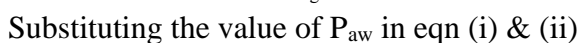
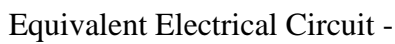


Determine the transfer function of the respiratory system shown in Fig. 3



$$Q_{pat} = \frac{\frac{1}{R_{lung}} P_{lung} + \frac{1}{R_{hose}} P_{out}}{R_{lung} \left(\frac{1}{R_{lung}} + \frac{1}{R_{hose}} + \frac{1}{R_{leak}} \right)} - \frac{1}{R_{lung}} P_{lung}$$

$$= \frac{\frac{1}{R_{lung}} - \left(\frac{1}{R_{lung}} + \frac{1}{R_{hose}} + \frac{1}{R_{leak}} \right)}{R_{lung} \left(\frac{1}{R_{lung}} + \frac{1}{R_{hose}} + \frac{1}{R_{leak}} \right)} P_{lung} + \frac{\frac{1}{R_{hose}}}{R_{lung} \left(\frac{1}{R_{lung}} + \frac{1}{R_{hose}} + \frac{1}{R_{leak}} \right)} P_{aw}$$

$$Q_{pat} = \left(- \frac{\frac{1}{R_{hose}} + \frac{1}{R_{leak}}}{R_{lung} \left(\frac{1}{R_{lung}} + \frac{1}{R_{hose}} + \frac{1}{R_{leak}} \right)} \right) P_{lung} + \left(\frac{\frac{1}{R_{hose}}}{R_{lung} \left(\frac{1}{R_{lung}} + \frac{1}{R_{hose}} + \frac{1}{R_{leak}} \right)} \right) P_{out} \dots\dots\dots(v)$$

$$P_{lung} = \frac{\frac{1}{R_{lung}} P_{lung} + \frac{1}{R_{hose}} P_{out}}{C_{lung} R_{lung} \left(\frac{1}{R_{lung}} + \frac{1}{R_{hose}} + \frac{1}{R_{leak}} \right)} - \frac{P_{lung}}{C_{lung} R_{lung}}$$

$$= \frac{\frac{1}{R_{lung}} - \left(\frac{1}{R_{lung}} + \frac{1}{R_{hose}} + \frac{1}{R_{leak}} \right)}{C_{lung} R_{lung} \left(\frac{1}{R_{lung}} + \frac{1}{R_{hose}} + \frac{1}{R_{leak}} \right)} P_{lung} + \frac{\frac{1}{R_{hose}}}{C_{lung} R_{lung} \left(\frac{1}{R_{lung}} + \frac{1}{R_{hose}} + \frac{1}{R_{leak}} \right)} P_{out}$$

$$P_{lung} = \left(- \frac{\frac{1}{R_{hose}} + \frac{1}{R_{leak}}}{C_{lung} R_{lung} \left(\frac{1}{R_{lung}} + \frac{1}{R_{hose}} + \frac{1}{R_{leak}} \right)} \right) P_{lung} + \left(\frac{\frac{1}{R_{hose}}}{C_{lung} R_{lung} \left(\frac{1}{R_{lung}} + \frac{1}{R_{hose}} + \frac{1}{R_{leak}} \right)} \right) P_{out} \dots\dots\dots(vi)$$

Here, input $\Rightarrow P_{out}$, output $\Rightarrow \begin{bmatrix} P_{aw} \\ Q_{pat} \end{bmatrix}$, state $\Rightarrow P_{lung}$

From eqn (iv) to (vi) we find:

$$P_{lung} = A_h P_{lung} + B_h P_{out} \dots\dots\dots(vii)$$

$$\begin{bmatrix} P_{aw} \\ Q_{pat} \end{bmatrix} = C_h P_{lung} + D_h P_{out} \dots\dots\dots(viii)$$

Where,

$$A_h = - \frac{\frac{1}{R_{hose}} + \frac{1}{R_{leak}}}{C_{lung} R_{lung} \left(\frac{1}{R_{lung}} + \frac{1}{R_{hose}} + \frac{1}{R_{leak}} \right)}$$

$$B_h = \frac{\frac{1}{R_{hose}}}{C_{lung} R_{lung} \left(\frac{1}{R_{lung}} + \frac{1}{R_{hose}} + \frac{1}{R_{leak}} \right)}$$

$$C_h = \left[\begin{array}{c} \frac{\frac{1}{R_{leak}}}{\frac{1}{R_{lung}} + \frac{1}{R_{hose}} + \frac{1}{R_{leak}}} \\ - \frac{\frac{1}{R_{hose}} + \frac{1}{R_{leak}}}{R_{lung} \left(\frac{1}{R_{lung}} + \frac{1}{R_{hose}} + \frac{1}{R_{leak}} \right)} \end{array} \right]$$

$$D_h = \left[\begin{array}{c} \frac{\frac{1}{R_{hose}}}{\frac{1}{R_{hose}} + \frac{1}{R_{leak}} + \frac{1}{R_{lung}}} \\ - \frac{\frac{1}{R_{hose}}}{R_{lung} \left(\frac{1}{R_{lung}} + \frac{1}{R_{hose}} + \frac{1}{R_{leak}} \right)} \end{array} \right]$$

We know that,

$$Y(s) = [C_n (sI - A_h)^{-1} B_h + D_h] u(s)$$

where $Y(s)$ is the output matrix and $u(s)$ is the input matrix

$$\text{so, } \frac{Y(s)}{u(s)} = H(s) = C_h (sI - A_h)^{-1} B_h + D_h$$

Using the values of parameters given in table 1 of the reference paper, H(s) was calculated using the code given below.

Rlung	5/1000
Clung	20
Rleak	60/1000
Rhose	4.5/1000
ω_n	$2\pi 30$

Code:

```
clc;
```

```
clearvars;
```

```
Rlung = 5/1000;
```

```
Clung = 20;
```

```
Rleak = 60/1000;
```

```
Rhose = 4.5/1000;
```

```
Ah = -((1/Rhose)+(1/Rleak))/(Rlung*Clung*((1/Rlung)+(1/Rhose)+(1/Rleak)))
```

```
Bh = (1/Rhose)/(Rlung*Clung*((1/Rlung)+(1/Rhose)+(1/Rleak)))
```

```
Ch = [(1/Rlung)/((1/Rlung)+(1/Rhose)+(1/Rleak));...
```

```
      -((1/Rhose)+(1/Rleak))/(Rlung*((1/Rlung)+(1/Rhose)+(1/Rleak)))]
```

```
Dh = [(1/Rhose)/((1/Rlung)+(1/Rhose)+(1/Rleak));...
```

```
      (1/Rhose)/(Rlung*((1/Rlung)+(1/Rhose)+(1/Rleak)))]
```

```
s = tf('s');
```

```
Hs = Ch*inv((s*eye(1) - Ah))*Bh + Dh
```

So, the calculated H(s) is:

$$H(s) = \begin{bmatrix} \frac{0.5063s + 5.063}{s + 5.443} \\ \frac{101.3s + 1.137e-13}{s + 5.443} \end{bmatrix}$$

Task 2:

Determine the overall transfer function of the closed loop control system shown in Fig. 4.

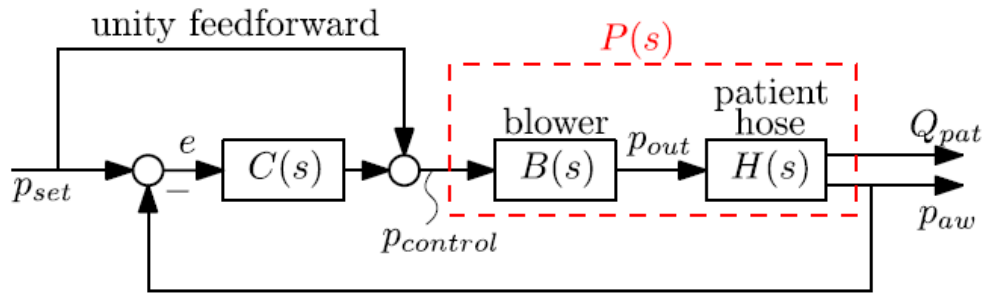
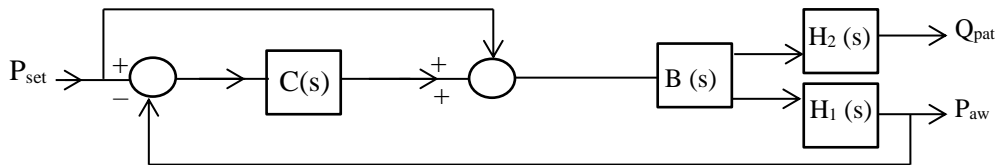


Fig. 4. Closed-loop control scheme with a linear controller $C(s)$.

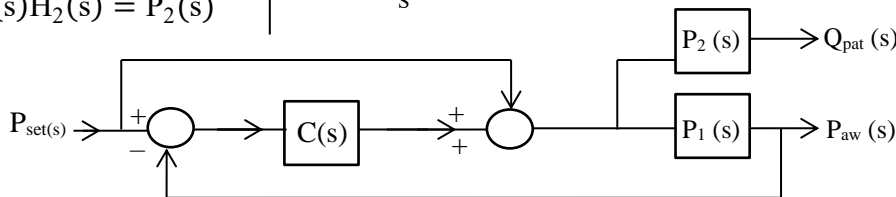
Changing the diagram to:



Let

$$\begin{aligned} B(s)H_1(s) &= P_1(s) \\ B(s)H_2(s) &= P_2(s) \end{aligned} \quad \left| \quad C(s) = \frac{K_i}{s} \right.$$

So,



Now,

$$\begin{aligned} P_{aw}(s) &= P_1(s)[P_{set}(s) + C(s)(P_{set}(s) - P_{aw}(s))] \\ &= P_1(s)P_{set}(s) + P_1(s)C(s)P_{set}(s) - P_1(s)C(s)P_{aw}(s) \\ \Rightarrow P_{aw}(s) + P_1(s)C(s)P_{aw}(s) &= P_{set}(s)(P_1(s) + P_1(s)C(s)) \\ \Rightarrow \frac{P_{aw}(s)}{P_{set}(s)} &= \frac{P_1(s) + C(s)P_1(s)}{1 + C(s)P_1(s)} = T_1(s) \quad \dots\dots\dots (1) \end{aligned}$$

Again,

$$\begin{aligned} Q_{pat}(s) &= P_2(s)[P_{set}(s) + C(s)(P_{set}(s) - P_{aw}(s))] \\ &= P_2(s)P_{set}(s) + P_2(s)C(s)P_{set}(s) - P_2(s)C(s)P_{aw}(s) \\ &= P_2(s)P_{set}(s) + P_2(s)C(s)P_{set}(s) - P_2(s)C(s)P_{set}(s)T_1(s) \\ &= P_{set}(s)[P_2(s) + P_2(s)C(s) - P_2(s)C(s)T_1(s)] \\ \Rightarrow \frac{Q_{pat}(s)}{P_{set}(s)} &= P_2(s)[1 + C(s)(1 - T_1(s))] \\ &= P_2(s) \left[1 + C(s) \times \frac{1 + C(s)P_1(s) - P_1(s) - C(s)P_1(s)}{1 + C(s)P_1(s)} \right] \\ &= P_2(s) \left[1 + \frac{C(s) - C(s)P_1(s)}{1 + C(s)P_1(s)} \right] \\ &= P_2(s) \times \frac{1 + C(s)P_1(s) + C(s) - C(s)P_1(s)}{1 + C(s)P_1(s)} \\ \frac{Q_{pat}(s)}{P_{set}(s)} &= \frac{P_2(s) + C(s)P_2(s)}{1 + C(s)P_1(s)} = T_2(s) \quad \dots\dots\dots (2) \end{aligned}$$

By running the following code:

```
clc;
clearvars;

ki = 1;
wn = 2*3.1416*30;
zeta = 1;
s = tf('s');
Hs = [(0.5063*s + 5.063)/(s + 5.443);...
      (101.3*s + 1.137e-13)/(s + 5.443)];
Bs = (wn^2)/(s^2+(2*zeta*wn*s)+wn^2);
Ps = Hs.*Bs;
Cs = ki/s;
Closed_Paw = (Ps(1)+(Cs*Ps(1)))/(1+(Cs*Ps(1)));
CLosed_Qpat = (Ps(2)+(Cs*Ps(2)))/(1+(Cs*Ps(1)));
```

We found $T_1(s)$ to be:

```
Closed_Paw =

1.799e04 s^9 + 1.396e07 s^8 + 4.135e09 s^7 + 5.68e11 s^6 + 3.387e13 s^5 + 5.755e14 s^4
+ 3.83e15 s^3 + 1.002e16 s^2 + 6.728e15 s
-----
s^11 + 1147 s^10 + 5.515e05 s^9 + 1.428e08 s^8 + 2.119e10 s^7 + 1.753e12 s^6
+ 7.044e13 s^5 + 8.957e14 s^4 + 4.759e15 s^3 + 1.052e16 s^2 + 6.728e15 s
```

And $T_2(s)$ to be:

```
Closed_Qpat =

3.599e06 s^9 + 2.757e09 s^8 + 7.997e11 s^7 + 1.057e14 s^6 + 5.721e15 s^5 + 5.794e16 s^4
+ 1.869e17 s^3 + 1.346e17 s^2 + 151.1 s
-----
s^11 + 1147 s^10 + 5.515e05 s^9 + 1.428e08 s^8 + 2.119e10 s^7 + 1.753e12 s^6
+ 7.044e13 s^5 + 8.957e14 s^4 + 4.759e15 s^3 + 1.052e16 s^2 + 6.728e15 s
```

Task 3:

Sketch the root locus of the control system shown in Fig. 4 for $0 < k_i < \infty$ of the integral controller $C(s)$.

Comparing equations 1 and 2 with,

$$T(s) = \frac{KG(s)}{1 + KG(s)H(s)} \equiv \frac{P_1(s) + C(s)P_1(s)}{1 + \frac{K_i}{s}P_1(s)} = T_1(s)$$

And,

$$T(s) = \frac{KG(s)}{1 + KG(s)H(s)} \equiv \frac{P_2(s) + C(s)P_2(s)}{1 + \frac{K_i}{s}P_2(s)} = T_2(s)$$

We Find that, for both closed loop transfer functions,

$$KG(s)H(s) \equiv K_i \frac{P_1(s)}{s}$$

So, the root locus will be drawn for $\frac{P(s)}{s}$ for $k_i > 0$

Code for plotting root locus:

```
clc;
```

```
clearvars;
```

```
s = tf('s');
```

```
Ps = [(1.799e04*s+1.799e05)/(s^3+382.4*s^2+3.758e04*s+1.934e05);...  
(3.599e06*s+4.04e-09)/(s^3+382.4*s^2+3.758e04*s+1.934e05)];
```

```
figure(1)
```

```
rlocus(Ps(1)/s);
```

```
axis([-200 5 -205 205]);
```

Root Locus:

