

1. Using basic calculations, prove that the maximum ionisation occurs at optical depth unity. Assume an isothermal atmosphere (i.e. $n(z) = n_0 \exp(-z/H)$) where H can be assumed constant) and use the definition of optical depth, $\tau = \sigma \int n \, dz$. Note that the formula for $n(z)$ allows for a very convenient representation of the integral or derivative of $n(z)$ with respect to z . You'll need that

$$I(s_\lambda) = \text{solar flux}$$

$$\sigma^a = \text{absorption crosssection}$$

The decrease intensity after it travels an incremental distance:

$$dI(s_\lambda) = -I(s_\lambda) n(z) \sigma^a ds_\lambda$$

$$\chi \rightarrow \text{Solar Zenith angle}$$

$$ds_\lambda = -dz \sec \chi$$

$$dI(s_\lambda) = -I(z) n(z) \sigma^a \sec \chi dz$$

$$\int_{I_\infty}^{I(z)} \frac{dI(z)}{I(z)} = \int_z^\infty \sigma^a \sec \chi n(z) dz$$

$$\ln\left(\frac{I_\infty}{I(z)}\right) = \sigma^a \sec \chi \int_z^\infty n(z) dz = \sec \chi \tau$$

$$I(z) = I_\infty \exp(-\tau \sec \chi)$$

$$\text{Optical Depth: } \tau = \sigma^a \int_z^\infty n(z) dz$$

$$\text{Isothermal atmosphere: } n(z) = n_0 \exp\left(-\frac{(z - z_0)}{H}\right)$$

$$\ln\left(\frac{I_\infty}{I(z)}\right) = \sigma^a \sec \chi \int_z^\infty n_0 \exp\left(-\frac{(z - z_0)}{H}\right) dz$$

$$= \sigma^a \sec \chi H n_0 \exp\left(-\frac{(z - z_0)}{H}\right)$$

$$= \sigma^a \sec \chi H n(z)$$

$$I(z) = I_\infty \exp(-\sigma^a \sec \chi H n(z))$$

$$\tau(z) = \sigma^a H n(z)$$

Photoionisation: $P_c(z, \chi) = I(z, \chi) \beta \sigma^a n(z)$

β = probability of ionisation

$P_c(z, \chi) = I_\infty \exp(-\tau(z) \sec \chi) \beta \sigma^a n(z)$

Maximum ionisation: $\frac{dP_c}{dz} = 0$

$\frac{dP_c}{dz} = I_\infty \beta \sigma^a [\exp(-\tau(z) \sec \chi) n'(z) - n(z) \exp(-\tau(z) \sec \chi) \sec \chi \tau'(z)] = 0$

$\Rightarrow n'(z) - n(z) \sec \chi \tau'(z) = 0$

$[n'(z) - n(z) \sec \chi \tau'(z)] = 0$

$\tau(z) = \sigma^a H n(z) \Rightarrow \tau'(z) = \sigma^a H n'(z)$ (assuming H constant)

$\frac{\tau'(z)}{\sigma^a H} - n(z) \sec \chi \tau'(z) = 0$

$\tau'(z) - \sigma^a H n(z) \sec \chi \tau'(z) = 0$

$\tau'(z) (1 - \sigma^a H n(z) \sec \chi) = 0$

$\tau'(z) (1 - \tau(z) \sec \chi) = 0$

$\tau(z) \sec \chi = 1$

For $\sec \chi = 1$: overhead sun $\tau(z) = 1$ for maximum ionisation

2. Having shown that $\tau=1$, substitute the atmospheric density variation according to the above formula and derive a value for the appropriate cross-section for maximum absorption as a function of altitude (cover the range from 50- 120 km)

Assuming all the energy absorbed goes into ionisation: $\tau(z) \sec \chi = 1$

$\sigma^a H n(z) \sec \chi = 1$

$n_0 \exp\left(\frac{-(z-z_0)}{H}\right) = \frac{1}{\sigma^a H \sec \chi}$

$-\frac{(z-z_0)}{H} = \ln\left(\frac{1}{H n_0 \sigma^a \sec \chi}\right)$

$z = z_0 + H \ln(H n_0 \sigma^a \sec \chi)$

Also:

$n_0 \exp\left(\frac{-(z-z_0)}{H}\right) = \frac{1}{\sigma^a H \sec \chi}$

$\sigma^a = \frac{1}{H \sec \chi n_0 \exp\left(\frac{-(z-z_0)}{H}\right)}$

$\sigma^a = \frac{1}{H n_0 \sec \chi} \exp\left(\frac{z-z_0}{H}\right)$

3. Assume pure N₂ absorption (for mars you would use CO₂), use the Henke curves, convert the cross-sections profile to energy, and hence wavelength of incident photon and present again as a function of altitude. This should give a profile of photon wavelength vs altitude where maximum absorption occurs. Then answer- what altitude corresponds to maximum absorption of the Fe XV line at 1.9 A?

Here I used this formula obtained from the previous part:

$$z = z_0 + H \ln \left(H n_0 \sigma^a \sec \chi \right)$$

Fe XV line at 1.9 A, the altitude comes out to be 65 km. From Henke, I got the cross-section to be 8.46E-22 cm²

4. Then you can answer the following: what sampling for the cross-section corresponds to a grid vertical resolution of:

- 10 km
- 1 per 7 km scale height
- 2 per 7 km scale height

Let the vertical resolution be ΔV

$$z_2 - z_1 = H \left(\ln \left(H n_0 \sigma_2^a(\lambda_2) \sec \chi \right) - \ln \left(H n_0 \sigma_1^a(\lambda_1) \sec \chi \right) \right)$$

$$z_2 - z_1 = H \ln \left(\frac{\sigma_2^a(\lambda_2)}{\sigma_1^a(\lambda_1)} \right)$$

$$\left| \frac{\sigma_2^a(\lambda_2)}{\sigma_1^a(\lambda_1)} \right| = \exp \left(\frac{z_2 - z_1}{H} \right)$$

$$\left| \frac{\sigma_2^a(\lambda_2)}{\sigma_1^a(\lambda_1)} \right| = \exp \left(\frac{\Delta V}{H} \right)$$

$$\left| \frac{\sigma_2^a(\lambda_2)}{\sigma_1^a(\lambda_1)} \right| = \exp \left(\frac{\Delta V}{H} \right)$$

Assuming scale height $H = 7 \text{ km}$

a. $\Delta V = 10 \text{ km}$

$$\left| \frac{\sigma_2^a(\lambda_2)}{\sigma_1^a(\lambda_1)} \right| = \exp \left(\frac{10}{7} \right) = 4.17$$

b. 1 cross-section per 7 km scale height: $\Delta V = 7 \text{ km}$

$$\left| \frac{\sigma_2^a(\lambda_2)}{\sigma_1^a(\lambda_1)} \right| = \exp \left(\frac{7}{7} \right) = e^1 = 2.7$$

c. 2 cross-sections per 7 km scale height: $\Delta V = 3.5 \text{ km}$

$$\left| \frac{\sigma_2^a(\lambda_2)}{\sigma_1^a(\lambda_1)} \right| = \exp \left(\frac{3.5}{7} \right) = e^{0.5} = 1.6$$

Here I have added all the sampling of the cross-sections data for the O₂ and N₂ for a vertical resolution of 5km, calculated using the above derived relationship.

O2 data for Vertical
resolution of 5km

calculated cross-section (cm ²)	H+F cross-section	H+F wavelength (Å)	H+F energy (eV)	Altitude(Tau=1) (km)
8.50E-24	8.5024E-024	0.4	30992.5	31
1.74E-23	1.44541E-023	0.5	24794	36
3.55E-23	2.56666E-023	0.6	20661.7	41
7.25E-23	7.91786E-023	0.8	15496.2	46
1.48E-22	7.91786E-023	0.8	15496.2	51
3.02E-22	3.04492E-022	1.3	9536.15	56
6.18E-22	5.8454E-022	1.5	8264.67	61
1.26E-21	1.53575E-021	2.1	5903.33	66
2.58E-21	2.62512E-021	2.5	4958.8	71
5.26E-21	6.3768E-021	3.4	3646.18	76
1.08E-20	1.19034E-020	4.2	2951.67	81
2.20E-20	2.52946E-020	5.4	2295.74	86
4.49E-20	3.51255E-020	6.1	2032.3	91
9.17E-20	8.5024E-020	8.3	1493.61	96
1.87E-19	1.9E-019	33.74	367.43	101
3.82E-19	3.84E-019	47.7	259.9	106

N2 data for Vertical
resolution of 5km

calculated cross- section (cm ²)	H+F cross-section	H+F wavelength (Å)	H+F energy (eV)	Altitude(Tau=1) (km)
4.54E-24	4.5357E-24	0.4	30992.5	31
9.26E-24	7.76884E-24	0.5	24794	36
1.89E-23	1.3863E-23	0.6	20661.7	41
3.86E-23	1.3863E-23	0.8	15496.2	46
7.90E-23	4.32171E-23	0.8	15496.2	51
1.61E-22	1.65611E-22	1.3	9536.15	56
3.29E-22	3.18662E-22	1.5	8264.67	61
6.73E-22	5.1172E-22	1.8	6887.22	66
1.37E-21	1.45608E-21	2.5	4958.8	71
2.81E-21	3.57739E-21	3.4	3646.18	76
5.74E-21	6.79192E-21	4.2	2951.67	81
1.17E-20	9.95528E-21	4.7	2637.66	86
2.39E-20	2.07479E-20	6.1	2032.3	91
4.89E-20	2.07479E-20	8.3	1493.61	96
9.99E-20	9.62964E-20	10.4	1192.02	101
2.04E-19	2.09E-19	47.7	259.9	106