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LPile for Version 2022-12.012

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Analysis of Individual Piles and Drilled Shafts
Subjected to Lateral Loading Using the p-y Method
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Austin, TX, USA

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This model was prepared by: SruthiRamya

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Files Used for Analysis

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Path to file locations:

 $\label{lem:condition} $$ \Users\SruthiRamya\ANS Geo\ANS Geo\Projects - Documents\3 - PROJECTS\Urban Grid\Porter Mills (MD)\6 - Reporting\Calcs\1. Inverter Foundation Design\2. LPile\Evenly spaced\$ 

Name of input data file:

Inverter\_Evenly\_Strong Axis\_PM.lp12d

Name of output report file:

Inverter\_Evenly\_Strong Axis\_PM.lp12o

Name of plot output file:

Inverter Evenly Strong Axis PM.lp12p

Name of runtime message file:

Inverter Evenly Strong Axis PM.lp12r

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Date and Time of Analysis	
Date: August 11, 2025 Time	: 9:08:07
Problem Title	
Project: Porter Mill Solar Project	
Client: Urban Grid Engineer: SR Description: Inverter SG4400UD-MV-US Evenly spaced pil	es - Strong Axis
Program Options and Settings	
Computational Options: - Conventional Analysis Engineering Units Used for Data Input and Computations - US Customary System Units (pounds, feet, inches)	:
Analysis Control Options:  - Maximum number of iterations allowed  - Deflection tolerance for convergence  - Maximum allowable deflection  - Number of pile increments	= 500 = 1.0000E-05 in = 100.0000 in = 100

Loading Type and Number of Cycles of Loading:

- Static loading specified
- Use of p-y modification factors for p-y curves not selected
- Analysis uses layering correction (Method of Georgiadis)
- No distributed lateral loads are entered
- Loading by lateral soil movements acting on pile not selected
- Input of shear resistance at the pile tip not selected
- Input of moment resistance at the pile tip not selected
- Computation of pile-head foundation stiffness matrix not selected
- Push-over analysis of pile not selected
- Buckling analysis of pile not selected

## Output Options:

- Output files use decimal points to denote decimal symbols.

- Values of pile-head deflection, bending moment, shear force, and soil reaction are printed for full length of pile.
- Printing Increment (nodal spacing of output points) = 1
- No p-y curves to be computed and reported for user-specified depths
- Print using wide report formats

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Pile Structural Properties and Geometry

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Number of pile sections defined = 1 Total length of pile = 30.250 ft Depth of ground surface below top of pile = 2.7500 ft

Pile diameters used for p-y curve computations are defined using 2 points.

p-y curves are computed using pile diameter values interpolated with depth over

the length of the pile. A summary of values of pile diameter vs. depth follows.

Point	Depth Below Pile Head feet	Pile Diameter inches
1	0.000	5.9287
2	30.250	5.9287

Input Structural Properties for Pile Sections:

Pile Section No. 1:

Section 1 is a H strong axis steel pile Length of section Pile width

= 30.250000 ft

= 5.928700 in

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Soil and Rock Layering Information

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The soil profile is modelled using 4 layers

Layer 1 is sand, p-y criteria by Reese et al., 1974

Distance from top of pile to top of layer Distance from top of pile to bottom of layer Effective unit weight at top of layer Effective unit weight at bottom of layer Friction angle at top of layer deg.	= = = =	2.750000 ft 4.250000 ft 115.000000 pcf 115.000000 pcf 38.000000
Friction angle at bottom of layer	=	38.000000
deg. Subgrade k at top of layer Subgrade k at bottom of layer	=	
Layer 2 is sand, p-y criteria by Reese et al., 1974		
Distance from top of pile to top of layer Distance from top of pile to bottom of layer Effective unit weight at top of layer Effective unit weight at bottom of layer Friction angle at top of layer	= = =	4.250000 ft 6.250000 ft 115.000000 pcf 115.000000 pcf 38.000000
deg. Friction angle at bottom of layer	=	38.000000
deg. Subgrade k at top of layer Subgrade k at bottom of layer	=	210.000000 pci 210.000000 pci
Layer 3 is stiff clay with user-defined k-value		
Distance from top of pile to top of layer Distance from top of pile to bottom of layer Effective unit weight at top of layer Effective unit weight at bottom of layer Undrained cohesion at top of layer Undrained cohesion at bottom of layer Epsilon-50 at top of layer Epsilon-50 at bottom of layer Subgrade k at top of layer Subgrade k at bottom of layer	= = = = = =	6.250000 ft 10.250000 ft 110.000000 pcf 110.000000 pcf 2250. psf 2250. psf 0.006000 0.006000 750.000000 pci 750.000000 pci
Layer 4 is sand, p-y criteria by Reese et al., 1974		
Distance from top of pile to top of layer Distance from top of pile to bottom of layer Effective unit weight at top of layer Effective unit weight at bottom of layer Friction angle at top of layer deg.	= = = =	10.250000 ft 30.250000 ft 50.000000 pcf 50.000000 pcf 37.000000
Friction angle at bottom of layer deg.	=	37.000000
Subgrade k at top of layer Subgrade k at bottom of layer	=	110.000000 pci 110.000000 pci

(Depth of the lowest soil layer extends 0.000 ft below the pile tip)

	Summa	ry of Input S	Soil Properties	5
	Soil Type E50	Layer	Effective	Cohesion
Num.	Name or	Depth kpy	Unit Wt.	
	(p-y Curve Type) krm pci	ft	pcf	psf
1	  Sand	2.7500	115.0000	
38.0000	(Reese, et al.)	4.2500	115.0000	
38.0000 2 38.0000	210. Sand 210.	4.2500	115.0000	
38.0000	(Reese, et al.) 210.	6.2500	115.0000	
3	Stiff Clay w/o 0.00600 750.0	6.2500		2250.
	Free Water, using k 0.00600 750.0	000		2250.
4 37.0000		10.2500	50.0000	
37.0000	(Reese, et al.) 110.	30.2500	50.0000	
		Static Load	ding Type	
Static loanalyses.	oading criteria were	used when cor	mputing p-y cu	rves for all
		<b></b>		

Pile-head Loading and Pile-head Fixity Conditions

## Number of loads specified = 1

Load	Load	Cond	dition			Condition		Axial
Thrust	Com	pute Top y	, R	un Ana	alysis			
No.	Type		1			2		Force,
lbs	vs. Pi	le Length						
1	1	V =	1103.	lbs	M =	0.0000	in-lbs	
10857.		Yes		Yes	3			

- V = shear force applied normal to pile axis
- ${\tt M}$  = bending moment applied to pile head
- y = lateral deflection normal to pile axis
- S = pile slope relative to original pile batter angle
- R = rotational stiffness applied to pile head

Values of top y vs. pile lengths can be computed only for load types with specified shear loading (Load Types 1, 2, and 3).

Thrust force is assumed to be acting axially for all pile batter angles.

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Computations of Nominal Moment Capacity and Nonlinear Bending Stiffness

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Axial thrust force values were determined from pile-head loading conditions

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

Dimensions and Properties of Steel H Strong Axis:

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Length of Section	=	30.250000 ft
Flange Width	=	5.928700 in
Section Depth	=	5.928700 in
Flange Thickness	=	0.198700 in
Web Thickness	=	0.168700 in
Yield Stress of Pipe	=	50.000000 ksi
Elastic Modulus	=	29000. ksi
Cross-sectional Area	=	3.289196 sq.
in.		
Moment of Inertia	=	21.725982
in^4		
Elastic Bending Stiffness	=	630053.
kip-in^2		

Plastic Modulus, Z =  $8.040483in^3$ Plastic Moment Capacity = Fy Z = 402.024162in-kip

Axial Structural Capacities:

Nom. Axial Structural Capacity = Fy As = 164.460 kips

Nominal Axial Tensile Capacity = -164.460 kips

Number of Axial Thrust Force Values Determined from Pile-head Loadings = 1

Number	Axial Thrust Force
	kips
1	10.857

Definition of Run Messages:

Y = part of pipe section has yielded.

Axial Thrust Force = 10.857 kips

Bending	Bending	Bending	Depth to	Max Total Run
Curvature	Moment	Stiffness	N Axis	Stress Msg
rad/in.	in-kip	kip-in2	in	ksi
0.00001188 0.00002376 0.00003564 0.00004752 0.00005940 0.00007128 0.00008316 0.00009504 0.0001069 0.0001188 0.0001307 0.0001426 0.0001544 0.0001663 0.0001782	in-kip  7.4756496  14.9512992  22.4269488  29.9025985  37.3782481  44.8538977  52.3295473  59.8051969  67.2808465  74.7564961  82.2321458  89.7077954  97.1834450  104.6590946  112.1347442	629287. 629287. 629287. 629287. 629287. 629287. 629287. 629287. 629287. 629287. 629287. 629287. 629287. 629287. 629287.	in	ksi 4.3118345 5.3228621 6.3338896 7.3449171 8.3559447 9.3669722 10.3779998 11.3890273 12.4000549 13.4110824 14.4221100 15.4331375 16.4441651 17.4551926 18.4662202
0.0001901	119.6103938	629287.	3.5631776	19.4772477
0.0002020	127.0860434	629287.	3.5279525	20.4882753
0.0002138	134.5616931	629287.	3.4966412	21.4993028
0.0002136 0.0002257 0.0002376	142.0373427 149.5129923	629287. 629287.	3.4686259 3.4434121	22.5103304 23.5213579

0.0002495 0.0002614 0.0002732 0.0002851 0.0002970 0.0003089 0.0003207 0.0003326 0.0003445 0.0003564 0.0003564 0.0003920 0.0004039 0.0004158 0.0004277 0.0004395 0.0004514 0.0004633 0.0004871 0.0005108 0.00045346 0.0005583 0.0005583 0.0005583 0.0005583 0.0005583 0.0005583 0.0005583 0.00057247 0.0006059 0.0006059 0.0006771 0.0007009 0.0007247 0.0007484 0.0007722 0.0007959 0.0008197 0.0008434 0.0007722 0.0007959 0.0008434 0.0007722 0.0007959 0.0008434 0.0007722 0.0007959 0.0008434 0.00099147 0.0009385 0.0009860 0.0010098 0.0010098 0.0011048 0.0011286 0.0011523 0.0011761 0.0011761	156.9886419 164.4642915 171.9399411 179.4155907 186.8912404 194.3668900 201.8425396 209.3181892 216.7938388 224.2694884 231.7451381 239.2207877 246.6964373 254.1720869 261.6477365 269.1233861 276.5990357 284.0746854 291.5503350 306.5016342 321.4529334 336.4042327 350.4095049 357.6503893 361.9302521 365.8690807 369.5049876 372.8634754 375.9770438 378.8179366 381.2208805 383.2322910 384.8363797 385.8589316 386.5498869 387.1848634 387.7702561 388.3076451 388.3076451 388.3076451 388.3076451 388.3076451 388.3076451 388.3076451 388.3076451 388.3076451 388.3076451 388.3076451 389.2701030 389.7015148 390.0993629 390.4713474 390.8216011 391.1438017 391.4509541 391.7346740 392.0026461 392.2548645	629287. 629287	3.4205996 3.3998610 3.3809258 3.3635684 3.3475997 3.3328593 3.3192108 3.3065372 3.2947377 3.2837247 3.2734223 3.2637638 3.2546907 3.2461512 3.2380998 3.2304956 3.2233025 3.2164880 3.2100229 3.1980388 3.1871696 3.1772665 3.1742590 3.2139161 3.2686848 3.3214552 3.3722859 3.4212912 3.4685141 3.5127548 3.5495905 3.5791405 3.6079459 3.6079056	24.5323855 25.5434130 26.5544406 27.5654681 28.5764957 29.5875232 30.5985508 31.6095783 32.6206059 33.6316334 34.6426610 35.6536885 36.6647161 37.6757436 38.6867712 39.6977987 40.7088262 41.7198538 42.7308813 44.7529364 46.7749915 48.7970466 50.0000000	Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y Y
0.0011286	391.7346740	347111.	3.6079949	50.0000000	Y
0.0011523	392.0026461	340186.	3.6078370	50.0000000	Y
0.0011761	392.2548645	333528.	3.6080630	50.0000000	Y
0.0011998	392.4913591	327121.	3.6110625	50.0000000	Y
0.0012236	392.7144982	320951.	3.6080018	50.0000000	Y
0.0012474	392.9265400	315008.	3.6122574	50.0000000	Y
0.0012711	393.1229252	309275.	3.6079638	50.0000000	Y
0.0012949	393.3137632	303747.	3.6078096	50.0000000	Y

0.0013186	393.4887201	298407.	3.6078973	50.0000000	Y
0.0013424	393.6605798	293253.	3.6080497	50.0000000	Y
0.0013661	393.8196827	288270.	3.6078011	50.0000000	Y
0.0013899	393.9691486	283450.	3.6079499	50.0000000	Y
0.0014137	394.1164826	278790.	3.6079919	50.0000000	Y
0.0015087	394.6258051	261566.	3.6077939	50.0000000	Y
0.0016037	395.0463670	246328.	3.6102708	50.0000000	Y
0.0016988	395.3996867	232756.	3.6101393	50.0000000	Y
0.0017938	395.6993774	220591.	3.6078047	50.0000000	Y
0.0018888	395.9562035	209628.	3.6077346	50.0000000	Y
0.0019839	396.1752635	199697.	3.6081139	50.0000000	Y
0.0020789	396.3615918	190657.	3.6079255	50.0000000	Y
0.0021740	396.5305018	182400.	3.6077267	50.0000000	Y
0.0022690	396.6729574	174823.	3.6080395	50.0000000	Y
0.0023640	396.8027015	167850.	3.6158962	50.0000000	Y

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Summary of Results for Nominal Moment Capacity for Section 1

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		Nominal
Load	Axial	Moment
No.	Thrust kips	Capacity in-kips
1	10.857000000	396.8027014870

Note that the values in the above table are not factored by a strength reduction factor for LRFD.

The value of the strength reduction factor depends on the provisions of the  $\,$ 

LRFD code being followed.

The above values should be multiplied by the appropriate strength reduction  $\ \ \,$ 

factor to compute ultimate moment capacity according to the LRFD structural  $\ensuremath{\mathsf{LRFD}}$ 

design standard being followed.

Layering Correction Equivalent Depths of Soil & Rock Layers

Layer	Layer Below	Top Depth Below	Same Layer Type As	Layer is Rock or	F0 Integral	F1
Integra		DOTON	1700 110	rtoon or	incograi	
No.	Pile Head	Grnd Surf	Layer	is Below	for Layer	for
Layer						
7	ft	ft	Above	Rock Layer	lbs	
lbs				1		
1	2.7500	0.00	N.A.	No	0.00	
1062.						
2	4.2500	1.4999	Yes	No	1062.	
6188.						
3	6.2500	1.6762	No	No	7250.	
30704.						
4	10.2500	6.5987	No	No	37954.	
N.A.						

Notes: The F0 integral of Layer n+1 equals the sum of the F0 and F1 integrals for Layer n. Layering correction equivalent depths are computed only for soil types with both shallow-depth and deep-depth expressions for peak lateral load transfer. These soil types are soft and stiff clays, non-liquefied sands, and cemented c-phi soil.

Computed Values of Pile Loading and Deflection for Lateral Loading for Load Case Number 1

Pile-head conditions are Shear and Moment (Loading Type 1)

1103.0 lbs Shear force at pile head Applied moment at pile head 0.0 inlbs

Axial thrust load on pile head 10857.0 lbs

Depth Deflect. Bending Shear Slope Total Bending Soil Res. Soil Spr. Distrib. S Stress X У Moment Force p Es\*H Lat. Load inches in-lbs lbs radians psi\* Stiffness feet lbin^2 lb/inch lb/inch lb/inch 

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0.00	0.2936		1103.	-0.00545	3301.
6.29E+08 0.3025	0.00 0.2738	0.00 4219.	0.00 1103.	-0.00544	3876.
6.29E+08	0.2738	0.00	0.00	-0.00344	30/0.
0.6050	0.2541	8436.	1103.	-0.00540	4452.
6.29E+08	0.00	0.00	0.00	0.00010	1102.
0.9075	0.2346	12652.	1103.	-0.00534	5027.
6.29E+08	0.00	0.00	0.00		
1.2100	0.2154	16865.	1103.	-0.00526	5602.
6.29E+08	0.00	0.00	0.00		
1.5125	0.1965	21074.	1103.	-0.00515	6176.
6.29E+08	0.00	0.00	0.00	0.00501	6850
1.8150	0.1780	25278.	1103.	-0.00501	6750.
6.29E+08	0.00	0.00	0.00	0 00405	7222
2.1175 6.29E+08	0.1601	29477. 0.00	1103. 0.00	-0.00485	7323.
2.4200	0.1428	33669.	1103.	-0.00467	7895.
6.29E+08	0.00	0.00	0.00	0.00407	7033.
2.7225	0.1262	37853.	1103.	-0.00447	8466.
6.29E+08	0.00	0.00	0.00	0.00117	0100.
3.0250	0.1103	42029.	1076.	-0.00424	9035.
6.29E+08	-14.798		0.00		
3.3275	0.09540	46000.	988.8781	-0.00398	9577.
6.29E+08	-33.281	1266.	0.00		
3.6300	0.08143	49522.	839.9575	-0.00371	10058.
6.29E+08	-48.769	2174.	0.00		
3.9325	0.06850	52390.	644.5641	-0.00341	10449.
6.29E+08	-58.886	3121.	0.00		
4.2350	0.05666	54470.	424.3893	-0.00310	10733.
6.29E+08	-62.423	3999.	0.00	0 00070	10000
4.5375 6.29E+08	0.04597 -62.864	55716. 4964.	196.9943	-0.00279	10903.
4.8400	0.03644	56120.	-25.371	-0.00246	10958.
6.29E+08		5943.	0.00	0.00240	10930.
5.1425	0.02808	55726.	-244.434	-0.00214	10904.
6.29E+08	-61.044	7891.	0.00	0.00211	10301.
5.4450	0.02089	54514.	-468.132	-0.00182	10739.
6.29E+08	-62.206	10807.	0.00		
5.7475	0.01485	52471.	-692.702	-0.00151	10460.
6.29E+08	-61.524	15042.	0.00		
6.0500	0.00990	49604.	-908.752	-0.00122	10069.
6.29E+08	-57.511	21087.	0.00		
6.3525	0.00599	45969.	-1223.	-9.44E-04	9573.
6.29E+08	-115.425	69932.	0.00	C 04E 04	0.0.00
6.6550 6.29E+08		40803. 123811.	-1621. 0.00	-6.94E-04	8868.
6.9575	9.53E-04	34258.	-1875.	-4.77E-04	7975.
6.29E+08	-36.104	137459.	0.00	4.776 04	7373.
7.2600		27230.	-1909.	-3.00E-04	7016.
6.29E+08		147342.	0.00		
7.5625		20421.	-1782.	-1.63E-04	6087.
6.29E+08	53.0729	157224.	0.00		
7.8650		14306.	-1552.	-6.25E-05	5253.
6.29E+08	73.7500	167107.	0.00		

0 1675	-0.00168	9161.	-1269.	5 10m 06	4551.
6.29E+08	81.8719	176990.	0.00	J.10E-00	4551.
8.4700	-0.00156	5092.	-974.441	4.63E-05	3996.
6.29E+08	80.5389	186872.	0.00		
8.7725	-0.00134	2083.	-696.126	6.70E-05	3585.
6.29E+08	72.8027	196755.	0.00		
9.0750	-0.00108	32.4113		7.31E-05	3305.
6.29E+08	61.3790	206638.	0.00	6.97E-05	2466
9.3775 6.29E+08	-8.13E-04 48.4724	-1209. 216520.	-253.206 0.00	6.9/E-05	3466.
9.6800	-5.72E-04	-1811.	-100.435	6.10E-05	3548.
6.29E+08	35.6986	226403.	0.00	0.100 00	33 10 <b>.</b>
9.9825	-3.70E-04	-1943.	8.0722	5.01E-05	3566.
6.29E+08	24.0852	236286.	0.00		
10.2850	-2.08E-04	-1757.	55.5481	3.95E-05	3540.
6.29E+08	2.0723	36105.	0.00		
10.5875	-8.35E-05	-1543.	60.8764	3.00E-05	3511.
6.29E+08	0.8635	37554.	0.00	0 175 05	2.401
10.8900 6.29E+08	9.12E-06 -0.09794	-1317. 39004.	62.2659 0.00	2.17E-05	3481.
11.1925	7.41E-05	-1092.	60.5890	1.48E-05	3450.
6.29E+08	-0.826	40453.	0.00	1.401 03	3430.
11.4950	1.16E-04	-878.387	56.6545	9.07E-06	3421.
6.29E+08	-1.342	41903.	0.00		
11.7975	1.40E-04	-681.829	51.1851	4.57E-06	3394.
6.29E+08	-1.672	43352.	0.00		
12.1000	1.49E-04	-507.143	44.8038	1.14E-06	3370.
6.29E+08	-1.844	44801.	0.00	1 25- 26	2240
12.4025	1.48E-04 -1.889	-356.644	38.0278	-1.35E-06	3349.
6.29E+08 12.7050	1.40E-04	46251. -230.955	0.00 31.2689	-3.04E-06	3332.
6.29E+08	-1.835	47700.	0.00	3.046 00	3332.
13.0075	1.26E-04	-129.392	24.8382	-4.08E-06	3318.
6.29E+08	-1.708	49150.	0.00		
13.3100		-50.308	18.9551	-4.60E-06	3308.
6.29E+08	-1.533	50599.	0.00		
13.6125	9.28E-05	8.5856	13.7587	-4.72E-06	3302.
6.29E+08	-1.330	52049.	0.00	4 555 06	2200
13.9150 6.29E+08	7.57E-05 -1.116	49.9523 53498.	9.3198 0.00	-4.55E-06	3308.
14.2175	5.97E-05	76.6060	5.6546	-4.19E-06	3311.
6.29E+08	-0.904	54948.	0.00	1.130 00	3311 <b>.</b>
14.5200	4.53E-05	91.3350	2.7372	-3.70E-06	3313.
6.29E+08	-0.704	56397.	0.00		
14.8225	3.28E-05	96.7698	0.5109	-3.16E-06	3314.
6.29E+08	-0.523	57847.	0.00		
15.1250	2.23E-05	95.2933	-1.101	-2.61E-06	3314.
6.29E+08	-0.365	59296.	0.00	2 000 06	2212
15.4275 6.29E+08	1.39E-05 -0.232	88.9853 60746.	-2.185 0.00	-2.08E-06	3313.
15.7300	7.28E-06	79.5966	-2.832	-1.59E-06	3312.
6.29E+08		62195.	0.00		3312.
16.0325		68.5471	-3.133	-1.16E-06	3310.
6.29E+08	-0.04101	63644.	0.00		

16.3350	-1.16E-06	56.9418	-3.170	-8.00E-07	3309.
6.29E+08	0.02085	65094.	0.00		
16.6375	-3.47E-06	45.5982	-3.016	-5.05E-07	3307.
6.29E+08	0.06365	66543.	0.00	0 700 07	2206
16.9400 6.29E+08	-4.83E-06 0.09041	35.0830 67993.	-2.737 0.00	-2.72E-07	3306.
17.2425	-5.45E-06	25.7511	-2.384	-9.65E-08	3304.
6.29E+08	0.1042	69442.	0.00	-9.63E-06	3304.
17.5450	-5.53E-06	17.7862	-1.999	2.91E-08	3303.
6.29E+08	0.1079	70892.	0.00	2.716 00	3303.
17.8475	-5.24E-06	11.2396	-1.613	1.13E-07	3302.
6.29E+08	0.1043	72341.	0.00	1.102 0.	0002.
18.1500	-4.71E-06	6.0652	-1.250	1.63E-07	3302.
6.29E+08	0.09571	73791.	0.00		
18.4525	-4.05E-06	2.1506	-0.924	1.86E-07	3301.
6.29E+08	0.08403	75240.	0.00		
18.7550	-3.35E-06	-0.657	-0.643	1.91E-07	3301.
6.29E+08	0.07088	76690.	0.00		
19.0575	-2.67E-06	-2.531	-0.410	1.82E-07	3301.
6.29E+08	0.05746	78139.	0.00		
19.3600	-2.04E-06	-3.647	-0.225	1.64E-07	3301.
6.29E+08	0.04466	79588.	0.00		
19.6625	-1.48E-06	-4.174	-0.08346	1.41E-07	3301.
6.29E+08	0.03306	81038.	0.00	4 4 5 - 0 5	0001
19.9650	-1.01E-06	-4.264	0.01830	1.17E-07	3301.
6.29E+08	0.02300	82487.	0.00	0 200 00	2201
20.2675 6.29E+08	-6.33E-07 0.01464	-4.051	0.08661	9.28E-08	3301.
20.5700	-3.38E-07	83937. -3.643	0.1276	7.06E-08	3301.
6.29E+08	0.00796	85386.	0.1278	7.00E-00	3301.
20.8725	-1.20E-07	-3.130	0.1473	5.11E-08	3301.
6.29E+08	0.00287	86836.	0.00	J.111 00	3301.
21.1750	3.25E-08	-2.578	0.1511	3.46E-08	3301.
	-7.91E-04	88285.	0.00	0.102 00	0001.
	1.31E-07	-2.036	0.1437	2.13E-08	3301.
6.29E+08	-0.00325	89735.	0.00		
21.7800	1.87E-07	-1.536	0.1293	1.10E-08	3301.
6.29E+08	-0.00471	91184.	0.00		
22.0825	2.11E-07	-1.098	0.1110	3.43E-09	3301.
6.29E+08	-0.00539	92634.	0.00		
22.3850	2.12E-07	-0.730	0.09120	-1.84E-09	3301.
6.29E+08	-0.00550	94083.	0.00		
22.6875	1.98E-07	-0.435	0.07175	-5.20E-09	3301.
6.29E+08	-0.00521	95533.	0.00	T 06- 00	2221
22.9900	1.75E-07	-0.209	0.05383	-7.06E-09	3301.
6.29E+08	-0.00466	96982.	0.00	7 700 00	2201
23.2925 6.29E+08	1.47E-07 -0.00398	-0.04407 98431.	0.03814	-7.79E-09	3301.
23.5950	1.18E-07	0.06845	0.02502	-7.72E-09	3301.
6.29E+08	-0.00325	99881.	0.02302	7.726 09	3301.
23.8975	9.07E-08	0.1382	0.01453	-7.12E-09	3301.
6.29E+08		101330.	0.00	, • 121 09	5501.
24.2000		0.1745	0.00652	-6.22E-09	3301.
6.29E+08		102780.	0.00		•

24.5025 4.56E-08 6.29E+08 -0.00131	0.1860 104229.	7.38E-04 0.00	-5.18E-09	3301.
24.8050 2.87E-08 6.29E+08 -8.36E-04	0.1802 105679.	-0.00315 0.00	-4.12E-09	3301.
25.1075 1.56E-08 6.29E+08 -4.61E-04	0.1634	-0.00551 0.00	-3.13E-09	3301.
25.4100 5.96E-09 6.29E+08 -1.78E-04	0.1405 108578.	-0.00667 0.00	-2.26E-09	3301.
25.7125 -7.59E-10 6.29E+08 2.30E-05	0.1152 110027.	-0.00695 0.00	-1.52E-09	3301.
26.0150 -5.07E-09 6.29E+08 1.56E-04	0.09016 111477.	-0.00663 0.00	-9.27E-10	3301.
	0.06716	-0.00592 0.00	-4.73E-10	3301.
26.6200 -8.50E-09 6.29E+08 2.68E-04	0.04722 114375.	-0.00501 0.00	-1.43E-10	3301.
26.9225 -8.53E-09 6.29E+08 2.72E-04	0.03079 115825.	-0.00403	8.16E-11	3301.
	0.01794 117274.	-0.00307 0.00	2.22E-10	3301.
27.5275 -6.92E-09 6.29E+08 2.26E-04	0.00846 118724.	-0.00220	2.98E-10	3301.
27.8300 -5.74E-09	0.00195	-0.00144	3.28E-10	3301.
	120173. -0.00205		3.28E-10	3301.
6.29E+08 1.52E-04 28.4350 -3.36E-09			3.10E-10	3301.
	123072. -0.00454		2.86E-10	3301.
6.29E+08 7.82E-05 29.0400 -1.29E-09		0.00 2.32E-04	2.61E-10	3301.
6.29E+08 4.47E-05 29.3425 -3.84E-10 6.29E+08 1.35E-05	125971. -0.00288 127421.	0.00 3.38E-04 0.00	2.41E-10	3301.
	-0.00158 128870.		2.28E-10	3301.
29.9475 1.27E-09	-4.88E-04	2.20E-04	2.22E-10	3301.
6.29E+08 -4.57E-05 30.2500 2.07E-09 6.29E+08 -7.53E-05	130320. 0.00 65884.	0.00 0.00 0.00	2.21E-10	3301.
U.ZYE+UO -/.33E-U5	00004.	0.00		

<sup>\*</sup> This analysis computed pile response using nonlinear moment-curvature rela-

tionships. Values of total stress due to combined axial and bending stresses

are computed only for elastic sections only and do not equal the actual stresses in concrete and steel. Stresses in concrete and steel may be inter-

polated from the output for nonlinear bending properties relative to the  $% \left( \frac{1}{2}\right) =\frac{1}{2}\left( \frac{1}{2}\right) +\frac{1}{2}\left( \frac{1}{2}\right) +\frac{$ 

magnitude of bending moment developed in the pile.

Pile-head deflection = 0.29360386 inches
Computed slope at pile head = -0.0054498 radians
Maximum bending moment = 56120. inch-lbs
Maximum shear force = -1909. lbs
Depth of maximum bending moment = 4.84000000 feet below pile head
Depth of maximum shear force = 7.26000000 feet below pile head
Number of iterations = 12
Number of zero deflection points = 6
Pile deflection at ground = 0.12471389 inches

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Pile-head Deflection vs. Pile Length for Load Case 1

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Boundary Condition Type 1, Shear and Moment

Shear = 1103. lbs
Moment = 0. in-lbs
Axial Load = 10857. lbs

Pile	Pile Head	Maximum	Maximum
Length	Deflection	Moment	Shear
feet	inches	ln-lbs	lbs
30.25000	0.29360386	56120.	-1909.
28.73750	0.29277576	56027.	-1915.
27.22500	0.29252849	56090.	-1921.
25.71250	0.29397748	55989.	-1900.
24.20000	0.29253494	56014.	-1907.
22.68750	0.29375383	56012.	-1902.
21.17500	0.29399141	56065.	-1911.
19.66250	0.29329419	56050.	-1920.
18.15000	0.29388434	56004.	-1906.
16.63750	0.29336045	56001.	-1916.
15.12500	0.29392894	56007.	-1905.
13.61250	0.29288431	56005.	-1925.
12.10000	0.29345686	56007.	-1919.
10.58750	0.29432018	55993.	-1896.
9.07500	0.29512709	55959.	-2015.
7.56250	0.61757637	55119.	-2753.
6.05000	-8.7799962	-19618.	3539.
4.53750	-3.8936393	4270.	1275.

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Summary of Pile-head Responses for Conventional Analyses

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Definitions of Pile-head Loading Conditions:

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Load Type 1: Load 1 = Shear, V, lbs, and Load 2 = Moment, M, in-lbs
Load Type 2: Load 1 = Shear, V, lbs, and Load 2 = Slope, S, radians
Load Type 3: Load 1 = Shear, V, lbs, and Load 2 = Rot. Stiffness, R, in-lbs/rad.
Load Type 4: Load 1 = Top Deflection, y, inches, and Load 2 = Moment, M, in-lbs
Load Type 5: Load 1 = Top Deflection, y, inches, and Load 2 = Slope, S, radians
```

Load Load		Load		Axial	Pile-head	Pile-
head Max S		oment				
2 L	Pile-head	Type	Pile-head	Loading	Deflection	
Rotation						
No. 1	Load 1	2	Load 2	lbs	inches	
radians	lbs	in-lbs				
· · · · · · · · · · · · · · · · · · ·	1103. -1909.	M, in-lb 56120.	0.00	10857.	0.2936	_

Maximum pile-head deflection = 0.2936038550 inches

Maximum pile-head rotation = -0.0054497529 radians = -0.312248 deg.

The analysis ended normally.