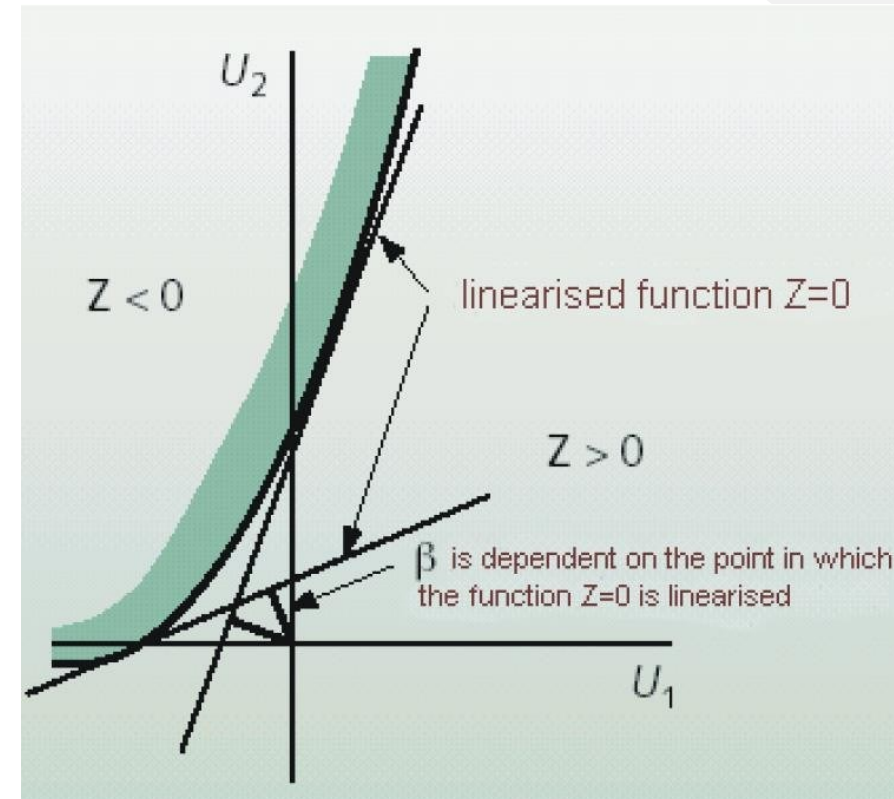


Level II Methods

Reliability Index According to Hasofer-Lind

- The definition of the reliability index according to Hasofer and Lind (1974) does not depend on whether or not the reliability function is **linear**.

$$\beta = \min_{Z=0} \left(\sqrt{U_1^2 + U_2^2} \right)$$



Level II Methods

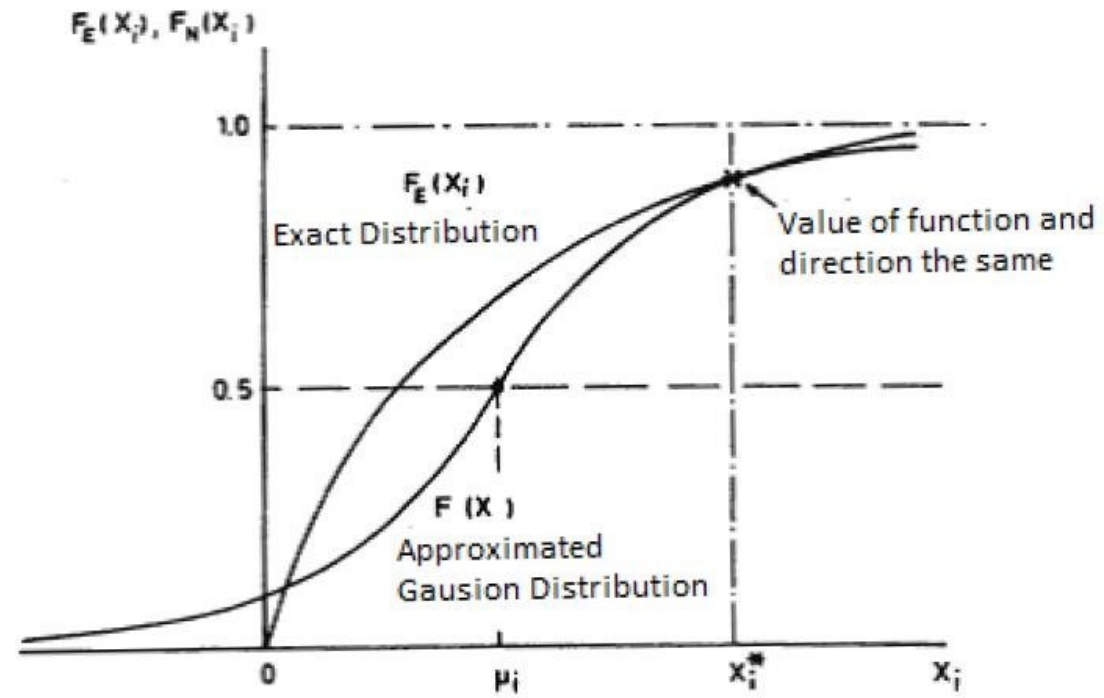
Reliability Index According to Hasofer-Lind

- The closest point to the origin is called **design point**.
- The design point is the point of the limit state equation with the highest probability density, hence in literature one often mentions this as the "**most probable failure point**".
- Finding the design point is **an iterative process**, for which several methods are available. Two methods are:
 1. Method 1: transformation to normal variables
 2. Method 2: direct iteration based on the limit state function

Level II Methods

Reliability Index According to Hasofer-Lind

- The **independent non-normally distributed** base variables have to be transformed to normally distributed base variables.
- Apply Rackwitz-Fiessler algorithm (1977).
- This transformation **assumes** that the values of the real and the approximated probability density function and probability distribution function are equal in the **design point**.




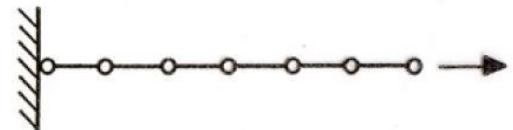
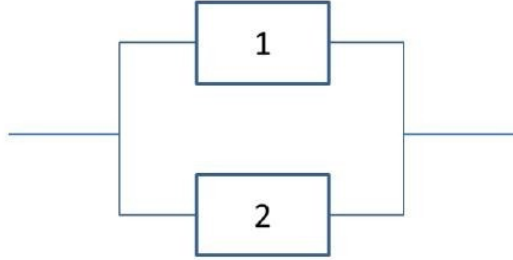
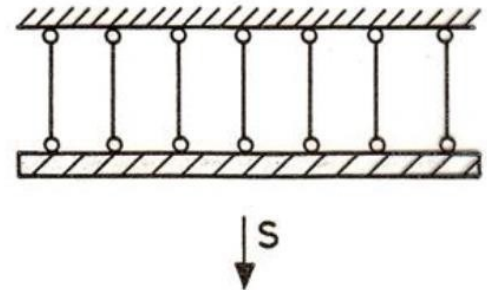
Level II Methods

Reliability Index According to Hasofer-Lind

- **Dependent random base variables:**
- Have to be transformed to independent variables.
- If there is a **clear functional relation** between the variables, it is often possible to formulate the reliability function in such a way that variables are eliminated.
- In many cases the relation between the variables is not known exactly and **statistical dependence is involved**. In this case the base variables can be transformed. A general transformation method is **the Rosenblatt-transformation**.

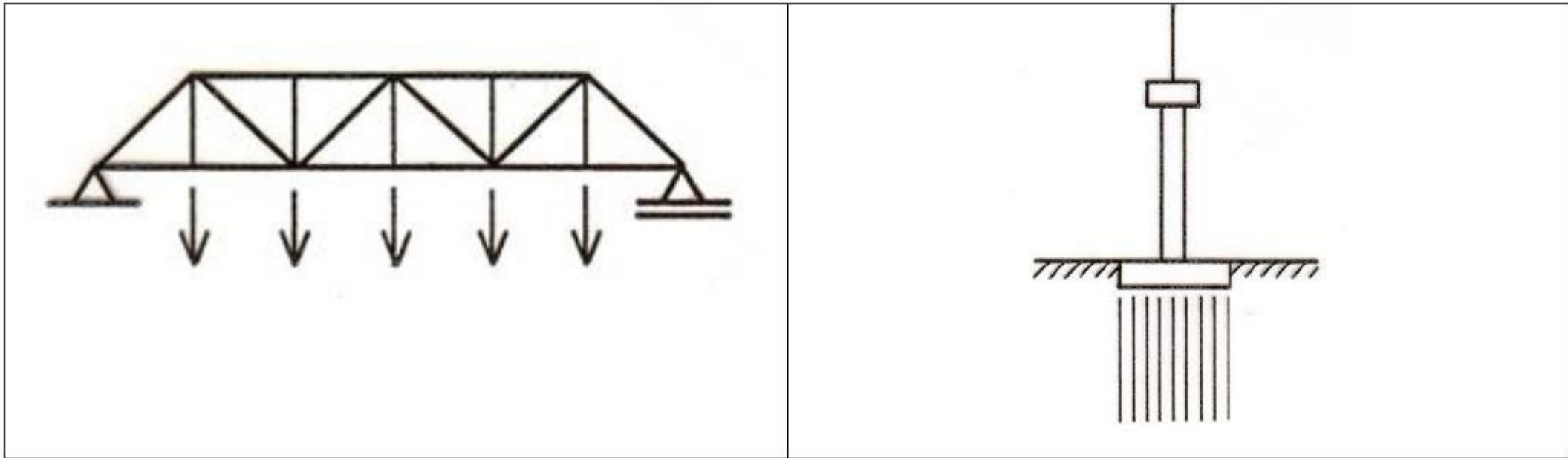
Reliability of systems

- Within a **series** system, failure of a single element will always lead to the failure of the entire system.
- Within a **parallel** system, failure of one element can be compensated by another element.

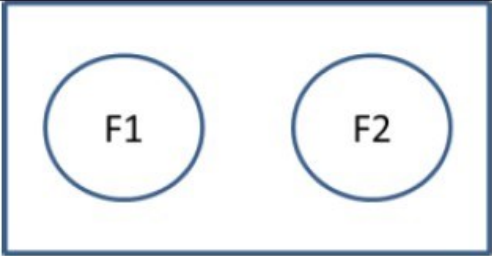
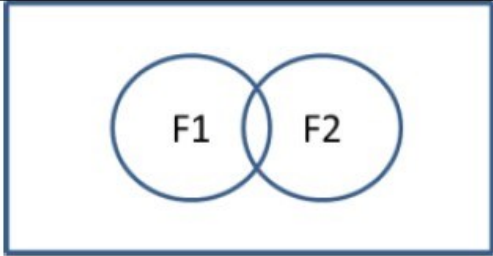
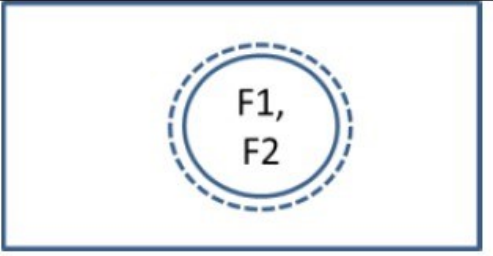
| Type | System representation | Simple example (structural engineering) |
|----------|--|--|
| Series |  |  |
| Parallel |  |  |

Reliability of systems

- Examples of a series and parallel system: a **bridge** (series system; left); and a **pile foundation** (parallel system, right)



Series system

| Case | Mutually exclusive | Independent | Dependent |
|---|--|---|---|
| Correlation coefficient. $\rho_{Z1,Z2} =$ | -1 | 0 | 1 |
| Venn diagram |  |  |  |
| System failure probability $P(F)$ | $P(F_1) + P(F_2)$ | $P(F_1) + P(F_2) - P(F_1) \cdot P(F_2)$ | $Max(P(F_1), P(F_2))$ |

Series system

- Bounds proposed by Ditlevsen (1977)

$$\text{Max}(\Phi(-\beta_1)\Phi(-\beta_2^*); \Phi(-\beta_1^*)\Phi(-\beta_2)) \leq \boxed{P(F_1 \cap F_2)} \leq \Phi(-\beta_1)\Phi(-\beta_2^*) + \Phi(-\beta_1^*)\Phi(-\beta_2)$$

in which:

$$\beta_1 = -\Phi^{-1}(P(F_1)), \text{ so } P(F_1) = \Phi(-\beta_1)$$

$$\beta_2 = -\Phi^{-1}(P(F_2))$$

$$\beta_1^* = \frac{\beta_1 - \rho\beta_2}{\sqrt{1-\rho^2}}$$

$$\beta_2^* = \frac{\beta_2 - \rho\beta_1}{\sqrt{1-\rho^2}}$$

ρ is the correlation coefficient between F_1 and F_2 .

Series system

- Three failure mechanisms

Lower bound:

$$P(F) = P(F_1) + P(F_2) - P(F_1 \cap F_2) + P(F_3) - P(F_1 \cap F_3) - P(F_2 \cap F_3)$$

Upper bound:

$$P(F) = P(F_1) + P(F_2) - P(F_1 \cap F_2) + P(F_3) - \text{Max}\{P(F_1 \cap F_3), P(F_2 \cap F_3)\}$$

Series system

- n failure mechanisms

$$P(F) \leq \sum_i P_i - \sum_{i \geq 2} \max_{j < i} P_{ij}$$

$$P(F) \geq \sum_i P_i - \sum_{i \geq 2} \sum_{j < i} P_{ij}$$

In which:

$$P_i = P\{Z_i < 0\} = \Phi(-\beta_i)$$

$$P_{ij} = P\{Z_i < 0 \text{ and } Z_j < 0\} = \Phi(-\beta_i)\Phi(-\beta_j^*) + \Phi(-\beta_i^*)\Phi(-\beta_j)$$

Parallel system

- The bounds for a system with multiple identical elements with each failure probability P_i are as follows:

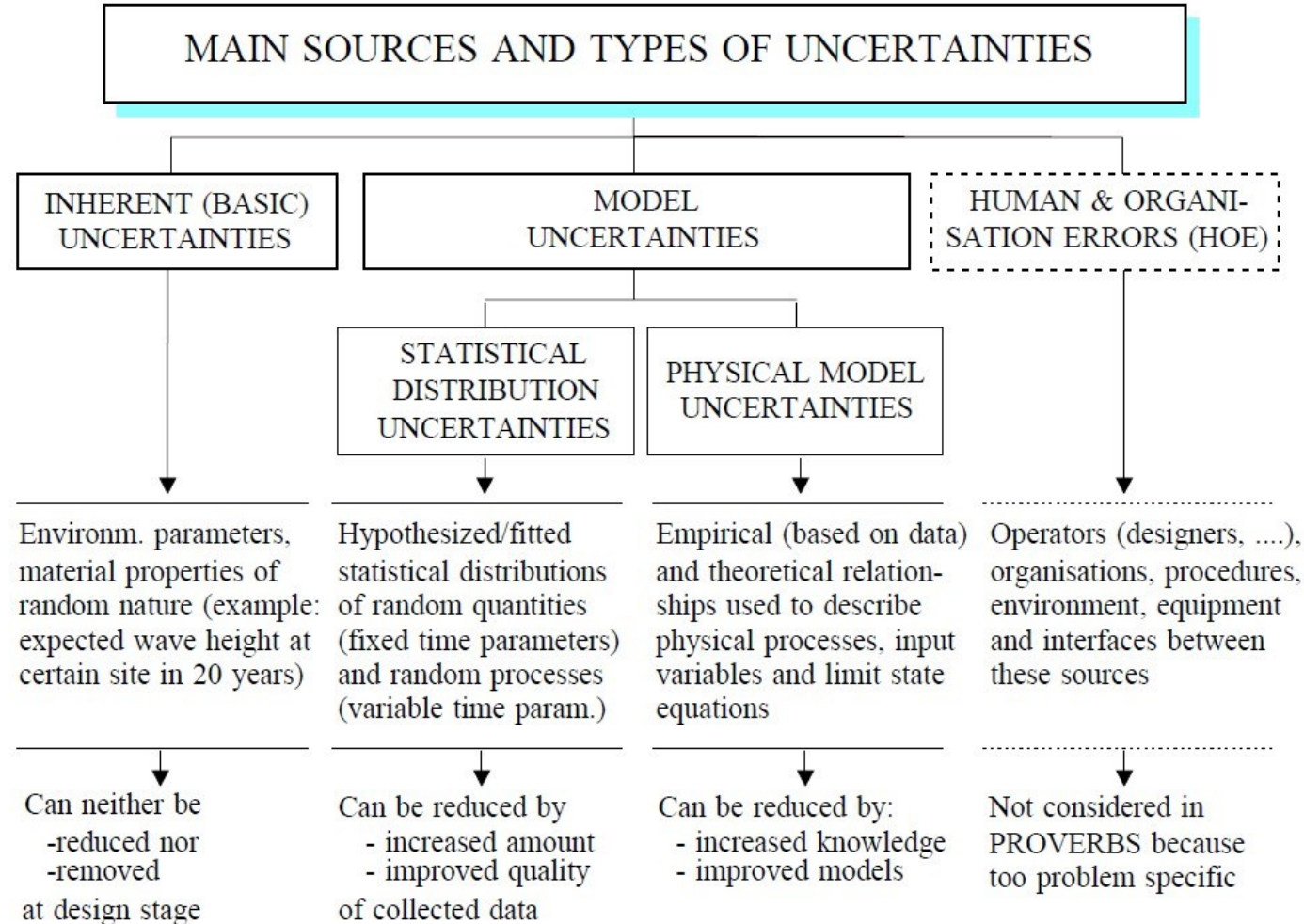
$$0 \leq P_f \leq \text{Min}(P_i)$$

- The **lower** bound is found for a situation in which failures are **mutually exclusive**.
- The **upper** bound is valid for a case in which the failure are **fully dependent**.

Reliability-based Design Optimization

Sources and types of uncertainties

- Ref.: PROVERBS



Why RBDO?

- Design under uncertainties
- Optimal balance between performance and cost
- Increasing safety
- The RBDO solution is basically achieved by jointly **performing a reliability analysis** and **solving an optimization problem**.

General formulation of a RBDO problem

$$d^* = \arg \min_{d \in \mathbb{D}} \underset{\substack{\downarrow \\ \text{Cost function}}}{c(d)} \quad \text{subject to:} \quad \left\{ \begin{array}{ll} \boxed{f_j(d) \leq 0,} & \text{Soft constraints} \\ \boxed{\mathbb{P}(g_k(\mathbf{X}(d), \mathbf{Z}) \leq 0) \leq \bar{P}_{f_k}}, & \text{Hard constraints} \end{array} \right. \quad \begin{array}{l} \{j = 1, \dots, s\}, \\ \{k = 1, \dots, n\}. \end{array}$$

- **Design variables (d):** to be optimized
- **\mathbf{X} :** a set of random variables indexed on the design variables which may represent **manufacturing tolerances**
- **\mathbf{Z} : environmental variables** which are parameters that may be random but cannot be controlled by the designer, e.g. the loading

General formulation of a RBDO problem

- **Soft constraints:** are simple functions that bound the design space.
- **Hard constraints:** are limit-state functions which describe the performance of the system.

An alternative formulation using the reliability index

$$d^* = \arg \min_{d \in \mathbb{D}} c(d) \quad \text{subject to: } \begin{cases} f_j(d) \leq 0, & \{j = 1, \dots, s\}, \\ \bar{\beta}_k - \beta_k(\mathbf{X}(d), \mathbf{Z}) \leq 0, & \{k = 1, \dots, n\}, \end{cases}$$

$$\bar{\beta}_k = \Phi^{-1}(1 - \bar{P}_{f_k}) \text{ and } \beta_k = \Phi^{-1}(1 - P_{f_k})$$

- are the target and structural reliability indices of the k -th limit-state
- Φ is the standard Gaussian cumulative distribution

Solution of a RBDO problem

Two-level approach

- Nested loops
- The outer loop explores the design space
- The inner one computes the corresponding failure probability
- **Two classical approaches:**
 1. Reliability index approach
 2. Performance measure approach
- **RIA:** uses FORM in the inner loop
 - Hasofer-Lind-Rackwitz-Fiessler (HLRF) and its improved version (iHLRF)
 - low numerical efficiency
 - easy to implement.
- **PMA:** inner loop consists of an inverse FORM analysis
 - searches for minimum performance target point (MPTP).

Solution of a RBDO problem

Mono-level approach

- Avoiding the reliability analysis at each iteration of the optimization process
- The problem is converted into an **equivalent single loop deterministic** process
- Enforcing the **Karush-Kuhn-Tucker optimality conditions** of the reliability analysis as additional constraints

Decoupled approach

- Sequentially solving a deterministic optimization problem followed by a reliability analysis
- Sequential Optimization and Reliability Assessment (SORA)
- Converts the probabilistic constraint into an **equivalent deterministic constraint** using the minimum performance target point

RBDO solution using surrogate models

- Avoid expensive model evaluations
- For highly non-linear or when multiple design points exist
- For real-world problems using time-consuming high-fidelity computational models (e.g. finite element).
- Gaussian process a.k.a. Kriging
- Polynomial chaos expansions
- Polynomial chaos-Kriging
- Low-rank approximation
- Support vector machines

Optimization algorithms

- Interior-point (see *fmincon* in MATLAB);
- Sequential quadratic programming (see *fmincon* in MATLAB);
- Genetic algorithm (see *ga* in MATLAB);
- Constrained (1 + 1)-CMA-ES (Arnold and Hansen (2012));
- Hybrid algorithms, which refine the solution identified by a genetic algorithm or (1+1)-CMA-ES by an additional gradient-based minimization.

UQLab intro

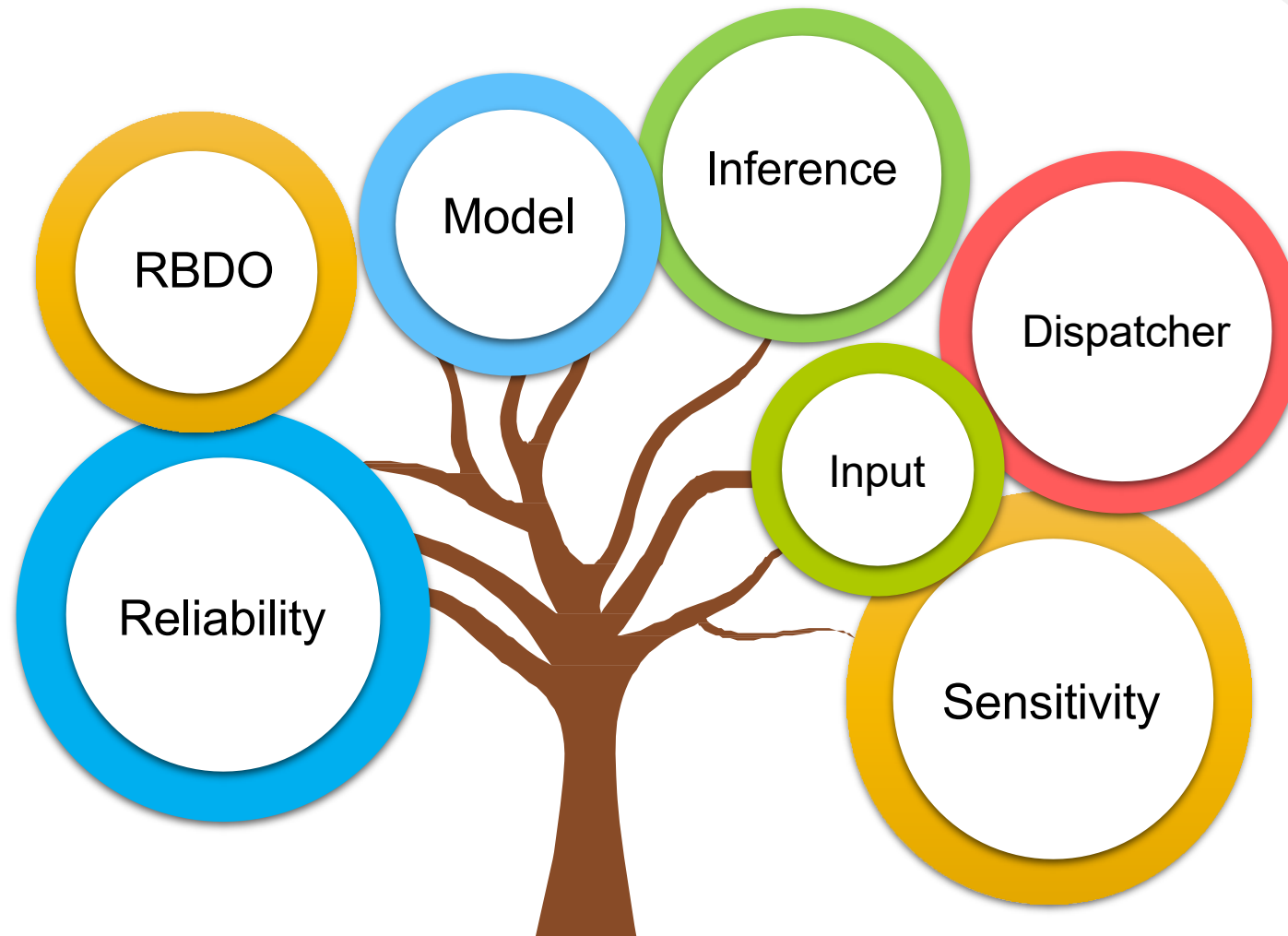
- MATLAB®-based Uncertainty Quantification framework
- Highly optimized open source algorithms
- Fast learning curve for beginners
- Modular structure, easy to extend
- Academic/ Commercial/ Group
- More that 3000 academic users

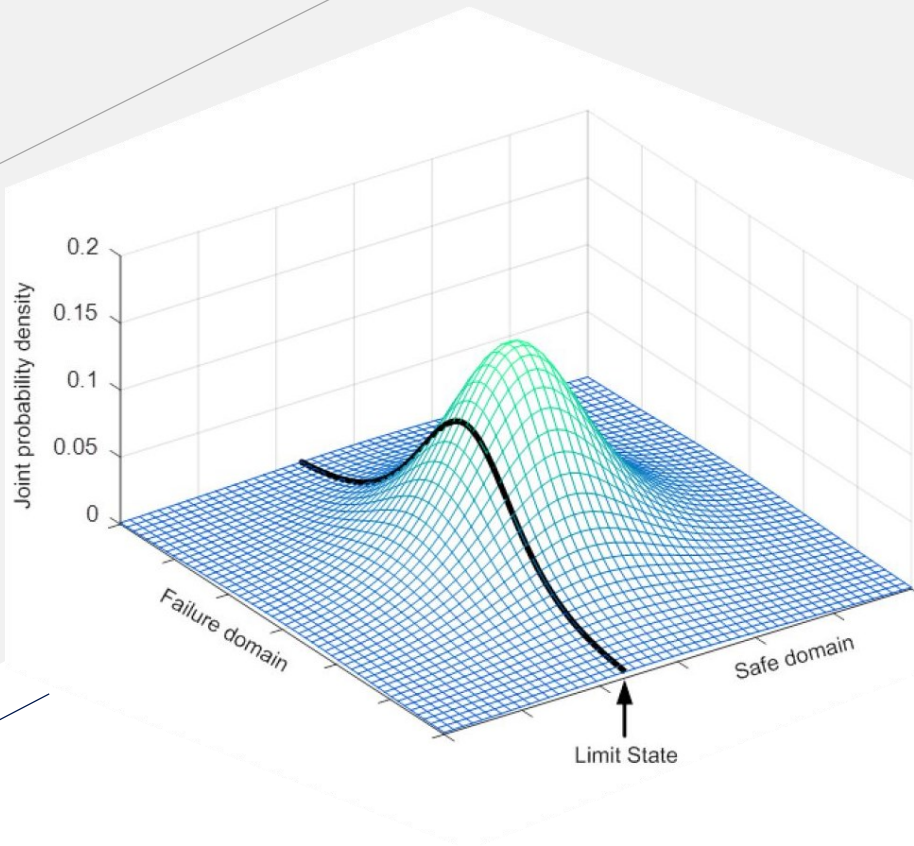


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UQLab modules





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