

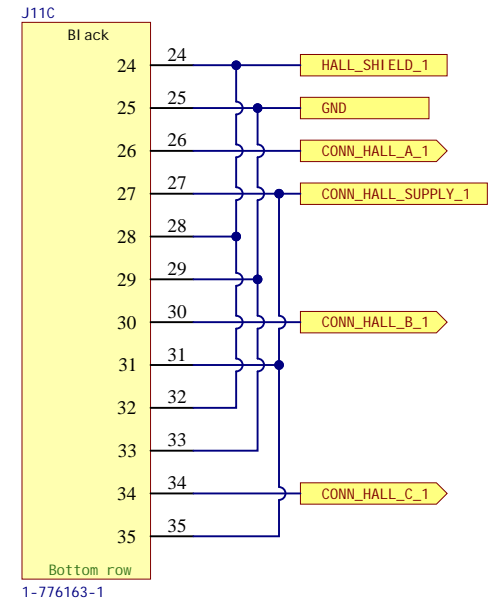
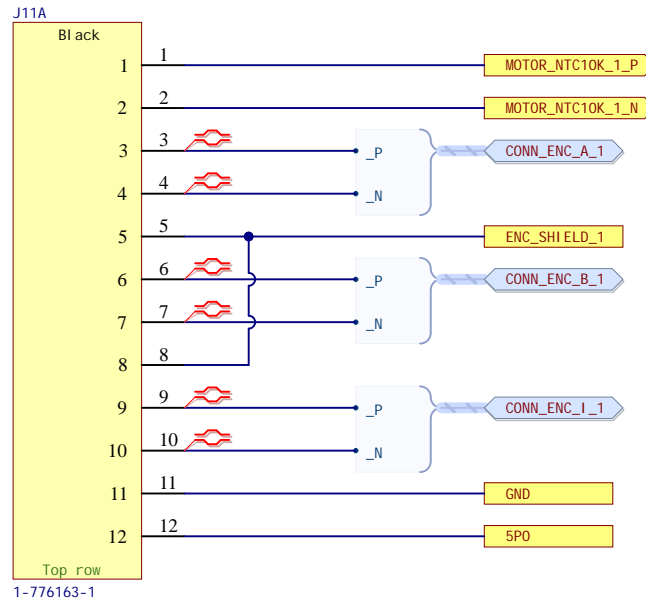
****Use with 22-24 AWG wire****

Mating crimps: 1-770520-1
Mating connector: 2371885-1
Sealing plugs: 776364-1
CPA: 2373965-1
Backshell: 2389807-1

Assumes 10k B = 3380K NTC thermistor.

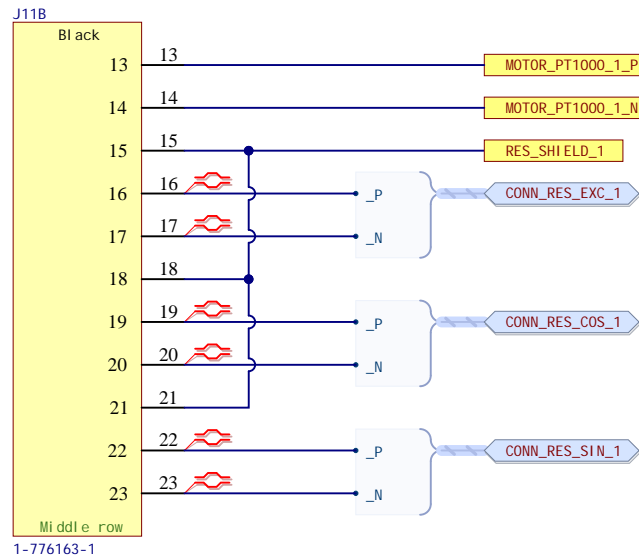
Assumes 5-volt differential encoder.

This board connects the shield to the CHASSIS net by default, but offers a OR stuffing option to connect it to GND instead.



Assumes PT1000 RTD temperature sensor.

This board connects the shield to the REFOUT of the AD2S1200 by default, but offers OR stuffing options to connect it to CHASSIS or GND nets instead.



Assumes 5-volt Hall effect sensors. Pull-ups are provided. The extra supply and return pins enable wiring to individual sensors that may not have bussed bias.

This board connects the shield to the CHASSIS net by default, but offers a OR stuffing option to connect it to GND instead.

****Use with 20-24 AWG wire****

Mating crimps 20-22 AWG: 770520-8

Mating crimps 22-24 AWG: 1-770520-1

Mating connector: 2371884-1

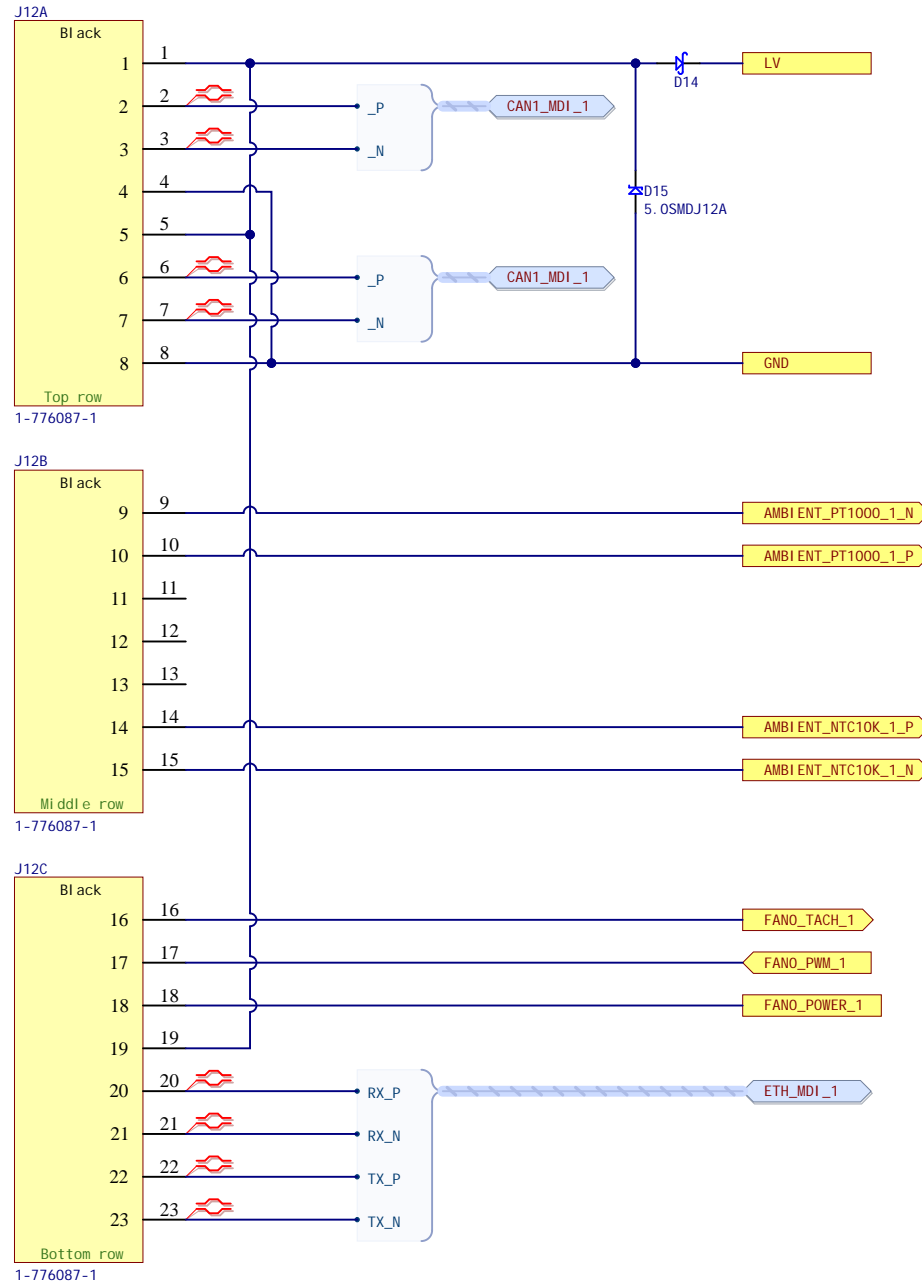
Sealing plugs: 776364-1

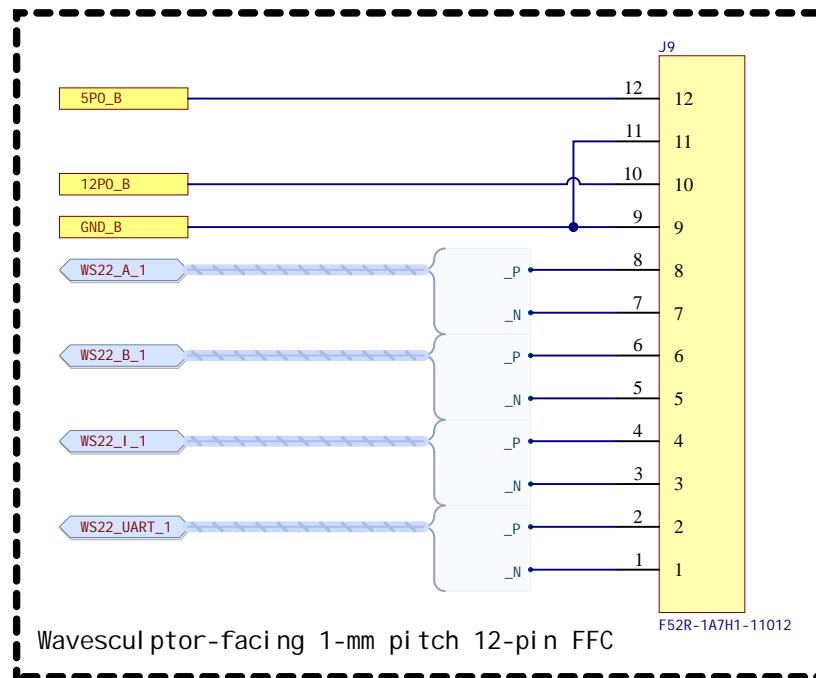
CPA: 2373965-1

Backshell: 2389806-1

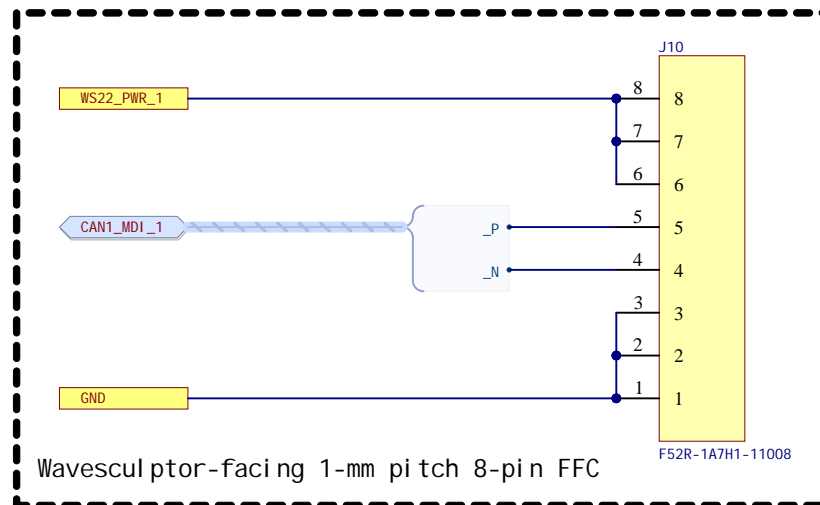
https://www.te.com/commerce/DocumentDelivery/DDEController?Action=srchrtv&DocNm=ict_ampsal_cat_a4_1-1773979-2_en&DocType=Catalog%20Section&DocLang=English&DocFormat=pdf&PartCntxt=1-776087-1

* Must use 3- or 4-wire PWM-controlled fan. *

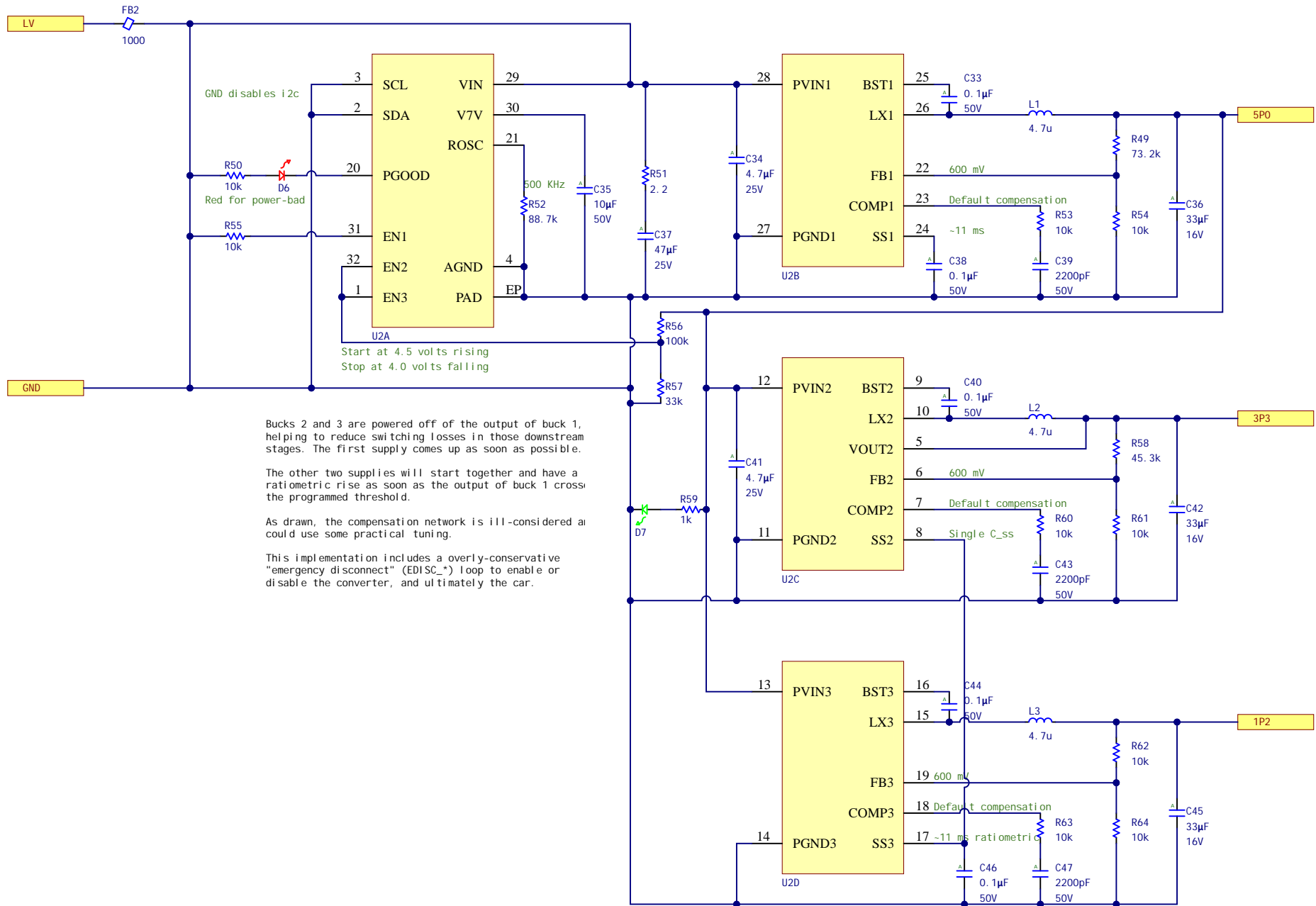




Note that the pin definition here is the mirror image of what is seen on the Wavesculptor 22 logic board. These signals appear to be referenced from the high-voltage domain and should not get connected back to the low voltage domain.



Note that the pin definition here is the mirror image of what is seen on the Wavesculptor 22 logic board. These signals are on the LV side of the Wavesculptor 2.



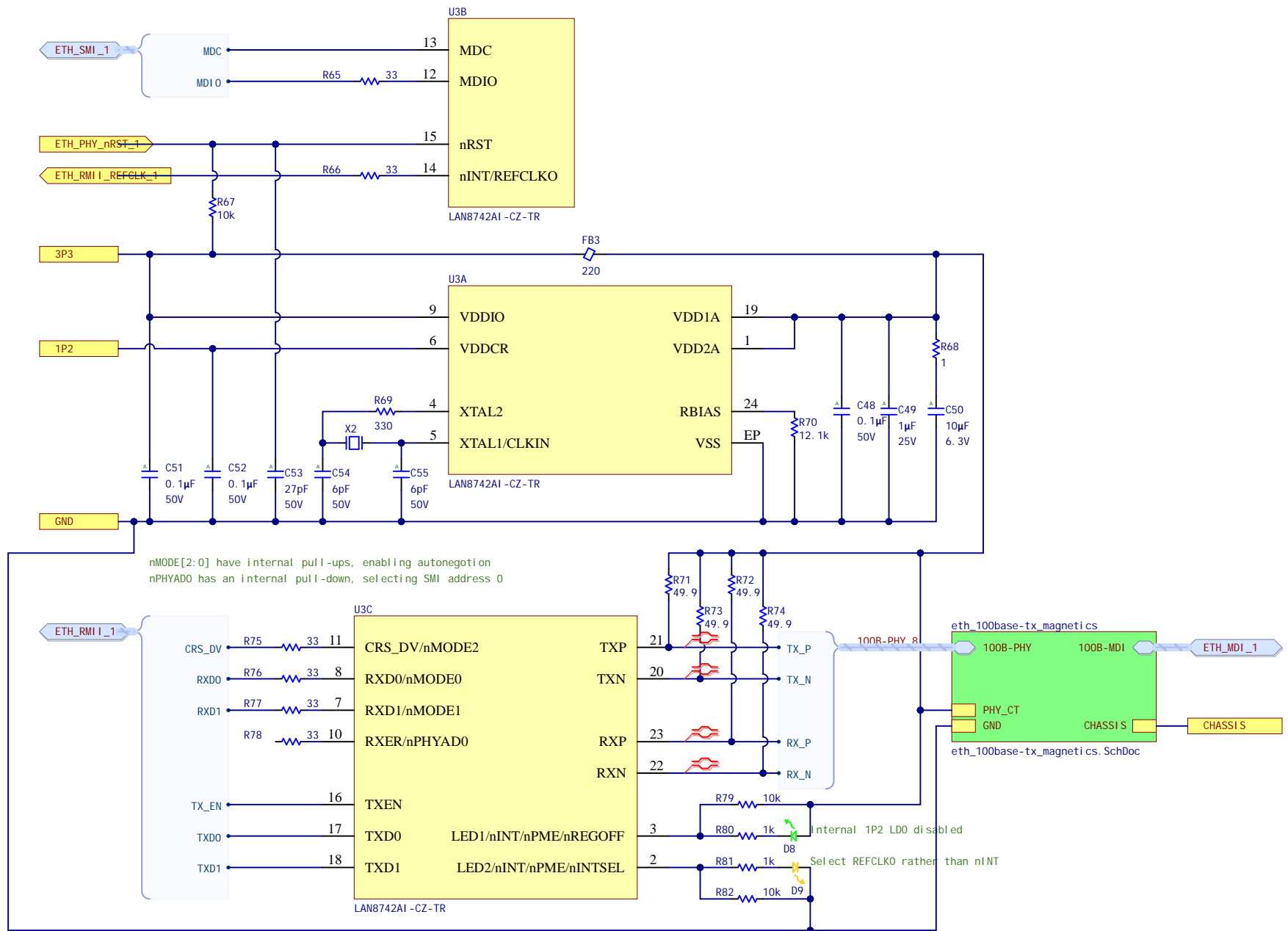
Bucks 2 and 3 are powered off of the output of buck 1, helping to reduce switching losses in those downstream stages. The first supply comes up as soon as possible.

The other two supplies will start together and have a ratiometric rise as soon as the output of buck 1 crosses the programmed threshold.

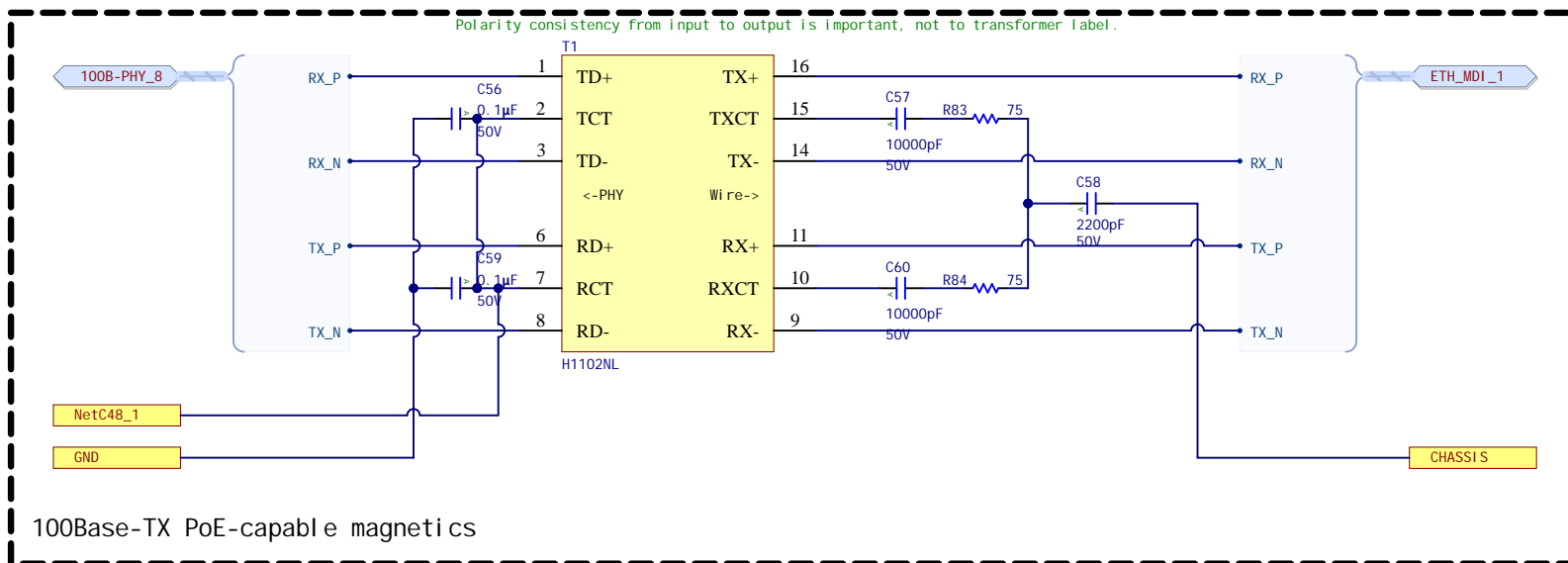
As drawn, the compensation network is ill-considered and could use some practical tuning.

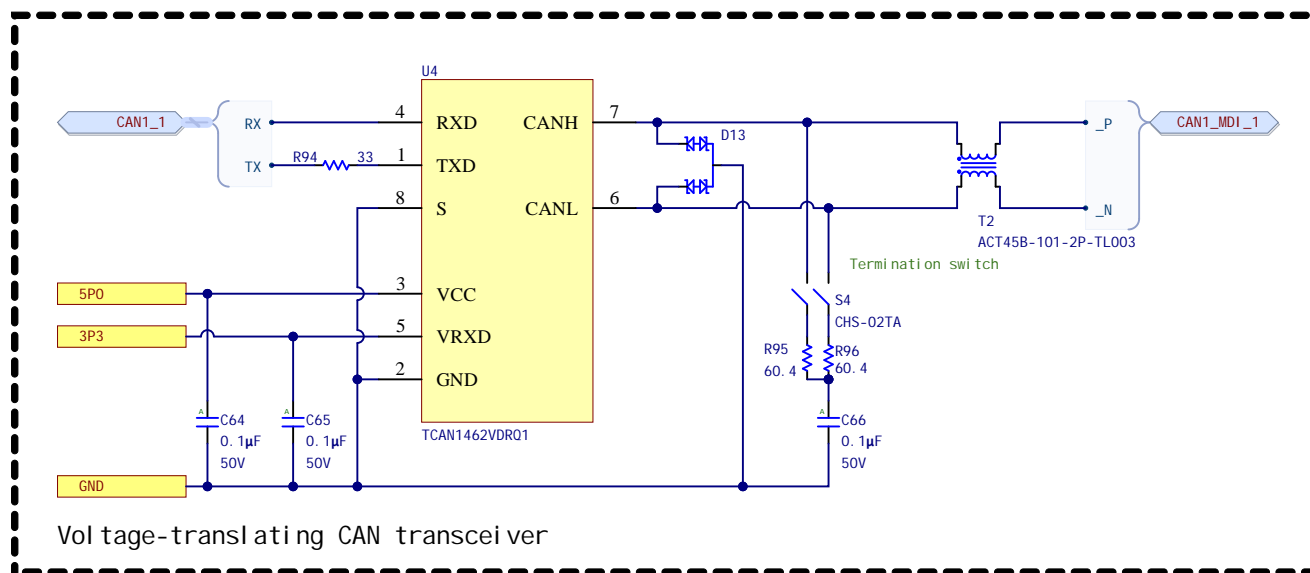
This implementation includes an overly-conservative "emergency disconnect" (EDISC_*) loop to enable or disable the converter, and ultimately the car.

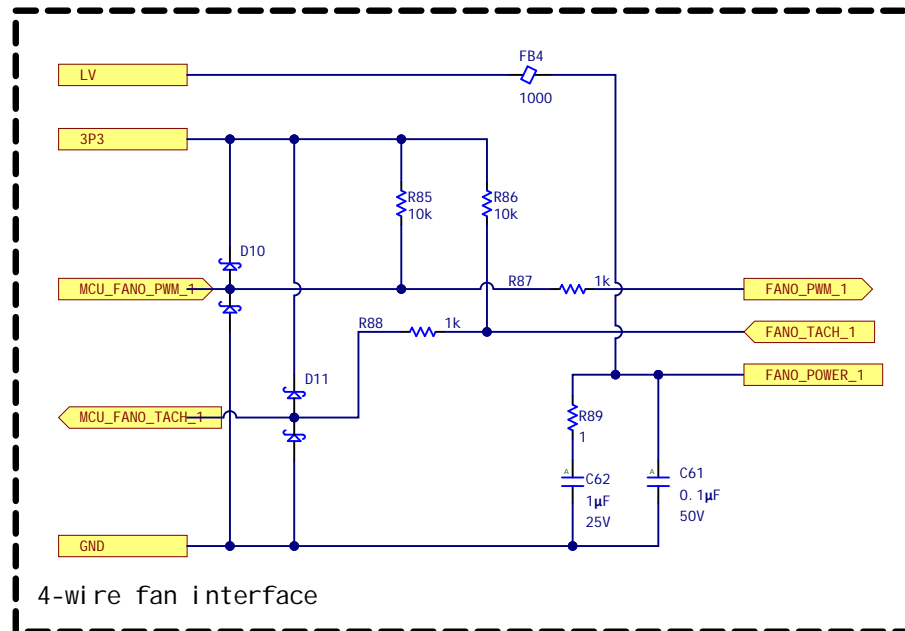
<=18 volt input, 3A/2A/2A triple buck

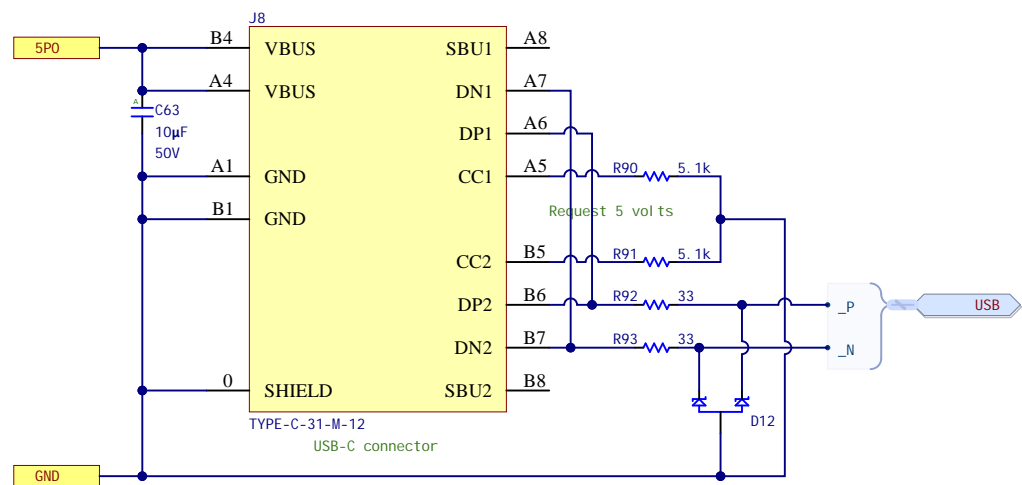


RMII-interface 100Base-TX PHY

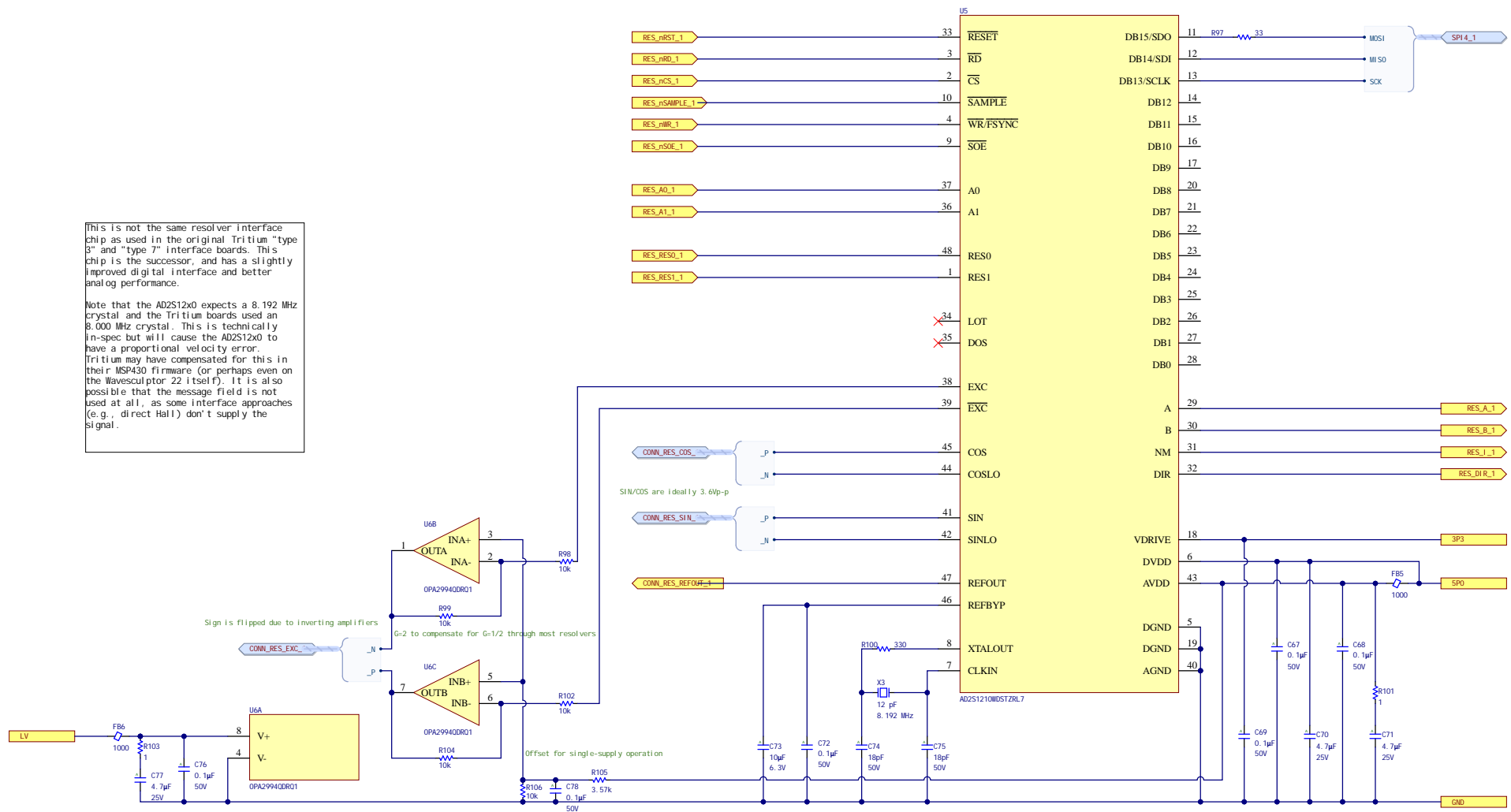




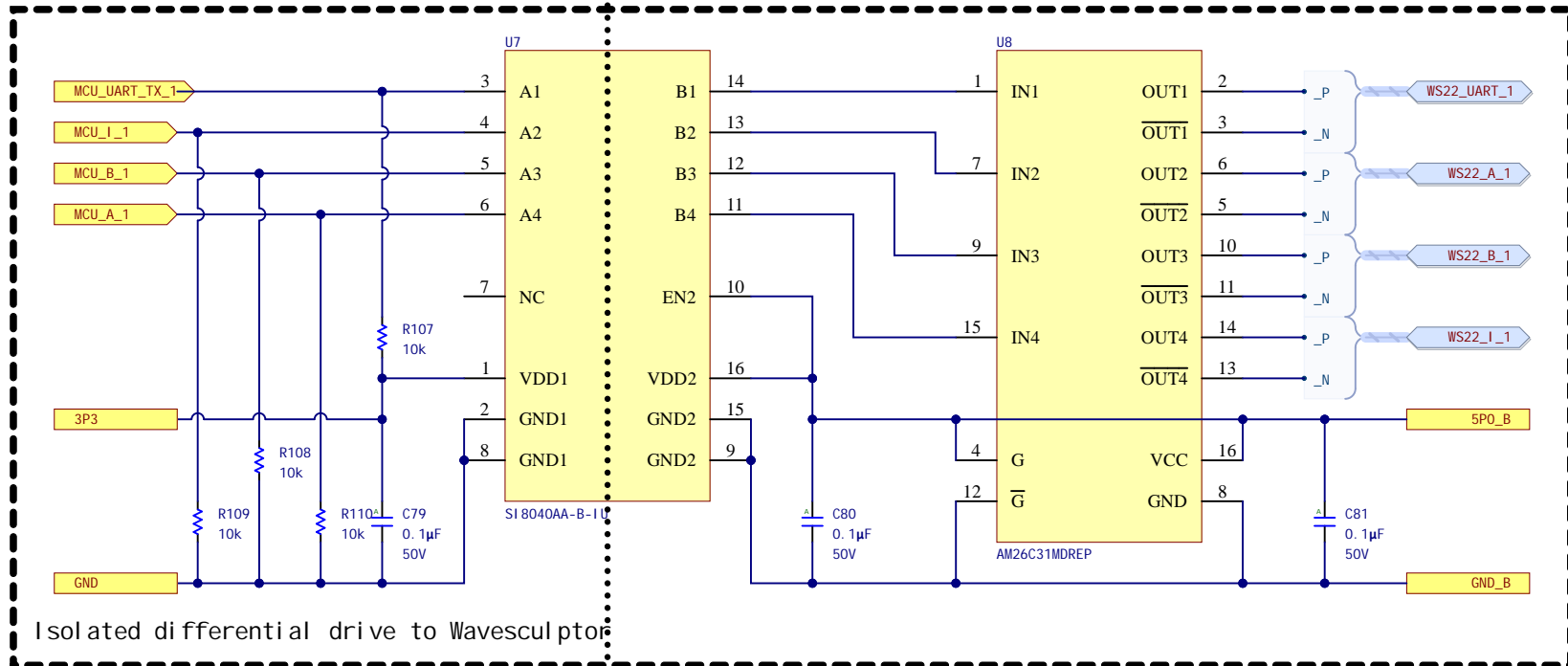


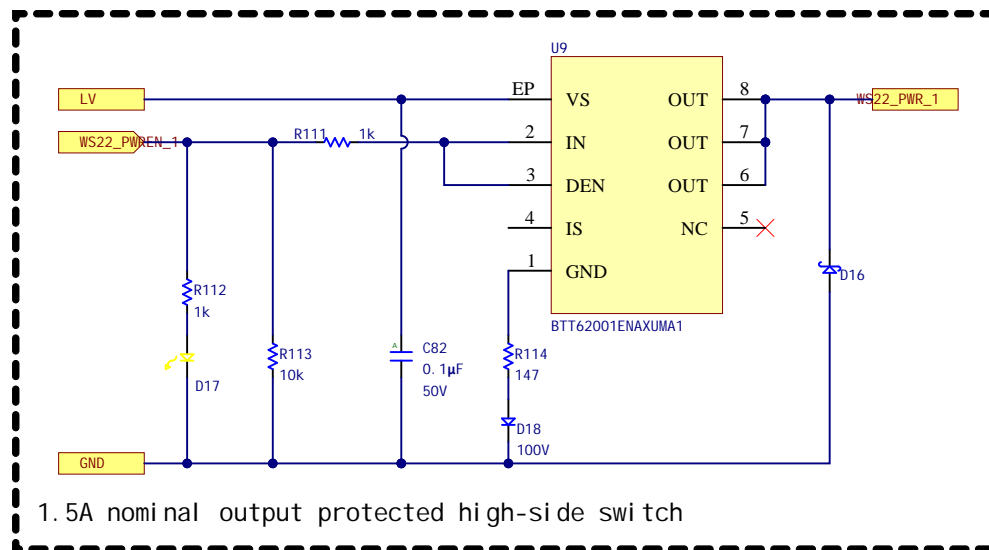


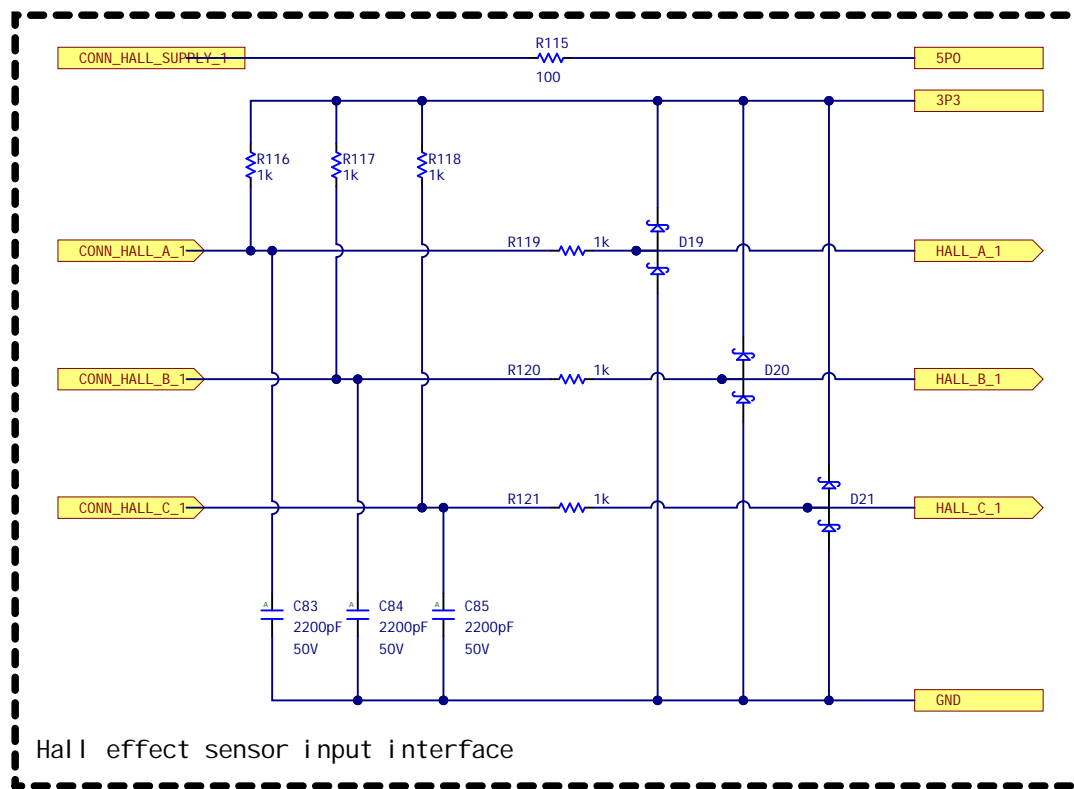
Note that the AD2S12X0 expects a 8.192 Mhz crystal and the Tritium boards used an 8.000 Mhz crystal. This is technically in-spec but will cause the AD2S12X0 to have a proportional velocity error. Tritium may have compensated for this in their MSP430 firmware (or perhaps even on the Wavesculptor 22 itself). It is also possible that the message field is not used at all, as some interface approaches (e.g., direct Hall) don't supply the signal.

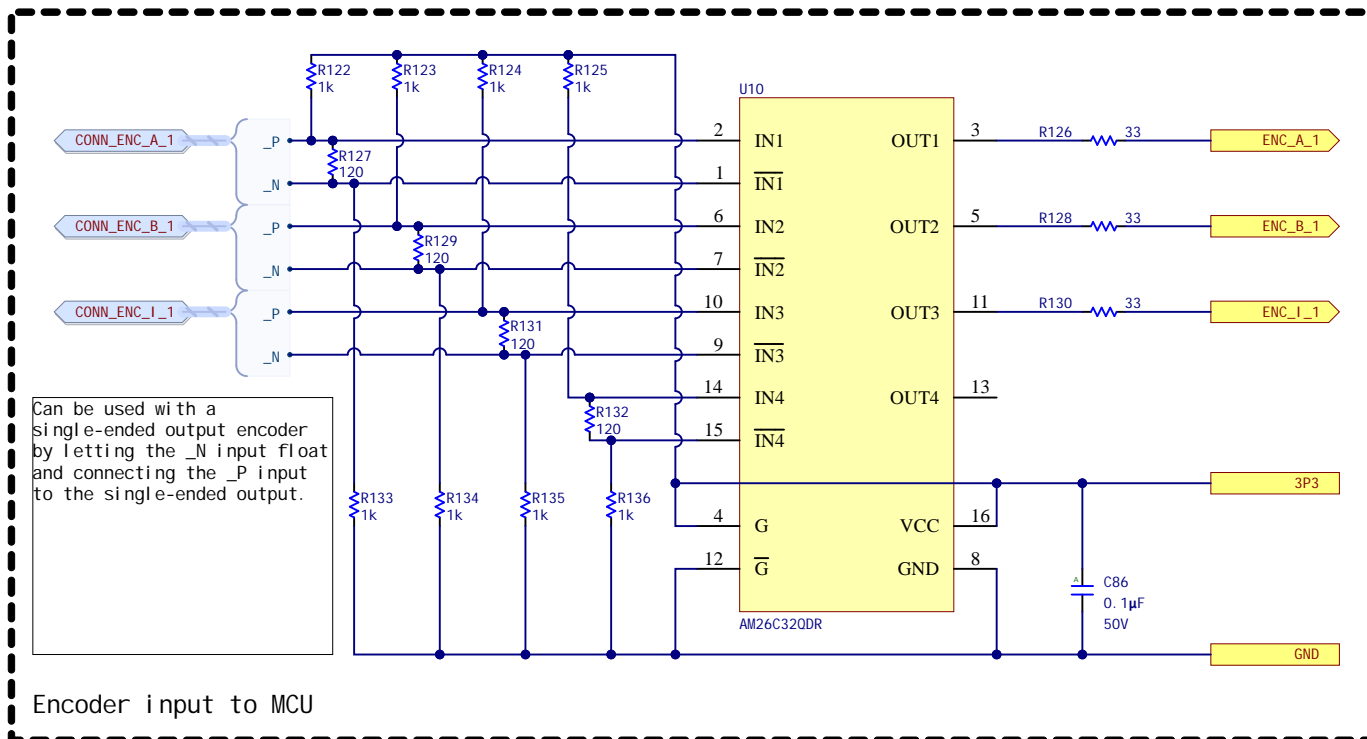


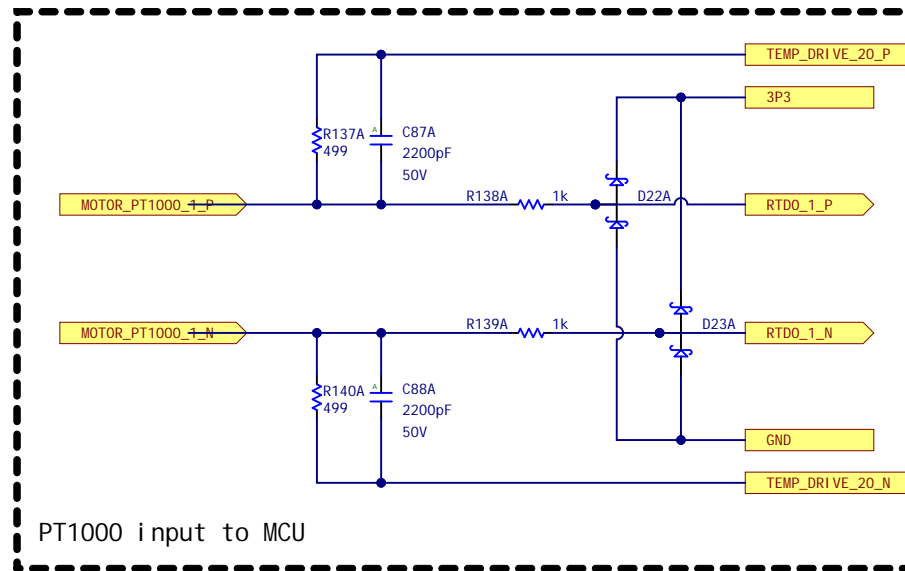
LV domain HV domain

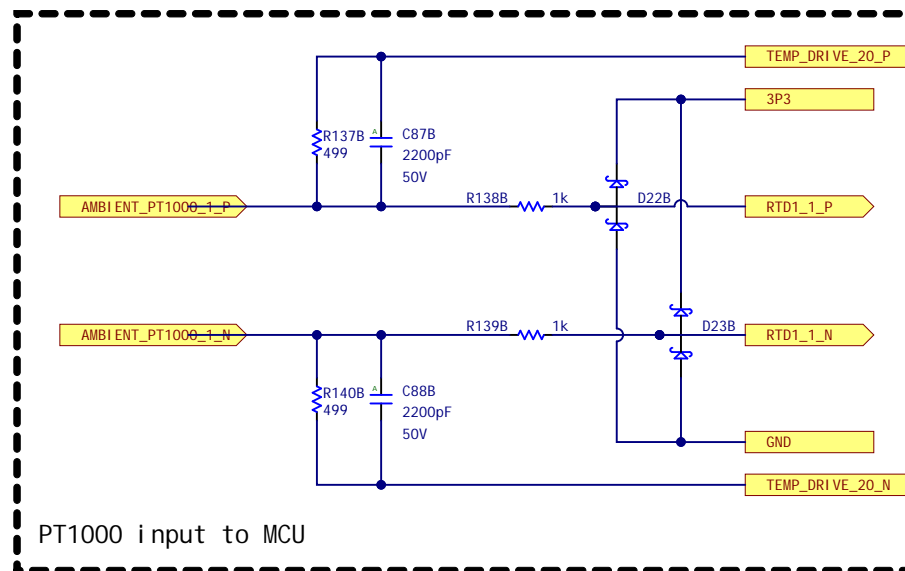


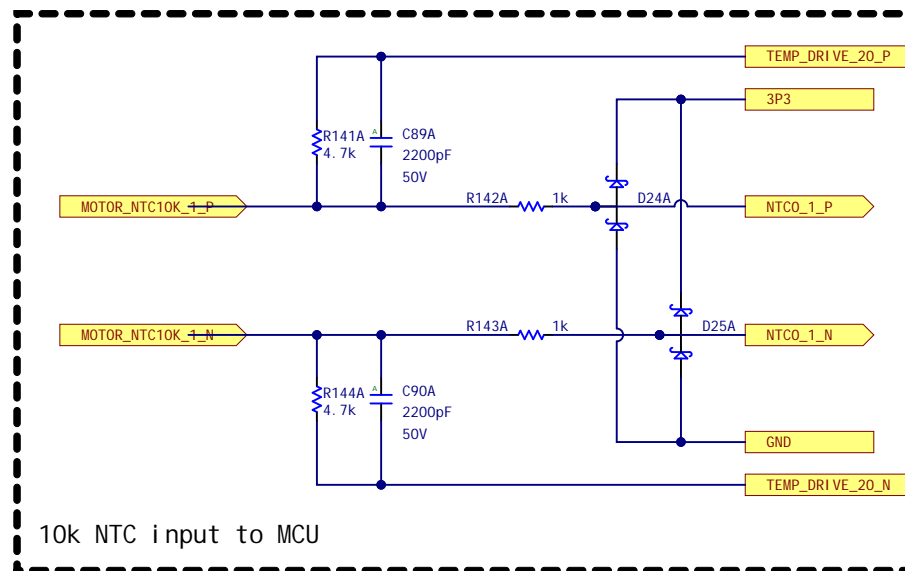


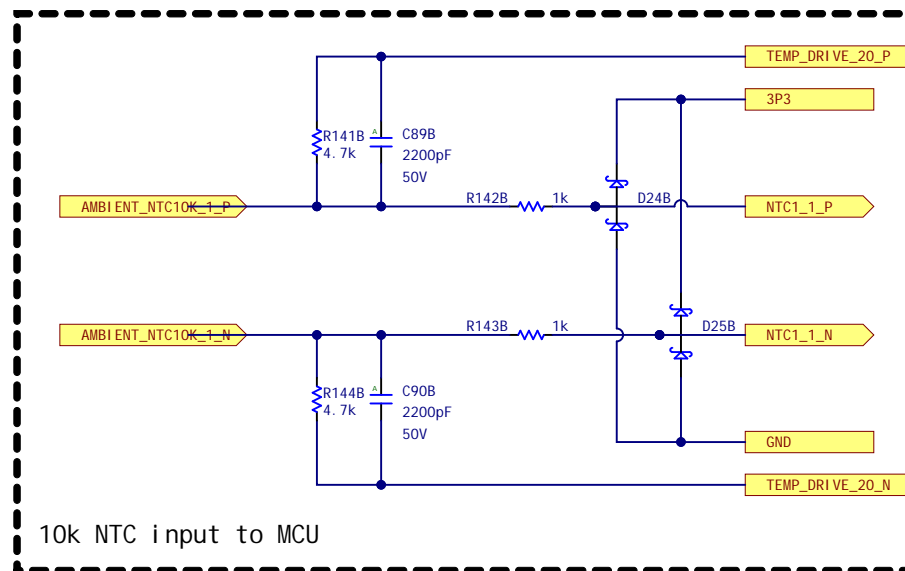


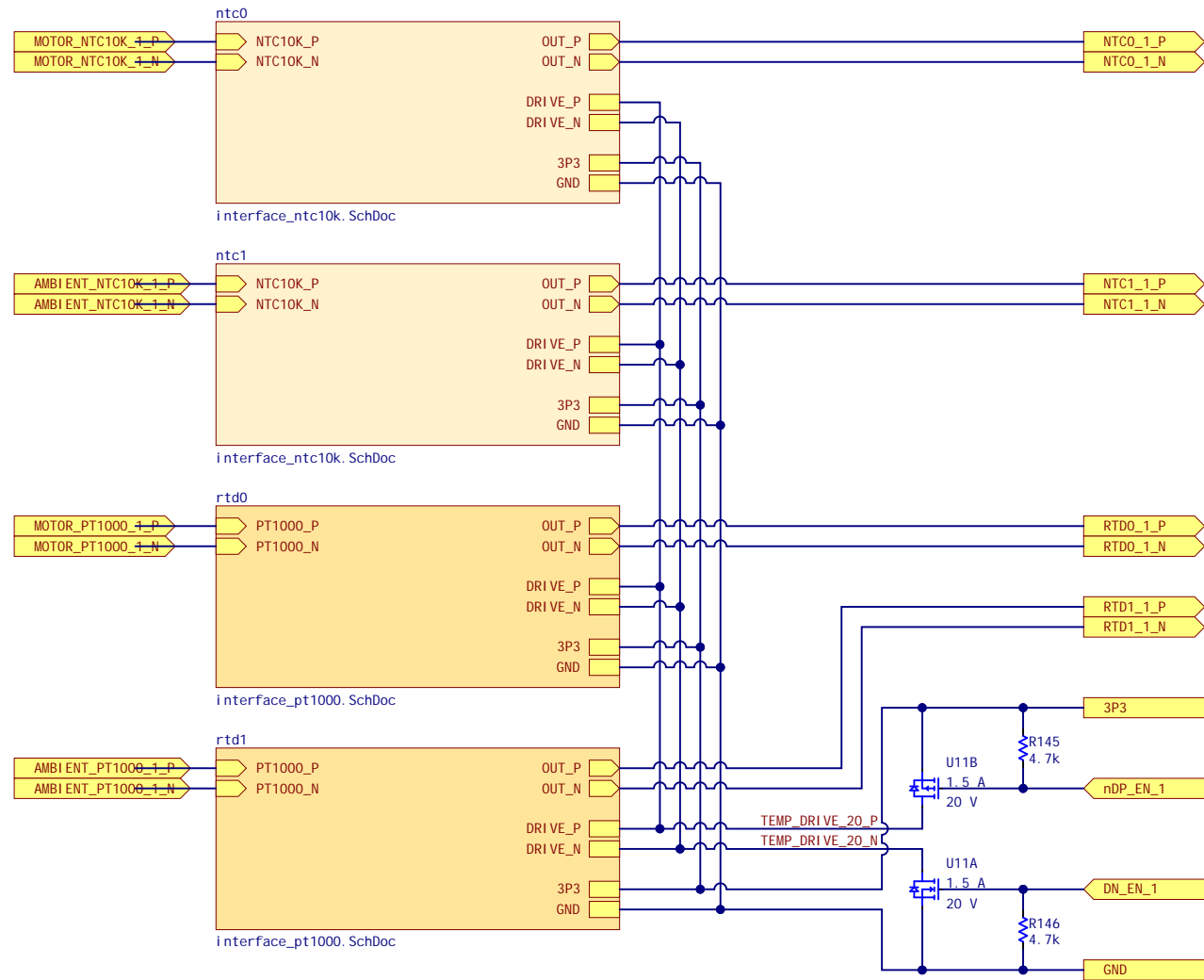












We're using pseudo-differential sampling of the temperature sensors along with switch drive signals so that we can detect when wires break and the temperature sensor goes open-circuit.