

# Major Project 1 ...

- Look at problem of transferring satellite to MEO (GPS) from Initial LEO Orbit
  - Code Continuous Thrust Example



- $a_{LEO} = 8530 \text{km}, a_{MEO} = 13,200 \text{ km}$
- You are going to compare (non-impulsive) low thrust, high  $I_{sp}$  transfer to high thrust, Low  $I_{sp}$  Hohmann transfer .. Both impulse and non-impulsive calculations
- •a) Low thrust (EP) transfer, Thrust F=10 N,  $I_{sp} = 2000 \text{ sec}$ 
  - Low Thrust final kick motor, Thrust F=2000 N,  $I_{sp}=270 \text{ sec}$
  - Assume final kick is performed impulsively
  - Calculate consumed mass for each system burn and total consumed mass
  - Accumulated  $\Delta V$  for each burn, total delta V
- b) High Thrust (Hohmann) transfer, Thrust F=2000 N,  $I_{sp}=270 \text{ sec}$ 
  - DV maneuvers are performed impulsively
  - Calculate consumed  $\Delta V$ , mass for each burn and total for both burns
  - Compare to low thrust maneuver

## Part a)

### • Continuous Small Thrust Problem

• For Part a)... assume final Orbit insertion  $\Delta V$  is delivered impulsively with Apogee Kick Motor Isp = 270 sec ..... Ignore atmospheric drag

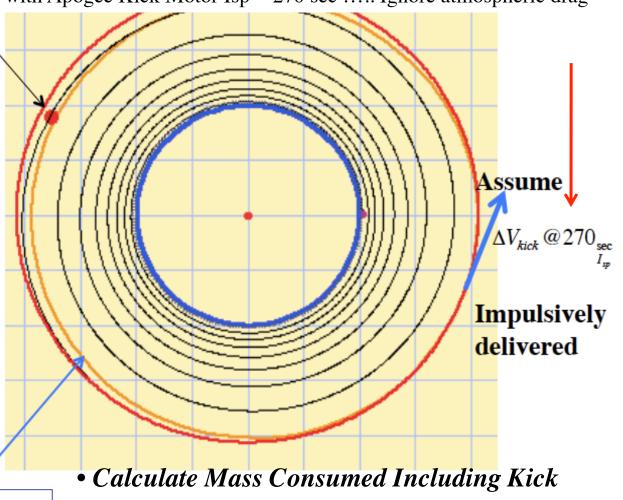
Terminate thrust when

$$R_{apogee} = a \cdot (1 + e)$$
$$= 13,200 km$$

#### Calculate:

- 1) Propellant mass req.  $+\Delta V$ For continuous transfer
- Propellant mass req. +∆V
   For kick delta V (impulsive)
   (orbit circularization)
- 3) Final mass = 1000 kg

**Orbit coast** 





### Part a)

### • Continuous Small Thrust Problem

... compare continuous thrust propellant mass calculations against Hohmann transfer calculations .. Assuming impulsively delivered Delta V for each burn

Burn 1: Isp = 2000 sec

Burn 2: Isp = 270 sec

... what can you conclude about the accuracy of the rocket equations and the impulsive Delta V assumption when applied to a long duration non-impulsive burn?



## Part a) Continuous Small Thrust

- ... Implement *both* Trapezoidal and Runge-Kutta Integration schemes
- ... Assume continuous thrust transfer to transfer orbit apogee using EP device, final orbit insertion using high thrust kick motor
- ... compare algorithm performance as Time interval  $\Delta T$  becomes progressively larger
- ... Is there a point where algorithm blows up?

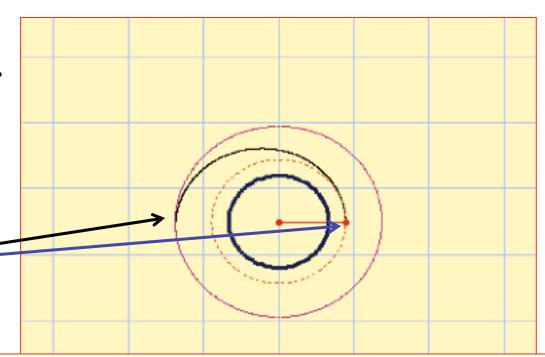


• Part b, Hohmann Transfer Calculations

#### Hohmann Transfer:

 $I_{sp}$ =270 sec  $F_{thrust}$ =2000 Nt

• Impulsive Burn Calculations



- Calculate  $\Delta V$ , Mass Consumed Including Kick
- Compare to Continuous Low Thrust Transfer Results

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Part c) Continuous Large Thrust Analysis

#### Terminate thrust when

$$R_{apogee} = a \cdot (1 + e)$$

=13,200km

Calculate:

**Orbit coast** 

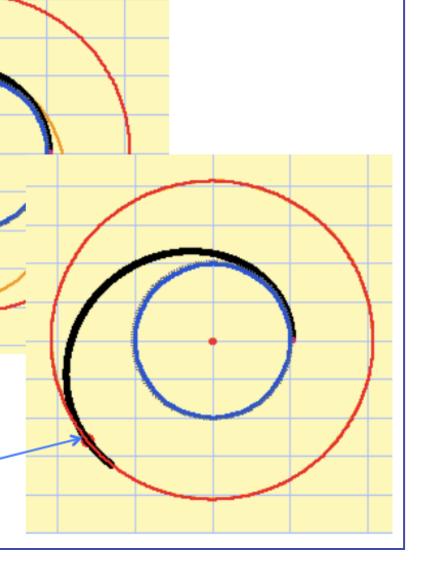
1) Propellant mass req.  $+\Delta V$ For continuous transfer

2) Propellant mass req. +ΔV
For kick delta V (Non-impulsively)
(orbit circularization)

3) Final mass = 1000 kg

Final Delta V delivered Non-impulsively

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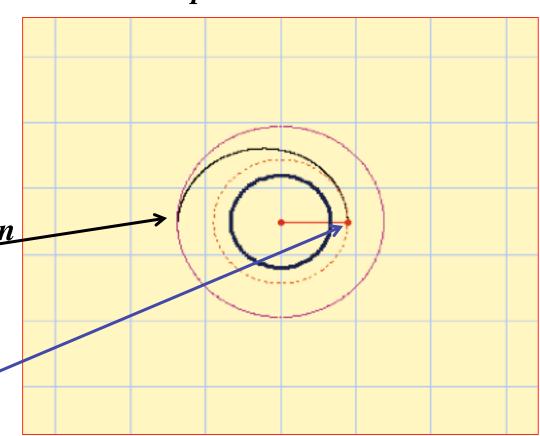
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• Part d) ... Work continuous large Thrust problem with *non-impulsive burns* at both ends

### Hohmann Transfer:

 $I_{sp}$ =270 sec  $F_{thrust}$ =2000 Nt

- Non-Impulsive Burn Calculations
- Continuous Thrust Burn Calculations



• Use Hohmann Transfer for Guidance on Burns times, positions



- Continuous Large Thrust Problem
- Assume BOTH burns are performed non-impulsively Terminate burn thrust when

$$R_{apogee} = a \cdot (1 + e)$$
$$= 13,200 \, km$$

- You decide when and how long to initiate the second burn to circularize the orbit
- Assume for large thrust .... 2000 Nt thrust (both burns) ... Isp = 270 sec
- Calculate required propellant mass for Burn1, Burn2 (and Total)
- Use integrator of your choice ... calculate actual delivered Delta V Based on consumed mass ... using rocket equation



# Continuous Large Thrust Problem

... compare Hohmann Transfer for 2000 Nt Rocket (assuming impulsive thrust) Versus 2000 Nt rocket with Non Impulsive Thrust .... Also compare consumed masses to High  $I_{sp}$  Continuous Thrust transfer

... what can you conclude about the accuracy of the rocket equation and the impulsive Delta V assumption when applied to a short duration non-impulsive burn?

... what can you conclude about the effect of  $I_{sp \text{ on}}$  required propellant mass?

Position within initial orbit:

$$\begin{bmatrix} r \\ v \end{bmatrix}_0 = \begin{bmatrix} a_0 \left( 1 - e_0^2 \right) \\ 1 + e_0 \cos \left( v_0 \right) \\ v_0 \end{bmatrix} \rightarrow \begin{bmatrix} \text{circular orbit} \rightarrow e_0 = 0 \\ \text{can assume} \rightarrow v_0 = 0 \rightarrow a_0 = r_0 \end{bmatrix}$$

Angular velocity within initial orbit:

$$\omega_{0} = \frac{\sqrt{\mu} \left[ 1 + e_{0} \cos(v_{0}) \right]^{2}}{\left[ a_{0} \left( 1 - e_{0}^{2} \right) \right]^{3/2}} \rightarrow \begin{bmatrix} \text{circular orbit} \rightarrow e_{0} = 0\\ \text{can assume} \rightarrow v_{0} = 0, a_{0} = r_{0} \end{bmatrix}$$

$$\omega_{0} = \frac{\sqrt{\mu} \left[ 1 + e_{0} \cos(v_{0}) \right]^{2}}{\left[ a_{0} \left( 1 - e_{0}^{2} \right) \right]^{3/2}} = \frac{1}{r_{0}} \sqrt{\frac{\mu}{r_{0}}}$$

Linear Velocity within initial orbit:

$$\begin{bmatrix} V_r \\ V_v \end{bmatrix}_0 = r_0 \omega_0 \begin{bmatrix} \frac{e_0 \sin[v_o]}{[1 + e_0 \cos(v_o)]} \\ 1 \end{bmatrix} \rightarrow \begin{bmatrix} \text{circular orbit} \rightarrow e_0 = 0 \\ \text{can assume} \rightarrow v_0 = 0, a_0 = r_0 \end{bmatrix}$$

$$\begin{bmatrix} V_r \\ V_v \end{bmatrix}_0 = \begin{bmatrix} 0 \\ r_0 \omega_0 \end{bmatrix} = \begin{bmatrix} 0 \\ \sqrt{\frac{\mu}{r_0}} \end{bmatrix}$$

Instantaneous (no-nonconservative foreces acting) Keplerian orbit  $\rightarrow given: \begin{bmatrix} v_r \\ V_v \end{bmatrix}, \begin{bmatrix} r \\ v \end{bmatrix}$ 

$$a = \frac{\mu}{\left[\frac{2\mu}{r} - \left[V_r^2 + V_v^2\right]\right]}$$

$$e = \frac{r}{\mu} \sqrt{\left(V_v^2 - \frac{\mu}{r}\right)^2 + \left(V_r V_v\right)^2}$$

$$r_{perigee} = a(1 - e)$$

$$r_{apogee} = a(1 + e)$$