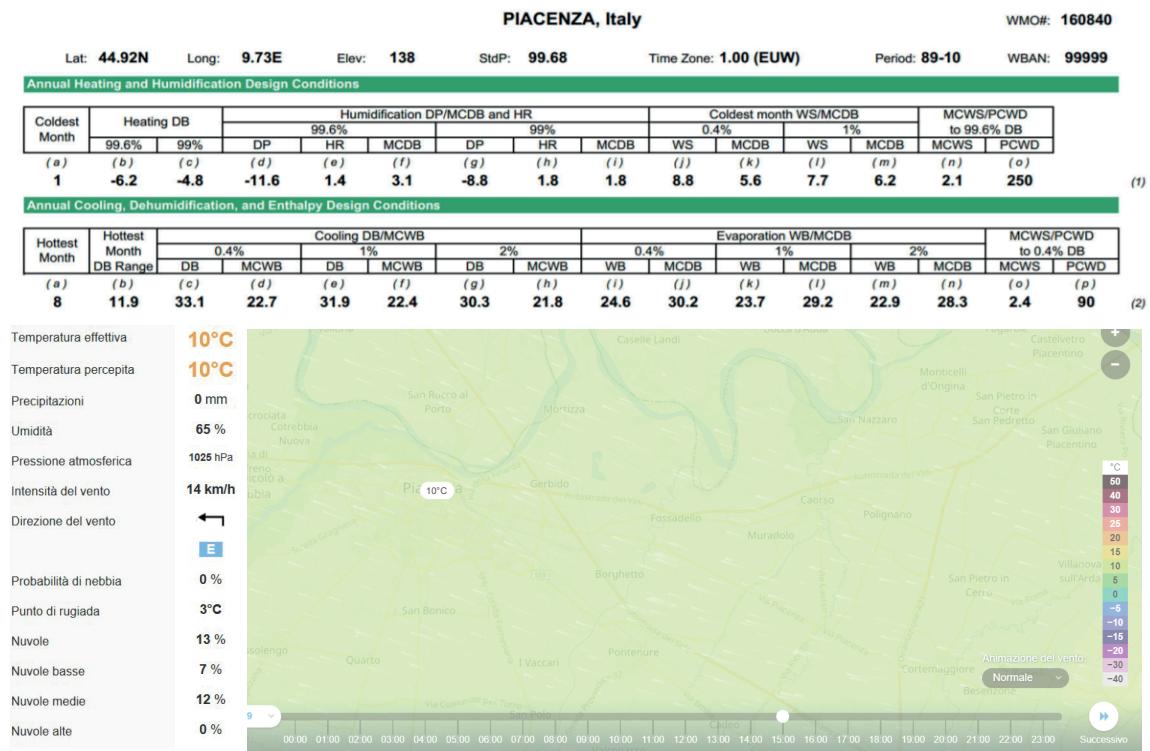


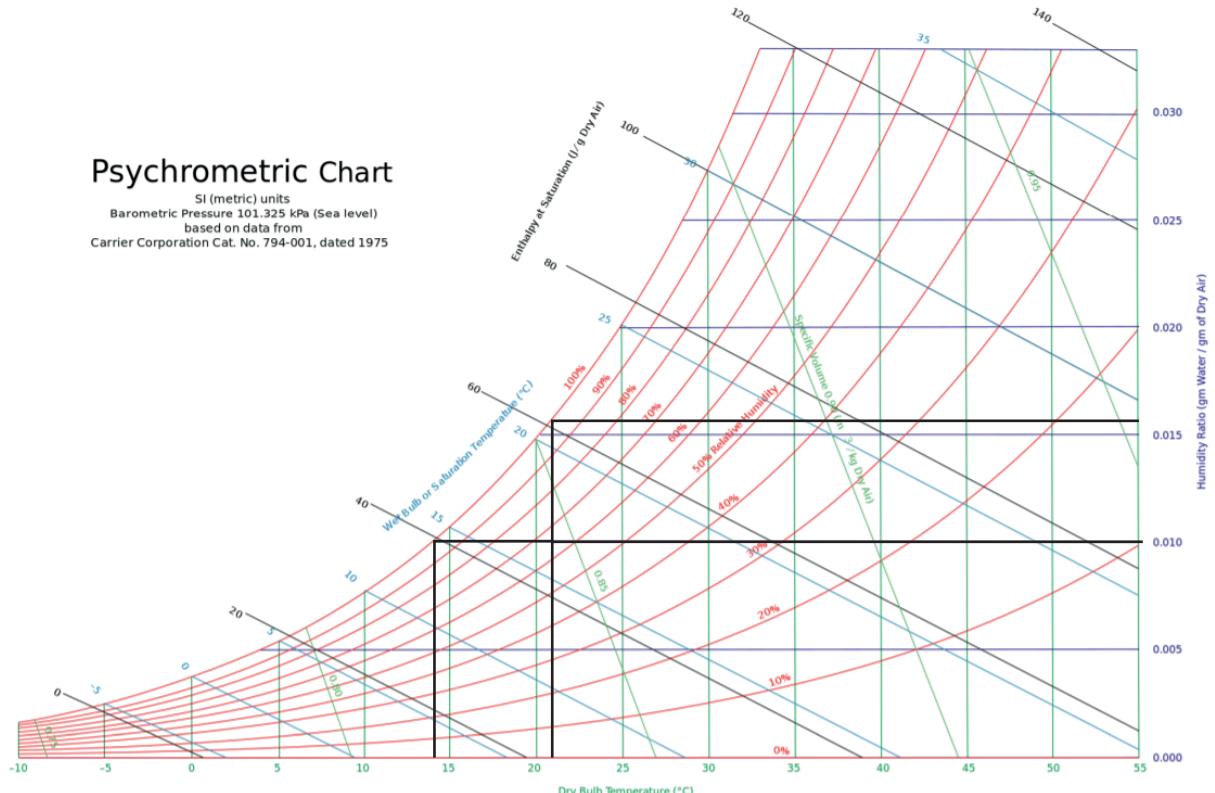
Task 1 Use a weather forecast website, and utilize the psychrometric chart and the formula we went through in the class to determine the absolute humidity, the wet-bulb temperature and the mass of water vapour in the air in ClassRoom A (Aula A) of Piacenza campus in the moment that you are solving this exercise (provide the inputs that you utilized)

Task 2 Utilize the same methodology we went through in the class and determine the sensible and latent load corresponding to internal gains, the ventilation, and the infiltration in a house with a good construction quality and with the same geometry as that of the example which is located in Brindisi, Italy



Psychrometric Chart

SI (metric) units
Barometric Pressure 101.325 kPa (Sea level)
based on data from
Carrier Corporation Cat. No. 794-001, dated 1975



$$T = 21^{\circ}\text{C}$$

From the chart: wet bulb temperature = 14C

$$\text{Humidity Ratio} = 0.010 \frac{\text{gr}_w}{\text{gr}_{da}}$$

$$P = 100 \text{ KPa}$$

$$\phi = 65\% = 0.65$$

$$\phi = \frac{m_v}{m_g} = \frac{P_v}{P_g} \longrightarrow P_g = P_{sat} 25^\circ C = 3.1698 \text{ kPa}$$

$$\rightarrow 25^{\circ}\text{C} : 21^{\circ}\text{C} = 3.1698 : x \quad \rightarrow P_{sat} 21^{\circ}\text{C} = 2.6626$$

$$\phi = \frac{P_v}{P_g} \rightarrow P_V = \phi \times P_g = 0.65 * 2.6626 = 1.73 \text{ kPa}$$

partial pressure of dry air: $P_a = P - P_v = 100 \text{ kPa} - 1.73 \text{ kPa} = 98.27 \text{ kPa}$

$$\omega = 0.622 \frac{P_v}{P_a} = 0.622 \frac{1.73}{98.27} = 0.0109 \frac{Kg_{vapour}}{kg_{dryAir}}$$

$$R_a = 0.287, R_v = 0.4615$$

$$m_a = \frac{98.27 * (5 * 15 * 3)}{0.287 * (273 + 21)} = 262 \text{ kg of dry air}$$

$$m_v = \frac{1.73 * (5 * 15 * 3)}{0.4615 * (273 + 21)} = 2.868 \text{ kg}$$

$$h_a = 1.005 * T = 1.005 * 21 = 21.105 \frac{kJ}{kg_{dry}}$$

$$h_v = 2501.3 + 1.82 * 21 = 2539.52 \frac{kJ}{kg_{water}}$$

$$h_{\square} = h_a + \omega h_v = 21.105 + 0.0109 * 2546.4 = 48.78 \frac{kJ}{kg_{dryAir}}$$

BRINDISI, Italy												WMO#: 163200				
Lat: 40.65N Long: 17.95E Elev: 10 StdP: 101.2			Time Zone: 1.00 (EUW)			Period: 86-10			WBAN: 99999							
Annual Heating and Humidification Design Conditions																
Coldest Month	Heating DB		Humidification DP/MCDB and HR						Coldest month WS/MCDB				MCWS/PCWD to 99.6% DB			
	99.6% 99%		99.6% DP		HR MCDB		99% DP		0.4% WS		1% MCDB		MCWS			
	(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)	(j)	(k)	(l)	(m)	(n)	(o)	
(1)	2	2.9	4.1	-5.1	2.5	7.2	-3.0	3.0	7.4	13.4	10.2	12.4	10.6	3.4	250	
Annual Cooling, Dehumidification, and Enthalpy Design Conditions														(1)		
Hottest Month	Hottest Month DB Range	Cooling DB/MCWB						Evaporation WB/MCDB						MCWS/PCWD to 0.4% DB		
		0.4% DB		1% MCWB		2% DB		0.4% WB		1% MCDB		2% WB		MCDB		
	(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)	(j)	(k)	(l)	(m)	(n)	(o)	(p)
(2)	8	7.1	32.8	23.6	31.1	24.3	29.9	24.3	27.2	29.7	26.3	29.0	25.6	28.3	4.2	180
Dehumidification DPM/CDB and HR														Hours 8 to 4 & 12.8/20.6		
DP	0.4% DP		1% HR		2% MCDB		0.4% DP		1% MCDB		2% Enth		Enthalpy/MCDB		(2)	
	(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)	(j)	(k)	(l)	(m)	(n)	(o)	(p)
(3)	26.3	21.8	29.2	25.4	20.7	28.5	24.7	19.7	27.9	86.0	30.1	82.2	29.1	78.5	28.3	1236
Extreme Annual Design Conditions														(3)		
Extreme Annual WS			Extreme Max WB	Extreme Annual DB						n-Year Return Period Values of Extreme DB						
				Mean		Standard deviation		n=5 years		n=10 years		n=20 years		n=50 years		
1%	2.5%		(d)	Min		Max		Min		Max		Min		Max		
	(a)	(b)		(e)	(f)	(g)	(h)	(i)	(j)	(k)	(l)	(m)	(n)	(o)	(p)	
(4)	11.3	9.9	8.7	31.4	0.4	37.3	1.4	3.0	-0.6	39.4	-1.4	41.1	-2.2	42.8	-3.2	44.9

Internal gains

$$\dot{Q}_{ig_{sensible}} = 136 + 2.2 * A_{cf} + 22 N_{oc} = 136 + 2.2 * 200 + 22 * 2 = 620 W$$

$$\dot{Q}_{ig_{latent}} = 20 + 0.22 * A_{cf} + 12 N_{oc} = 20 + 0.22 * 200 + 12 * 2 = 88 W$$

Average quality-> $A_{ul} = 2.8 \frac{cm^2}{m^2}$

Exposed surface = Wall area + roof area

$$A_{es} = 200 + 144 = 344 m^2$$

$$A_L = A_{es} \times A_{ul} = 344 \times 2.8 = 963.2 cm^2$$

$$IDF_{heating} = 0.0645 \frac{L}{s.cm^2} \quad IDF_{cooling} = 0.0315 \frac{L}{s.cm^2}$$

$$\dot{V}_{infiltration_{heating}} = A_L \times IDF$$

$$= 963.2 * 0.0645 = 62.12 \frac{L}{s}$$

$$\dot{V}_{infiltration_{cooling}} = A_L \times IDF = 963.2 * 0.0315$$

$$= 30.34 \frac{L}{s}$$

$$\dot{V}_{ventilation}$$

$$= 0.05 A_{cf} + 3.5 (N_{br} + 1) = \\ .05 * 200 + 3.5 * 2 = 17 L/S$$

$$\dot{V}_{inf-ventilation_{heating}} = 62.12 + 17 \\ = 79.12 L/s$$

$$\dot{V}_{inf-ventilation_{cooling}} = 30.34 + 17 = 47.34 L/s$$

$$C_{sensible} = 1.23, C_{latent} = 3010$$

$$\dot{Q}_{inf-ventilation_{cooling_sensible}} = C_{sensible} \dot{V} \Delta T_{Cooling}$$
$$= 1.23 * 47.34 * 7.9 = 460 W$$

$$\dot{Q}_{inf-ventilation_{cooling_latent}} = C_{latent} \dot{V} \Delta \omega_{Cooling}$$
$$= 3010 * 47.34 * 0.0039 = 555.72 W$$

$$\dot{Q}_{inf-ventilation_{heating_sensible}} = C_{sensible} \dot{V} \Delta T_{heating}$$
$$= 1.23 * 79.12 * 24.8 = 2413.47 W$$