PARALLEL MONTE CARLO SYNTHETIC ACCELERATION METHODS FOR DISCRETE TRANSPORT PROBLEMS

by

Stuart R. Slattery

A dissertation submitted in partial fulfillment of
the requirements for the degree of

Doctor of Philosophy

(Nuclear Engineering and Engineering Physics)

at the

UNIVERSITY OF WISCONSIN–MADISON

21 August 2013

For my parents.

Acknowledgments

Abstract

Predictive modeling and simulation is an important and developing component of modern nuclear reactor analysis. New high performance computing hardware and algorithms that leverage this hardware are needed to help meet the goals and requirements of engineering analysis. Current practices in neutron transport and fluid flow leverage methods based on subspace iterations to achieve good convergence properties and quality parallel scaling on large machines. However, the next generation of machines is expected to possess both high levels of concurrency and low memory availability per core compared to today's machines with a potentially rate of faults. Therefore, we seek new algorithms to solve these problems in reactor analysis that have the potential to perform well on forthcoming hardware with the goal of improving both iterative performance and parallel scalability.

This work researches and develops Monte Carlo Synthetic Acceleration (MCSA) methods as a new class of solution techniques for discrete neutron transport and fluid flow problems. Monte Carlo Synthetic Acceleration methods use a traditional Monte Carlo process to approximate the solution to the discrete problem as a means of accelerating traditional fixed-point methods. To apply these methods to neutronics and fluid flow and determine the feasibility of these methods on modern hardware, three complementary research and development exercises are performed.

First, solutions to the SP_N discretization of the linear Boltzmann neutron transport equation are obtained using MCSA with a difficult criticality calculation for a light water reactor fuel assembly used as the driving problem. It was discovered that basic Jacobi-based preconditioning as used in previous work was not sufficient to achieve convergence due to the dominating effect of the light water moderator. To enable MCSA as a solution technique a group of modern preconditioning strategies are researched. The new preconditioning techniques, however, create unwanted growth in both memory consumption and computation time for these problems. MCSA was verified to produce the correct solution for the fuel

assembly criticality problem when compared to conventional Krylov methods and demonstrated improved iterative performance over GMRES by converging in fewer iterations when using the same preconditioning.

Second, solutions to the compressibleNavier-Stokes equations were obtained by developing the Forward-Automated Newton-MCSA (FANM) method for nonlinear systems based on Newton's method. Three difficult fluid benchmark problems in both convective and driven flow regimes were used to drive the research and development of the method. It was found for all benchmarks that FANM produced identical solutions when compared to those generated by modern Newton-Krylov methods. For each benchmark, performance comparisons between FANM and Newton-Krylov were also conducted. For 8 out of 12 benchmark cases, it was found that FANM had better iterative performance than the Newton-Krylov method by converging the nonlinear residual in fewer linear solver iterations with the same preconditioning.

Third, a new domain decomposed algorithm to parallelize MCSA aimed at leveraging leadership-class computing facilities was developed by utilizing parallel strategies from the radiation transport community. The new algorithm utilizes the Multiple-Set Overlapping-Domain strategy in an attempt to reduce parallel overhead and add a natural element of replication to the algorithm. A large number of parallel scaling studies using a neutron diffusion problem were performed on the Titan Cray XK7 machine at Oak Ridge National Laboratory with up to 65,356 cores used in the strong scaling studies and 131,072 cores used in the weak scaling studies. It was found that for the current implementation of MCSA, both weak and strong scaling were superior to production implementations of Krylov methods. In addition, the replication in the algorithm was able to boost parallel efficiencies by up to 20% at large core counts in the strong scaling studies. By using the principle of superposition, replicating the Monte Carlo sequence was also demonstrated to enhance time to solution. Finally, it was discovered that MCSA exhibits the most scalable behavior when it is formulated as a stochastic realization of an additive Schwarz method.

Each of these research and development activities meet the goals of this work by pro-

ducing methods that in many cases were demonstrated to converge in fewer iterations than conventional methods and exhibit better parallel efficiencies at high levels of concurrency. All the components of this work are required to enable future simulation of nonlinear transport phenomena on the next generation of hardware. To enable high performance simulations with FANM, we require the MCSA techniques developed in the research on the neutron transport problem and in turn, effectively leveraging MCSA on leadership-class hardware requires the new parallel algorithm developed by this work. With the further development of these methods based on this work, future nuclear reactor simulations may potentially be enabled that have an improved time to solution and more efficiently utilize the available computational resources.

Contents

List of Tables

List of Figures

List of Algorithms

Chapter 1

Introduction

In nearly all high-fidelity nuclear reactor simulations, linear and nonlinear transport problems are a primary focus of study. Neutronics, fluid flow, and heat transfer are among the predominant physics that fall into this category and simulation technologies to solve these problems make up much of the analysis suite used for modern engineering calculations. Recent focus on multiple physics systems in the nuclear reactor modeling and simulation community adds a new level of complexity to common linear and nonlinear systems as solution strategies change when they are coupled to other problems [32]. Furthermore, a desire for predictive simulations to enhance the safety and performance of nuclear systems creates a need for extremely high fidelity computations to be performed for these transport systems as a means to capture effects not modeled by coarser methods.

In order to achieve this high fidelity, state-of-the-art computing must be leveraged in a way that is both efficient and considerate of hardware-related issues. As scientific computing moves beyond petascale facilities with machines of $O(1,000,000)$ cores already coming on-line, new algorithms to solve these complex problems must be developed to leverage this new hardware [69]. Issues such as resiliency to node failure, limited growth of memory available per node, and scaling to large numbers of cores will be pertinent to robust algorithms aimed at this new hardware.

Considering these physics and hardware issues, this goal of this work is to research and develop Monte Carlo Synthetic Acceleration methods for neutron transport problems and a new method leveraging the synthetic acceleration techniques to advance solution algorithms for nonlinear problems in fluid flow. These methods are based on using the Monte Carlo method to directly accelerate the convergence of traditional fixed-point iterative schemes for

these problems. We aim to address both their benefits and their shortcomings in the context of the physics of interest and desire to identify areas in which improvements can be made. Once the linear and nonlinear methods have been developed, we look forward to parallelizing them with the goal that they may be leveraged competitively on leadership class computing platforms.

To achieve these goals, three complementary research and development activities are performed. First, Monte Carlo Sythetic Acceleration (MCSA) is applied to the neutron transport problem in a light water reactor calculation to develop the necessary preconditioning techniques and understanding required to solve difficult problems. Second, using these new techniques, a series of benchmarks for the Navier-Stokes equations are solved in different flow regimes to research the performance of the Monte Carlo algorithm for nonlinear problems using the new Forward-Automated Newton-MCSA (FANM) algorithm developed by this work. Third, a novel parallel algorithm based on domain decomposed Monte Carlo methods for particle transport is developed to fully parallelize the solution techniques developed to solve the neutron transport and fluid flow problems on leadership class hardware with scaling studies performed in this work using a neutron diffusion problem.

We discuss in this chapter physics-based motivation for advancing Monte Carlo Synthetic Acceleration methods and studying their application to transport phenomena by providing problems of interest in nuclear reactor analysis. Hardware-based motivation is also provided by considering the potential impact of these methods on forthcoming high performance computing architectures. In addition, background on the current solver techniques for these physics problems and a brief comparison to the proposed methods are provided to further motivate this work. Finally, the statement of work is given and the organization of the document is then reviewed.

1.1 Physics-Based Motivation

Predictive modeling and simulation capability requires the combination of high fidelity models, high performance computing hardware that can handle the intense computational loads required by these models, and modern algorithms for solving these problems that leverage this high performance hardware. For nuclear reactor analysis, this predictive capability can enable tighter design tolerances for improved thermal performance and efficiency, higher fuel burn-up and therefore reduction in generated waste, and high confidence in accident scenario models. The physics that dominate these types of analysis include neutronics, thermal hydraulics, computational fluid dynamics, and structural mechanics.

Although solution techniques in each of these individual categories has advanced over the last few decades and in fact leveraged modern algorithms and computer architectures, true predictive capability for engineered systems can only be achieved through a coupled, multiple physics analysis where the effects of feedback between physics are modeled. For example, consider the safety analysis of a departure from nucleate boiling scenario in the subchannel of a nuclear fuel assembly as shown in Figure 1.1.

When this event occurs, heat transfer is greatly reduced between the fuel and the coolant due to the vapor layer generated by boiling, causing the fuel center-line temperature to rapidly rise. To characterize this boiling phenomena and how it affects fuel failure we must consider a neutronics analysis in order to compute power generation in the fuel pins, fluid dynamics analysis to characterize coolant boiling, temperature, and density, solid material heat transfer to characterize fuel and cladding temperature and heat transfer with the coolant, and nuclear data processing to characterize how changing material temperatures and densities changes the cross sections needed for the neutronics calculation.

As shown in Figure 1.1, many couplings are required among individual physics components in order to accurately model this situation with each physics generating and receiving many responses. Those variables that are very tightly coupled, such as the temperatures generated
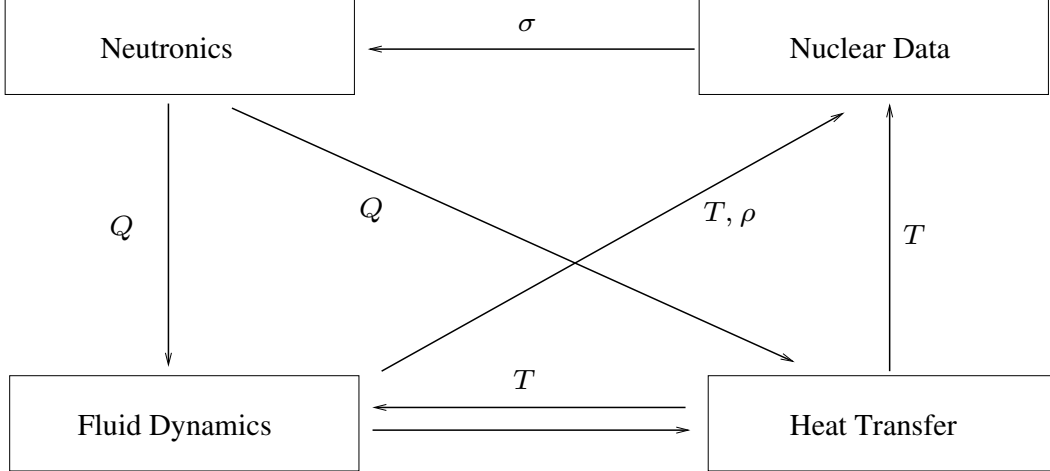
Figure 1.1: **Multiphysics dependency analysis of departure from nucleate boiling.**
*A neutronics solution is required to compute power generation in the fuel pins, fluid dynamics
is required to characterize boiling and fluid temperature and density, heat transfer is required to
compute the fuel and cladding temperature, and the nuclear data modified with the temperature
and density data. Strong coupling among the variables creates strong nonlinearities.*

by the fluid dynamics and heat transfer components, will have strong nonlinearities in their
behavior and would therefore benefit from fully implicit nonlinear solution schemes such
as that developed by this work instead of fixed-point type iterations between physics[1]. To
leverage such a method for analysis such as a departure from nucleate boiling calculation,
we also require effective solutions for each of the physics involved including the neutronics
problem and the fluid problem, both of which we discuss next.

1.1.1   Solutions for the SP_N Equations

The neutron transport problem is complicated. Solutions cover a large phase space and the
problems of interest are often geometrically complex, contain large numbers of degrees of
freedom, or both, requiring tremendous computational resources to generate an adequate
solution. Modern high fidelity deterministic methods for large scale problems are commonly
variants on the discrete ordinates (S_N) method [89]. For fission reactor neutronics simulations,

[1]Fixed-point iterations between physics are commonly referred to as Picard iterations in the multiphysics
community.

the S_N method requires potentially trillions of unknown angular flux moments to be computed to achieve good accuracy for the responses of interest [25]. Other forms of the transport problem, including the P_N method, take on a simpler form than the more common S_N methods but lack in accuracy when compared while still requiring considerable computational resources for solutions in multiple dimensions.

In the 1960's, Gelbard developed an ad-hoc multidimensional extension of the simple single dimension planar P_N equations that created a system of coupled, diffusion-like equations known as the simplified P_N (SP_N) equations. Up until around the 1990's, the SP_N method was either widely unknown, widely unused, or combination of both even though numerical studies showed promising results with better solutions than diffusion theory and a significant reduction in computational time over more accurate methods such as discrete ordinates. Why did this happen? A significant problem, pointed out by Brantley and Larsen [2], was that little rigor had been applied to the formulation of the SP_N equations since their derivation through primarily heuristic arguments. Instead, studies at that time focused on simply comparing the results of the method to other contemporary transport solution strategies. In addition, many problems of interest from the literature at the time were either solved using nodal-type methods for reactor-sized problems or S_N-type methods for benchmark problems with intricate material configurations and potentially large flux gradients over small spatial domains.

So why reconsider the SP_N equations? Starting in the 1990's and primarily due to Larsen and his colleagues, the SP_N equations have been given a more rigorous treatment in many forms with both variational and asymptotic derivations performed as a means of verification [99]. In addition, these equations have been more rigorously studied as solution methods to MOX fuel problems and have been shown to provide accurate solutions [2]. With this mathematical literature to provide a solid numerical footing for the method, we look at its application to today's challenge problems in neutron transport for fission reactor analysis. The reduction in numerical complexity compared to current deterministic solution methods

using the S_N approximation could mean significant savings in both compute time and memory required.

In order to leverage Monte Carlo Synthetic Acceleration as a solution technique for neutron transport problems, its current formulation requires the physics operator and all preconditioners to be explicitly formed. Recent developments in the Exnihilo neutronics package at Oak Ridge National Laboratory have permitted generation of the SP_N system of equations for detailed neutronics models of fission reactor-based systems [1]. By fully forming these equations and formulating them as a linear algebra problem instead of using the explicit iterative methods of the past, we now have access to all of the modern advancements in computational linear algebra including the use of Krylov solvers for asymmetric systems without the need to implement the action of the physics operator on a vector and easy application of algebraic preconditioning methods for improved convergence properties and time to solution.

This leads us to then research the applicability of Monte Carlo Synthetic Acceleration methods as a possible solution method for the SP_N equations. In addition, solving the SP_N equations in this way also breaks away from the S_N forms of parallelism where spatial parallelism is achieved by an efficient parallel sweep, angular efficiency achieved by pipe-lining, and energy parallelism achieved by decoupling the groups. With the SP_N equations as a full matrix system, we now can parallelize the problem as prescribed by the Monte Carlo algorithm, which may be significantly more scalable than current S_N transport practices. In this work we therefore apply Monte Carlo Synthetic Acceleration to the SP_N equations and research its applicability, performance, and convergence properties in the context of a light water reactor system.

1.1.2 Solutions for the Navier-Stokes Equations

Nonlinear transport problems are a common occurrence in single and multiple physics problems in nuclear engineering. Systems of partial differential equations, such as the Navier-Stokes

equations that describe fluid flow, yield discrete sets of stiff equations with nonlinearities present in the variables when discretized by conventional methods. These sets of equations characterize momentum and energy transport through diffusion, viscous forces and convection, and inertial forces. Traditionally, such systems have been solved by linearizing them in a form where the nonlinearities in the variables are eliminated and more traditional linear methods can be used for solutions. Often characterized as segregated methods where physics operators are split and their action on the system approximated in steps, such methods lack consistency and accuracy in resolving the nonlinear component of the solution. In the last 30 years, fully implicit nonlinear methods based on Newton's method have become more popular and many advances have been made in the nuclear engineering field to employ these methods.

In the context of solving standalone linear systems, Monte Carlo methods do not provide significant merit over subspace methods due to the fact that the physics operator must be explicitly formed. For many applications including higher fidelity neutron transport discretizations beyond the SP_N equations discussed in the previous section, such a requirement is prohibitive and perhaps not even feasible to implement. Therefore, a discrete Monte Carlo solution method is best suited for situations in which the operator is readily, if not naturally, formed. Modern nonlinear methods meet this requirement with Newton methods used in conjunction with Krylov methods operating on a fully formed matrix for a robust solution strategy. Furthermore, modern techniques exist that permit the automatic construction of the Jacobian operator generated within a Newton method based on the nonlinear residual evaluations, giving all of the components necessary for a Monte Carlo solver to provide value. We therefore devise a new nonlinear method in this work based on the Monte Carlo Synthetic Acceleration algorithm and Newton's method and research its properties, applicability, and performance in the context of fluid flow problems.

1.1.3 Domain Decomposed Monte Carlo Synthetic Acceleration

The computational resources required to solve the neutronics and fluid dynamics problems can be tremendous. Recent work in modeling coupled fluid flow and solid material heat and mass transfer in a reactor subsystem, similar to the same components of the departure from nucleate boiling example, was performed as part of analysis for the Department of Energy's Consortium for Advanced Simulation of Light Water Reactors (CASL) modeling and simulation hub. CASL used the Drekar multiphysics code developed at Sandia National Laboratories [46] for modeling goals in grid-to-rod-fretting analysis and will use a similar coupled physics structure for future departure from nucleate boiling analysis with comparison to experimental data. Using Drekar, multiphysics simulations have been performed with fully implicit methods for the solution of nonlinear systems using meshes of $O(1 \times 10^9)$ elements leveraging $O(100,000)$ cores on leadership class machines. Neutronics components to be implemented in CASL for multiphysics analysis, such as the Exnihilo radiation transport suite developed at Oak Ridge National Laboratory [89], compute trillions of unknowns for full core reactor analysis on $O(1 \times 10^9)$ element meshes and $O(100,000)$ cores as well. Given the large scale and complexity of these problems, if we aim to advance solution techniques in neutronics and fluid flow for reactor analysis, then we are motivated to advance the solution of complex physics problems exploiting leadership class levels of parallelism.

For Monte Carlo Synthetic Acceleration methods to be viable at the production scale for nuclear engineering applications, scalable parallel implementations of the algorithm are required. Reviewing the literature, Monte Carlo Synthetic Acceleration has yet to be parallelized and the Neumann-Ulam Monte Carlo method on which it is built has only been parallelized through history-level parallelism with full domain replication [5]. In order to solve large linear physics systems with Monte Carlo Synthetic Acceleration, a domain decomposed parallel strategy is required. In the formulation of a parallel Monte Carlo Synthetic Acceleration algorithm, we recognize that the algorithm occurs in two stages, an

initial step performing a fixed point iteration and a secondary step leveraging a Monte Carlo solver that is providing the acceleration. The parallel aspects of both these components must be considered. Therefore, in this work we will develop and implement parallel algorithms for the fundamental random walk sequence and Monte Carlo Synthetic Acceleration methods leveraging both the knowledge gained from the general parallel implementations of subspace methods reviewed in Appendix A and modern parallel strategies for domain decomposed Monte Carlo as developed by the reactor physics community.

1.2 Hardware-Based Motivation

As leadership class machines move beyond the petascale, new algorithms must be developed that leverage their strengths and adapt to their shortcomings. Basic research is required now to advance methods in time for these new machines to become operational. Organized work is already moving forward in this area with the Department of Energy's Advanced Scientific Computing Research office specifically allocating funding for the next several years to research resilient solver technologies for next generation facilities [31]. Based on the language in this call for proposals, we can identify key issues for which a set of robust, massively parallel Monte Carlo solvers could provide a solution. As machines begin to operate at hundreds of petaflops peak performance and beyond, trends toward reduced energy consumption will require incredibly high levels of concurrency to achieve the desired computation rates. Furthermore, this drop in power consumption will mean increased pressure on memory as memory per node is expected to stagnate while cores per node is expected to increase. As the number of cores increases, their clock speed is expected to stagnate or even decrease to further reduce power consumption and manufacturing costs.

The end result of these hardware changes is that the larger numbers of low-powered processors will be prone to both soft failures such as bit errors in floating point operations and hard failures where the data owned by that processor cannot be recovered. Because these

failures are predicted to be common, resilient solver technologies are required to overcome these events at the application level. With linear and nonlinear solution schemes based on Monte Carlo techniques, such issues are potentially alleviated by statistical arguments. In the case of soft failures, isolated floating point errors in Monte Carlo simulation are absorbed within tally statistics while completely losing hardware during a hard failure is manifested as a high variance event where some portion of the Monte Carlo histories are lost. These stochastic methods are a paradigm shift from current deterministic solver techniques that will in their current form potentially suffer greatly from the non-deterministic behavior expected from the next generation of machines.

In addition to resiliency concerns, the memory restrictions on future hardware will hinder modern solvers that derive their robustness from using large amounts of memory. Stochastic methods that are formulated to use less memory than conventional methods will serve to alleviate some of this pressure. New parallel strategies that may be implemented with stochastic methods could offer a new avenue for leveraging the expected levels of high concurrency in machines operating at hundreds of petaflops and beyond.

1.3 Research and Development Outline

For some time, the particle transport community has been utilizing Monte Carlo methods for the solution of transport problems [61]. The partial differential equation (PDE) community has focused on various deterministic methods for solutions to linear problems [56, 78]. In between these two areas are a not widely known group of Monte Carlo methods for solving sparse linear systems [79, 80, 81, 88]. In recent years, these methods have been further developed for radiation transport problems in the form of Monte Carlo Synthetic Acceleration (MCSA) [18, 75] but have yet to be applied to more general sparse linear systems commonly generated by the computational physics community. Compared to other methods in this regime, MCSA offers three attractive qualities; (1) the physics operator need not be symmetric

or positive-definite, (2) the stochastic nature of the solution method provides a natural solution to some aspects of the issue of resiliency, and (3) is amenable to parallelization using modern methods developed by the transport community [37]. The development of MCSA as a general solution technique and the development of a parallel MCSA method are new and unique features of this work, providing a framework with which other issues such as resiliency or performance may be addressed in the future.

In addition to advancements in the parallel solution of linear problems, nonlinear problems may also benefit from a general and parallel MCSA scheme. In the nuclear engineering community, nonlinear problems are often addressed by either linearizing the problem or building a segregated scheme and using traditionally iterative or direct methods to solve the resulting system [55]. In the mathematics community, various Newton methods have been popular [78]. Recently, Jacobian-Free Newton-Krylov (JFNK) schemes [91] have been utilized in multiple physics architectures and advanced single physics codes [86]. The benefits of JFNK schemes are that the Jacobian is never formed, simplifying the implementation, and a Krylov solver is leveraged (typically GMRES or a method based on Conjugate Gradient), providing excellent convergence properties for well-conditioned and well-scaled systems. However, there are two potential drawbacks to these methods for high fidelity predictive simulations: (1) the Jacobian is approximated by a first-order differencing method on the order of machine precision such that this error can grow beyond that of those in a fine-grained system [78] and (2) for systems that are not symmetric positive-definite (which will be the case for most multiphysics systems and certainly for most preconditioned systems) the Krylov subspace generated by the GMRES solver may become prohibitively large [65].

In this work, the Forward-Automated Newton-MCSA (FANM) method is developed as new nonlinear solution method. The key features of FANM are: full Jacobian generation using modern Forward Automated Differentiation (FAD) methods [23], and MCSA as the inner linear solver. This method has several attractive properties. First, the first-order approximation to the Jacobian used in JFNK type methods is eliminated by generating the

Jacobian explicitly with the model equations through FAD. Second, the Jacobian need not be explicitly formed by the user but is instead automated through FAD; this eliminates the complexity of hand-coding derivatives and has also been demonstrated to be more efficient computationally than evaluating difference derivatives. Third, unlike GMRES, MCSA does not build a subspace during iterations. Although the Jacobian must be explicitly formed to use MCSA, for problems that take more than a few GMRES iterations to converge the size of the Krylov subspace will typically grow beyond that of the Jacobian. Finally, using MCSA to solve the linear model provides its benefits of potential parallelism and iterative performance.

1.4   Statement of Work

The goal of this work is to improve the iterative performance and parallel scalability of solutions to discrete linear and nonlinear transport problems by researching and developing a new set of domain decomposed Monte Carlo Synthetic Acceleration methods. Improvements in iterative performance and parallel scalability will be demonstrated in a wide variety of numerical experiments using both simple model neutron transport problems and neutron transport and fluid flow problems generated by production physics codes in both simple and complex geometries.

1.5   Outline of the Document

To present the research and development required to meet the goals of this work this document is arranged in the following manner. First, in Chapter 2, the fundamentals of the Monte Carlo method for linear systems are presented. Using this background on Monte Carlo, synthetic acceleration methods are then presented and new analysis is provided using a simple model transport problem. Next, in Chapter 3, the Monte Carlo methods developed in Chapter 2 are applied to the neutron transport problem. Specifically, the SP_N form of the Boltzmann neutron transport equation is developed and solved using the Monte Carlo methods. Using

a difficult light water reactor fuel assembly criticality calculation to drive research and development for these Monte Carlo methods, several important issues regarding Monte Carlo solver applicability, performance, and preconditioning will be discussed along with solutions to these problems. Using these solutions, the Monte Carlo methods are then verified against modern solution techniques for the SP_N equations in order verify correctness for the fuel assembly criticality calculation. In Chapter 4, the Monte Carlo methods are applied to the Navier-Stokes equations as a model nonlinear fluid flow system. A new nonlinear solution technique is developed based on Newton's method and both verified against and compared to conventional solution techniques. In Chapter 5, the Monte Carlo methods are parallelized using modern reactor physics techniques for domain decomposed particle transport with a full parallel scaling analysis provided using a leadership-class computing facility. Finally, the work is summarized in Chapter 6 and topics of future work derived from the results of this research presented.

Chapter 2

Monte Carlo Synthetic Acceleration Methods

An alternative approach to approximate matrix inversion is to employ Monte Carlo methods that sample a distribution with an expectation value equivalent to that of the inverted operator. Such methods have been in existence for decades with the earliest reference noted here a manuscript published in 1950 by Forsythe and Leibler [88]. In their outline, Forsythe and Leibler in fact credit the creation of this technique to J. Von Neumann and S.M. Ulam some years earlier than its publication. In 1952 Wasow provided a more formal explanation of Von Neumann and Ulam's method [36] and Hammersley and Handscomb's 1964 monograph [79] and Spanier and Gelbard's 1969 book [30] present additional detail on this topic using a collection of references from the 1950's and early 1960's.

Following this work, Halton presented a residual Monte Carlo scheme that improved dramatically on the performance of these methods [81]. Recent work in this area has utilized these residual Monte Carlo methods in particle transport [94], giving accelerated convergence over traditional methods. As an expansion of Halton's work, Evans and others have leveraged these methods in a synthetic acceleration scheme that has been shown to be competitive with production Krylov methods for radiation transport problems and improve performance significantly over Halton's sequential method [75].

In this chapter, we will present the fundamentals of the Monte Carlo method for discrete linear systems. Both the forward and adjoint methods will be presented and analyzed including a brief variance analysis of several Monte Carlo estimators. The Sequential Monte Carlo method of Halton and Monte Carlo Synthetic Acceleration methods will then be

presented as a means of leveraging the basic Monte Carlo methods devised by Neumann and Ulam in an iterative refinement scheme that accelerates their convergence. Using these iterative schemes, a set of modest variance reduction techniques will be introduced and their effects along with other parameters of the algorithms on the Monte Carlo solutions explored using a simple model transport problem.

2.1 Preliminaries

We seek solutions of the general linear problem in the following form:

$$\mathbf{A}\mathbf{x} = \mathbf{b}\,, \tag{2.1}$$

where $\mathbf{A} \in \mathbb{R}^{N \times N}$ is a matrix operator such that $\mathbf{A} : \mathbb{R}^N \to \mathbb{R}^N$, $\mathbf{x} \in \mathbb{R}^N$ is the solution vector, and $\mathbf{b} \in \mathbb{R}^N$ is the forcing term. The solutions to Eq (2.1) will be generated by inverting $\mathbf{A}$ either directly or indirectly:

$$\mathbf{x} = \mathbf{A}^{-1}\mathbf{b}\,. \tag{2.2}$$

In addition we can define the residual:

$$\mathbf{r} = \mathbf{b} - \mathbf{A}\mathbf{x}\,, \tag{2.3}$$

such that an exact solution $\mathbf{x}$ has been found when $\mathbf{r} = \mathbf{0}$. From the statement in Eq (2.2) we can already place a restriction on $\mathbf{A}$ by requiring that it be *nonsingular*, meaning that we can in fact compute $\mathbf{A}^{-1}$. In this work we will focus our efforts on approximately inverting the operator through various means.

In a discussion of methods for solving linear systems, several mathematical tools are useful in characterizing the qualities of the linear system. Among the most useful are the

eigenvalues of the matrix, $\sigma(\mathbf{A})$. We find these by solving the eigenvalue problem:

$$\mathbf{Ax} = \lambda\mathbf{x}, \ \lambda \in \sigma(\mathbf{A}) \,. \tag{2.4}$$

By writing Eq (2.4) in a different form,

$$(\mathbf{A} - \lambda\mathbf{I})\mathbf{x} = 0 \,, \tag{2.5}$$

and demanding that non-trivial solutions for $\mathbf{x}$ exist, it is then required that $|\mathbf{A} - \lambda\mathbf{I}| = 0$. Expanding this determinant yields a characteristic polynomial in terms of λ with roots that form the set of eigenvalues, $\sigma(\mathbf{A})$. Each component of $\sigma(\mathbf{A})$ can then be used to solve Eq (2.5) for a particular permutation of $\mathbf{x}$. The set of all permutations form the *eigenvectors* of $\mathbf{A}$. A quantity of particular interest that is computable from the eigenvalues of a matrix $\mathbf{A}$ is the *spectral radius*, $\rho(\mathbf{A})$, defined by Saad [56] as:

$$\rho(\mathbf{A}) = \max_{\lambda\in\sigma(\mathbf{A})} |\lambda| \,, \tag{2.6}$$

which is the radius of the largest circle in the complex plane centered about the origin that encapsulates the entire eigenvalue spectrum of the operator.

2.2   Neumann-Ulam Method

We begin our discussion of Monte Carlo methods by seeking a solution to Eq (2.1). For a given linear operator $\mathbf{A}$, we can use diagonal splitting[1] similar to the stationary method in Eq (A.3) to define the *iteration matrix*, $\mathbf{H}$:

$$\mathbf{H} = \mathbf{I} - \mathbf{A} \,, \tag{2.7}$$

---

[1]It should be noted that non-diagonal splittings have been recently explored [35] and have the potential to improve efficiency. However, it was observed in this work that this type of splitting did not improve performance in the asymptotic limit of $\rho(\mathbf{H}) \to 1$ for non-trivial problems.

such that we are solving the system:

$$\mathbf{x} = \mathbf{Hx} + \mathbf{b} \,. \tag{2.8}$$

We can then form an alternative representation for $\mathbf{A}^{-1}$ by generating the *Neumann series*:

$$\mathbf{A}^{-1} = (\mathbf{I} - \mathbf{H})^{-1} = \sum_{k=0}^{\infty} \mathbf{H}^k \,, \tag{2.9}$$

which will converge if the spectral radius of $\mathbf{H}$ is less than 1. If we then apply this Neumann series to the right hand side of Eq (2.1) we acquire the solution to the linear problem:

$$\mathbf{A}^{-1}\mathbf{b} = \sum_{k=0}^{\infty} \mathbf{H}^k \mathbf{b} = \mathbf{x} \,. \tag{2.10}$$

An approximation of this summation by truncation will therefore lead to an approximation of the solution. If we expand the summation with a succession of matrix-vector multiply operations, we arrive at an alternative perspective of this summation by considering the ith component of the solution vector:

$$x_i = \sum_{k=0}^{\infty} \sum_{i_1}^{N} \sum_{i_2}^{N} \ldots \sum_{i_k}^{N} h_{i,i_1} h_{i_1,i_2} \ldots h_{i_{k-1},i_k} b_{i_k} \,, \tag{2.11}$$

which can interpreted as a series of transitions between states,

$$\nu = i \rightarrow i_1 \rightarrow \cdots \rightarrow i_{k-1} \rightarrow i_k \,, \tag{2.12}$$

in $\mathbf{H}$ where ν is interpreted as a particular random walk sequence permutation. We can generate these sequences of transitions through Monte Carlo random walks by assigning them both a probability and weight. As a reinterpretation of the iteration matrix, we then form

the *Neumann-Ulam decomposition* of $\mathbf{H}$:

$$\mathbf{H} = \mathbf{P} \circ \mathbf{W} \,, \tag{2.13}$$

where $\circ$ denotes the Hadamard product operation[2], $\mathbf{P}$ denotes the transition probability matrix, and $\mathbf{W}$ denotes the transition weight matrix. This decomposition, a generalization of Dimov's work [7], is an extension of the original Neumann-Ulam scheme in that now a weight cutoff can be used to terminate a random walk sequence and therefore truncate the Neumann series it is approximating. The formulation of $\mathbf{P}$ and $\mathbf{W}$ will be dependent on whether we choose a direct or adjoint Monte Carlo sequence to estimate the state transitions in Eq (2.11). In the direct method, we will use the provided linear operator $\mathbf{A}$ to form the Neumann Ulam decomposition while the adjoint method will use the adjoint linear operator ($\mathbf{A}^T$ for real-valued systems) to form the decomposition.

2.3 Direct Monte Carlo Method

In the context of matrix inversion, a direct (forward) method resembles an adjoint Monte Carlo method in the reactor physics community where the solution state is sampled and the source terms that contribute to it are assembled. To achieve this, we build the forward Neumann-Ulam decomposition per Dimov's approach by first choosing a probability matrix that is a row scaling of $\mathbf{H}$ such that its components are:

$$p_{ij} = \frac{|h_{ij}|}{\sum_j |h_{ij}|} \,. \tag{2.14}$$

From this, we then see that the probability of transitioning from a state i to a state j is implicitly linked to the original operator $\mathbf{A}$ in that those terms with large values, and therefore those that make the greatest contribution to the numerical solution, will be sampled with a

---

[2]The Hadamard product $\mathbf{A} = \mathbf{B} \circ \mathbf{C}$ is defined element-wise as $a_{ij} = b_{ij} c_{ij}$.

higher probability than smaller terms. In addition, the row scaling provides a normalization over the state to which we are transitioning such that $\sum_j p_{ij} = 1$, meaning that we sample the probabilities over the rows of the matrix. The components of the weight matrix are then defined by Eq (2.13) as:

$$w_{ij} = \frac{h_{ij}}{p_{ij}} \, . \tag{2.15}$$

It should be noted here that if $\mathbf{A}$ is sparse, then $\mathbf{H}$, $\mathbf{P}$, and $\mathbf{W}$ must be sparse as well by definition. Additionally, we only compute $\mathbf{P}$ and $\mathbf{W}$ from the non-zero elements of $\mathbf{H}$ as those components that are zero will not participate in the random walk and thus produce identical sparsity patterns for all matrices.

Using these matrices, we can then form the expectation value of the forward solution. For a given random walk permutation ν, we define the weight of that permutation on the mth step to be:

$$W_m = W_0 w_{i_0,i_1} w_{i_1,i_2} \cdots w_{i_{m-1},i_m} \, , \tag{2.16}$$

such that the weight of each transition event contributes to the total through multiplication with $W_0 = 1$ as the starting weight. The contribution to the solution from a particular random walk permutation with k total events is then the *forward estimator*:

$$X_{i_0=i}(\nu) = \sum_{m=0}^{k} W_m b_{i_m} \, , \tag{2.17}$$

where $X_{i_0=i}(\nu)$ signifies that the solution state, i_0, in which the random walk ν started is also the state, i, in which we are tallying. We then define the probability that a particular random walk permutation of k events will occur:

$$P_\nu = P_{i_0=i} p_{i,i_1} p_{i_1,i_2} \cdots p_{i_{k-1},i_k} \, , \tag{2.18}$$

with $P_{i_0=i} = 1$ for the direct method. Finally, we define the expectation value of X to be the

collection of all random walk permutations and their probabilities:

$$E\{X_i\} = \sum_{\nu} P_{\nu} X_i(\nu) \, , \tag{2.19}$$

which, if expanded, directly recovers the exact solution by forming the Neumann series:

$$E\{X_i\} = \sum_{k=0}^{\infty} \sum_{i_1}^{N} \sum_{i_2}^{N} \ldots \sum_{i_k}^{N} p_{i,i_1} p_{i_1,i_2} \ldots p_{i_{k-1},i_k} w_{i,i_1} w_{i_1,i_2} \ldots w_{i_{k-1},i_k} b_{i_k}$$
$$= x_i \, , \tag{2.20}$$

therefore providing an unbiased Monte Carlo estimator.

In cases where we seek only approximate solutions, we need only to perform a predetermined number of random walks in order to generate an approximation for **x**. If we are only to approximate the solution, we also need conditions by which we may terminate a random walk as the Neumann Ulam decomposition defined by Eqs (2.14) and (2.15) will create a random walk weight in Eq (2.16) that approaches, but never reaches zero. We do this by noticing that if the problem is convergent, the factors added to Eq (2.16) will make W_m become diminishingly small due to their definition in Eq (2.15) and therefore the contribution of the history to the solution estimate will become negligible. Using this, we choose terminate a random walk sequence with a *weight cutoff*, W_c, that is enforced when $W_m < W_c$ for a particular random walk permutation.

2.3.1 Forward Estimator Variance

We can compute the variance of the forward estimator through traditional methods by defining the variance, σ_i, for each component in the solution:

$$\sigma_i^2 = E\{X_i - (\mathbf{A}^{-1}\mathbf{b})_i\}^2 = E\{X_i^2\} - x_i^2 \, , \tag{2.21}$$

where the vector exponentials are computed element-wise. Inserting Eq (2.19) gives:

$$\sigma_i^2 = \sum_\nu P_\nu X_i(\nu)^2 - x_i^2 \, , \tag{2.22}$$

and applying Eq (2.17) and expanding the square of the summation:

$$\sigma_i^2 = \sum_\nu P_\nu \left(\sum_{m=0}^{k} \left[W_m^2 b_{i_m}^2 + 2 \sum_{j=0}^{m-1} W_m W_j b_{i_m} b_{i_j} \right] \right) - x_i^2 \, . \tag{2.23}$$

We can distribute the random walk probability to yield an expanded form of the variance:

$$\sigma_i^2 = \sum_\nu P_\nu \sum_{m=0}^{k} W_m^2 b_{i_m}^2 + 2 \sum_\nu P_\nu \sum_{m=0}^{k} \sum_{j=0}^{m-1} W_m W_j b_{i_m} b_{i_j} - x_i^2 \, . \tag{2.24}$$

In particular, we will isolate the first term of the variance by expanding it:

$$\sum_\nu P_\nu \sum_{m=0}^{k} W_m^2 b_{i_m}^2 = \sum_{k=0}^{\infty} \sum_{i_1}^{N} \sum_{i_2}^{N} \cdots \sum_{i_k}^{N} p_{i,i_1} p_{i_1,i_2} \cdots p_{i_{k-1},i_k} w_{i,i_1}^2 w_{i_1,i_2}^2 \cdots w_{i_{k-1},i_k}^2 b_{i_k}^2 \, . \tag{2.25}$$

Using this expansion, we can arrive at a more natural reason for enforcing $\rho(\mathbf{H}) < 1$ for our Monte Carlo method to converge. Per the Hadamard product, we can concatenate the summation in Eq (2.25):

$$(\mathbf{P} \circ \mathbf{W} \circ \mathbf{W})^k = \sum_{k=0}^{\infty} \sum_{i_1}^{N} \sum_{i_2}^{N} \cdots \sum_{i_k}^{N} p_{i,i_1} p_{i_1,i_2} \cdots p_{i_{k-1},i_k} w_{i,i_1}^2 w_{i_1,i_2}^2 \cdots w_{i_{k-1},i_k}^2 \, . \tag{2.26}$$

If we assign $\mathbf{G} = \mathbf{P} \circ \mathbf{W} \circ \mathbf{W}$ as in Eq (2.13), we then have:

$$(\mathbf{P} \circ \mathbf{W} \circ \mathbf{W})^k = \sum_{k=0}^{\infty} \sum_{i_1}^{N} \sum_{i_2}^{N} \cdots \sum_{i_k}^{N} g_{i,i_1} g_{i_1,i_2} \cdots g_{i_{k-1},i_k} \, , \tag{2.27}$$

which is the general Neumann series for $\mathbf{G}$,

$$\mathbf{T} = \sum_{k=0}^{\infty} \mathbf{G}^k \, , \tag{2.28}$$

where $\mathbf{T} = (\mathbf{I} - \mathbf{G})^{-1}$. We can then insert T back into the variance formulation for a more concise definition:

$$\sigma_i^2 = (\mathbf{Tb}^2)_i + 2 \sum_\nu P_\nu \sum_{m=0}^k \sum_{j=0}^{m-1} W_m W_j b_{i_m} b_{i_j} - x_i^2 \,. \tag{2.29}$$

We can relate $\mathbf{G}$ to $\mathbf{H}$ by noting that $\mathbf{G}$ simply contains an additional Hadamard product with the weight matrix. The Hadamard product has the property that:

$$|\mathbf{H} \circ \mathbf{W}| \geq |\mathbf{H}|\,|\mathbf{W}| \,. \tag{2.30}$$

Using the norm property of the Hadamard product and Eq (2.13), we can define the norm of $\mathbf{W}$ as:

$$\frac{|\mathbf{H}|}{|\mathbf{P}|} \geq |\mathbf{W}| \,. \tag{2.31}$$

Choosing the infinity norm of the operator, the row normalized probability matrix will yield a norm of 1 giving the following inequality for relating $\mathbf{G}$ and $\mathbf{H}$:

$$|\mathbf{G}| \geq |\mathbf{H}|^2 \tag{2.32}$$

Using these relations to analyze Eq (2.29), we see that if $\rho(\mathbf{G}) > 1$, then the first sum in Eq (2.28) will not converge and an infinite variance will arise as the elements of $\mathbf{T}$ become infinite in Eq (2.29). We must restrict $\mathbf{G}$ to alleviate this and therefore restrict $\mathbf{H}$ due to Eq (2.32) with $\rho(\mathbf{H}) < 1$ so that our expectation values for the solution may have a finite variance.

2.3.2 Direct Method: Evolution of a Solution

As a means of visually demonstrating the direct Monte Carlo method, consider a 2-dimensional thermal diffusion problem with sources on the left and right hand sides of the domain and a
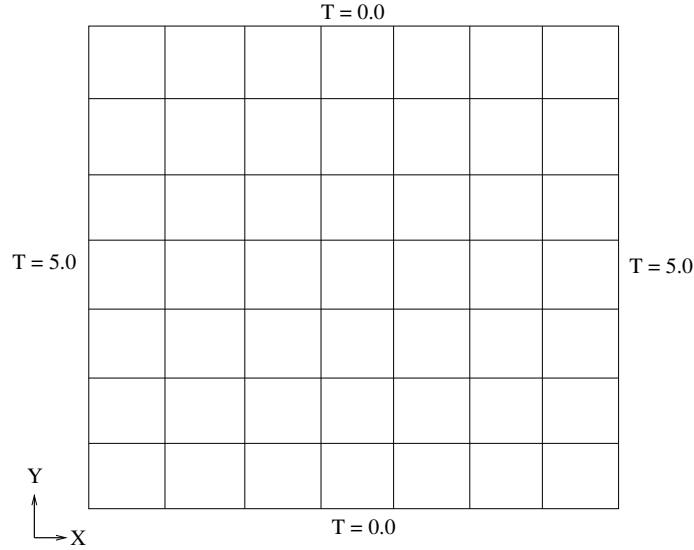
Figure 2.1: **Problem setup for 2D heat equation.** *Dirichlet conditions are set for the temperature on all 4 boundaries of the Cartesian grid. Background source of 1/5 the value of the boundary sources present.* 50×50 *grid.*

uniform source throughout the domain of $1/5$ the strength of the boundary sources as shown in Figure 2.1. For this problem, the number of histories used to compute the solution at each grid point (state) in the domain was increased from 1 to 1000 in order to demonstrate the effects on the solution and the statistical nature of the method. Figure 2.2 gives these results. As the number of histories used per state is increased, the statistical variance of the solutions is decreased as more tallies are made. Starting with a single history at each state in the domain, the high variance prevents a precise solution from being obtained although we begin to see the solution take shape as expected. It is interesting to note here that as the statistical uncertainty is reduced at each grid point in the domain, the solution is resolved in a certain sense, analogous to the convergence of a traditional iterative method.
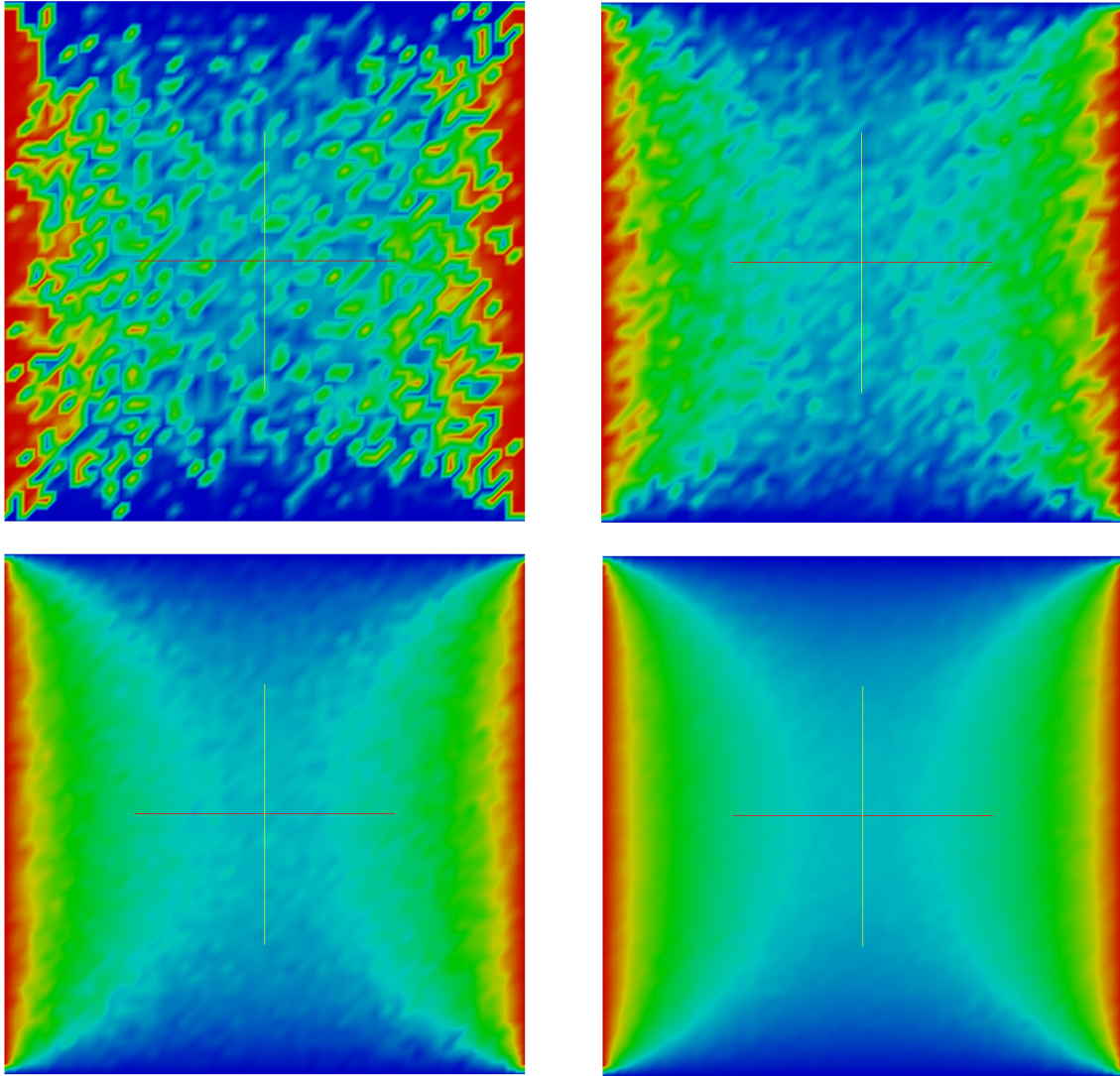
Figure 2.2: **Direct Monte Carlo solution to the heat equation with varying numbers of histories.** *Top left: 1 history per state. Top right: 10 histories per state. Bottom left: 100 histories per state. Bottom right: 1000 histories per state.*

2.4 Adjoint Monte Carlo Method

Often a more useful form, an alternative to forward Monte Carlo matrix inversion is the adjoint method. We begin by defining the linear system adjoint to Eq (2.1):

$$\mathbf{A}^T\mathbf{y} = \mathbf{d}\,, \tag{2.33}$$

where $\mathbf{y}$ and $\mathbf{d}$ are the adjoint solution and source vectors respectively and $\mathbf{A}^T$ is the adjoint operator for $\mathbf{A} \in \mathbb{R}^{N \times N}$. We can split this equation to mirror Eq (2.8):

$$\mathbf{y} = \mathbf{H}^T\mathbf{y} + \mathbf{d}\,. \tag{2.34}$$

As was required for convergence with the direct method using Eq (2.8), the spectral radius of $\mathbf{H}$ must remain less than 1 as $\mathbf{H}^T$ contains the same eigenvalues and therefore has the same spectral radius. By defining the following inner product equivalence [30]:

$$\langle \mathbf{A}^T\mathbf{y}, \mathbf{x} \rangle = \langle \mathbf{y}, \mathbf{A}\mathbf{x} \rangle\,. \tag{2.35}$$

it follows that:

$$\langle \mathbf{x}, \mathbf{d} \rangle = \langle \mathbf{y}, \mathbf{b} \rangle\,. \tag{2.36}$$

Using these definitions, we can derive an estimator from the adjoint method that will also give the solution vector, $\mathbf{x}$. As with the direct method, we can acquire the adjoint solution by forming the Neumann series by writing Eq (2.34) as:

$$\mathbf{y} = (\mathbf{I} - \mathbf{H}^T)^{-1}\mathbf{d}\,, \tag{2.37}$$

which in turn yields the Neumann series using the adjoint operator:

$$\mathbf{y} = \sum_{k=0}^{\infty} (\mathbf{H}^T)^k \mathbf{d} \,. \tag{2.38}$$

We expand this summation to again yield a series of transitions that can be approximated by a Monte Carlo random walk sequence, this time forming the Neumann series in reverse order:

$$y_i = \sum_{k=0}^{\infty} \sum_{i_1}^{N} \sum_{i_2}^{N} \cdots \sum_{i_k}^{N} h_{i_k,i_{k-1}} \cdots h_{i_2,i_1} h_{i_1,i} d_{i_k} \,. \tag{2.39}$$

We can readily build an estimator for the adjoint solution from this series expansion, but we instead desire the solution to Eq (2.1). Here we have 2 unknowns, $\mathbf{y}$ and $\mathbf{d}$, and therefore we require two constraints to close the system. We use Eq (2.36) as the first constraint and as a second constraint we select:

$$\mathbf{d} = \boldsymbol{\delta}_j \,, \tag{2.40}$$

where $\boldsymbol{\delta}_j$ is one of a set of vectors in which the jth component is the Kronecker delta function $\delta_{i,j}$. If we apply Eq (2.40) to our first constraint Eq (2.36), we get the following convenient outcome:

$$\langle \mathbf{y}, \mathbf{b} \rangle = \langle \mathbf{x}, \boldsymbol{\delta}_j \rangle = x_j \,, \tag{2.41}$$

meaning that if we compute the inner product of the original source and the adjoint solution using a delta function source, we recover one component of the original solution.

In terms of radiation transport, this adjoint method is equivalent to a traditional forward method where the initial state i_0 of the random walk is determined by sampling the source vector $\mathbf{b}$ with probabilities:

$$P_{i_0=i}(\nu) = \frac{|b_i|}{||\mathbf{b}||_1} \,, \tag{2.42}$$

with a random walk starting weight of:

$$W_0 = ||\mathbf{b}||_1 \frac{b_i}{|b_i|} \, , \tag{2.43}$$

which gives the additional useful relation:

$$b_{i_0} = W_0 P_{i_0 = i} \, . \tag{2.44}$$

As a result of using the adjoint system, we modify our probabilities and weights using the *adjoint Neumann-Ulam decomposition* of $\mathbf{H}$:

$$\mathbf{H}^T = \mathbf{P} \circ \mathbf{W} \, , \tag{2.45}$$

where now we are forming the decomposition with respect to the transpose of $\mathbf{H}$. We then follow the same procedure as the direct method for forming the probability and weight matrices in the decomposition. Using the adjoint form, probabilities should instead be column-scaled:

$$p_{ij} = \frac{|h_{ji}|}{\sum_j |h_{ji}|} \, , \tag{2.46}$$

such that we expect to select a new state, j, from the current state in the random walk, i, by sampling column-wise (or row-wise if an adjoint probability matrix is formed). Per Eq (2.45), the transition weight is then defined as:

$$w_{ij} = \frac{h_{ji}}{p_{ij}} \, . \tag{2.47}$$

Using the decomposition we can then define an expectation value for the adjoint method. Given Eq (2.16) as the weight generated for a particular random walk permutation as in Eq (2.12) and our result from Eq (2.41) generated by applying the adjoint constraints, the contribution to the solution in state j from a particular random walk permutation of k events

is then the *collision estimator*:

$$X_j(\nu) = \sum_{m=0}^{k} W_m \delta_{i_m,j} \,, \tag{2.48}$$

where the Kronecker delta indicates that the tally contributes only in the current state, i_m, of the random walk. Note here that the estimator in Eq (2.48) does not have a dependency on the source state as in Eq (2.17), providing a remedy for the situation in the direct method where we must start a random walk in each source state for every permutation if we want to compute a solution estimate for that state. In the adjoint method, we instead tally in all states and those of lesser importance will not be visited as frequently by the random walk. Finally, the expectation value using all permutations is:

$$E\{X_j\} = \sum_{\nu} P_\nu X_j(\nu) \tag{2.49}$$

which, if expanded in the same way as the direct method and utilizing Eq (2.44) to insert the source term, directly recovers the exact solution:

$$
\begin{aligned}
E\{X_j\} &= \sum_{k=0}^{\infty} \sum_{i_1}^{N} \sum_{i_2}^{N} \ldots \sum_{i_k}^{N} b_{i_0} h_{i_0,i_1} h_{i_1,i_2} \ldots h_{i_{k-1},i_k} \delta_{i_k,j} \\
&= x_j \,,
\end{aligned}
\tag{2.50}
$$

therefore, also providing an unbiased Monte Carlo estimate of the solution. Note that this expansion produces the effective sequence of matrix-vector multiplications with the b_{i_0} component of the source vector which will be selected at random for each walk permutation and the unbiasedness of the estimator relies on an unbiased sampling of the source. It should also be noted here that Eq (2.50) only computes a single component of our desired solution vector when really what we desire is the entire solution vector. In an adjoint Monte Carlo simulation using this estimator, the w_{ij} elements that are added into the tally for each state are only selected if/when the random walk currently resides in that state. Much like a mesh

tally in a particle transport simulation, we have N simultaneous tallies for $\mathbf{A} \in \mathbb{R}^{N \times N}$ that will yield the entire solution vector.

Like the direct method, we also desire a criteria for random walk termination for problems where only an approximate solution is necessary. For the adjoint method, we utilize a *relative weight cutoff*:

$$W_f = W_c b_{i_0} \,, \tag{2.51}$$

where W_c is defined as in the direct method. The adjoint random walk will then be terminated after m steps if $W_m < W_f$ as tally contributions become increasingly small.

2.4.1   Collision Estimator Variance

We can compute the variance of the collision estimator in the same way as the direct estimator for each component in the solution where now:

$$\sigma_j^2 = \sum_\nu P_\nu \sum_{m=0}^{k} W_m^2 \delta_{i_m,j} + 2 \sum_\nu P_\nu \sum_{m=0}^{k} \sum_{l=0}^{m-1} W_m W_l \delta_{i_m,j} \delta_{i_l,j} - x_j^2 \,. \tag{2.52}$$

In this case, in the second summation $m \neq l$ for all states due to the form of the summation and therefore the combination of delta functions, $\delta_{i_m,j}$ of $\delta_{i_l,j}$, will only be nonzero for random walks that are in the current solution state (when $i_m = i_l = j$) and other states visited do not contribute to the variance of the current state (when $i_m \neq i_l$). This is important as it shows a decoupling of the variance among the solution vector states, meaning that the variance in solution state i does not depend on the variance in solution state j.

Expanding the transition probabilities in the first sum again yields a Neumann series in the same form as that explored for the forward estimator, this time with the terms in reverse

order and the introduction of the Kronecker delta:

$$\sigma_j^2 = \sum_{k=0}^{\infty} \sum_{i_1}^{N} \sum_{i_2}^{N} \cdots \sum_{i_k}^{N} p_{i_k,i_{k-1}} \cdots p_{i_2,i_1} p_{i_1,i_0} w_{i_k,i_{k-1}}^2 \cdots w_{i_2,i_1}^2 w_{i_1,i_0}^2 b_{i_0}^2 \delta_{i_k,j} +$$

$$2 \sum_{\nu} P_{\nu} \sum_{m=0}^{k} \sum_{l=0}^{m-1} W_m W_l \delta_{i_m,j} \delta_{i_l,j} - x_j^2 . \quad (2.53)$$

If we again define $\mathbf{G} = \mathbf{P} \circ \mathbf{W} \circ \mathbf{W}$, we then have:

$$\sigma_j^2 = \sum_{k=0}^{\infty} \sum_{i_1}^{N} \sum_{i_2}^{N} \cdots \sum_{i_k}^{N} g_{i_k,i_{k-1}} \cdots g_{i_2,i_1} g_{i_1,i_0} b_{i_0} \delta_{i_k,j} +$$

$$2 \sum_{\nu} P_{\nu} \sum_{m=0}^{k} \sum_{l=0}^{m-1} W_m W_l \delta_{i_m,j} \delta_{i_l,j} - x_j^2 , \quad (2.54)$$

where now $\mathbf{G}$ in this case is the transpose of that used in Eq (2.27). The Kronecker delta again implies that the variance contribution from each random walk will only be in its current state and for many random walks, many starting weights of b_{i_0} will contribute to the variance in the same way as they contribute to the solution tally. As the transpose is formed and the Neumann series of $\mathbf{G}$ is in reverse order in Eq (2.54) relative to its formulation in the forward estimator, then Eq (2.54) and Eq (2.27) are equivalent and therefore the collision estimator is bound by the same restrictions on $\rho(\mathbf{G})$ and $\rho(\mathbf{H})$ to ensure that the variance is finite.

2.4.2 Expected Value Estimator

In addition to the collision estimator, an additional estimator is available due to the work of Okten [45] that uses the method of expected values as a means to improve the Monte Carlo estimate. As outlined by Spanier and Gelbard [30], the method of expected values is a deterministic averaging of events that may potentially occur in the Monte Carlo random walk sequence. Okten applied this principle directly to discrete Monte Carlo by forming the

expected value estimator for a random walk of k events:

$$X_j(\nu) = b_j + \sum_{m=0}^{k} W_m h_{j,i_m} \qquad (2.55)$$

where now the contribution of the iteration matrix is deterministically averaged at step m over all potential states j that may be reached from the current state i_m. Via Okten, the estimator can be shown to be unbiased through a comparison to the collision estimator. We can first rewrite the summation in Eq (2.55):

$$X_j(\nu) = b_j + \sum_{m=0}^{k} \sum_{i=1}^{N} W_m \delta_{i_m,i} h_{ji} \qquad (2.56)$$

where N is the number of states in the system. Immediately, we see the collision estimator as defined by Eq (2.48) and can therefore write the expectation value as:

$$E\{X_j\} = b_j + \sum_{i=1}^{N} E\{X_i\} h_{ji} \qquad (2.57)$$

which is equivalently is the jth component of Eq (2.8):

$$E\{X_j\} = b_j + \sum_{i=1}^{N} x_i h_{ji} \qquad (2.58)$$

and is therefore an unbiased estimate. Compared to the collision estimator, the expected value estimator provides additional information at every step of the random walk, yielding potentially better statistics with the same amount of transport work. Conveniently, even if no Monte Carlo histories are computed, the expected value estimator still deterministically computes the first term of the Neumann Series, $\mathbf{H^0 b}$, whereas the collision estimator will provide no information.

2.4.2.1 Expected Value Estimator Variance

Following the collision estimator variance, the expected value estimator variance is given as:

$$\sigma_j^2 = \sum_\nu P_\nu b_j^2 + 2 \sum_\nu P_\nu b_j \sum_{m=0}^{k} W_m h_{j,i_m} +$$

$$\sum_\nu P_\nu \sum_{m=0}^{k} W_m^2 h_{j,i_m}^2 + 2 \sum_\nu P_\nu \sum_{m=0}^{k} \sum_{l=0}^{m-1} W_m W_l h_{j,i_m} h_{j,i_l} - x_j^2 . \quad (2.59)$$

As the delta functions are no longer present, the final summation in Eq (2.59) contains contributions for all valid state combinations in the same row of the iteration matrix and therefore the variance of each state in the solution tally is coupled to a group of other states as defined by the sparsity pattern of the iteration matrix. This coupling of variances is expected due to the deterministic averaging used to generate the expected value estimator.

2.4.3 Adjoint Method: Evolution of a Solution

As a means of visually demonstrating the adjoint Monte Carlo method, again consider the 2-dimensional thermal diffusion problem with sources on the left and right hand sides of the domain and a smaller uniform source as shown in Figure 2.1. Using the adjoint method with the collision estimator, the number of histories sampled from the source was increased from 10 to 10,000,000 in order to show its effects on the solution and the statistical nature of the method. Figure 2.3 gives these results. As the number of histories used per state (or DOF) is increased, the statistical variance of the solutions is decreased as more tally contributions are made. At 10,000,000 histories per state, enough information has been tallied to generate a reasonable estimate for the structure of the solution. The visual difference between Figures 2.2 and 2.3 is precisely that determined by their mathematics. As the adjoint solution evolves with the addition of histories, more histories emanate from the boundary the smaller uniform source in the domain with more penetrating from the boundary into the domain and making contributions to the tallies in those states as they are transported.
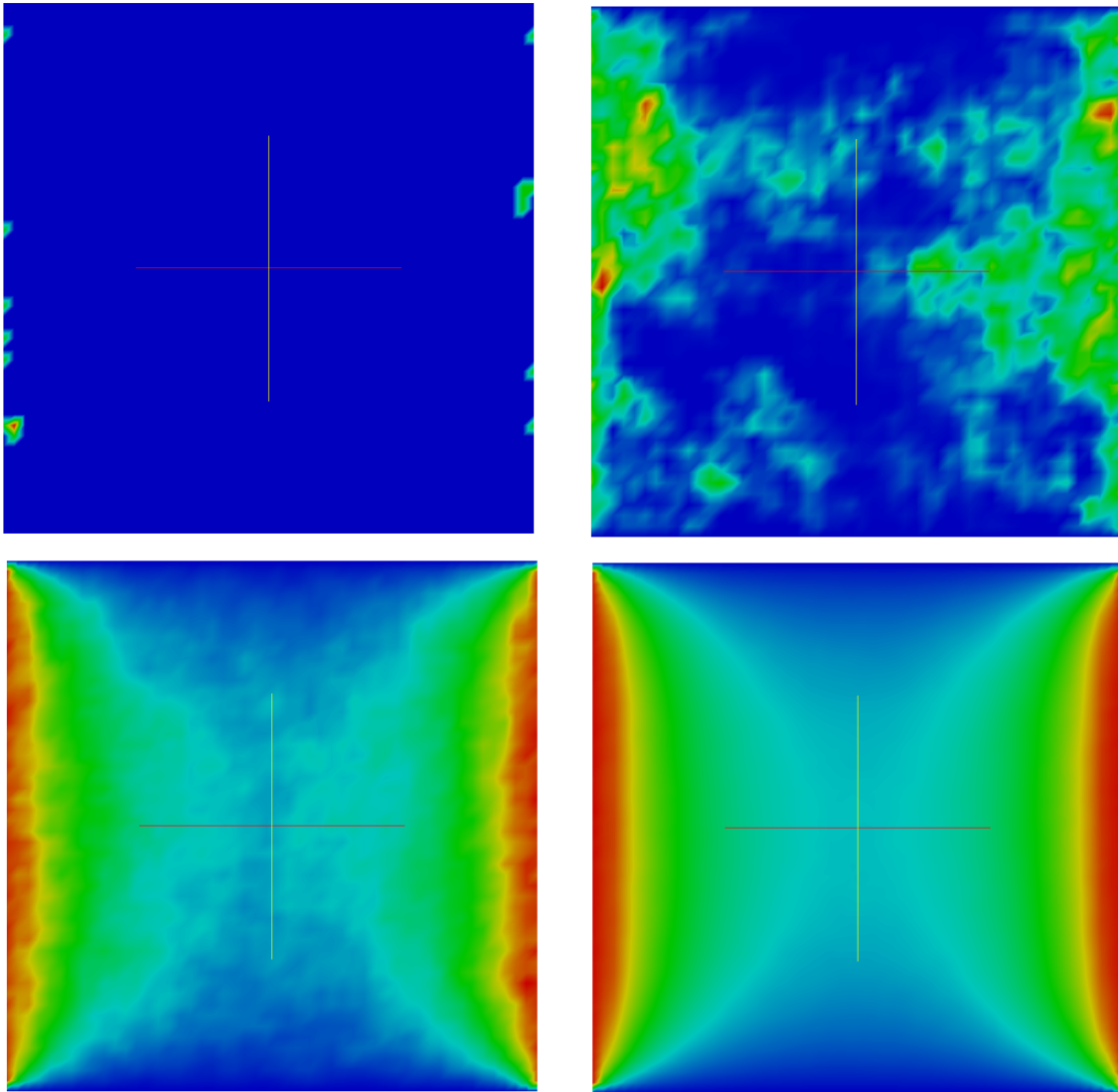
Figure 2.3: **Adjoint Monte Carlo solution to the heat equation with varying numbers of histories.** *Top left: 10 histories per state. Top right: 1,000 histories per state. Bottom left: 100,000 histories per state. Bottom right: 10,000,000 histories per state.*

2.5   Sequential Monte Carlo

The direct and adjoint Neumann-Ulam methods described are limited by a convergence rate of $1/\sqrt{N}$ by the Central Limit Theorem where N is the number of random walk permutations. In 1962, Halton presented a residual Monte Carlo method that moves towards exponential convergence rates [81] and further refined his work some years later [80]. Applications of his work by the transport community have confirmed convergence rates on the order of of e^{-N} [94]. In much the same way as the projection methods outlined in Appendix A, Halton's method, sequential Monte Carlo, utilizes the adjoint Monte Carlo solver as a means of directly reducing the elements residual vector. He proposed the following iterative scheme as a solution to Eq (2.1)

$$\mathbf{r}^k = \mathbf{b} - \mathbf{A}\mathbf{x}^k \,, \tag{2.60a}$$

$$\mathbf{A}\boldsymbol{\delta}^k = \mathbf{r}^k \,, \tag{2.60b}$$

$$\mathbf{x}^{k+1} = \mathbf{x}^k + \boldsymbol{\delta}^k \,, \tag{2.60c}$$

where the correction $\boldsymbol{\delta}^k$ is computed by the adjoint Monte Carlo method at each iteration. The merits of Halton's approach are immediately visible in that we have now broken the binding of the convergence rate to the Central Limit Theorem. Here, the Monte Carlo solver is used to produce a correction from the residual, analogous to using the residual to extract a correction from the search subspace in a projection method. By doing this, the Monte Carlo error is bound in the correction used to update the solution and therefore does not explicitly manifest itself in the overall convergence of the solution. The downside of such a method is that if the solution guess is poor, then many iterations are required in order to reach exponential converge as the Monte Carlo error (and therefore the Central Limit Theorem) does dominate in this situation.

2.6 Monte Carlo Synthetic Acceleration

Using the ideas of Halton, Evans and Mosher recently developed a Monte Carlo solution method that was not prohibited severely by the quality of the initial guess for the system [18] and later applied it more rigorously as a solution mechanism for the radiation diffusion equation [75]. With their new methods, they achieved numerical results identical to conventional Krylov solvers as well as comparable performance in both number of iterations and CPU time. Their approach was instead to use residual Monte Carlo as a synthetic acceleration for a stationary method. To derive this method, we begin by splitting the operator in Eq (2.1)

$$\mathbf{x} = (\mathbf{I} - \mathbf{A})\mathbf{x} + \mathbf{b} \,. \tag{2.61}$$

With this we can then define the stationary method *Richardson's iteration* as:

$$\mathbf{x}^{k+1} = (\mathbf{I} - \mathbf{A})\mathbf{x}^k + \mathbf{b} \,, \tag{2.62}$$

which will converge if $\rho(\mathbf{I} - \mathbf{A}) < 1$. We then define the solution error at the kth iterate relative to the true solution:

$$\delta\mathbf{x}^k = \mathbf{x} - \mathbf{x}^k \,. \tag{2.63}$$

Subtracting Eq (2.62) from Eq (2.61) we get:

$$\delta\mathbf{x}^{k+1} = (\mathbf{I} - \mathbf{A})\delta\mathbf{x}^k \,. \tag{2.64}$$

Subtracting from this $(\mathbf{I} - \mathbf{A})\delta\mathbf{x}^{k+1}$ yields:

$$\begin{aligned} \mathbf{A}\delta\mathbf{x}^{k+1} &= (\mathbf{I} - \mathbf{A})(\mathbf{x}^{k+1} - \mathbf{x}^k) \\ &= \mathbf{r}^{k+1} \,. \end{aligned} \tag{2.65}$$

Using this, we define the following scheme that will converge in one iteration if $\mathbf{A}$ is inverted exactly:

$$\mathbf{x}^{k+1} = (\mathbf{I} - \mathbf{A})\mathbf{x}^k + \mathbf{b} \,, \tag{2.66a}$$

$$\mathbf{A}\delta\mathbf{x}^{k+1} = \mathbf{r}^{k+1} \,, \tag{2.66b}$$

$$\mathbf{x} = \mathbf{x}^{k+1} + \delta\mathbf{x}^{k+1} \,. \tag{2.66c}$$

However, $\mathbf{A}$ is only approximately inverted by our numerical methods and therefore we instead pose an iterative scheme in which the Monte Carlo solvers are used to invert the operator. The *Fixed-Point Monte Carlo Synthetic Acceleration* (MCSA) method is defined as:

$$\mathbf{x}^{k+1/2} = \mathbf{x}^k + \mathbf{r}^k \,, \tag{2.67a}$$

$$\mathbf{r}^{k+1/2} = \mathbf{b} - \mathbf{A}\mathbf{x}^{k+1/2} \,, \tag{2.67b}$$

$$\mathbf{A}\delta\mathbf{x}^{k+1/2} = \mathbf{r}^{k+1/2} \,, \tag{2.67c}$$

$$\mathbf{x}^{k+1} = \mathbf{x}^{k+1/2} + \delta\mathbf{x}^{k+1/2} \,, \tag{2.67d}$$

$$\mathbf{r}^{k+1} = \mathbf{b} - \mathbf{A}\mathbf{x}^{k+1} \,, \tag{2.67e}$$

where a Neumann-Ulam Monte Carlo method is used to generate the solution correction from the residual and Richardson's iteration in the first step has been rewritten as a residual correction. Using Monte Carlo in this way achieves the same effect as Halton's method, decoupling its convergence rate from the overall convergence rate of the method. Here, the approximate Monte Carlo solution is not driven to a particular convergence as it merely supplies a correction for the initial guess generated by Richardson's iteration. Rather, only a set number of histories are required using the Neumann-Ulam method to generate the correction. In addition, the fact that the scheme in Eq (2.66) will converge in one iteration if $\mathbf{A}$ is inverted exactly means that as more and more stochastic histories are used to compute

the correction and the error is reduced towards zero, the number of iterations required for MCSA to converge should decrease accordingly, thus accelerating the solution.

In addition to the Monte Carlo solver parameters dictating the number of histories and weight cutoff, the outer MCSA iterations also have the following stopping criteria:

$$||\mathbf{r}||_\infty < \epsilon\, ||\mathbf{b}||_\infty \,, \tag{2.68}$$

where ϵ is a user-defined parameter. As with any iterative method, other stopping criteria using other vector norms could be computed, however, for this work we will only use Eq (2.68). We therefore have 3 parameters to tune in an MCSA implementation: the number of Monte Carlo histories computed in the Neumann-Ulam solve during each MCSA iteration, the weight cutoff for those histories, and the total MCSA convergence tolerance as specified by ϵ.

2.6.1   Alternative Fixed Point Iterations

In addition to the basic Richardson iteration, the MCSA algorithm presented in Eq (2.67) can be used to accelerate any fixed point iteration which only depends on the state (typically the residual) of the last iteration. As outlined in Appendix A, subspace methods take on a general form using the Petrov-Galerkin conditions as constraints for extracting a correction from the search subspace as given by Eq (A.16). Those that are one-dimensional may be used with fixed-point MCSA as they only depend the previous iteration for information. As an example, for positive-definite but not necessarily symmetric problems, the minimal residual iteration [56] can be used in conjunction with MCSA where the residual vector, $\mathbf{r}$, defines the search subspace and the action of the linear operator on the residual vector, $\mathbf{Ar}$, defines the constraint subspace. Using this, we can then define an MCSA scheme that accelerates the

minimal residual iteration:

$$\alpha = \frac{\langle \mathbf{Ar}^k, \mathbf{r}^k \rangle}{\langle \mathbf{Ar}^k, \mathbf{Ar}^k \rangle} \ , \tag{2.69a}$$

$$\mathbf{x}^{k+1/2} = \mathbf{x}^k + \alpha \mathbf{r}^k \ , \tag{2.69b}$$

$$\mathbf{r}^{k+1/2} = \mathbf{b} - \mathbf{Ax}^{k+1/2} \ , \tag{2.69c}$$

$$\mathbf{A}\delta\mathbf{x}^{k+1/2} = \mathbf{r}^{k+1/2} \ , \tag{2.69d}$$

$$\mathbf{x}^{k+1} = \mathbf{x}^{k+1/2} + \delta\mathbf{x}^{k+1/2} \ , \tag{2.69e}$$

$$\mathbf{r}^{k+1} = \mathbf{b} - \mathbf{Ax}^{k+1} \ . \tag{2.69f}$$

where α is an optimal extrapolation parameter generated from the constraints. Interestingly, this scheme is nearly identical to the Richardson iteration version in Eq (2.67) except now the additional extrapolation parameter, α, is applied to the residual correction in Eq (2.69b) as a means of selecting a more optimal search direction at each iteration, potentially further improving convergence.

2.6.2 Preconditioning MCSA

In most cases, at least a minimal amount of *preconditioning* of the linear system will be required in order to use the class of stochastic methods described. Although these methods have no symmetry requirements for convergence, they do require that the spectral radius of the iteration matrix be less than one. Preconditioning serves as a means of achieving this by altering the eigenvalue spectrum of the iteration matrix.

2.6.2.1 Basic Preconditioning

As an example of basic preconditioning, to achieve a spectral radius of less than one for diagonally dominant matrices point Jacobi preconditioning can be used such that the precon-

ditioning matrix $\mathbf{M}$ is:

$$\mathbf{M} = diag(\mathbf{A}) \, , \tag{2.70}$$

which may be trivially inverted. With the application of this preconditioner we are instead solving the following scaled linear system:

$$\mathbf{M}^{-1}\mathbf{A}\mathbf{x} = \mathbf{M}^{-1}\mathbf{b} \, . \tag{2.71}$$

Next, we can apply MCSA to solve Eq (2.71):

$$\mathbf{x}^{k+1/2} = \mathbf{x}^k + \mathbf{M}^{-1}\mathbf{r}^k \, , \tag{2.72a}$$

$$\mathbf{r}^{k+1/2} = \mathbf{b} - \mathbf{A}\mathbf{x}^{k+1/2} \, , \tag{2.72b}$$

$$\mathbf{M}^{-1}\mathbf{A}\delta\mathbf{x}^{k+1/2} = \mathbf{M}^{-1}\mathbf{r}^{k+1/2} \, , \tag{2.72c}$$

$$\mathbf{x}^{k+1} = \mathbf{x}^{k+1/2} + \delta\mathbf{x}^{k+1/2} \, , \tag{2.72d}$$

$$\mathbf{r}^{k+1} = \mathbf{b} - \mathbf{A}\mathbf{x}^{k+1} \, , \tag{2.72e}$$

where the Neumann-Ulam Monte Carlo solve now has a preconditioned operator from which to build weights and probabilities for transport and a preconditioned source vector to sample.

Choosing point Jacobi preconditioning with MCSA is advantageous for several reasons. First, $\rho(\mathbf{I} - \mathbf{M}^{-1}\mathbf{A}) < 1$ is true for all $\mathbf{A}$ that is diagonally dominant and is easy to formulate because the inversion of $\mathbf{M}$ is trivial. Second, because the Monte Carlo method used within MCSA to compute the correction operates on a linear problem with the preconditioned operator, then $\mathbf{H}$ in the Neumann-Ulam solver will have a zero term in each of its diagonal elements, thereby eliminating all in-state transitions during the random walk sequence. Because of this, point Jacobi preconditioning should be considered for many classes of problems, regardless of any other preconditioning that is applied to the system. In addition, Jacobi preconditioning has been shown to be an effective preconditioning mechanism for MCSA when used with the thermal radiation diffusion equation [75].

2.6.2.2 General Preconditioning Strategies

It is possible to use general left, right, and left/right preconditioning with MCSA by carefully considering the underlying Monte Carlo problem that will be solved with the Neumann-Ulam method. We consider here the general left/right preconditioned method as the left or right preconditioned methods can be inferred from its formulation. We consider a left preconditioner $\mathbf{M_L}$ and a right preconditioner $\mathbf{M_R}$. The left/right preconditioned linear problem is then:

$$\mathbf{M}_L^{-1}\mathbf{A}\mathbf{M}_R^{-1}\mathbf{M}_R\mathbf{x} = \mathbf{M}_L^{-1}\mathbf{b} \,. \tag{2.73}$$

To handle the right preconditioning, the system is written with a substitution of variables:

$$\mathbf{M}_L^{-1}\mathbf{A}\mathbf{M}_R^{-1}\mathbf{u} = \mathbf{M}_L^{-1}\mathbf{b} \,, \tag{2.74}$$

with

$$\mathbf{x} = \mathbf{M}_R^{-1}\mathbf{u} \,. \tag{2.75}$$

To apply such a method to MCSA, we solve for the substituted variable $\mathbf{u}$ during the iteration sequence:

$$\mathbf{u}^{k+1/2} = \mathbf{u}^k + \mathbf{r}^k \,, \tag{2.76a}$$

$$\mathbf{r}^{k+1/2} = \mathbf{M}_L^{-1}(\mathbf{b} - \mathbf{A}\mathbf{M}_R^{-1}\mathbf{u}^{k+1/2}) \,, \tag{2.76b}$$

$$\mathbf{M}_L^{-1}\mathbf{A}\mathbf{M}_R^{-1}\delta\mathbf{u}^{k+1/2} = \mathbf{r}^{k+1/2} \,, \tag{2.76c}$$

$$\mathbf{u}^{k+1} = \mathbf{u}^{k+1/2} + \delta\mathbf{u}^{k+1/2} \,, \tag{2.76d}$$

$$\mathbf{r}^{k+1} = \mathbf{M}_L^{-1}(\mathbf{b} - \mathbf{A}\mathbf{M}_R^{-1}\mathbf{u}^{k+1}) \,, \tag{2.76e}$$

and then recover the original solution vector with Eq (2.75) after convergence. For the Monte Carlo problem, we isolate the generation of the correction:

$$\mathbf{M}_L^{-1}\mathbf{A}\mathbf{M}_R^{-1}\delta\mathbf{u}^{k+1/2} = \mathbf{r}^{k+1/2} \, , \tag{2.77}$$

and note that the preconditioned residual of the substituted variable is now serving as the source and the new iteration matrix is:

$$\mathbf{H} = \mathbf{I} - \mathbf{M}_L^{-1}\mathbf{A}\mathbf{M}_R^{-1} \, . \tag{2.78}$$

As we require (i, j) element-wise access to the iteration matrix in order to construct probabilities and weights for the Monte Carlo procedure from the Neumann-Ulam decomposition, the *composite operator*, $\mathbf{M}_L^{-1}\mathbf{A}\mathbf{M}_R^{-1}$, must be formed via matrix-matrix multiplication.

Several possible shortcomings of this preconditioning approach are readily observed. First, the matrix-matrix multiplication operation for sparse, parallel distributed matrices is significantly more expensive than a matrix-vector multiplication operation. Second, each preconditioner must be explicitly inverted, an operation in itself that may be expensive and which prohibits the use of any preconditioners which provide no mechanism to extract their inverse. Third, for many modern preconditioning methods, this inversion may yield dense matrices, destroying sparsity and further impeding the performance of a matrix-matrix multiplication operation. It is also interesting to note that the Monte Carlo problem in the general left/right preconditioned scheme given by Eq (2.77) is not fully left/right preconditioned (meaning that we do not recover $\mathbf{x}$), but instead part of a sequence for finding the substituted variable $\mathbf{u}$. We do, however, gain the benefits of this general preconditioning by building the iteration matrix in Eq (2.78) from the fully preconditioned linear operator. In addition, for MCSA to apply to increasingly difficult problems, more advanced preconditioning techniques that require the generation of the composite operator may be necessary for convergence.

2.7 Monte Carlo Method Selection

The MCSA method defined in Eq. (2.67) uses the adjoint method to estimate the error in a residual Monte Carlo solve instead of the direct method outlined in §2.3. To demonstrate the effectiveness of the adjoint method over the direct method within the context of MCSA, we choose the two-dimensional time-dependent Poisson equation as a simple model transport problem[3]:

$$\frac{\partial \mathbf{u}}{\partial t} = \nabla^2 \mathbf{u} \,. \tag{2.79}$$

For all comparisons, a single time step is computed with backwards Euler time integration. The Laplacian is differenced on a square Cartesian grid with a second-order five-point stencil,

$$\nabla_5^2 = \frac{1}{\Delta^2} \left[u_{i-1,j} + u_{i+1,j} + u_{i,j-1} + u_{i,j+1} - 4u_{i,j} \right], \tag{2.80}$$

and a fourth-order nine-point stencil,

$$\nabla_9^2 = \frac{1}{6\Delta^2} [4u_{i-1,j} + 4u_{i+1,j} + 4u_{i,j-1} + 4u_{i,j+1} + u_{i-1,j-1}$$
$$+ u_{i-1,j+1} + u_{i+1,j-1} + u_{i+1,j+1} - 20u_{i,j}], \quad (2.81)$$

both assuming a grid size of Δ in both the i and j directions. For a single time step solution, we then have the following sparse linear system to be solved with the MCSA method:

$$\mathbf{A}\mathbf{u}^{n+1} = \mathbf{u}^n \,. \tag{2.82}$$

Both the stencils will be used to vary the size and density of the sparse linear system in Eq. (2.82).

A timing and convergence study is used to demonstrate the effectiveness of the adjoint

---

[3]The Poisson equation is a simple form of the diffusion equation and has a similar elliptic character in its time-dependent form to the neutron transport equations that will be solved in the next chapter.

method with the collision estimator as compared to the direct method. To assess both the CPU time and number of iterations required to converge to a solution, a problem of constant Δ was used with varying values of the number of mesh elements, fixing the spectral radius of the system at a constant value for each variation. Both the five-point and nine-point stencils were used with both the direct and adjoint solvers. For each case, $N \times N$ total random walk permutations were computed per MCSA iteration where $N \times N$ is the number of discrete grid points (or degrees of freedom) in the system. Solver parameters were set to a weight cutoff of 1×10^{-4} for the stochastic linear solver and a convergence tolerance of 1×10^{-8} for the MCSA iterative solver. Figure 2.4 gives the CPU time needed for each case to converge in seconds, and Figure 2.5 gives the number of iterations needed for each case to converge to the specified tolerance, both as a function of the problem size. All computations presented in this section and the remaining sections of this chapter were completed on a 3.0 GHz Intel Core 2 Quad Q9650 CPU machine with 16 GB 1067 MHz DDR3 memory.

We see clearly in Figure 2.4 that the using the adjoint solver with MCSA results in a speedup over the direct solver while the number of iterations required to converge is also reduced as shown in Figure 2.5. We expect this for several reasons. First, with an equivalent number of histories specified for both solvers per MCSA iteration and a system of size $N \times N$, the direct solver will compute a single random walk for each state in the system per iteration to acquire a solution in that state. This is necessary in the direct method to ensure a contribution from each state as the random walk sequence will only contribute to the starting state. For the adjoint method, a total of $N \times N$ random walk events will have their starting state determined by sampling the residual vector. Because the random walk sequence contributes to the state in which it currently resides, sampling the residual vector as the Monte Carlo source gives a higher density of random walk events in regions with a high residual, thus giving a more accurate correction in that region due to reduced statistical error. From an iteration perspective, Figure 2.5 shows that using the direct method yields a roughly unchanging number of iterations required to converge as the problem size increases. Again, if
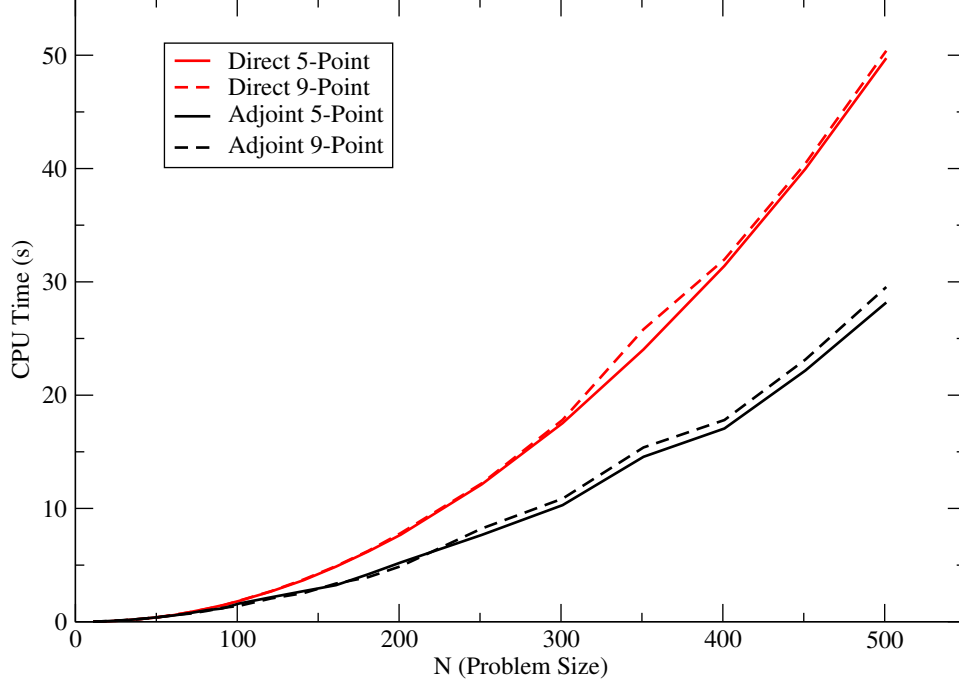
Figure 2.4: **CPU Time (s) to converge vs. Problem Size (N for an $N \times N$ square mesh).** *Both the adjoint and direct solvers are used with the five point and nine point stencils. A CPU time speedup is noted with the adjoint method due to the higher density of random walk events in regions with a large residual.*

we desire a correction value for all states in the problem, then we must start a random walk in each state in the system without taking into account the structure of the residual vector. Because of this, as the problem size grows adding histories is ineffective as many are added in states where the error is smaller than in other parts of the problem, ultimately not reducing the number of iterations needed to converge. Conversely, as the problem size grows in the adjoint method, the additional stochastic histories that will be computed are concentrated in regions with a large residual, further reducing the stochastic error in the correction in those regions and subsequently reducing the required number of iterations to converge.

As an additional comparison, the convergence behavior of MCSA can be analyzed using both the adjoint and direct solvers to detect any performance benefits. To assess the convergence properties of MCSA using each solver and stencil, the infinity norm of the residual computed in Eq. (2.67) was collected at each iteration for a fixed problem size of
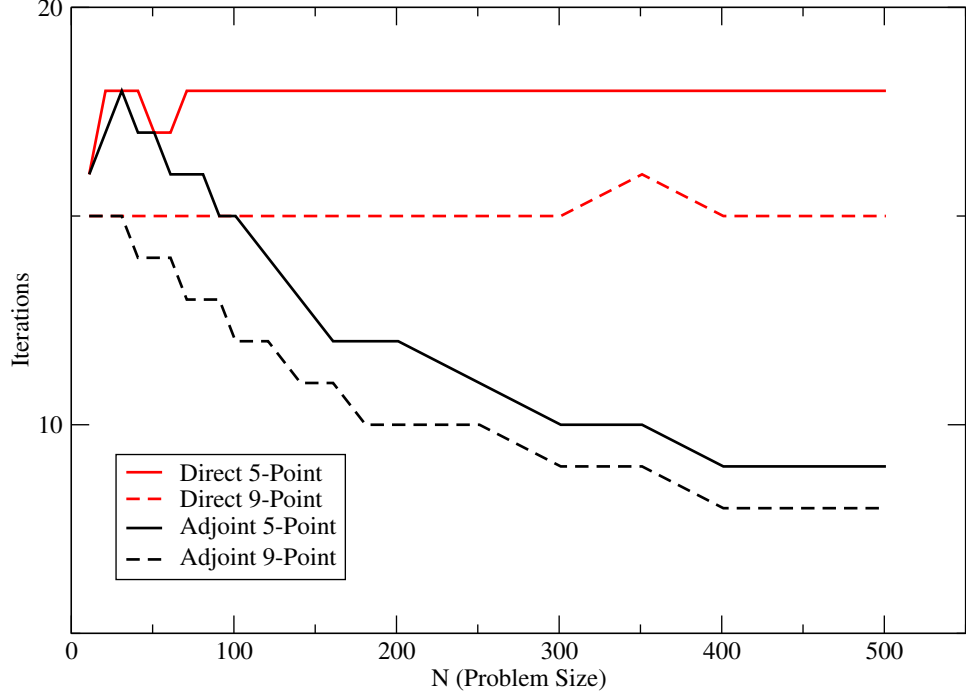
Figure 2.5: **Iterations to converge vs. Problem Size (N for an $N \times N$ square mesh).** *Both the adjoint and direct solvers are used with the five-point and nine-point stencils.*

$N = 500$. Figure 2.6 gives the results of these computations. First, it is worthy to note on the semi-log plot that we are indeed achieving the expected exponential convergence from MCSA with both Monte Carlo solvers. Second, we note that using the adjoint method with the same number of stochastic histories per MCSA iteration gives a faster rate of converge for the same reasons as above. We also note here that fewer iterations are required for convergence when the 9-point stencil is used to discretize the Laplacian operator (although at no gain in speed as given by the results in Figure 2.4). This is due to the fact that the smaller discretization error directly corresponds to a more well defined residual source generated by the Richardson extrapolation for the Monte Carlo calculation. In addition, the better defined source is transported through a domain described more accurately by the 9-point stencil, thus yielding a more accurate correction vector from the Monte Carlo calculation.
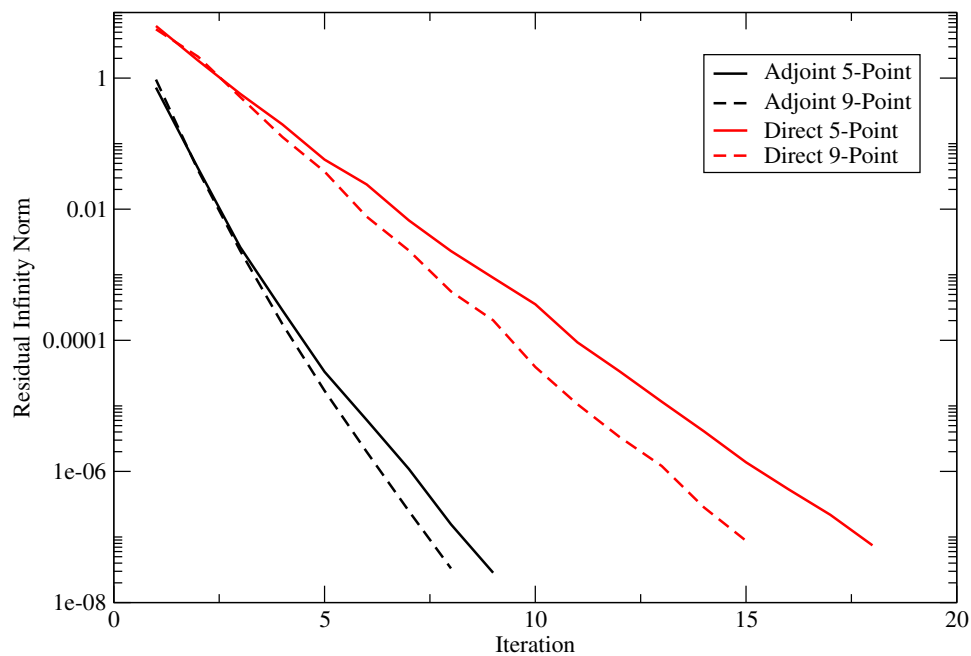
Figure 2.6: **Infinity norm of the solution residual vs. iteration number for a problem of size** $N = 500$**.** *Both the adjoint and direct solvers are used with the five point and nine point stencils. A higher rate of convergence is observed for MCSA using the adjoint Monte Carlo solver as compared to the direct method when both solvers compute the same number of random walks per iteration.*

2.8 MCSA Comparison to Sequential Monte Carlo

To further motivate using Monte Carlo Synthetic Acceleration, we compare its performance to Halton's Sequential Monte Carlo method on which previous work in this area was based. For this comparison, we use the same transient Poisson problem as described in the previous section and choose only the 5-point stencil to discretize the Laplacian operator as the previous results yielded little qualitative difference between the discretizations. Both MCSA and Halton's method are used with the adjoint Monte Carlo solver and the collision estimator. In order to complete the same study as in the previous section, the number of histories computed by the Monte Carlo solver at each iteration had to be doubled to $2 \times N \times N$ in order to ensure convergence in Sequential Monte Carlo Method. For the majority of the problems in the previous section, the Sequential method used with $N \times N$ histories would not converge. Figure 2.7 gives the CPU time results for this comparison as a function of problem size while Figure 2.8 gives the number of iterations to converge as a function of problem size with a convergence tolerance of 1×10^{-8}. In both cases, using the Monte Carlo solver as a synthetic acceleration rather than in a pure residual Monte Carlo scheme resulted in a reduction in both CPU time and iterations required to converge. The additional Richardson extrapolation between each Monte Carlo solve in the MCSA method gives a better converged residual source to use with the Monte Carlo calculation while the Sequential method requires more iterations to achieve the same level of convergence in the residual.

The benefits of using a synthetic acceleration scheme are also noted when the infinity norm of the residual computed at each iteration for both methods was collected at each iteration for a fixed problem sizes of $N = 100$ and $N = 500$ as shown in figures Figure 2.9 and 2.10 respectively. In both cases, the Sequential method is subject to two regimes of exponential convergence with high frequency error modes removed in the first regime leaving lower frequency and slower converging error modes in the second. Using MCSA we a see a single rate of exponential convergence observed to be much higher than that computed by
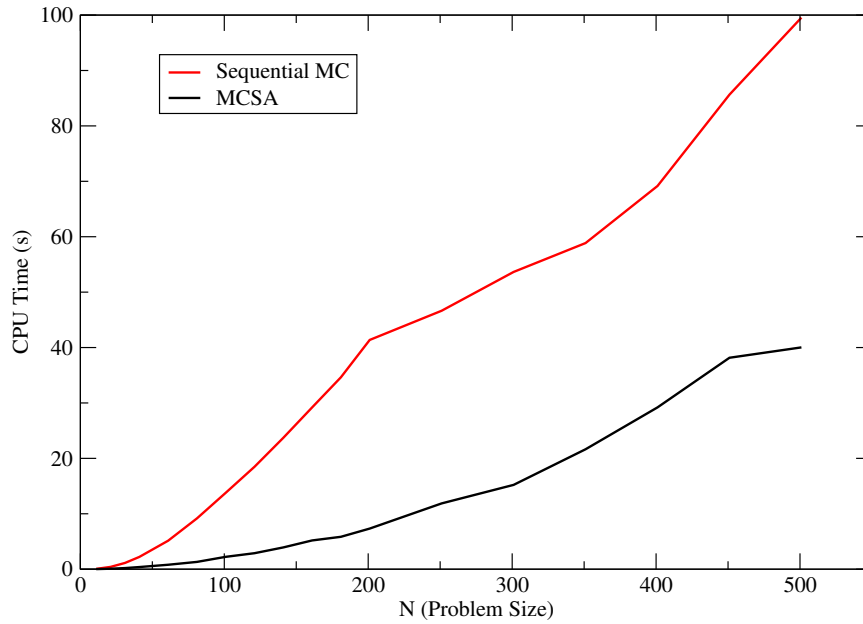
Figure 2.7: **CPU Time (s) to converge vs. Problem Size (N for an $N \times N$ square mesh).** *Both the Sequential Monte Carlo and MCSA solvers are used with the five point stencils and the adjoint Monte Carlo solver. The number of random walks was twice the number of discrete states in the system in order to ensure convergence in the Sequential Monte Carlo method.*
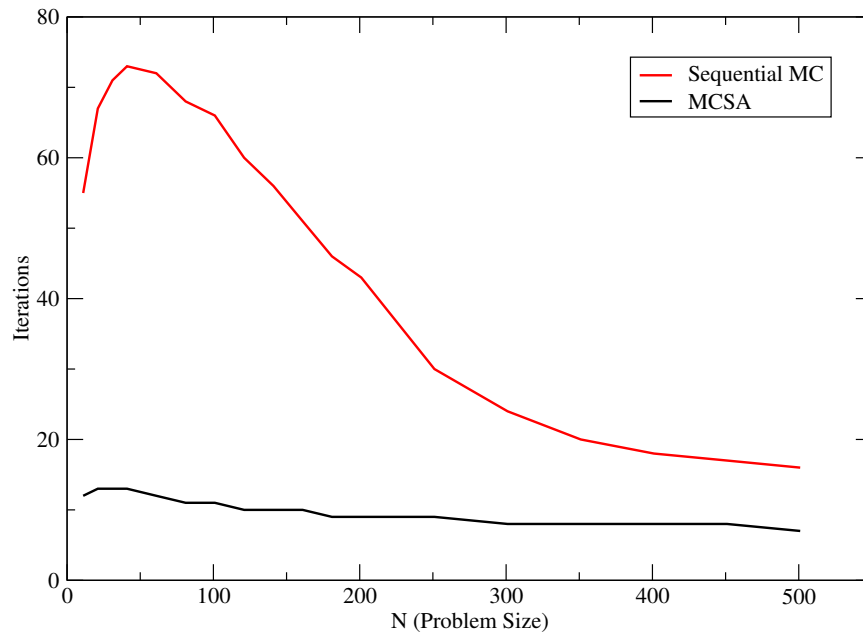
Figure 2.8: **Iterations to converge vs. Problem Size (N for an $N \times N$ square mesh).** *Both the Sequential Monte Carlo and MCSA solvers are used with the five point stencils and the adjoint Monte Carlo solver.*
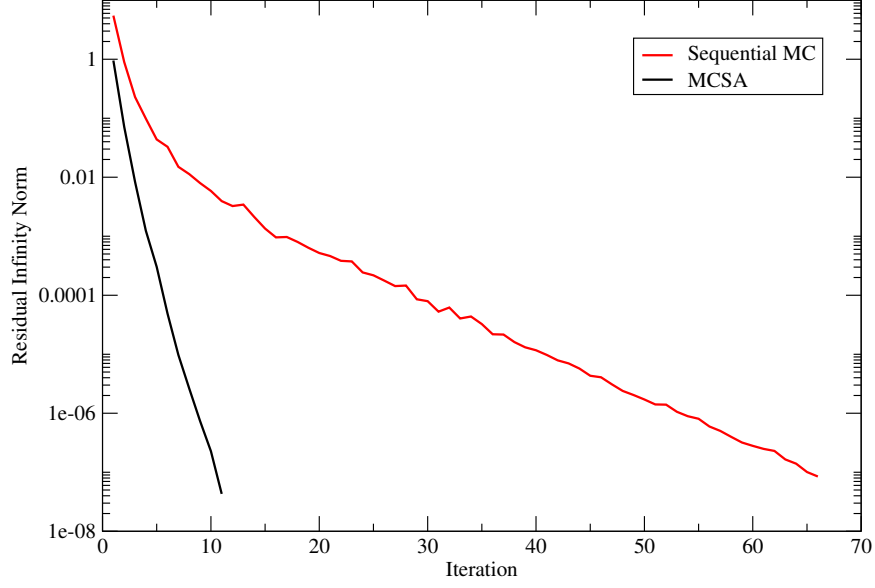
Figure 2.9: **Infinity norm of the solution residual vs. iteration number for a problem of size** $N = 100$**.** *Both the Sequential Monte Carlo and MCSA solvers are used with the five point stencils and the adjoint Monte Carlo solver.*

Halton's method due to the fact that the extra Richardson iteration is providing a smoothing effect to alleviate the error mode variations. Even with the doubling of the number of stochastic histories computed per time step in order to ensure convergence for the Sequential method, we still see robustness issues with a non-monotonically decreasing residual observed for the $N = 100$ case. In both cases the MCSA solver is observed to be robust with a monotonically decreasing residual.
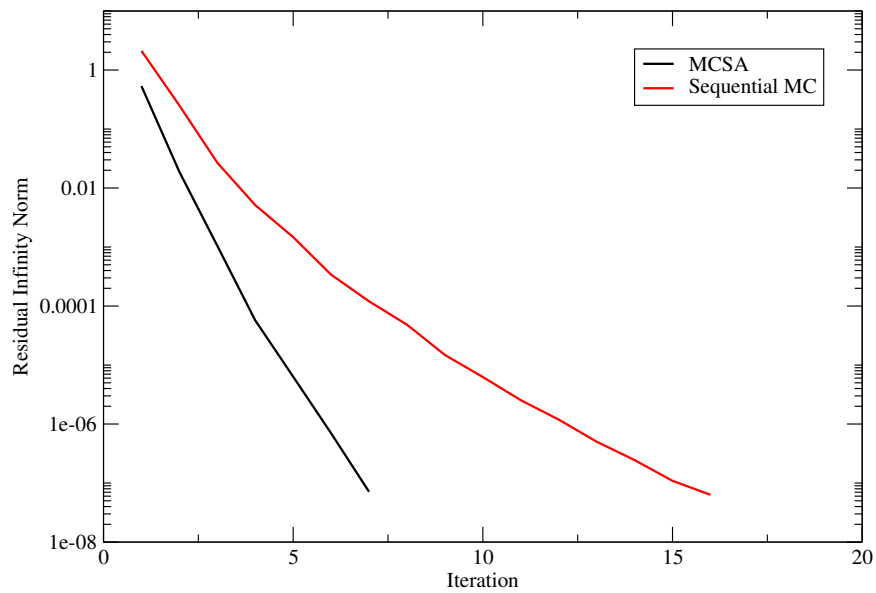
Figure 2.10: **Infinity norm of the solution residual vs. iteration number for a problem of size** $N = 500$. *Both the Sequential Monte Carlo and MCSA solvers are used with the five point stencils and the adjoint Monte Carlo solver.*

2.9 Monte Carlo Parameter and Estimator Analysis

With the adjoint method shown to be more effective than the direct method and MCSA to have better iterative and timing performance than sequential Monte Carlo, we now aim to study the effects of the adjoint Monte Carlo parameters, weight cutoff and number of histories, on MCSA performance with both the collision and expected value estimators. With the same Poisson problem, we will use a 200×200 grid and a convergence tolerance of 1×10^{-8} for all calculations. To study the effects of the number of Monte Carlo histories per MCSA iteration, the weight cutoff was fixed at 1×10^{-4} while the number of histories per iteration was varied from 6,000 to 100,000. It was observed that MCSA would not converge for this problem using the collision estimator with less than 6,000 histories while the expected value estimator permitted convergence with only 2,000 histories.

Figure 2.11 gives the number of iterations required to converge for both estimators as a function of the number of histories per iteration. For smaller numbers of histories, the performance of the expected value estimator is significantly better than the collision estimator. This result is valuable in that less transport is required to achieve the same MCSA iterative performance with the expected value estimator, important for situations where transport is expensive (i.e. in domain decomposed calculations). Interestingly, as the number of histories per iteration are increased, the iterative performance with the collision estimator approaches that of the expected value estimator. However, given the performance of the expected value estimator at a fractional number of histories, one should strongly consider its use over using the collision estimator with more histories. The CPU time required to converge is presented in Figure 2.12 and reflects the results of the iterative performance. In general, using the collision estimator is slightly slower overall, but the time per iteration is faster due to the fact that the estimator does not have to cycle through multiple states during the tally procedure.

For the weight cutoff study, the number of histories per iteration was fixed at 40,000 and the weight cutoff varied from 5×10^{-1} down to 1×10^{-10}. Surprisingly, the number of
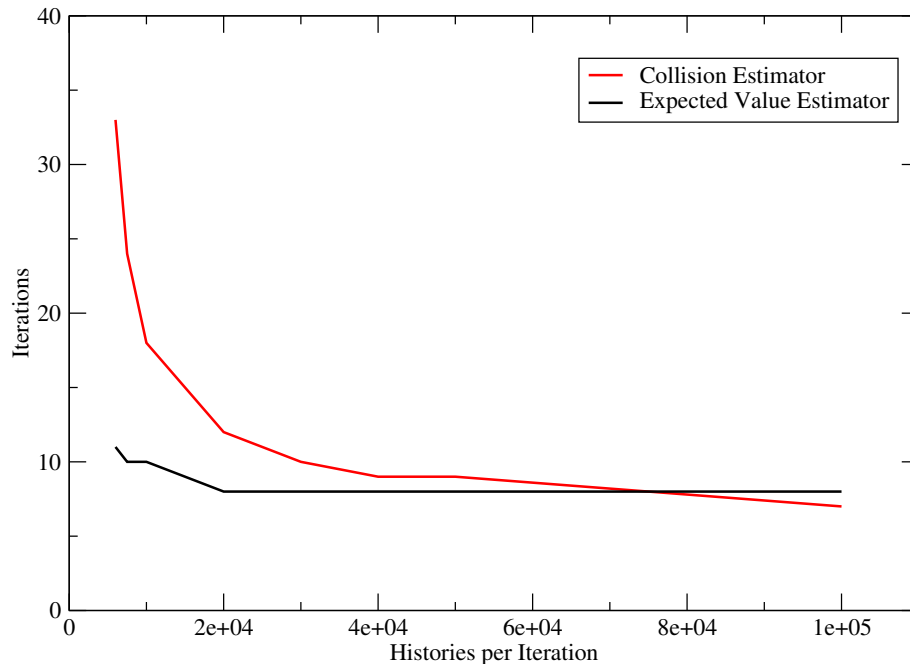
Figure 2.11: **Iterations (s) to converge vs. Monte Carlo histories per MCSA iteration for a** 200×200 **square mesh and a weight cutoff of** 1×10^{-4}**.** *For low numbers of histories, the expected value estimator performance is significantly better than the collision estimator. At higher numbers of histories, the estimators become roughly equivalent.*

iterations to converge given by Figure 2.13 is effectively invariant to the weight cutoff, only seeing detrimental effects on the number of iterations at a very large weight cutoff. This suggests that a fairly large weight cutoff can be used in practice with both adjoint estimators and that the preliminary components of the random walk are more important to MCSA convergence than those that occur later and with lower weight contributions. To further motivate using a larger weight cutoff, Figure 2.14 gives the CPU time need to converge as a function of weight cutoff. As expected, lowering the weight cutoff lengthens the random walk lengths and increases CPU time at no gain of iterative performance. In general, these results suggest using the expected value estimator over the collision estimator with MCSA as well as using a larger weight cutoff.

Figure 2.12: **CPU Time (s) to converge vs. Monte Carlo histories per MCSA iteration for a** 200×200 **square mesh and a weight cutoff of** 1×10^{-4}**.** *For low numbers of histories, the expected value estimator performance is better than the collision estimator due to a lower iteration count while the actual compute time per iteration is higher.*
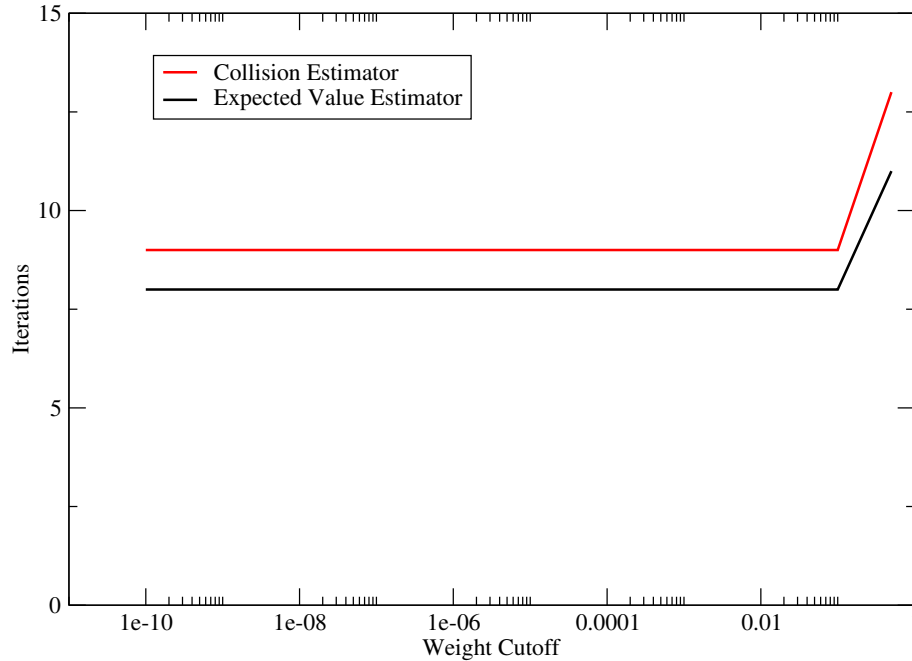
Figure 2.13: **Iterations (s) to converge vs. history weight cutoff for a** 200×200 **square mesh and 40,000 histories.** *For low numbers of histories, the expected value estimator performance is significantly better than the collision estimator. At higher numbers of histories, the estimators become roughly equivalent.*

Figure 2.14: **CPU Time (s) to converge vs. history weight cutoff for a** 200×200 **square mesh and 40,000 histories.** *For low numbers of histories, the expected value estimator performance is better than the collision estimator due to a lower iteration count while the actual compute time per iteration is higher.*

2.10 Variance Reduction Techniques

Variance reduction is a mechanism by which the probabilities and weights of the Monte Carlo problem are modified to improve the performance of a given estimator. In the context of improving MCSA results, such modifications may potentially introduce bias into the system. However, using Monte Carlo within an MCSA iterative scheme provides a potential buffer for the solution from this bias as the correction generated by the Monte Carlo solve will contain large statistical error even without variance reduction. For this work, any method that alters the weights and probabilities of the Monte Carlo method with the aim of improving either iterative performance or time to convergence will be defined as a variance reduction scheme.

2.10.1 Artificial Absorption

The random walk sequences generated by the adjoint Neumann Ulam decomposition in Eqs (2.46) and (2.47) will continue on indefinitely without the implementation of a weight cutoff procedure (which in itself is effectively a form of biased variance reduction). This is due to the fact that all states to which a stochastic history may move in a given transition exist within the system and have a non-zero weight. A preliminary variance reduction scheme is to introduce *artificial absorption* into the system such that at each transition event, a stochastic history will now have some finite probability of being terminated through absorption as well as transitioning to other states in the system. This probability, p_{abs}, modifies the probabilities and weights in the adjoint random walk sequence as:

$$p_{ij} = \frac{|h_{ji}|}{\sum_j |h_{ji}|} (1 - p_{abs}) \,, \tag{2.83}$$

and

$$w_{ij} = \frac{sign(h_{ji})}{(1 - p_{abs})} \sum_j |h_{ji}| \,. \tag{2.84}$$

At each transition step, a history at state i will then sample the probability distribution function generated by Eq (2.83) with an additional absorption state added to the distribution. If the sampling procedure results in a transition to the absorption state, the history is immediately terminated. The advantages of this for residual Monte Carlo are that increasing the absorption probability decreases the length of each random walk (resulting in speedup), while the random walk has a higher weight contribution at every step. This higher weight means that each history is depositing more information near its birth site which will on average be located where the system residual is the largest. An additional advantage of this formulation is that the full Neumann-Ulam decomposition is maintained.

To observe the effects of this variance reduction on MCSA solutions, the transient Poisson problem was again solved with the adjoint method, this time with varying values of artificial absorption. A 200×200 grid was used with 40,000 histories at every iteration with the expected value estimator converged to a tolerance of 1×10^{-8}. To reduce the effect of the weight cutoff on this study, the weight cutoff was set to 1×10^{-12} such that it is significantly more likely that a history will be terminated by absorption rather than weight cutoff. Figure 2.15 gives the number of iterations to converge as a function of the artificial absorption probability. Up to a probability of roughly 0.5, the iterative performance is not significantly affected with the information lost due to shortened random walks causing a small increase in the number of iterations. At a probability of 0.6, the number of iterations required grows rapidly as the shortened randow walks create an MCSA correction that has a larger statistical error. Convergence was observed to be lost at probabilities of 0.7 and higher.

The random walk length has a strong effect on CPU time as well. Figure 2.16 gives the CPU time in seconds required to converge as a function of artificial absorption probability. Initially, small absorption probabilities not only maintain iterative performance, but also drastically reduced the time required to converge as absorption was more frequent than even a large weight cutoff but the weights themselves were not significantly modified. As the number of iterations grow rapidly, so does the time required to converge to a solution.
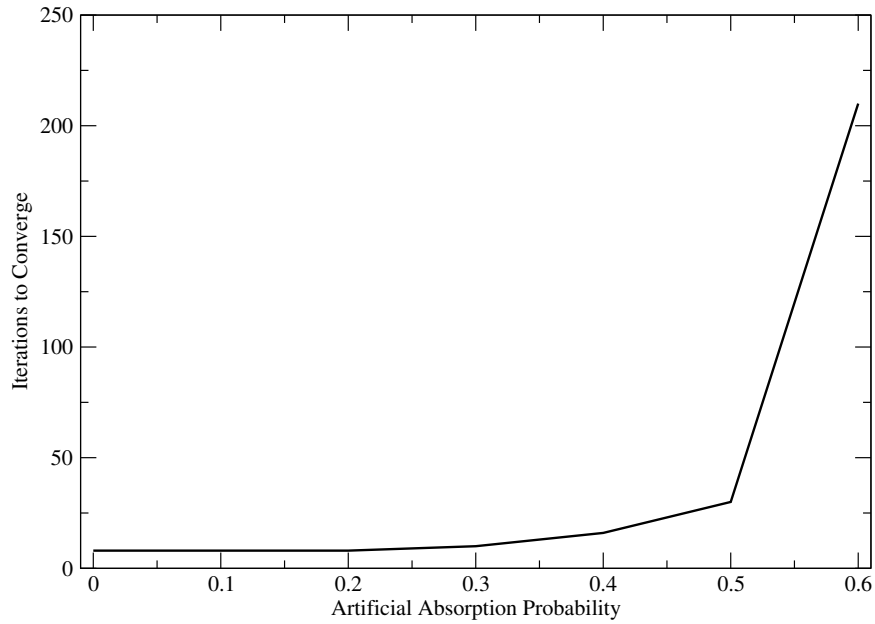
Figure 2.15: **Iterations (s) to converge vs. artificial absorption probability for a** 200×200 **square mesh and 40,000 histories.** *The addition of absorption is detrimental to iterative performance due to both the shortening of the random walks as well as the modification of the transition weight.*

Based on these results, using a small amount of artificial absorption should provide some CPU speedup while maintaining iterative performance. For the problem presented here, an absorption probability of around 0.25 may be the best choice as it minimizes CPU time.
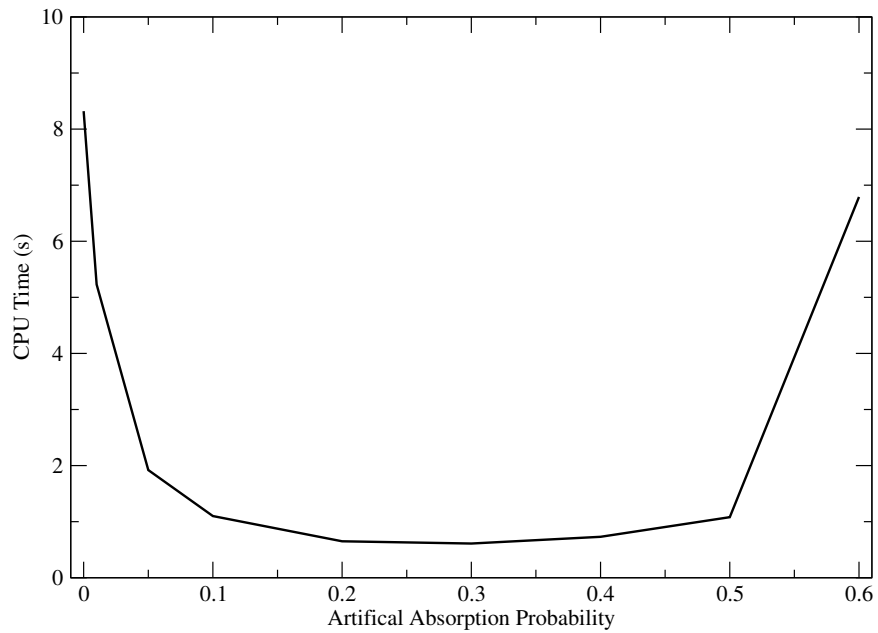
Figure 2.16: **CPU Time (s) to converge vs. artificial absorption probability for a** 200×200 **square mesh and 40,000 histories.** *The reduced random walk length speeds up the calculation with a fixed number of histories. Too much artificial absorption increases iterations rapidly giving an increasing CPU time.*

2.10.2   Reduced Domain Approximation

For scalable parallel implementations and efficient Monte Carlo transport, the domain is required to be sparse. We may find through general preconditioning operations as outlined by the Monte Carlo problem in Eq (2.77) that this sparsity is lost. To alleviate this, we propose modifying the domain sampled by the Monte Carlo method to generate the correction within MCSA by removing terms in the iteration matrix through some predetermined criteria in order to recover sparsity. As the Neumann-Ulam scheme is a stochastic realization of multiple matrix-vector multiplies, the criteria we choose should be based on maintaining those elements that will make the largest contributions to the multiplication and therefore recover as much of the original product as possible.

For each row in the preconditioned system, we can then apply the reduced domain approximation to eliminate those elements that either fall below a specified tolerance level, keep the N largest elements in each row, or both giving:

$$\mathbf{x}^{k+1/2} = \mathbf{x}^k + \mathbf{r}^k \,, \tag{2.85a}$$

$$\mathbf{r}^{k+1/2} = \mathbf{b} - \mathbf{A}\mathbf{x}^{k+1/2} \,, \tag{2.85b}$$

$$\hat{\mathbf{A}}\delta\mathbf{x}^{k+1/2} = \mathbf{r}^{k+1/2} \,, \tag{2.85c}$$

$$\mathbf{x}^{k+1} = \mathbf{x}^{k+1/2} + \delta\mathbf{x}^{k+1/2} \,, \tag{2.85d}$$

$$\mathbf{r}^{k+1} = \mathbf{b} - \mathbf{A}\mathbf{x}^{k+1} \,, \tag{2.85e}$$

where $\hat{\mathbf{A}}$ in Eq (2.85c) means that the reduced domain approximation has been applied to the iteration matrix in the Monte Carlo method. If enough of the terms in the original iteration matrix have been maintained, the character of the original iteration matrix should be retained and continue to accelerate the iterative scheme. The effects of the reduced domain approximation on neutron transport systems where it is required due to the explicit preconditioning strategy will be presented in Chapter 3.

2.11   Summary

In this chapter, the fundamentals of Monte Carlo Synthetic Acceleration methods were presented and explored in the context of a simple model transport system. The following are the significant observations and findings.

- Monte Carlo Synthetic Acceleration (MCSA) has been generalized for all discrete linear transport problems

- MCSA can be preconditioned using a general left/right scheme but requires the explicit inversion of the preconditioners and construction of the composite linear operator

- The adjoint Neumann-Ulam method performs better when used with MCSA compared to the forward method

- MCSA has superior performance when compared to Halton's residual Monte Carlo method

- The Richardson iteration in MCSA behaves as a smoother for the stochastic Monte Carlo error

- MCSA iterative performance when used with the expected value estimator is insensitive to histories per iteration

- MCSA iterative performance is insensitive to the stochastic history weight cutoff

- Variance reduction with artificial absorption can enhance time to solution

- The reduced domain approximation was introduced to mitigate the consequences of composite linear operator generation

Chapter 3

Monte Carlo Synthetic Acceleration Methods for the SP_N Equations

In this chapter, we briefly derive the simplified P_N (SP_N) equations, closely following the work of Evans [1], in order to gain full understanding of the underlying system and its potential behavior in a Monte Carlo context. From the P_N equations, we apply a set of approximations to yield the SP_N equations for fixed source and criticality problems. Using the fully-formed linear operator for the transport problem, we explore solutions to the SP_N equations with Monte Carlo Synthetic Acceleration using a challenging light water reactor fuel assembly criticality calculation as the driving problem. Several difficulties arise when applying MCSA to these problems that were not observed when investigating the simple transport system in the previous chapter.

For Jacobi-based preconditioners, convergence with MCSA is difficult if not impossible for ill-conditioned systems with this behavior demonstrated using a simple neutron diffusion problem. In order to effectively solve the SP_N equations for the fuel assembly problem, a suite of preconditioners along with a relaxation scheme is developed and studied within the context of MCSA. Using these preconditioners, several additional issues are observed and alleviated to a certain extent by applying the reduced domain approximation. MCSA solutions for the fuel assembly problem are then verified by comparing the solutions against production Krylov solvers for problems with varying numbers of energy groups. Finally performance is analyzed through comparison with those same Krylov solvers in terms of both iterative performance and CPU timing using the same set of problems utilized for the verification.

3.1 The Neutron Transport Equation

As a starting point for the SP_N equations we define the time-independent neutron transport equation [61]:

$$\hat{\Omega} \cdot \vec{\nabla} \psi(\vec{r}, \hat{\Omega}, E) + \sigma(\vec{r}, E)\psi(\vec{r}, \hat{\Omega}, E) =$$
$$\iint \sigma_s(\vec{r}, E' \to E, \hat{\Omega}' \cdot \hat{\Omega})\psi(\vec{r}, \hat{\Omega}', E')d\Omega'dE' + q(\vec{r}, \hat{\Omega}, E) \, , \quad (3.1)$$

with the variables defined as:

- $\vec{r}$ - neutron spatial position

- $\hat{\Omega}$ - neutron streaming direction with radial component μ and azimuthal component ω

- $\hat{\Omega}' \cdot \hat{\Omega} = \mu_0$ is the angle of scattering

- E - neutron energy

- $\psi(\vec{r}, \hat{\Omega}, E)$ - angular flux

- $\sigma(\vec{r}, E)$ - total interaction cross section

- $\sigma_s(\vec{r}, E' \to E, \hat{\Omega}')$ - probability of scattering from direction $\hat{\Omega}'$ into an angular domain $d\hat{\Omega}'$ about the direction $\hat{\Omega}$ and from energy E' to an energy domain dE' about energy E

- $q(\vec{r}, \hat{\Omega}, E)$ - external source of neutrons.

For this work, it is sufficient to formulate Eq (3.1) in 1-dimensional Cartesian geometry:

$$\mu \frac{\partial}{\partial x}\psi(x, \mu, E) + \sigma(x, E)\psi(x, \mu, E) =$$
$$\iint \sigma_s(x, E' \to E, \hat{\Omega}' \cdot \hat{\Omega})\psi(x, \hat{\Omega}', E')d\Omega'dE' + \frac{q(x, E)}{4\pi} \, , \quad (3.2)$$

where the angular component of the solution is no longer dependent on the azimuthal direction of travel and an isotropic source of neutrons is assumed. In addition, for fission systems the eigenvalue form of the transport equation is:

$$\hat{\Omega} \cdot \vec{\nabla}\psi(\vec{r}, \hat{\Omega}, E) + \sigma(\vec{r}, E)\psi(\vec{r}, \hat{\Omega}, E) =$$
$$\iint \sigma_s(\vec{r}, E' \to E, \hat{\Omega}' \cdot \hat{\Omega})\psi(\vec{r}, \hat{\Omega}', E')d\Omega'dE' +$$
$$\frac{1}{k}\chi(E) \iint \nu\sigma_f(\hat{r}, E')\psi(\vec{r}, \hat{\Omega}', E')d\Omega'dE' + q(\vec{r}, \hat{\Omega}, E) , \quad (3.3)$$

with the additional variables defined as

- k - multiplication factor

- $\chi(E)$ - fission neutron energy spectrum

- ν - average number of neutrons per fission

- $\sigma_f(r, E')$ - fission cross section .

In 1-dimensional Cartesian geometry, Eq (3.3) becomes:

$$\mu\frac{\partial}{\partial x}\psi(x, \mu, E) + \sigma(x, E)\psi(x, \mu, E) =$$
$$\iint \sigma_s(x, E' \to E, \hat{\Omega}' \cdot \hat{\Omega})\psi(x, \hat{\Omega}', E')d\Omega'dE' +$$
$$\frac{1}{k}\chi(E) \iint \nu\sigma_f(x, E')\psi(x, \hat{\Omega}', E')d\Omega'dE' + \frac{q(x, E)}{4\pi} . \quad (3.4)$$

3.2 Derivation of the Monoenergetic SP_N Equations

The P_N equations as derived in [61] give $N + 1$ coupled first-order equations capturing the spatial and angular-dependence of the solution:

$$\frac{1}{2n + 1}\frac{\partial}{\partial x}\left[(n + 1)\phi_{n+1} + n\phi_{n-1}\right] + \Sigma_n\phi_n = q\delta_{n0} , \quad (3.5)$$

where $\Sigma_n = \sigma - \sigma_{sn}$ and the summations are truncated at some level of approximation N such that $n = 0, 1, \ldots, N$. This yields a set of $N+1$ equations for $N+2$ flux moments. In multiple dimensions, the equation set becomes large and coupled not only through angular moments but also through the spatial variables. As a simpler alternative to multidimensional P_N solutions, Gelbard recognized in 1960 that the planar P_N equations could be simplified and applied an ad-hoc method to extend them to multiple dimensions, yielding the SP_N equations. These equations are not only fewer in number, but also take on a diffusion-like form while maintaining the angular character of the flux, making them amenable to solutions with modern diffusion methods.

First, the P_N equations can be simplified to $(N+1)/2$ second-order equations by solving for the nth Legendre flux moment in the odd-order equations:

$$\phi_n = \frac{1}{\Sigma_n} \left[q\delta_{no} - \frac{\partial}{\partial x} \left(\frac{n}{2n+1}\phi_{n-1} + \frac{n+1}{2n+1}\phi_{n+1} \right) \right] , \tag{3.6}$$

for $n = 1, 3, \cdots, N$ and $\delta_{no} = 0 \; \forall n \neq 0$. We can insert the odd moments into Eq (3.5) to get a reduced group of equations for the even moments:

$$-\frac{\partial}{\partial x} \left[\frac{n}{2n+1} \frac{1}{\Sigma_{n-1}} \frac{\partial}{\partial x} \left(\frac{n-1}{2n-1}\phi_{n-2} + \frac{n}{2n-1}\phi_n \right) \right.$$
$$\left. + \frac{n+1}{2n+1} \frac{1}{\Sigma_{n+1}} \frac{\partial}{\partial x} \left(\frac{n+1}{2n+3}\phi_n + \frac{n+2}{2n+3}\phi_{n+2} \right) \right]$$
$$+ \Sigma_n \phi_n = q\delta_{n0} \qquad n = 0, 2, 4, \cdots, N . \tag{3.7}$$

Immediately, we note the diffusion-like nature of Eq (3.7) as compared to the original P_N equations. To extend these equations to multiple dimensions, Gelbard simply replaced the planar spatial derivatives in the reduced set of equations with general multidimensional

gradient operators:

$$-\nabla \cdot \left[\frac{n}{2n+1} \frac{1}{\Sigma_{n-1}} \nabla \left(\frac{n-1}{2n-1} \phi_{n-2} + \frac{n}{2n-1} \phi_n \right) \right.$$

$$\left. + \frac{n+1}{2n+1} \frac{1}{\Sigma_{n+1}} \nabla \left(\frac{n+1}{2n+3} \phi_n + \frac{n+2}{2n+3} \phi_{n+2} \right) \right]$$

$$+ \Sigma_n \phi_n = q \delta_{n0} \qquad n = 0, 2, 4, \cdots, N, \quad (3.8)$$

yielding a multidimensional set of $(N+1)/2$ angular coupled equations defined as the SP_N equations. As with the P_N equations, we provide closure to this set of equations with $\phi_{N+1} = 0$. As a concrete example, we will consider the SP_7 equations:

$$-\nabla \cdot \frac{1}{3\Sigma_1} \nabla(\phi_0 + 2\phi_2) + \Sigma_0 \phi_0 = q \qquad (3.9a)$$

$$-\nabla \cdot \left[\frac{2}{15\Sigma_1} \nabla(\phi_0 + 2\phi_2) + \frac{3}{35\Sigma_3} \nabla(3\phi_2 + 4\phi_4) \right] + \Sigma_2 \phi_2 = 0 \qquad (3.9b)$$

$$-\nabla \cdot \left[\frac{4}{63\Sigma_3} \nabla(3\phi_2 + 4\phi_4) + \frac{5}{99\Sigma_5} \nabla(5\phi_4 + 6\phi_6) \right] + \Sigma_4 \phi_4 = 0 \qquad (3.9c)$$

$$-\nabla \cdot \left[\frac{6}{143\Sigma_5} \nabla(5\phi_4 + 6\phi_6) + \frac{7}{195\Sigma_7} \nabla(7\phi_6) \right] + \Sigma_6 \phi_6 = 0. \qquad (3.9d)$$

To further modify these equations, we can use a change of variables to create a new group of equations such that the gradients are operating on a single vector:

$$u_1 = \phi_0 + 2\phi_2 \qquad (3.10a)$$

$$u_2 = 3\phi_2 + 4\phi_4 \qquad (3.10b)$$

$$u_3 = 5\phi_4 + 6\phi_6 \qquad (3.10c)$$

$$u_4 = 7\phi_6. \qquad (3.10d)$$

When substituted into Eq (3.9), these terms give:

$$-\nabla \cdot \frac{1}{3\Sigma_1}\nabla u_1 + \Sigma_0 \left[u_1 - \frac{2}{3}u_2 + \frac{8}{15}u_3 - \frac{16}{35}u_4 \right] = -q \tag{3.11a}$$

$$-\nabla \cdot \left[\frac{2}{15\Sigma_1}\nabla u_1 + \frac{3}{35\Sigma_3}\nabla u_2 \right] + \Sigma_2 \left[\frac{1}{3}u_2 - \frac{4}{15}u_3 + \frac{8}{35}u_4 \right] = 0 \tag{3.11b}$$

$$-\nabla \cdot \left[\frac{4}{63\Sigma_3}\nabla u_2 + \frac{5}{99\Sigma_5}\nabla u_3 \right] + \Sigma_4 \left[\frac{1}{5}u_3 - \frac{6}{35}u_4 \right] = 0 \tag{3.11c}$$

$$-\nabla \cdot \left[\frac{6}{143\Sigma_5}\nabla u_3 + \frac{7}{195\Sigma_7}\nabla u_4 \right] + \Sigma_6 \left[\frac{1}{7}u_4 \right] = 0 \, . \tag{3.11d}$$

If we rearrange Eq (3.11) such that only one divergence operation is present in each equation, we can formulate this as a matrix system of 4 equations in the case of the SP_7 approximation:

$$-\nabla \cdot D_n \nabla u_n + \sum_{m=1}^{4} A_{nm}u_m = q_n \qquad n = 1, 2, 3, 4 \, , \tag{3.12}$$

with $\mathbf{u}$ the vector of solution variables:

$$\mathbf{u} = \begin{pmatrix} u_1 & u_2 & u_3 & u_4 \end{pmatrix}^T \, , \tag{3.13}$$

$\mathbf{D}$ the vector of effective diffusion coefficients:

$$\mathbf{D} = \left(\frac{1}{3\Sigma_1} \quad \frac{1}{7\Sigma_3} \quad \frac{1}{11\Sigma_5} \quad \frac{1}{15\Sigma_7} \right)^T \, , \tag{3.14}$$

$\mathbf{q}$ the vector of source terms where the 0th moment source has now been distributed through the system:

$$\mathbf{q} = \left(q \quad -\frac{2}{3}q \quad \frac{8}{15}q \quad -\frac{16}{35}q \right)^T \, , \tag{3.15}$$

and $\mathbf{A}$ a matrix of angular scattering terms:

$$\mathbf{A} = \begin{bmatrix} (\Sigma_0) & (-\frac{2}{3}\Sigma_0) & (\frac{8}{15}\Sigma_0) & (-\frac{16}{35}\Sigma_0) \\[2ex] (-\frac{2}{3}\Sigma_0) & (\frac{4}{9}\Sigma_0 + \frac{5}{9}\Sigma_2) & (-\frac{16}{45}\Sigma_0 - \frac{4}{9}\Sigma_2) & (\frac{32}{105}\Sigma_0 + \frac{8}{21}\Sigma_2) \\[2ex] (\frac{8}{15}\Sigma_0) & (-\frac{16}{45}\Sigma_0 - \frac{4}{9}\Sigma_2) & (\frac{64}{225}\Sigma_0 + \frac{16}{45}\Sigma_2 + \frac{9}{25}\Sigma_4) & (-\frac{128}{525}\Sigma_0 - \frac{32}{105}\Sigma_2 - \frac{54}{175}\Sigma_4) \\[2ex] (-\frac{16}{35}\Sigma_0) & (\frac{32}{105}\Sigma_0 + \frac{8}{21}\Sigma_2) & (-\frac{128}{525}\Sigma_0 - \frac{32}{105}\Sigma_2 - \frac{54}{175}\Sigma_4) & (\frac{256}{1225}\Sigma_0 + \frac{64}{245}\Sigma_2 + \frac{324}{1225}\Sigma_4 + \frac{13}{49}\Sigma_6) \end{bmatrix}. \quad (3.16)$$

Note that the term $\sum_{m=1}^{4} A_{nm} u_m$ in Eq (3.12) couples the moments in each equation while the diffusive term in each equation is only for a single 'pseudo-moment' u_n. As noted by Evans [1], lower order SP_N approximations can be generated by setting higher order even moments in this system to zero (e.g. $\phi_6 = \phi_4 = 0$ yields the SP_3 equations). For these equations, the SP_N order defines the largest order flux moment maintained in the calculation and the P_N order defines the largest order of the cross section expansion maintained.

3.2.1 Eigenvalue Form of the SP_N Equations

For criticality problems, the space, angle, and energy discretizations for the SP_N equations can be applied to the general eigenvalue form of the transport equation given by Eq (3.3). We can readily replace the fixed source in Eq (3.12) with a fission source this time considering the multigroup form of the SP_N equations derived in Appendix B:

$$-\nabla \cdot \left[\frac{n}{2n+1} \mathbf{\Sigma_{n-1}}^{-1} \nabla \left(\frac{n-1}{2n-1} \mathbf{\Phi_{n-2}} + \frac{n}{2n-1} \mathbf{\Phi_n} \right) \right.$$

$$\left. + \frac{n+1}{2n+1} \mathbf{\Sigma_{n+1}}^{-1} \nabla \left(\frac{n+1}{2n+3} \mathbf{\Phi_n} + \frac{n+2}{2n+3} \mathbf{\Phi_{n+2}} \right) \right]$$

$$+ \mathbf{\Sigma_n} \mathbf{\Phi_n} = \frac{1}{k} \mathbf{F} \mathbf{\Phi_n} \delta_{n0} \qquad n = 0, 2, 4, \cdots, N. \quad (3.17)$$

with $\mathbf{\Phi_n}$ the vector of multigroup flux moments and the fission matrix, $\mathbf{F}$, given by [1]. We again apply the change of variables to yield the set of multigroup pseudo-moments $\mathbb{U}_n$ where

now the application of the fission matrix to the moment vectors will be expanded into a set of block matrices in identical fashion to the scattering matrices:

$$-\nabla \cdot \mathbb{D}_n \nabla \mathbb{U}_n + \sum_{m=1}^{4} \mathbb{A}_{nm} \mathbb{U}_m = \frac{1}{k} \sum_{m=1}^{4} \mathbb{F}_{nm} \mathbb{U}_m \qquad n = 1, 2, 3, 4 \,. \tag{3.18}$$

It should be noted here that with respect to a general MCSA scheme, the introduction of fission in the system will only affect the source vector in the linear system for the eigenvalue schemes used in this work. The linear operator, and therefore overall MCSA performance will be dictated by streaming and scattering as defined on the left-hand side.

3.3 Spectral Analysis of the SP_N Equations

Before we can move on to solving the SP_N equations with both conventional and Monte Carlo methods, we must first understand their spectral character to ensure that MCSA will be applicable. As presented in Chapter 2, the spectral radius of the iteration matrix must be less than unity to ensure convergence. Therefore, we will compute the spectral radius of the iteration matrix formed by the SP_N equations while parametrically varying the SP_N order, the P_N order, the number of energy groups, and upscattering/downscattering between energy groups. For each problem in the parameter study, the values given in Table 3.1 were fixed for each spatial location and energy group. Mesh element sizes were the same in all cardinal directions with reflecting conditions on each boundary. For the energy parameter, 1 and 10 energy groups were used with upscatter/downscatter varied for the 10 group case. For the downscatter cases, all groups could scatter to all lower energy groups with the cross sections given in Table 3.1 while for the upscatter case all groups could scatter to all other energy groups with different cross sections for upscatter and downscatter used. A uniform isotropic source of neutrons is given in each group as well.

The matrices generated by the discretization of this problem are sparse with a block-based form as dictated by Eq (B.8). Figure 3.1 gives the sparsity pattern for a monoenergetic SP_7

Parameter	Value
Mesh Element Size	1.0
Mesh Elements	$4 \times 4 \times 4$
Reflecting Boundaries	True
Materials	1
Source Strength	1.0
Total Cross Section	5.0
In-Group Cross Section	0.25
Downscatter Cross Section	1.0
Upscatter Cross Section	0.1
Eigenvalue Solver Tolerance	1.0×10^{-8}

Table 3.1: **Fixed parameters for the SP_N spectral radius parameter study.** *The parameters were fixed for each spatial location and energy group.*
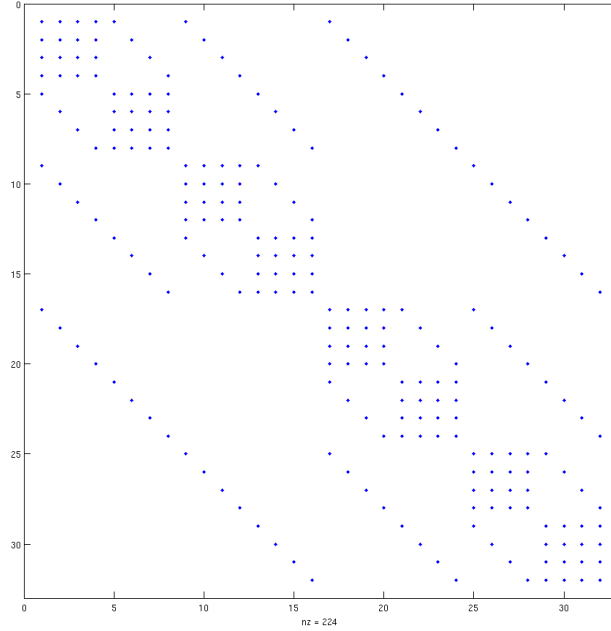
Figure 3.1: **Sparsity pattern for 1-group SP_7 discretization.** *A $2 \times 2 \times 2$ element mesh was used to show detail of the blocks formed by the discretization.*

discretization while Figures 3.2 and 3.3 give the sparsity patterns for the same problem for 10 energy groups without and with upscatter respectively. For these figures, the parameters in Table 3.1 with the number of spatial elements reduced to $2 \times 2 \times 2$ to show the blocks generated by the discretization. We note a few key features of the sparsity plots. The first
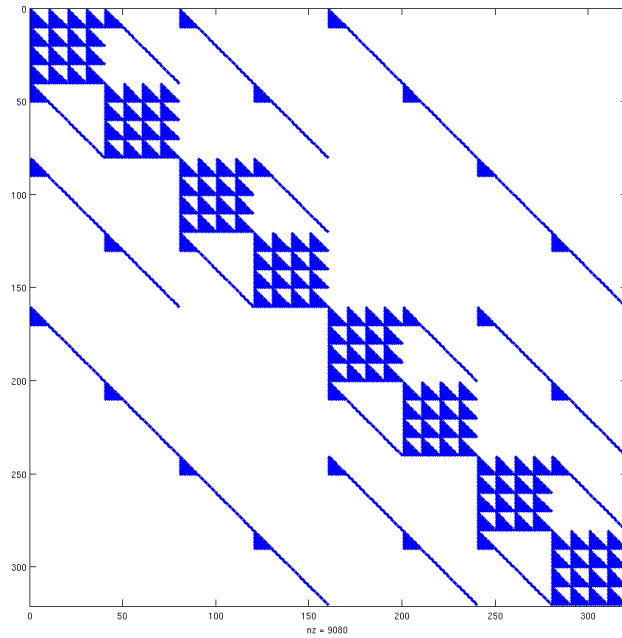
Figure 3.2: **Sparsity pattern for 10-group SP_7 discretization with downscatter only.** *A $2 \times 2 \times 2$ element mesh was used to show detail of the blocks formed by the discretization.*
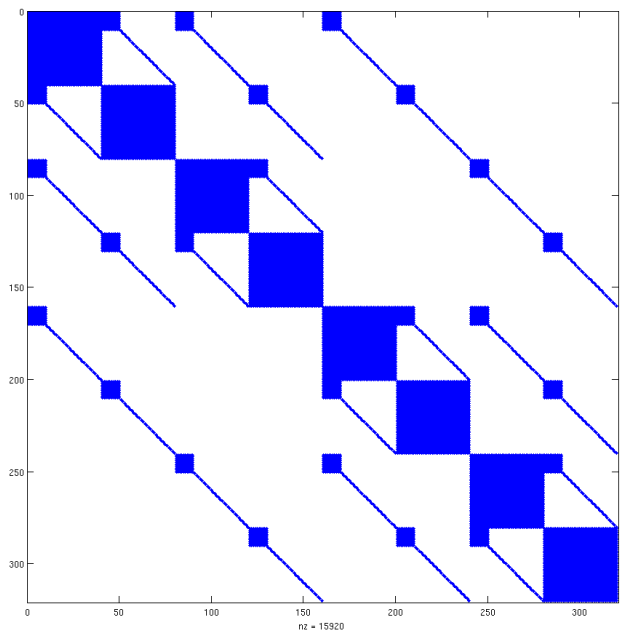
Figure 3.3: **Sparsity pattern for 10-group SP_7 discretization with downscatter and upscatter.** *A $2 \times 2 \times 2$ element mesh was used to show detail of the blocks formed by the discretization.*

is that for multigroup problems without full upscatter and downscatter (i.e. Figure 3.2), the resulting matrix is asymmetric and therefore a linear solver that can handle asymmetric linear systems is required. Nearly all problems of interest will not have full upscattering or downscattering. Second we note the largely diagonal character of these systems, although the blocks from Eq (B.9) are readily apparent. Our first attempt at preconditioning this system will be to use the point Jacobi preconditioning from §2.6.2.1 due to this diagonal form and the success achieved by applying it to MCSA solutions of the thermal radiation diffusion equation as presented in [75].

3.3.1   Point Jacobi Spectral Analysis Results

Spectral radius computations were performed for the cases described above for the point Jacobi preconditioned iteration matrix, $\mathbf{H} = \mathbf{I} - \mathbf{M}^{-1}\mathbf{A}$, with $\mathbf{M} = diag(\mathbf{A})$. Table 3.2 gives the results for the 1-group case, Table 3.3 for the 10-group case with full downscatter only and Table 3.4 for the 10-group case with full downscatter and full upscatter.

		SP_N Order			
		1	**3**	**5**	**7**
	0	0.0635	0.6722	1.3144	1.976
	1	0.0666	0.6728	1.3141	1.9755
P_N Order	**3**	0.0666	0.6822	1.3141	1.9755
	5	0.0666	0.6822	1.3278	1.9847
	7	0.0666	0.6822	1.3278	1.9917

Table 3.2: **Spectral radius results for the point Jacobi preconditioned iteration matrix with 1 energy group.**

It is readily apparent from the tabulated data that point Jacobi preconditioning is insufficient. For problems of order SP_5 and SP_7, the method will not converge at all and for the upscatter case with SP_3 the spectral radius is still quite large for large P_N orders and therefore convergence is expected to be slow. These eigenvalues signal a need for a better preconditioning strategy to both ensure and improve convergence for Monte Carlo methods.

		SP_N Order			
		1	**3**	**5**	**7**
	0	0.0655	0.677	1.32	1.982
	1	0.071	0.6777	1.319	1.982
P_N Order	**3**	0.071	0.687	1.327	1.9872
	5	0.071	0.687	1.336	1.997
	7	0.071	0.687	1.336	1.9995

Table 3.3: **Spectral radius results for the point Jacobi preconditioned iteration matrix with 10 energy groups and full downscatter.**

		SP_N Order			
		1	**3**	**5**	**7**
	0	0.7283	0.81	1.47	2.1446
	1	0.7317	0.8	1.46	2.1368
P_N Order	**3**	0.7317	0.91	1.526	2.2274
	5	0.7317	0.91	1.5344	2.2562
	7	0.7317	0.91	1.5345	2.2842

Table 3.4: **Spectral radius results for the point Jacobi preconditioned iteration matrix with 10 energy groups, full downscatter and full upscatter.**

3.3.2 Block Jacobi Preconditioning

If Monte Carlo methods are to be used to solve the SP_N system of equations, a different preconditioning strategy is required in order to ensure convergence for systems of all SP_N and P_N orders with arbitrary energy group structures. As another means of achieving this, we look back to the sparsity plots we generated in Figures 3.1, 3.2 and 3.3 as well as the multigroup SP_N equations. Initially, the diagonal character of the system and previous success with the thermal radiuation difussion equation led us to try point Jacobi preconditioning with only marginal results. From the sparsity plots we note the block structure that ultimately arises from the multigroup scattering matrices and their insertion into Eq (B.9). When full upscatter and downscatter are used the resulting blocks are completely dense while only downscatter gives a lower triangular scattering matrix and the block structure shown in Figure 3.2.
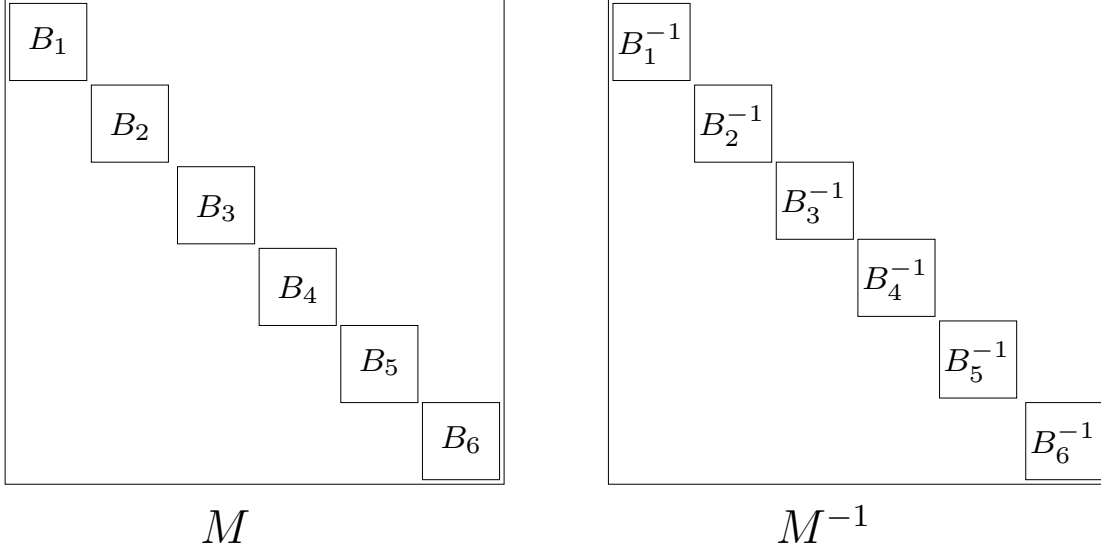
Figure 3.4: **Block Jacobi preconditioning strategy used for the** SP_N **equations.** *Left: The preconditioner is formed by the diagonal blocks of the matrix. Right: Inversion of the preconditioner is trivial and decoupled by block.*

Based on this both block and diagonally dominant structure for matrices formed by the general multigroup SP_N equations, we instead choose *block Jacobi* preconditioning as a left preconditioner for the system. Like point Jacobi preconditioning, block Jacobi preconditioning extracts the diagonal elements of the matrix as the preconditioner where now the elements extracted are the blocks on the diagonal as shown on the left side of Figure 3.4. Shown on the right side of Figure 3.4, inversion of the preconditioner is trivial with each diagonal block inverted separately. For the SP_N equations, Eq (B.9) gives a block size of $N_g \times (N + 1)/2$. In addition, in the limit of a block size of one, the block Jacobi method reduces to the point Jacobi method.

For high performance implementations this has several attractive properties. First, the blocks in the matrix come from the energy/angle discretization of the transport equation as given by Eq (B.9). Each block on the diagonal is bound to a mesh element in the system (note there are 8 blocks on the diagonal in each of the sparsity patterns with a mesh of $2 \times 2 \times 2$) and therefore we expect the matrix elements forming the block to be entirely local

in domain decomposed calculations. Second, these blocks are typically dense and nearly lower triangular for many transport problems meaning that established dense matrix methods can be used for fast inversion.

3.3.3   Block Jacobi Spectral Analysis Results

Spectral radius computations for the block Jacobi preconditioned iteration matrix were performed for the same problems as the point Jacobi preconditioned case. Table 3.5 gives the results for the 1-group case, Table 3.6 for the 10-group case with full downscatter only and Table 3.7 for the 10-group case with full downscatter and full upscatter. A block size of $N_g \times (N+1)/2$ was used for the preconditioner in all cases.

		SP_N Order			
		1	**3**	**5**	**7**
	0	0.0635	0.1269	0.1444	0.1513
	1	0.0666	0.1315	0.1474	0.1534
P_N Order	**3**	0.0666	0.1365	0.154	0.1592
	5	0.0666	0.1365	0.1562	0.163
	7	0.0666	0.1365	0.1562	0.164

Table 3.5: **Spectral radius results for the block Jacobi preconditioned iteration matrix with 1 energy group.**

		SP_N Order			
		1	**3**	**5**	**7**
	0	0.0647	0.1275	0.1449	0.1514
	1	0.0686	0.1338	0.1484	0.1547
P_N Order	**3**	0.0687	0.1399	0.1582	0.1625
	5	0.0692	0.1399	0.1582	0.1657
	7	0.0678	0.1393	0.1624	0.166

Table 3.6: **Spectral radius results for the block Jacobi preconditioned iteration matrix with 10 energy groups and full downscatter.**

From the tabulated block Jacobi data it is clear that this is a viable preconditioning choice for all SP_N problems in terms of Monte Carlo solution methods. All cases were observed to

		SP_N Order			
		1	**3**	**5**	**7**
	0	0.1887	0.2267	0.2285	0.2286
	1	0.4535	0.5044	0.5045	0.5045
P_N Order	**3**	0.4535	0.6453	0.6506	0.6506
	5	0.4535	0.6453	0.6802	0.6818
	7	0.4535	0.6453	0.6802	0.6927

Table 3.7: **Spectral radius results for the block Jacobi preconditioned iteration matrix with 10 energy groups, full downscatter and full upscatter.**

have a spectral radius below unity and often significantly smaller than that, greatly improving convergence rates over the point Jacobi preconditioned problem. Based on these results, the block Jacobi method should be the first preconditioning strategy applied to more complicated problems representative of physical nuclear systems.

3.4 Fuel Assembly Criticality Calculations

Fuel assembly calculations are a critical piece of nuclear engineering infrastructure for reactor core analysis and design. At this level, individual fuel pins may be resolved at fine resolution in a variety of configurations. As a sophisticated problem of interest to push the limits of MCSA, a hot zero-power 17×17 pin assembly will be used with varying energy group structure and SP_N discretization in a criticality calculation. A cross section along the vertical axis showing homogenized fuel pin, control rod, and moderator materials and the associated grid is given by Figure 3.5 while a cross section of the materials configuration along the horizontal axis is given by Figure 3.6. A detailed view of the assembly bottom is given in Figure 3.7. On the top and bottom of the assembly, vacuum conditions are used as well as on the top and right boundaries in Figure 3.5. Reflecting conditions are used on the left and bottom boundaries of Figure 3.5, effectively giving a representation of one quarter of the assembly. For the spatial discretization, each fuel pin (gray regions in Figure 3.5) is resolved by a 2×2 mesh with materials and cross sections homogenized over this region.
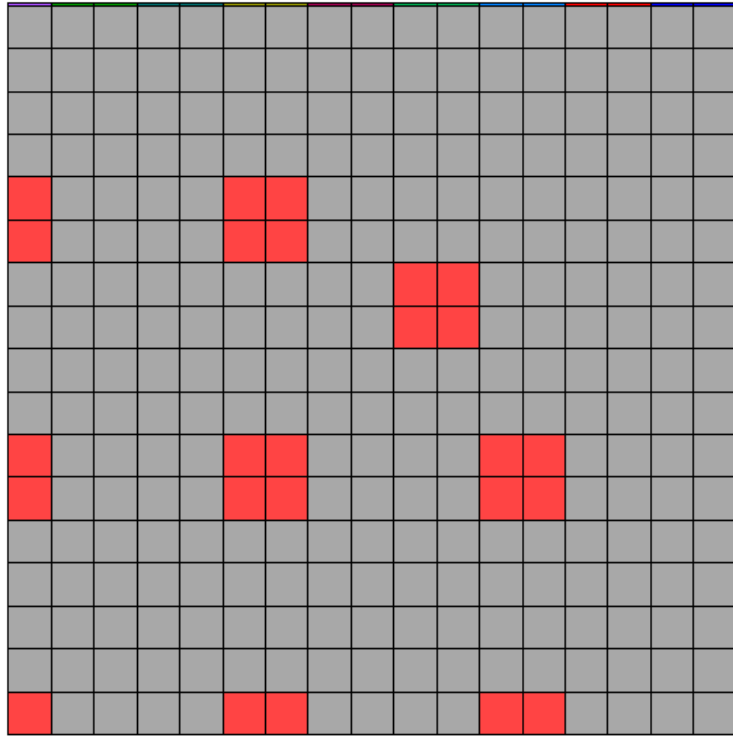
Figure 3.5: **Fuel assembly mesh and geometry cross section.** *Reflecting boundaries are used on the left and lower boundaries to create a complete 17×17 assembly geometry. Gray regions are homogenized fuel and red regions are homogenized control rods. The control rods were removed for these problems. Each fuel pin is resolved by a 2×2 mesh.*
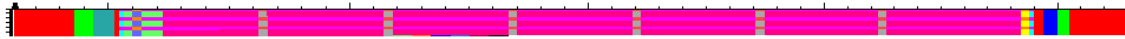
Figure 3.6: **Fuel assembly geometry cross section.** *The geometry is subdivided along the axial direction into 50 zones spaced to capture material boundaries. Important details include spacer grids along the length of the fuel pins and reactor core structures on the top and bottom of the assembly. Lighter purple material in the center of the assembly is moderator and darker purple/red material is fuel.*

Significant geometric details are contained in the model including spacer grids, fuel pins with homogenized cladding and gas gap, core plenum, and moderator with boron. Group cross sections and other discrete nuclear data are generated as needed by a cross-section processing module dependent on the meshing parameters used to discretize the geometry and single-dimension pin-cell calculations for initial flux spectrum generation. Table 3.8 gives
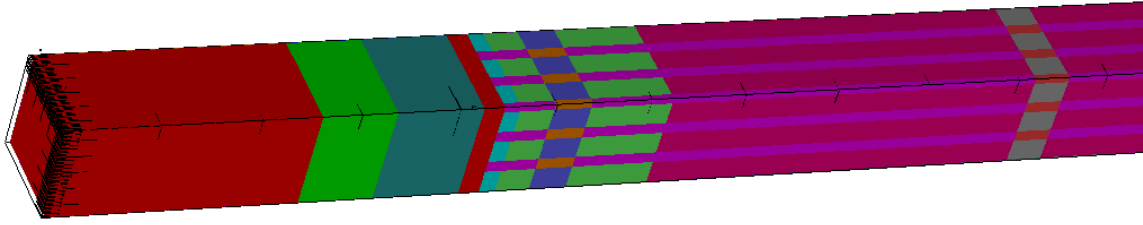
Figure 3.7: **Fuel assembly geometry end detail.** *Reactor core structure including spacer grids and plenum has been included. Lighter purple material on the right of the figure is moderator and darker purple/red material is fuel.*

the primary design parameters for the fuel assembly calculations.

Parameter	Value
Power Level	0 MW
Inlet Temperature	326.85C
Fuel Temperature	600C
Boron Concentration	1300 ppm
Moderator Density	0.743 g/cc
Helium Density	1.79×10^{-4} g/cc
Zirconium Density	6.56 g/cc
Stainless Steel Density	8.0 g/cc
Inconel Density	8.19 g/cc
UO2 Density	10.257 g/cc
Fuel Pin Radius (w/o clad)	0.4096 cm

Table 3.8: **Design parameters for the** 17×17 **pin fuel assembly criticality calculation.**

To generate the multiplication factor and steady-state flux distribution for this problem, at every eigenvalue iteration MCSA is used to solve the resulting SP_N problem using the provided fission source. Algorithm 3.1 presents the use of MCSA within a power iteration strategy to find the multiplication factor. Here, $\mathbf{M}$ is the transport operator generated on the left-hand side of the SP_N discretization, $\mathbf{F}$ is the fission matrix, and $\mathbf{\Phi}$ the multigroup neutron flux. This problem is significantly more complicated than the simple test problem used for the previous spectral analysis. Fission has been introduced into the set of equations and the addition of moderator into the system will increase the amount of scattering, creating a significantly

---

Algorithm 3.1 Power Iteration MCSA Scheme

k_0 = initial guess
$\mathbf{\Phi}_0$ = initial guess
$n = 0$
while $\left| \frac{k^n - k^{n-1}}{k^n} \right| < \epsilon$ **do**   ▷ Iterate until convergence of the eigenvalue
$\quad \mathbf{M}\mathbf{\Phi}^{n+1} = \frac{1}{k^n}\mathbf{F}\mathbf{\Phi}^n$ ▷ Solve for the new flux state with MCSA
$\quad k^{n+1} = k^n \frac{\int \mathbf{F}\mathbf{\Phi}^{n+1} d\mathbf{r}}{\int \mathbf{F}\mathbf{\Phi}^n d\mathbf{r}}$ ▷ Update the multiplication factor
$\quad n = n + 1$
end while

---

more difficult problem manifesting itself in an iteration matrix with a larger spectral radius. When using MCSA, the linear operator applied to $\mathbf{\Phi}^{n+1}$ at each eigenvalue iteration will dictate convergence and remain unchanged throughout the computation[1] while the addition of fission to the system will only modify the source of neutrons and the multiplication factor at every eigenvalue iteration while not affecting Monte Carlo transport.

3.4.1   Preliminary Jacobi Preconditioned Calculations

Based on the success of block Jacobi preconditioning with the test problem used for the spectral radius parameter study, we use it first to solve the 17×17 fuel assembly problem. A single energy group problem was first solved with SP_1 discretization, effectively giving the one-speed neutron diffusion system for the fuel assembly resulting in 20,088 degrees of freedom in the problem. Figure 3.8 gives the residual infinity norm as a function of iteration for the MCSA linear solve in the first eigenvalue iteration using 25,000 stochastic histories at every iteration for the adjoint Neumann-Ulam solve. Convergence was not achieved as noted by the rapid rise in the residual over a few iterations. Based on the spectral radius computations performed, these results are not in line with expectations for this problem. Additional computations performed with 1×10^6 histories per iteration exhibited the same divergent behavior at a significant computational cost and compute time. Even if the problem

---

[1]The operator will change if, for example, physics feedback through temperature or potentially burnup is considered. These additional physics will modify the cross sections used to assemble $\mathbf{M}$. The calculations presented here will consist of a single eigenvalue calculation with a static $\mathbf{M}$.
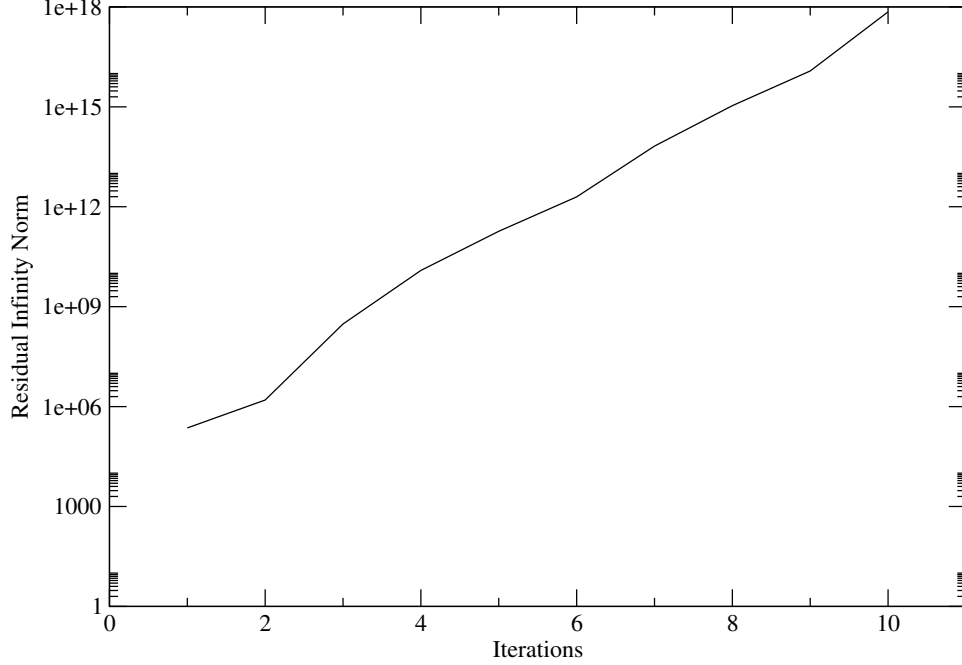
Figure 3.8: **Residual infinity norm vs. iteration for the block Jacobi preconditioned MCSA solve during the first eigenvalue iteration of the 1-group** 17×17 **fuel assembly problem.** *Convergence was not achieved with the block Jacobi preconditioned method.*

may be ill-conditioned, we do expect convergence of MCSA given that the spectral radius requirement was met. To investigate further, a block Jacobi preconditioned Richardson iteration was used to solve the same problem. Figure 3.9 gives the residual infinity norm as a function of iteration for the Richardson linear solve in the first eigenvalue iteration. Poor convergence is observed for the Richardson iteration, however, convergence is achieved meaning that the preliminary eigenvalue criteria needed to satisfy MCSA convergence has also been met. The number of iterations required for the Richardson iteration to converge will give an approximation for the spectral radius via Eq (A.10). With 7291 iterations required to converge to a tolerance of 1×10^{-6}, $\rho(\mathbf{H}) \approx 0.998$, nearing the limits of MCSA applicability and well beyond the spectral radii generated in the initial spectral analysis.

Based on these results, it then appears that even if the simple criteria of a spectral radius of less than one is met and the Richardson iteration will converge with the same
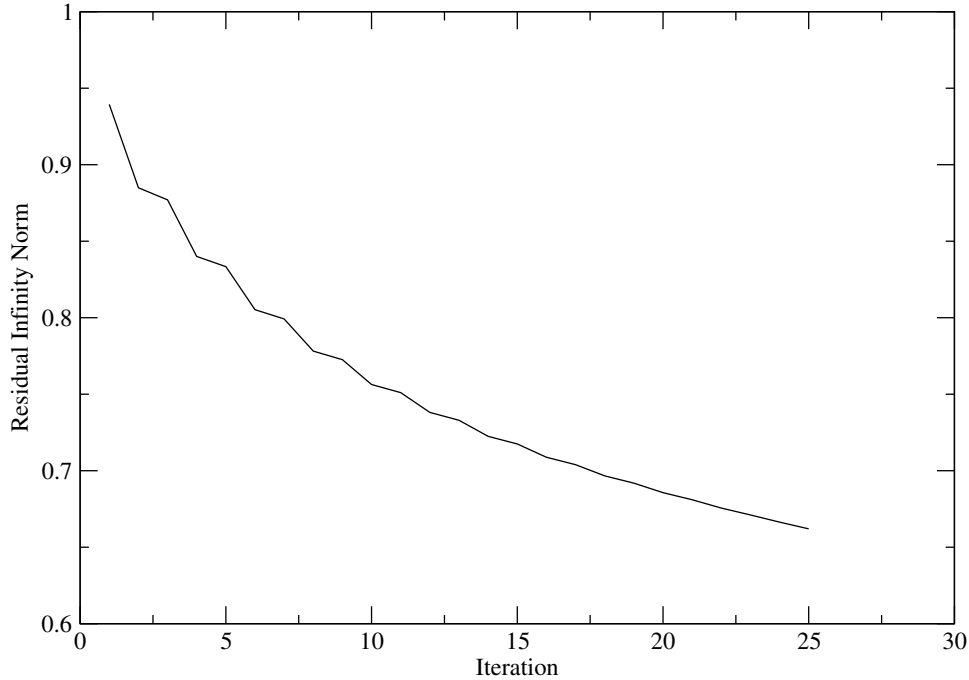
Figure 3.9: **Residual infinity norm vs. iteration for the block Jacobi preconditioned Richardson solve during the first eigenvalue iteration of the 1-group** 17×17 **fuel assembly problem.** *A spectral radius near 1 was observed for the iteration matrix.*

preconditioning, MCSA still may not converge. We then expect the issue to reside with the Neumann-Ulam solve providing the correction as the Richardson iteration is known to provide the correct result. Furthermore, the fact that the spectral radius is less than one means that the stochastic histories in the block Jacobi preconditioned Neumann-Ulam method are eventually being terminated by the weight cutoff as no artificial absorption was used for these preliminary calculations. Based on this, the correction being generated by the Neumann-Ulam solve is the component of MCSA causing a divergent solution.

3.4.2   MCSA Breakdown

For the fuel assembly problem, the initial block Jacobi preconditioned[2] calculations used a one-speed SP_1 discretization, effectively giving a diffusion system. To study the breakdown of MCSA at iteration matrix spectral radii near one, we will use the simpler homogeneous

---

[2]For 1-group SP_1 problems the block size is 1, giving a point Jacobi preconditioner.

2-dimensional one-speed neutron diffusion system presented in Appendix C to isolate this behavior. In this system, we can vary the cross sections while maintaining a fixed grid in order to achieve varying spectral radii. For these studies, we neglect fission as MCSA behavior is dictated by the transport operator $\mathbf{M}$ in an eigenvalue scheme with the fission matrix used to generate a fixed source.

For each solver and estimator combination, the spectral radius of the iteration matrix generated by the diffusion problem was varied by changing the absorption cross section from 0.25 to 100 while fixing the grid size at 100×100 with $h = 0.1$ and a fixed scattering cross section of unity. For each parameter variation, a minimum of one stochastic history per degree of freedom (DOF) in the problem was used to compute the Monte Carlo correction. If the solver could not converge in less than 100 iterations, the number of histories was increased by increments of 5,000 until convergence was achieved in less than 100 iterations. The number of iterations required to converge MCSA and the time to converge was recorded as a means to capture the breakdown.

Figure 3.10 gives the number of iterations required to converge for the chosen number of histories per iteration given by Figure 3.11 using the adjoint solver with the collision and expected value estimators and the forward solver with the collision estimator. For spectral radii less than 0.97, all MCSA problems converged with 1 history per DOF (10,000 for this problem) with the number of iterations required to converge increasing as a function of spectral radius. Near a spectral radius of 0.97, the number of histories required to converge MCSA in less than 100 iterations takes a dramatic rise that exhibits neither exponential nor power law behavior. As the spectral radius approaches 1, the number of histories required becomes significant and effectively impractical to compute. Even with this simple diffusion problem, the behavior is consistent with that observed for the fuel assembly problem with SP_1 discretization. In that case, we estimated a spectral radius of ≈ 0.998, larger than any of the spectral radii that could be computed within even 90 minutes of compute time for this simple two dimensional problem. For that problem, even 1,000,000 histories (≈ 50 per
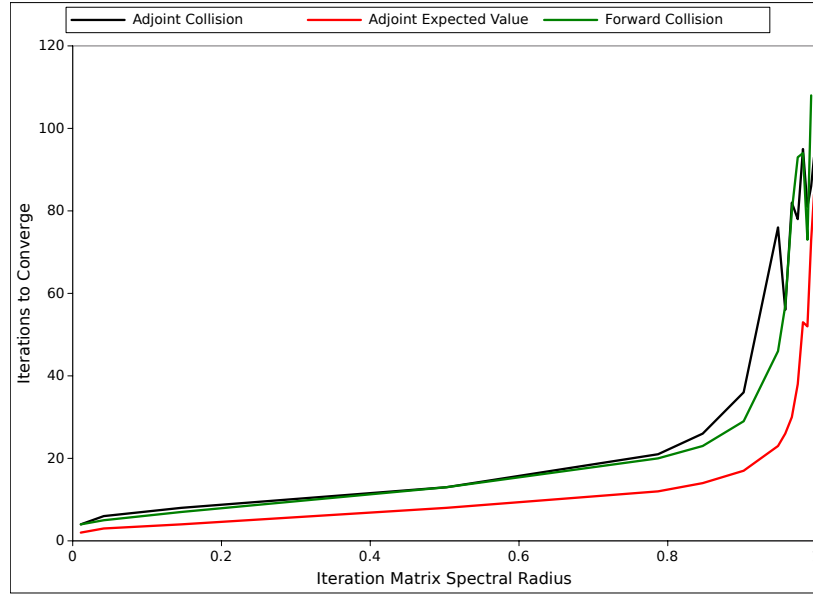
Figure 3.10: **Iterations required to converge as a function of spectral radius for the neutron diffusion problem.** *The number of histories was increased to achieve convergence in less than 100 iterations. At least 10,000 histories were used for each calculation.*

DOF) was not enough to provide convergence. Even if single solve times of an hour can be tolerated, dozens of solves are typically required to compute the multiplication factor and flux spectrum within the SP_N eigenvalue scheme for more difficult problems like the fuel assembly, making the method unusable.

In addition to the significantly larger number of histories required to achieve convergence for ill-conditioned problems another penalty is paid due to histories that take longer to compute. Figure 3.12 gives the CPU time in seconds required to compute a single random walk averaged over the entire set of histories run in the calculation over all iterations. As the spectral radius increases (correlating to a higher ratio of scattering in the system) the random walk lengths increase, using more CPU time to finish the computation. Compared to spectral radii of 0.5, larger spectral radii over 0.97 have histories that require two orders of magnitude more computation time. This significant increase in computation time per history coupled with the significant increase in the number of histories required to converge is evidence that for problems with spectral radii above ≈ 0.97, using MCSA to solve any
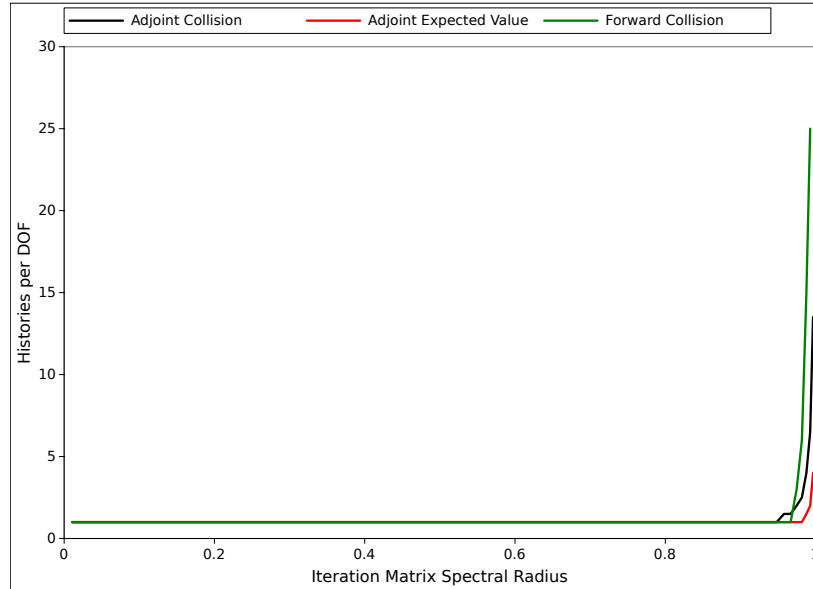
Figure 3.11: **Histories per DOF required to converge as a function of spectral radius for the neutron diffusion problem.** *The number of histories was increased to achieve convergence in less than 100 iterations. At least 10,000 histories were used for each calculation with 10,000 DOFs in the problem.*

problems of interest is entirely ineffective and not practical. At iteration matrix spectral radii this large, using significant numbers of stochastic histories in the Monte Carlo solve are not enough to reduce the stochastic uncertainty in the correction, causing the MCSA sequence to diverge instead of accelerating convergence. We therefore require a more expansive set of preconditioning techniques to move the eigenvalue spectrum of the SP_N problem into a regime in which MCSA is more applicable and in which performance is improved.
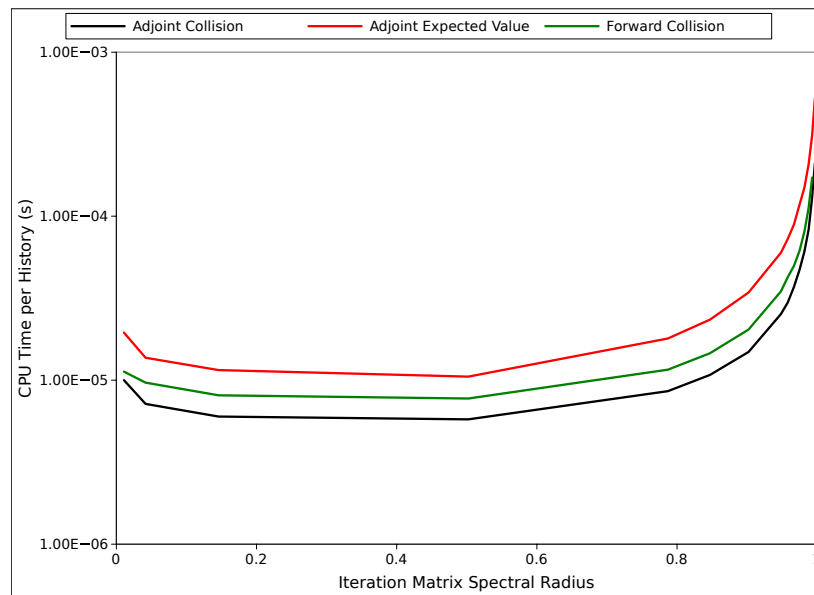
Figure 3.12: **CPU time per history as a function of spectral radius for the neutron diffusion problem.** *As the spectral radius grows, so do the length of the random walks. Longer random walks require more CPU time to compute.*

3.5   Advanced Preconditioning Strategies

For the fuel assembly criticality problem presented in the previous section, the spectral radius was near one using Jacobi preconditioning and in a regime in which MCSA breakdown is observed. In this regime the number of stochastic histories required to converge MCSA increases rapidly and the resulting poor performance is compounded by those histories being increasingly expensive to compute. To overcome this difficulty, advanced preconditioning strategies for the SP_N problem are required beyond simple Jacobi methods that can reduce the spectral radius into a region of better MCSA performance. Several modern algebraic preconditioning strategies will be presented here and used within the explicit preconditioning framework given by Eq (2.76). Data showing their effects on MCSA solutions of the fuel assembly criticality problem will be presented.

3.5.1   ILUT Preconditioning

Incomplete lower-upper (ILU) factorizations of the linear operator can be used a simple mechanism to form an approximate inverse of a preconditioner. To build the factorization, the sparse upper and lower triangular factors, $\mathbf{L}$ and $\mathbf{U}$, are computed such that the residual matrix formed by the factorization [56]:

$$\mathbf{R} = \mathbf{LU} - \mathbf{A} \,, \tag{3.19}$$

has a specified sparsity pattern and element magnitude. When a magnitude threshold is used, elements generated in the factors below that magnitude are dropped, resulting in ILU threshold (ILUT) preconditioning. The sparsity pattern in this case is determined from the input matrix to be preconditioned and the number of elements maintained in the factor is specified by a fill level parameter. A fill level of 1 will generate the same number of elements as the sparsity pattern of the input matrix while a fill level of 2 will contain twice as many

elements in the factorization, resulting in a better representation of the true LU factorization. The inverse of the lower and upper triangular factors may then be easily inverted by means of simple elimination to produce the preconditioner. For MCSA, $\mathbf{L}^{-1}$ will be used on the left and $\mathbf{U}^{-1}$ on the right to precondition the system.

For modern subspace methods, only the action to the preconditioner on a vector is required for efficient implementations and therefore a triangular solve can be used for this purpose. For the explicit preconditioning scheme presented in Eq (2.76), the fully inverted operator must be generated in order to build the set of probabilities and weights required for Monte Carlo sampling. Therefore, for a linear system of size N, N triangular solves will be required in order to extract the inverse matrices from production ILU implementations. In addition, parallel implementations typically generate lower and upper factors that are only triangular locally, providing an easily parallelizable mechanism to generate the action of the preconditioner inverse. A consequence of this choice for parallel scalability is a degradation of the preconditioning quality as the size of the parallel system is increased. For serial computations, the triangular factorization is potentially exact depending on the parameters chosen while at thousands of parallel tasks, the global triangular factors differ significantly from the true factorization. As a result, more iterations are required at higher levels of parallelism to converge the system and will ultimately degrade overall scalability of the system with respect to total wall time to converge.

MCSA preconditioned with ILUT was used to solve the fuel assembly problem presented in the previous section for a 1-group SP_1 discretization. Unlike the Jacobi preconditioned strategy, convergence was achieved with ILUT preconditioning. To study convergence sensitivity to ILUT parameters, the fill level and drop tolerance were parametrically varied with the number of iterations to converge an eigenvalue iteration for the fuel assembly problem recorded along with the maximum number of non-zero entries observed in all matrix rows for the left/right preconditioned composite linear operator. To provide some sparsity to the factorization, the ILUT drop tolerance was used to drop elements in the extracted

inverse triangular factors. For each calculation, the number of iterations required to converge reported was for a single eigenvalue iteration with 3×10^4 histories at each MCSA iteration to compute the Monte Carlo correction using the adjoint collision estimator. All ILUT calculations reported here were performed on a single CPU and therefore this data does not take into account the aforementioned effects of parallel decomposition on the quality of the ILUT preconditioning.

Figure 3.13 gives the number of iterations to converge the fixed source problem to a tolerance of 1×10^8. As expected, the higher the fill level chosen for the ILUT factorization, the fewer iterations are required to converge the problem (only 9 MCSA iterations were required to converge the problem for the fill level of 3 and drop tolerance of 1×10^{-5} case). For higher levels of fill, the iterations needed to converge were not as sensitive, signaling that a larger drop tolerance can perhaps be used without a significant degradation in iterative performance. At smaller fill levels, the sensitivity to the ILUT drop tolerance is more significant. For all fill levels used, convergence was not achieved for the fuel assembly problem with a drop tolerance larger than 1×10^{-3}.

Unfortunately, gaining convergence (and excellent iterative performance) with MCSA for the SP_N fuel assembly problem comes at an immediate cost. Figure 3.14 gives the maximum number of non-zero entries in the composite linear operator generated by preconditioning as a function ILUT drop tolerance for varying values of fill level. For the 1-group SP_1 discretization, the original linear operator will contain only a maximum of 7 non-zero entries per row in the system. As observed in Figure 3.14, performing the explicit preconditioning yields composite linear operators with $O(1,000)$ elements in a row for all combinations of fill level and drop tolerance, over 10% of the total row size for this particular problem. This large number of row entries, observed for a significant fraction of rows in the system, creates several problems. First, sparsity is completely destroyed with each state in the system now coupled to over 10% of the total states in the system through the composite iteration matrix. This means that Monte Carlo sampling tables will be large, requiring significant memory to
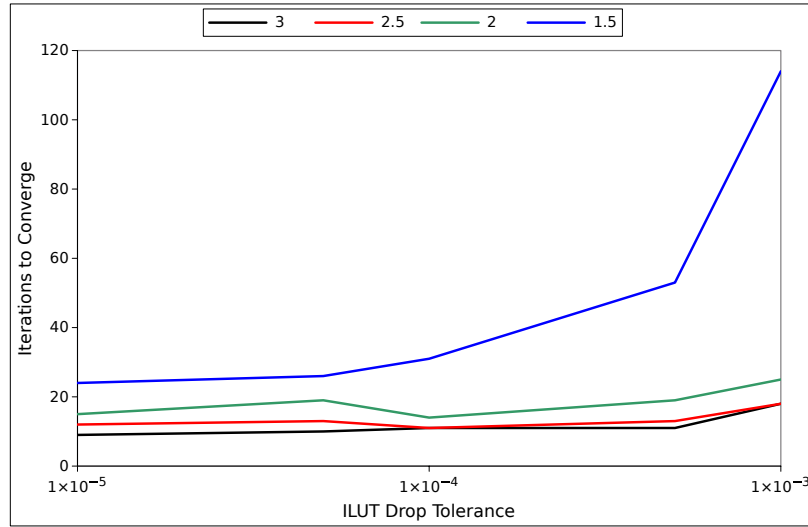
Figure 3.13: **Number of MCSA iterations required to converge an eigenvalue iteration for the fuel assembly problem with ILUT preconditioning as a function of ILUT drop tolerance.** *Each colored curve represents the iteration behavior for a different ILUT fill level. Fill levels of 1.5, 2.0, 2.5, and 3.0 were used.*

store them and a substantial overhead in the sampling procedure during transport. Second, the matrix-matrix multiply operations required to build the composite operator see significant performance losses due to the amount of data that must be handled. In parallel, losing sparsity severely inhibits performance where now parallel operations require communications among orders of magnitude more processors for nearest-neighbor type algorithms.

As a means to assess the quality of the preconditioning, a simple metric is developed to address these concerns and allow comparison to future developments. For our studies, our core performance metric will be iterative performance with the minimum number of MCSA iterations required to converge the problem desired. For Monte Carlo calculations, this improved performance is balanced by the creation of a dense composite system and we seek to reduce the number of non-zero entries to a minimum value in order to lower the amount of coupling among states in the system and reduce the amount of memory used along with the potential latency overhead. Given these two objectives, the following metric is
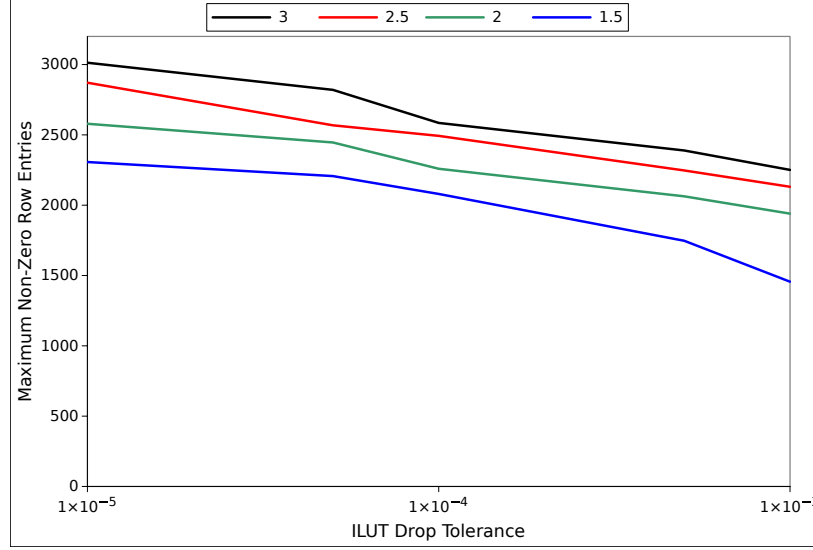
Figure 3.14: **Maximum number of non-zero entries observed for all rows in the composite linear operator for the fuel assembly problem with ILUT preconditioning given as a function of ILUT drop tolerance.** *Each colored curve represents the row size for a different ILUT fill level. Fill levels of 1.5, 2.0, 2.5, and 3.0 were used.*

proposed:

$$\text{Quality Metric} = (\#\ \text{iterations}) \times (\text{maximum}\ \#\ \text{non-zero values}), \qquad (3.20)$$

where the highest quality preconditioning is one that minimizes this metric. For the ILUT preconditioned data provided, Figure 3.15 provides the computed metric as a function of ILUT drop tolerance for each fill level used. In general, the metric is similar to the data observed for the number of iterations required to converge as the non-zero row entries changed by a smaller fraction over drop tolerances tested.

It should be noted here that although only the behavior of the linear solve during a single eigenvalue iteration is reported, the behavior of the linear solver was observed to be consistent throughout the eigenvalue iterations (25 total eigenvalue iterations were required to converge the 1-group SP_1 problem). We expect this as the linear operator (which is unchanging in the fuel assembly criticality problem) dictates the convergence of MCSA. At each iteration
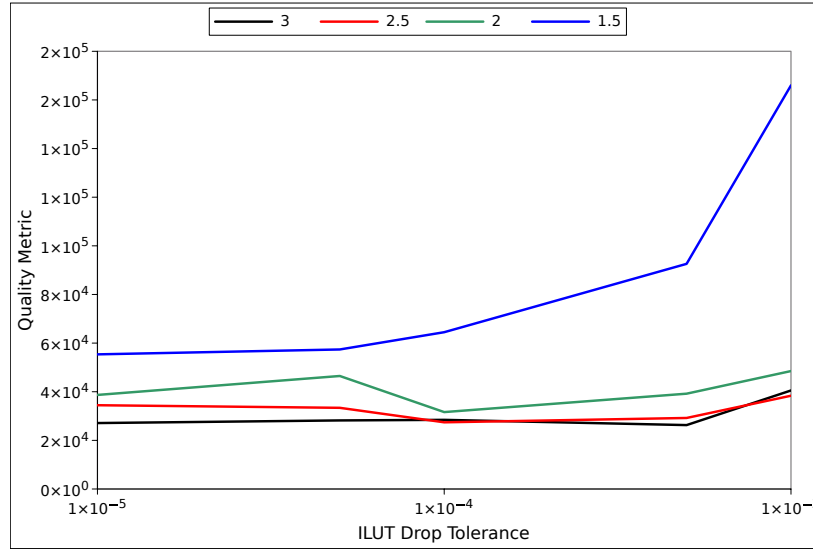
Figure 3.15: **ILUT preconditioning quality metric for the fuel assembly problem given as a function of ILUT drop tolerance.** *Each colored curve represents the quality metric behavior for a different ILUT fill level. Fill levels of 1.5, 2.0, 2.5, and 3.0 were used.*

the fission source provided to the linear problem is changing, however, we expect the same convergence behavior for all source vectors $\mathbf{b} \in \mathbb{R}^N$ where $||\mathbf{b}||_1 \neq 0$.

3.5.2   Sparse Approximate Inverse Preconditioning

Explicit formation of the preconditioner inverse is a requirement of the current MCSA preconditioning strategy. As a result, although ILUT preconditioning provided excellent iterative performance, a significant time penalty is paid to extract the inverse of the triangular factors through N triangular solves. In addition, this explicit inversion yielded a composite linear operator that was dense, requiring modification of the system in order to achieve better scalability and Monte Carlo performance. Sparse approximate inverse (SPAINV) preconditioning is a technique that may potentially alleviate both of these constraints at the cost of reduced iterative performance. The method produces a sparse approximation of the

inverse matrix directly by minimizing the Frobenius norm of the residual matrix [56]:

$$||\mathbf{I} - \mathbf{AM}||_F^2 = \sum_{j=1}^{N} ||\mathbf{e}_j - \mathbf{Am}_j||_2^2 \, , \tag{3.21}$$

where the inverse preconditioning matrix $\mathbf{M}$ minimizes the norm on the right and $\mathbf{e}_j$ and $\mathbf{m}_j$ are the jth columns of the identity and preconditioning matrices respectively. Here, $\mathbf{M}$ is the actual inverse of the preconditioner and is formed directly by the algorithm. On the right hand side of Eq (3.21), the Frobenius norm is represented as a effective sum of N linear system residual norms.

A few iterations of a subspace method or other iterative scheme can be used to effectively solve these systems to a loose tolerance and yield the columns of the approximate preconditioning matrix. At each iteration, threshold values are used to eliminate the components of each $\mathbf{m}_j$ column to maintain the desired level of sparsity. In addition, a sparsity pattern can be predetermined and enforced during this process. For the SPAINV implementation used for this work, the sparsity pattern was defined by levels such that a level of N for an input operator $\mathbf{A}$ will generate a preconditioning matrix $\mathbf{M}$ with the same sparsity pattern as $\mathbf{A}^{N+1}$. By using the norm minimization strategy instead of a factorization such as ILUT, parallel results are reproduced regardless of parallel problem size, meaning that a serial computation will converge in the same number of iterations as a computation with thousands of cores.

MCSA preconditioned with SPAINV was used to solve the fuel assembly problem as with ILUT for a 1-group SP_1 discretization. To study convergence sensitivity to SPAINV parameters, the number of levels in the sparsity pattern and threshold were parametrically varied with the number of iterations to converge a single eigenvalue iteration for the fuel assembly problem recorded along with the maximum number of non-zero entries observed in all matrix rows for the preconditioned composite linear operator. For each calculation, the number of iterations required to converge reported was for a single eigenvalue iteration with 3×10^4 histories at each MCSA iteration to compute the Monte Carlo correction using

the adjoint collision estimator. All SPAINV calculations reported here were performed on a single CPU.

Figure 3.16 gives the number of MCSA iterations needed to converge the fuel assembly problem and Figure 3.17 the maximum number of non-zero entries per row observed in the composite linear operator as a function the SPAINV threshold. For this analysis, the number of levels in the sparsity pattern was varied from 3 to 7 with convergence of the fuel assembly problem not achieved for smaller level values. Compared to ILUT preconditioning, at higher levels we see comparable iterative performance with a relative invariance to the threshold value. The threshold did have a significant effect, however, on the time required to generate the preconditioner with a threshold of 0.001 over an order of magnitude slower than a threshold of 0.01 due to the inclusion of a significant number of extra values in the input operator. In addition to comparable iterative performance, the sparsity of the composite operator is greatly improved with nearly an order of magnitude reduction in number of non-zero entries per row for lower level values.

With the comparable iterative performance and improved sparsity, SPAINV preconditioning should then have a more favorable quality metric than ILUT preconditioning. Figure 3.18 gives the quality metric as a function of the threshold value for each of the sparsity levels computed. Not only do we see an improved quality metric over ILUT preconditioning (about an order of magnitude less), but we also note that the ideal sparsity level is not the largest nor the smallest. In fact, the largest and smallest levels (3 and 7) performed the worst in terms of the quality metric with a level of 4 performing the best. When CPU time to generate the preconditioner is considered, 4 is the clear choice for this problem as more time is required to do the approximate inversion as the sparsity pattern of the preconditioner grows in size.
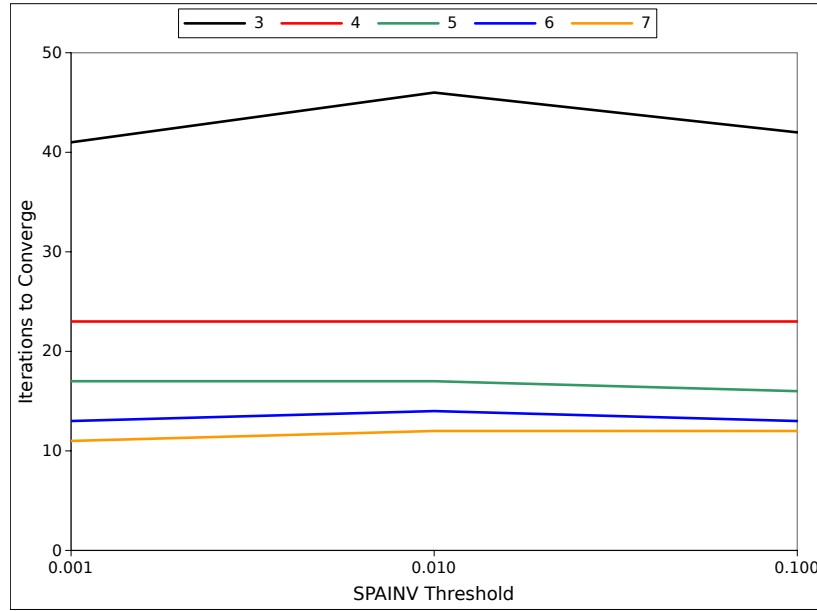
Figure 3.16: **Number of MCSA iterations required to converge a single eigenvalue iteration for the fuel assembly problem with SPAINV preconditioning as a function of SPAINV threshold.** *Each colored curve represents the iteration behavior for a different SPAINV level pattern. Levels of 3, 4, 5, 6, and 7 were used.*
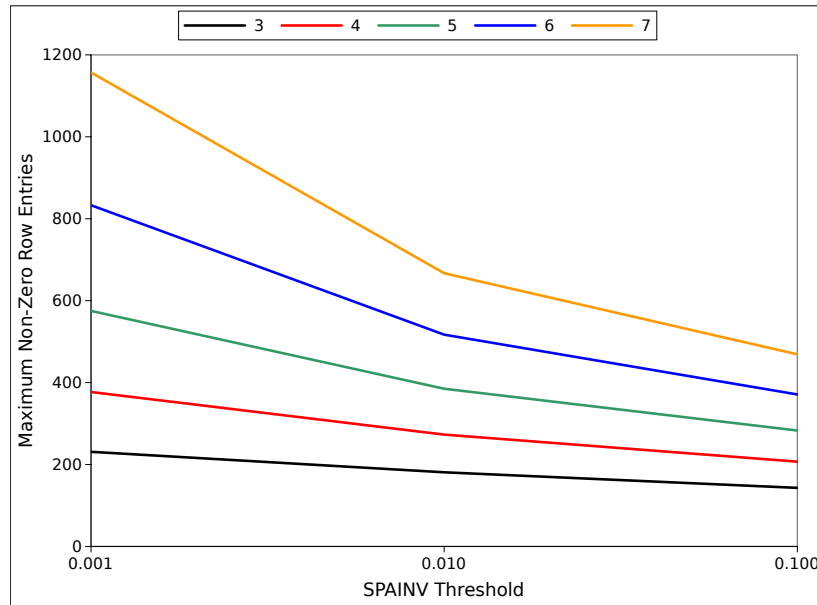
Figure 3.17: **Maximum number of non-zero entries observed for all rows in the composite linear operator for the fuel assembly problem with SPAINV preconditioning given as a function of SPAINV threshold.** *Each colored curve represents the row size for a different SPAINV level pattern. Levels of 3, 4, 5, 6, and 7 were used.*
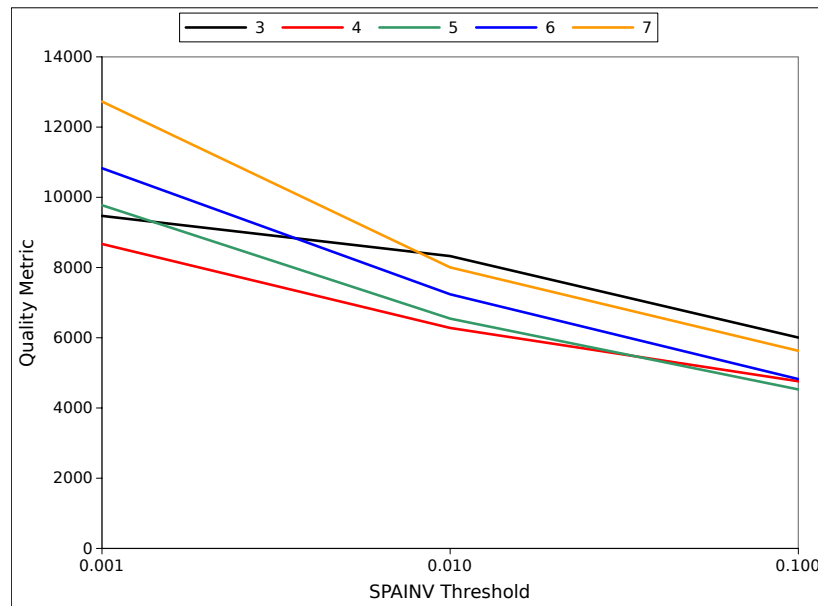
Figure 3.18: **SPAINV preconditioning quality metric for the fuel assembly problem given as a function of SPAINV threshold.** *Each colored curve represents the quality metric behavior for a different SPAINV level pattern. Levels of 3, 4, 5, 6, and 7 were used.*

3.5.3   SPAINV Improved ILUT Preconditioning

As a means to improve convergence over using only SPAINV preconditioning, ILUT preconditioning may be modified through an additional application of SPAINV (SPAINV-ILUT)[56]. For the ILUT preconditioning case we have the following linear problem to solve for the substituted variable:

$$\mathbf{L}^{-1}\mathbf{A}\mathbf{U}^{-1}\mathbf{u} = \mathbf{L}^{-1}\mathbf{b}\,. \tag{3.22}$$

We then apply SPAINV and minimize the following problem, this time on the left:

$$||\mathbf{I} - \mathbf{M}\mathbf{L}^{-1}\mathbf{A}\mathbf{U}^{-1}||_F^2\,, \tag{3.23}$$

giving a new preconditioned system:

$$\mathbf{M}\mathbf{L}^{-1}\mathbf{A}\mathbf{U}^{-1}\mathbf{u} = \mathbf{M}\mathbf{L}^{-1}\mathbf{b}\,. \tag{3.24}$$

Doing this permits a smaller fill level to be used with ILUT and a lower-order sparsity pattern to be used with SPAINV, giving marginally more sparsity in the resulting composite linear operator while maintaining good iterative performance.

MCSA preconditioned with SPAINV-ILUT was also used to solve the same fuel assembly problem as with the other preconditioners for the same 1-group SP_1 discretization. To study convergence sensitivity to SPAINV-ILUT parameters, the ILUT drop tolerance and ILUT fill level were parametrically varied with the number of iterations to converge a single eigenvalue iteration for the fuel assembly problem recorded along with the maximum number of non-zero entries observed in all matrix rows for the left/right preconditioned composite linear operator. SPAINV parameters for the data presented here were fixed as it was found that the preconditioning quality was largely insensitive to their variation. In addition, the fact that SPAINV is being used to preconditioned a problem already preconditioned with ILUT means that the input matrix sparsity pattern is already somewhat dense and large SPAINV

levels would result in an even denser system. Therefore, a smaller SPAINV sparsity pattern level will be used for this preconditioning. For each calculation, the number of iterations required to converge reported was for a single eigenvalue iteration. Again, 3×10^4 histories are used at each MCSA iteration to compute the Monte Carlo correction using the adjoint collision estimator. All SPAINV-ILUT calculations reported here were performed on a single CPU.

Figure 3.19 gives the number of iterations required to converge as a function of ILUT drop tolerance for ILUT fill levels of 1.5, 2.0, 3.0, 4.0 and 5.0 with a fixed SPAINV threshold of 1.0 and sparsity level of 1. SPAINV threshold values higher than 1.0 resulted in a loss of convergence and lower values did not significantly affect performance. Larger sparsity levels resulted in a composite operator that was too dense and a prohibitive amount of CPU time required to compute the preconditioner. At smaller levels of fill, the benefits of using an additional step of SPAINV preconditioning are readily observed with the number of iterations required to converge cut in half for large drop tolerances. For smaller drop tolerances and higher ILUT levels of fill, the additional step of SPAINV preconditioning offers marginal improvement to iterative performance. As shown in Figure 3.20, because ILUT is used in the preconditioning sequence, sparsity is again lost with only marginally improved non-zero entry numbers due to the application of the SPAINV threshold. As a result, the quality metrics given by Figure 3.21 are only marginally better than those observed for ILUT preconditioning and much larger than the SPAINV quality metric values.
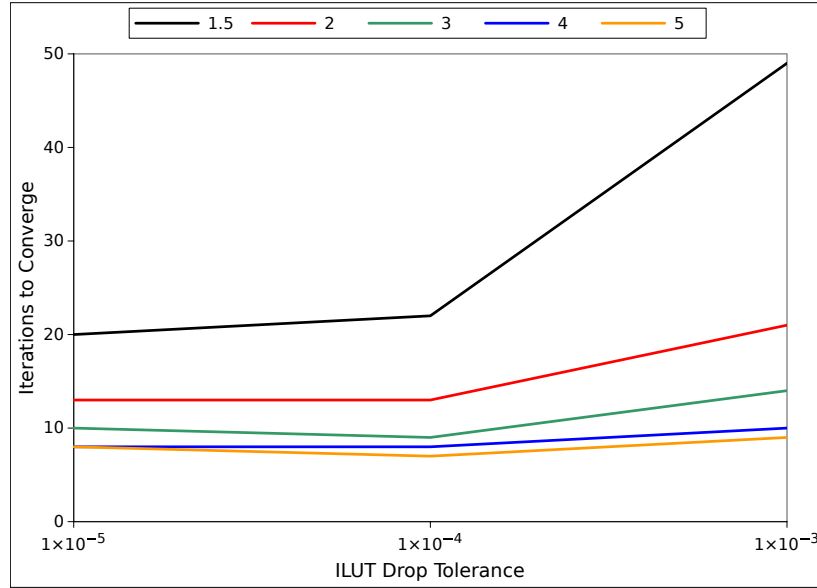
Figure 3.19: **Number of MCSA iterations required to converge a single eigenvalue iteration for the fuel assembly problem with SPAINV-ILUT preconditioning as a function of ILUT drop tolerance.** *Each colored curve represents the row size for a different ILUT fill level. Fill levels of 1.5, 2.0, 3.0, 4.0, and 5.0 were used.*
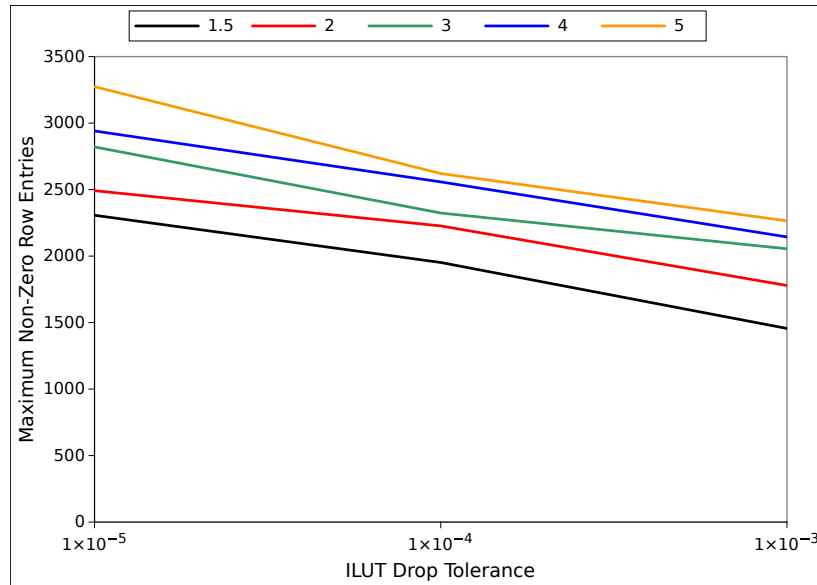
Figure 3.20: **Maximum number of non-zero entries observed for all rows in the composite linear operator for the fuel assembly problem with SPAINV-ILUT preconditioning given as a function of ILUT drop tolerance.** *Each colored curve represents the row size for a different ILUT fill level. Fill levels of 1.5, 2.0, 3.0, 4.0 and 5.0 were used.*
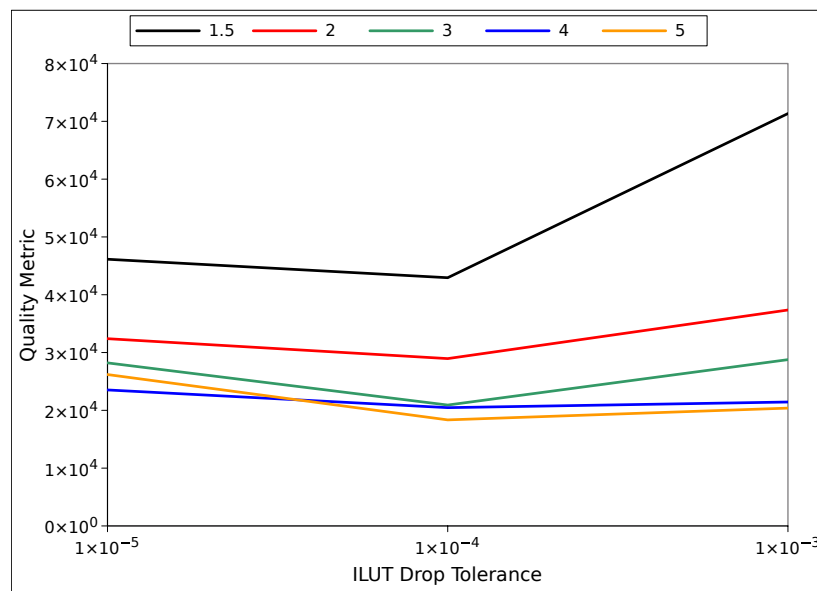
Figure 3.21: **SPAINV-ILUT preconditioning quality metric for the fuel assembly problem given as a function of ILUT drop tolerance.** *Each colored curve represents the row size for a different ILUT fill level. Fill levels of 1.5, 2.0, 3.0, 4.0 and 5.0 were used.*

3.5.4   Applying the Reduced Domain Approximation

For each preconditioning technique presented convergence was achieved for the single fuel assembly problem. However, a primary concern is the number of non-zero states in each row of the system generated by the explicit preconditioning strategy. In many cases, orders of magnitude more matrix elements were generated resulting in poor scalability for domain decomposed algorithms and overall performance issues for Monte Carlo. As outlined in § 2.10.2, the reduced domain approximation may be used as a mechanism to potentially alleviate this problem by filtering elements of the composite matrix in each row that fall below a certain threshold value or by maintaining the largest N elements in each row where N is a designated fill level.

For the ILUT, SPAINV, and SPAINV-ILUT preconditioning strategies the reduced domain approximation will be applied to reduce the density of the composite linear operator to more manageable levels. For each preconditioner, the parameters that achieved the best quality metric results from the previous analysis were used. These correspond to ILUT parameters of a fill level of 5.0 and a drop tolerance of 1×10^{-5}, SPAINV parameters of a sparsity level of 4 and a threshold of 0.1 and SPAINV-ILUT with ILUT parameters of a fill level of 4.0 and a drop tolerance of 1×10^{-5} and SPAINV parameters of a sparsity level of 1 and a threshold of 1.0. The reduced domain threshold was set to 1×10^{-10} in order to eliminate any exceedingly small values from the matrix (often this is simply removing non-zero elements within the floating point tolerance of zero). The reduced domain fill level was then varied, starting with the largest non-zero entries per row value observed for each of the preconditioning types in order to assess its effects relative to the case where no reduced domain approximation was applied.

Figure 3.22 gives the number of iterations required to converge for each preconditioner type as a function of reduced domain fill level. Figure 3.23 gives the corresponding quality metric for each data point where the number of non-zero entries used to compute the metric

is equivalent to the reduced domain fill level. We first note that SPAINV preconditioning alone is significantly more sensitive to the reduction in domain size over the ILUT-based methods, although the preconditioner was of $O(100)$ non-zero entries per row without any approximation applied. For the ILUT-based methods, performance was significantly better with convergence achieved in less than 40 MCSA iterations with only 10 non-zero entries in each row (vs. 7 non-zero entries for the case with no preconditioning). SPAINV-ILUT iterative performance was marginally better than ILUT alone for all reduced domain fill levels. However, it should be noted that the ILUT level of fill used for the ILUT only calculations was set to 4 for this case while the SPAINV-ILUT preconditioner used an ILUT level of fill of 5 and therefore the marginally better performance is more likely a result of this addition of fill rather than the extra SPAINV preconditioning. Looking at the quality metric data, we see a reduction in the quality metric as a function of the reduced domain fill level, achieving 2 orders of magnitude reduction in the quality metric for the ILUT-based preconditioning methods.

Although applying the reduced domain approximation results in a successful recovery of sparsity for the Monte Carlo problem while maintaining good convergence properties, there is still an issue of forming the composite operator before applying the approximation and potentially generating the transpose of this operator in the case of the adjoint Monte Carlo method. Because of this, memory and scaling issues may still be observed when building the probability and weight matrices for the Monte Carlo problem. In addition, the expensive extraction of the inverse of the preconditioning operators for the explicit scheme creates a significant cost in overall performance. Future work in this area should be considerate of these important components of the preconditioned MCSA algorithm.
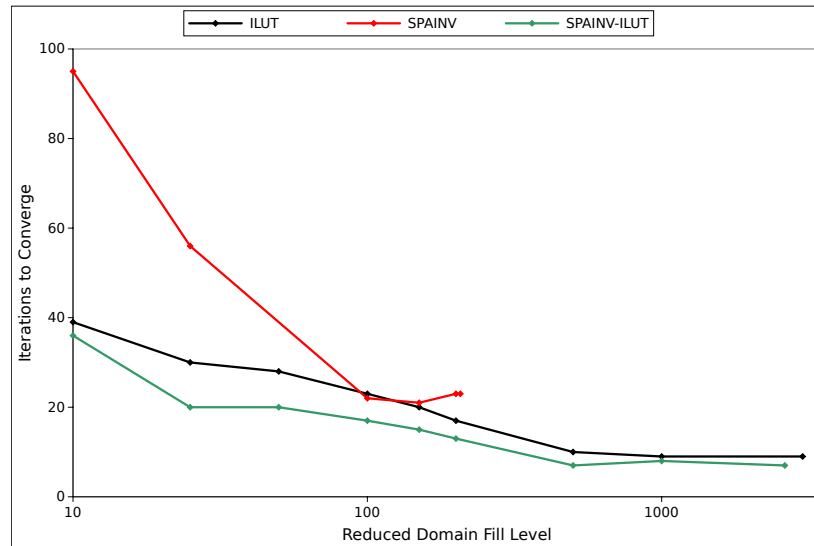
Figure 3.22: **Number of MCSA iterations required to converge a single eigenvalue iteration for the fuel assembly problem with each preconditioning as a function of reduced domain approximation fill level.** *The largest fill level for each preconditioning presented is that using the parameters that gave the best results without the approximation.*
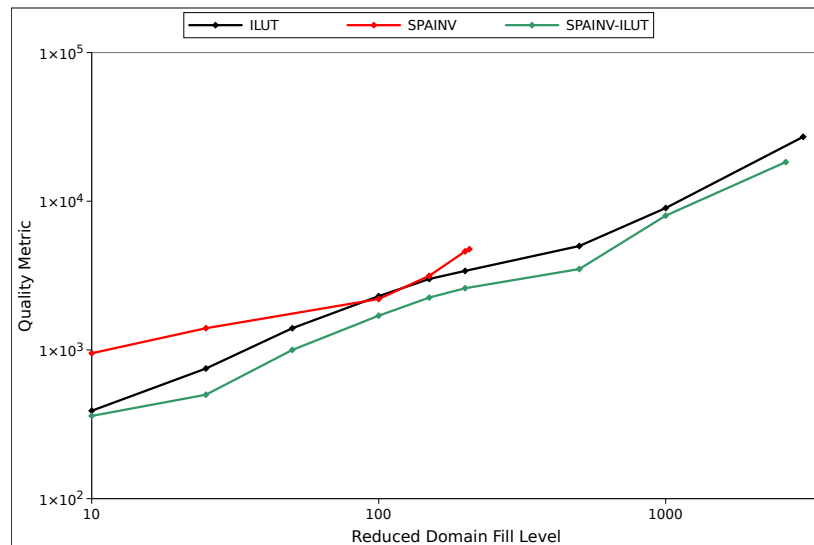
Figure 3.23: **Preconditioning quality metric for the fuel assembly problem given as a function of reduced domain approximation fill level.** *The largest fill level for each preconditioning presented is that using the parameters that gave the best results without the approximation.*

3.5.5 MCSA Relaxation Parameters

As another means of preconditioning (or variance reduction) to meet the goal of improving iterative performance, the Richardson iteration upon which the Neumann-Ulam method is built may be implemented with an adjustable scalar relaxation parameter:

$$\mathbf{x} = \mathbf{x} + \omega \mathbf{r} \,, \tag{3.25}$$

where ω is the relaxation parameter. This is very similar to point Jacobi preconditioning where the system is now being scaled on the left by a constant value in all rows. Analogously, these relaxation parameter techniques can be applied to Monte Carlo to improve convergence as demonstrated by Dimov [7]. In this case, building an iteration matrix from Eq (3.25) gives:

$$\mathbf{H} = \mathbf{I} - \omega \mathbf{A} \,, \tag{3.26}$$

with the probabilities and weights for the Monte Carlo procedure appropriately scaled via a modified Neumann-Ulam decomposition. For MCSA, we can stage this scheme with two separate relaxation parameters; one for the outer Richardson iteration and one for the inner Monte Carlo solve:

$$\mathbf{x}^{k+1/2} = \mathbf{x}^k + \omega_R \mathbf{r}^k \,, \tag{3.27a}$$

$$\mathbf{r}^{k+1/2} = \mathbf{b} - \mathbf{A}\mathbf{x}^{k+1/2} \,, \tag{3.27b}$$

$$\omega_N \mathbf{A} \delta \mathbf{x}^{k+1/2} = \omega_N \mathbf{r}^{k+1/2} \,, \tag{3.27c}$$

$$\mathbf{x}^{k+1} = \mathbf{x}^{k+1/2} + \delta \mathbf{x}^{k+1/2} \,, \tag{3.27d}$$

$$\mathbf{r}^{k+1} = \mathbf{b} - \mathbf{A}\mathbf{x}^{k+1} \,, \tag{3.27e}$$

where ω_R is the Richardson iteration relaxation parameter and ω_N is the Neumann-Ulam Monte Carlo solve relaxation parameter.

We apply these relaxation parameters to the fuel assembly problem along with the reduced domain approximation as a means of studying their effects. For each calculation presented, the number of iterations required to converge reported was for a single eigenvalue iteration. Again, 3×10^4 histories are used at each MCSA iteration to compute the Monte Carlo correction using the adjoint collision estimator. A reduced domain fill level of 100 is used with a threshold of 1×10^{-10} to filter small values. ILUT preconditioning with a drop tolerance of 1×10^{-5} and fill level of 5 is used as well.

Figure 3.24 gives the number of iterations required to converge the fuel assembly problem for a 1-group SP1 discretization using varying combinations of the relaxation parameters. First, both parameters were fixed at the base case of 1 while the other parameter was varied as shown in the left-hand side plots of Figure 3.24. For the Richardson relaxation parameter, using a value larger than 1 gave better iterative performance up to a point, effectively providing a stronger extrapolation using the residual at each iteration. For the Neumann relaxation parameter, a value of less than 1 is observed to be ideal. Although initially counter-intuitive, the fact that the correction computed by the Monte Carlo solver has a stochastic error associated with it means that by using a Neumann relaxation parameter less than 1, the correction and its error are effectively dampened to improve iterative performance. Considering the CPU time required to converge a single eigenvalue iteration, similar results are also observed for the relaxation parameters as given by Figure 3.25. For the base cases given by the plots on the left, it was found the a Richardson relaxation parameter of 1.1 and a Neumann relaxation parameter of 0.7 provided the fastest CPU time for convergence. Fixing each parameter at these new values, the calculations were repeated as shown for the plots on the right hand sides of both Figures 3.24 and 3.25. For each repeated timing calculation, it was found that the same combination of relaxation parameters found in the base cases performed the best although they did not necessarily have the best iterative performance.
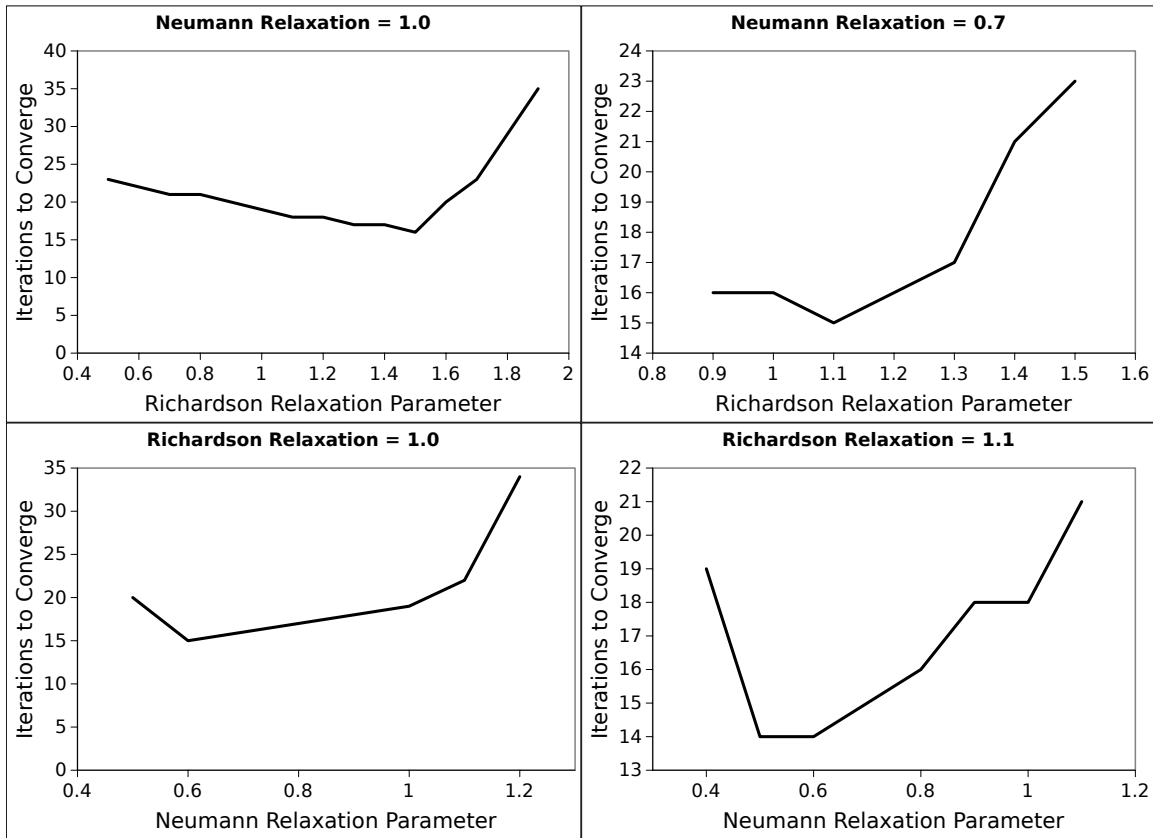
Figure 3.24: **Number of iterations to converge a single eigenvalue iteration of the fuel assembly problem as a function of the relaxation parameters.** *Starting in upper left and moving counter-clockwise: Neumann relaxation parameter fixed at 1.0, Richardson relaxation parameter fixed at 1.0, Neumann relaxation parameter fixed at 0.7, Richardson relaxation parameter fixed at 1.1. For each calculation 3×10^4 stochastic histories were used to compute the MCSA correction at each iteration.*
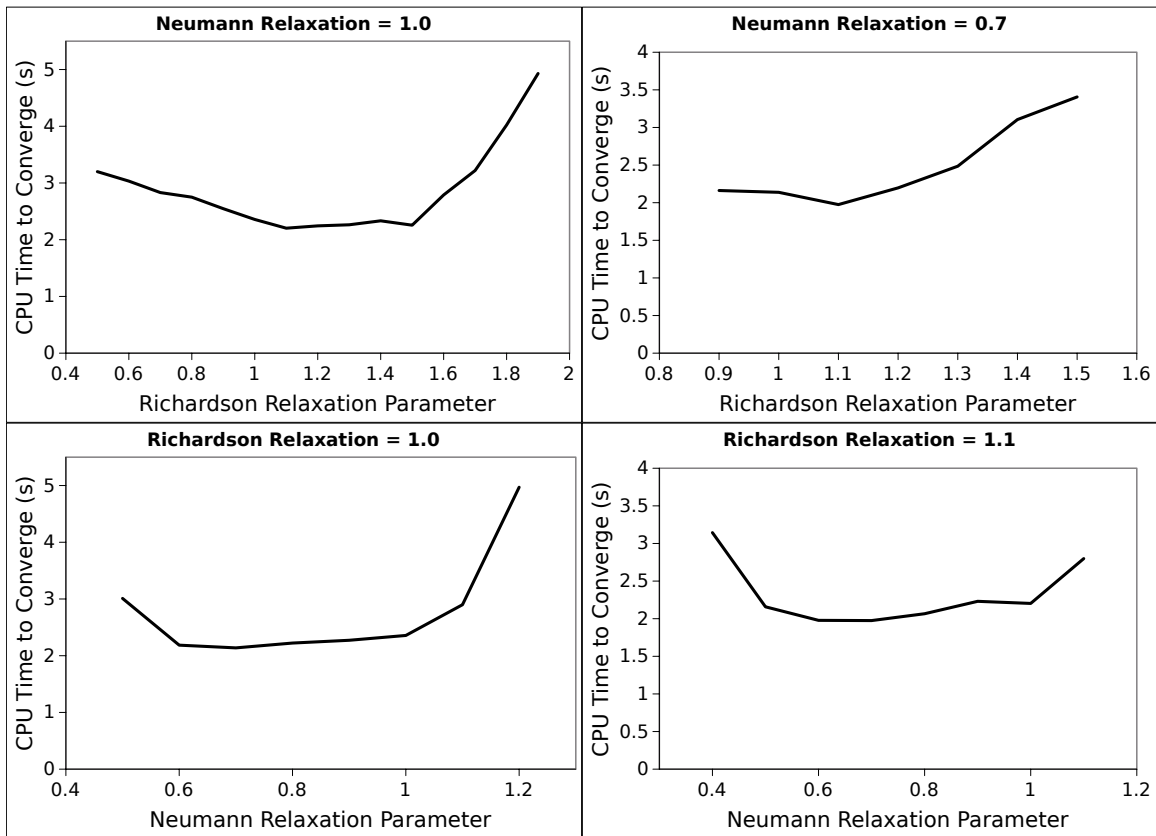
Figure 3.25: **CPU time in seconds to converge a single eigenvalue iteration of the fuel assembly problem as a function of the relaxation parameters.** *Starting in upper left and moving counter-clockwise: Neumann relaxation parameter fixed at 1.0, Richardson relaxation parameter fixed at 1.0, Neumann relaxation parameter fixed at 0.7, Richardson relaxation parameter fixed at 1.1. For each calculation 3×10^4 stochastic histories were used to compute the MCSA correction at each iteration.*

3.5.6 MCSA Estimator and Fixed Point Iteration Analysis

With convergence obtained for the fuel assembly problem, the iterative performance of MCSA will next be studied with both the collision and expected value estimators using the best preconditioning and relaxation parameter combinations found by the previous analysis. Additionally, both the Richardson-based MCSA iteration given by Eq (2.67) and the minimal residual-based MCSA iteration given by Eq (2.69) will be used. Although the expected value estimator achieved the best iterative performance in the previous comparison and analysis for the simple Poisson problem in § 2.9, it is possible that the collision estimator may perform better from a timing perspective due to the sparsity lost by explicit preconditioning. The deterministic component of the expected value estimator that couples the current state to other local states through the iteration matrix stencil requires application of the estimator to potentially several orders of magnitude more states at every transition event.

For this study, the fuel assembly problem with a 1-group SP_1 discretization was solved using MCSA with the adjoint Monte Carlo solver using both the collision and expected value estimators and both the Richardson and minimal residual fixed point iterations. Using the results from the previous section, a Neumann relaxation parameter of 0.7 was used with both estimators and fixed point iterations. For the collision estimator, a Richardson relaxation parameter of 1.1 was used with the Richardson iteration while it was found the expected value estimator had the best performance when a Richardson relaxation parameter of 1.0 was used instead. In addition, ILUT preconditioning with a drop tolerance of 1×10^{-5} and a fill level of 5 was used with a reduced domain approximation fill level of 100 and a threshold of 1×10^{-10} as in the previous analysis. Artificial absorption was also introduced with a value of 0.2 for the MCSA calculations that used the collision estimator as CPU timing performance was improved without a loss in iterative performance while no absorption was used for calculations using the expected value estimator. For each estimator, the number of stochastic histories used to compute the MCSA correction was varied from 25 to 50,000 with

the number of MCSA iterations required to converge to a tolerance of 1×10^{-8} recorded for a single eigenvalue iteration along with the CPU time required to achieve convergence.

Figure 3.26 gives the iteration count results and Figure 3.27 gives the timing results. Remarkably, although the fuel assembly problem is significantly more complicated than the simple Poisson problem studied in § 2.9, the results here are largely the same with Figure 3.26 and Figure 2.11 having identical qualitative behavior. Using the expected value estimator with both fixed point iterations again creates a relative insensitivity to the number of histories used to compute the correction. Marginally better iterative and timing performance was observed for the expected value estimator when using the Richardson iteration. Better timing performance is expected as computing the extrapolation parameter in the minimal residual iteration requires several additional parallel operations. Compared to the collision estimator, the minimal residual iteration permits fewer stochastic histories to be used with each MCSA iteration while still maintaining good iterative performance. With respect to CPU time, there is a more pronounced effect due to the larger density of states created by the explicit ILUT preconditioning. Using a reduced domain fill level of 100 creates a situation where the expected value estimator is significantly more expensive per history to compute that the collision estimator due to the coupling of states.

From both Figure 3.26 and Figure 3.27 we see that both estimators and fixed point iterations have comparable iterative and timing performance when 1,000 histories are used at each MCSA iteration. Using 1,000 histories per MCSA iteration, the infinity norm of the residual vector is presented at every MCSA iteration for both estimators and both fixed point iterations in Figure 3.28 as an additional means of comparison. At this number of histories, all MCSA combinations converge the fuel assembly problem monotonically at approximately the same rate, giving little reason to choose one over the other. The end result is that both estimators provide a viable method for getting good MCSA iterative performance with comparable timing performance. For the collision estimator, using around 20,000 stochastic histories at every iteration gave the best iterative performance while 500 histories per iteration
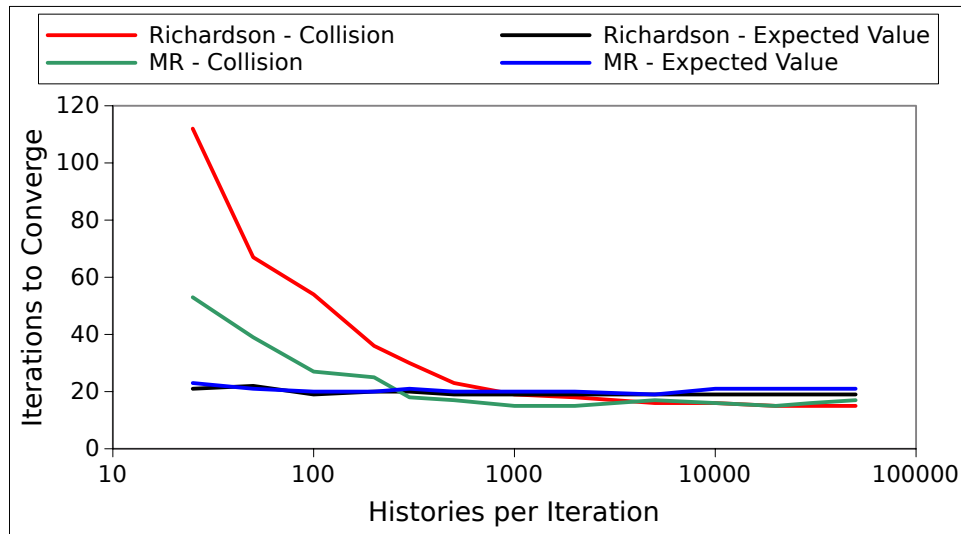
Figure 3.26: **MCSA iterations required to converge the fuel assembly problem to a tolerance of** 1×10^{-8}**.** *Both the collision and expected value estimators were used with the adjoint Monte Carlo solver to compute the correction at each iteration. Each estimator was used with the Richardson and minimal residual fixed point iterations within an MCSA iteration.*
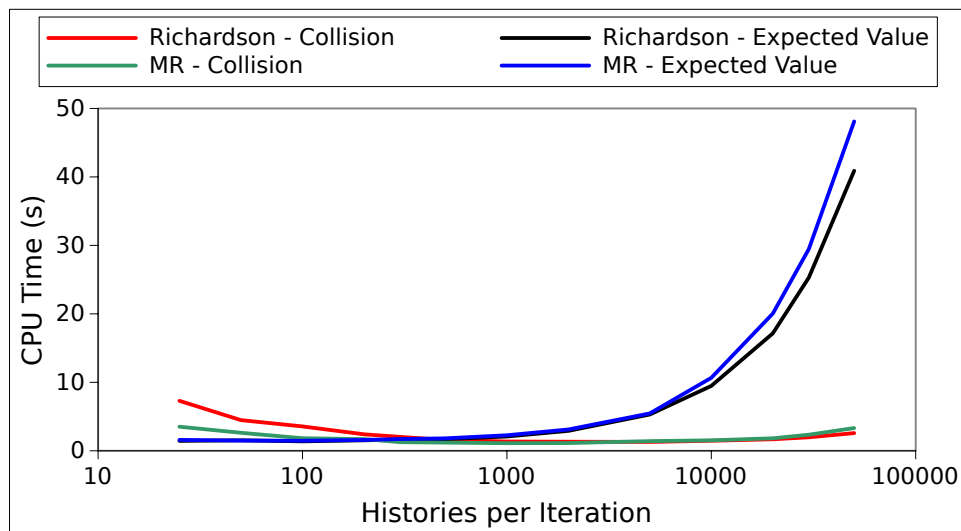
Figure 3.27: **Total CPU time in seconds required to converge the fuel assembly problem to a tolerance of** 1×10^{-8}**.** *Both the collision and expected value estimators were used with the adjoint Monte Carlo solver to compute the correction at each iteration. Each estimator was used with the Richardson and minimal residual fixed point iterations within an MCSA iteration.*
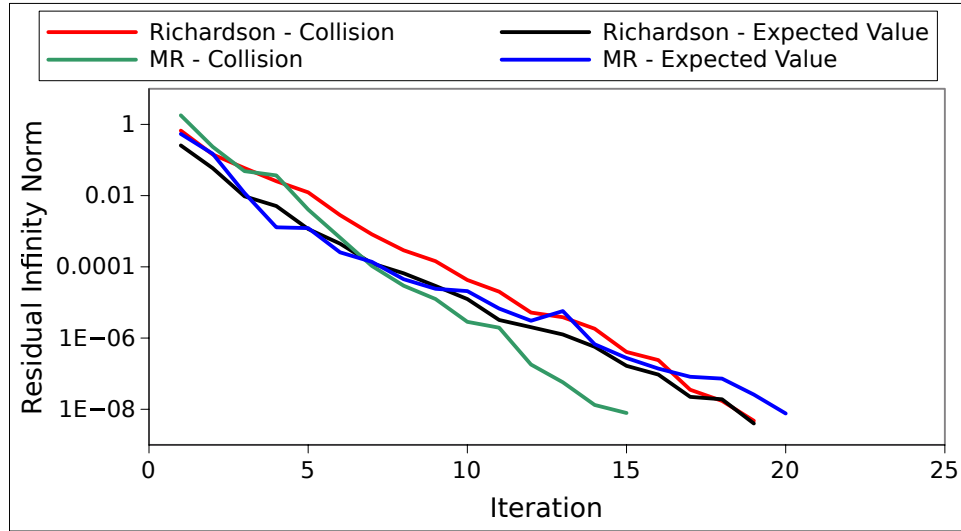
Figure 3.28: **Residual infinity norm as a function of MCSA iteration with 1,000 stochastic histories per iteration.** *Both the collision and expected value estimators were used with the adjoint Monte Carlo solver to compute the correction at each iteration. Each estimator was used with the Richardson and minimal residual fixed point iterations within an MCSA iteration.*

gave the best iterative performance when using the expected value estimator. For purely serial computational performance, there is not a distinguishing feature for the fuel assembly problem presented that would cause one to choose one of the estimators and fixed point iterations over the other as they all have similar minimum CPU times over the range of values tested.

3.6 MCSA Verification

Through the numerical studies presented in this chapter, we have developed a set of pre-conditioning techniques that permit MCSA to be used with the SP_N form of the neutron transport equation and applied to a difficult fuel assembly criticality problem. Along with these preconditioning techniques, a set a varying MCSA parameters were analyzed to find those that yielded the best performance for this particular problem. In addition, several steps were taken to mitigate the dense composite linear operators that arise when performing explicit MCSA preconditioning necessary for achieve convergence. Using these results, we know compare MCSA directly to conventional linear solvers that would be typically used to solve the SP_N form of the transport equation as presented here. In particular, we will use a pair of production Krylov solvers with which we will compare direct numerical results in order to verify MCSA solutions in this section.

In order to verify the correctness of the MCSA method and implementation used for this work, MCSA solutions to the fuel assembly problem with 1, 2, and 4 energy groups using SP_1 discretization will be directly compared point-wise over all group and cell fluxes computed by converging the criticality problem using both BiCGStab and GMRES production implementations from the Trilinos scientific computing library Aztec [77]. In addition to comparing the cell and group fluxes, the number of eigenvalue iterations required to converge the problem along with the eigenvalue itself will be compared as a means of verification. For the flux values, we look to the 2-norm and infinity norm of the relative difference vector between the reference case and the comparison case in each energy group:

$$\text{Relative Difference} = \frac{\mathbf{\Phi}_{ref}^g - \mathbf{\Phi}^g}{\mathbf{\Phi}_{ref}^g} \,, \tag{3.28}$$

where the addition and subtraction operations are performed element-wise to construct the vector. For this work, the BiCGStab results will be taken as the reference case.

For the verification calculations, all solvers will be preconditioned with ILUT using a drop tolerance of 1×10^{-5} and a fill level of 5. For GMRES, no restrictions were placed on the size of the subspace and therefore no restarts occurred. When the collision estimator was used with MCSA, 2×10^4 stochastic histories were used to compute the correction for every energy group in the problem (4×10^4 and 8×10^4 histories total for the 2 and 4 group calculations respectively) corresponding to approximately 1 stochastic history per DOF. When the expected value estimator was used, 5×10^2 stochastic histories used for each energy group (1×10^3 and 1.5×10^3 histories total for the 2 and 4 group calculations) giving approximately 1 stochastic history for every 5 DOFs. The reduced domain approximation was also applied in conjunction with the ILUT preconditioning using a fill level of 100 and a threshold value of 1×10^{-10} to reduce the density of states in the Monte Carlo problem. For relaxation parameters, all MCSA computations used a Neumann relaxation parameter of 0.7 while a Richardson relaxation of 1.1 was used with the collision estimator and 1.0 with the expected value estimator as determined by the previous analysis of the relaxation parameters. Table 3.9 gives definitions for the solvers used to generate the results in the remainder of this section. For the energy group structures, Table 3.10 gives the lower bounds of each group in eV (an implicit upper bound of 2×10^6 eV is assumed for group 0).

Name	Definition
BiCGStab-ILUT	BiCGStab preconditioned with ILUT
GMRES-ILUT	GMRES preconditioned with ILUT
MCSA-ILUT-R-C	MCSA preconditioned with ILUT using Richardson fixed point iteration and collision estimator
MCSA-ILUT-MR-C	MCSA preconditioned with ILUT using minimal residual fixed point iteration and collision estimator
MCSA-ILUT-R-EV	MCSA preconditioned with ILUT using Richardson fixed point iteration and expected value estimator
MCSA-ILUT-MR-EV	MCSA preconditioned with ILUT using minimal residual fixed point iteration and expected value estimator
Richardson-ILUT	Richardson iteration preconditioned with ILUT

Table 3.9: **Solver definitions used for MCSA verification and performance analysis.** *The ILUT preconditioner parameters were identical for all calculations and solvers.*

Number of Groups	Lower Bounds (eV)
1	$\{ 1 \times 10^{-5} \}$
2	$\{ 1 \times 10^{-1}, 1 \times 10^{-5} \}$
4	$\{ 1 \times 10^{1}, 1 \times 10^{0}, 1 \times 10^{-1}, 1 \times 10^{-5} \}$

Table 3.10: **Energy group lower bounds for the multigroup fuel assembly criticality problem in electron volts.** *An implicit upper bound of* 2×10^{6} *eV is assumed for group zero.*

For every combination of energy group structure and solver, the eigenvalue problem was converged with an eigensolver tolerance of 1×10^{-6} and a linear solver tolerance of 1×10^{-8} in a serial calculation. Table 3.11 gives the eigenvalue computed by each solver for each problem as well as the number of eigenvalue iterations required to converge. For every problem, each solver converged to the same eigenvalue up to the number of digits reported by the eigensolver eigensolver in the same number of eigenvalue iterations.

Table 3.12, Table 3.13, and Table 3.14 give the infinity norms and 2-norms of the flux relative difference vectors given by Eq (3.28) for all calculations and all energy groups. In general, we see good agreement in the two norm between the MCSA variants and the GMRES calculation, meaning that the have approximately the same variation from the BiCGStab calculation. We do note larger infinity norm values of this vector for some of the MCSA variants (i.e. group 1 in the 2-group calculation), however this large maximum value was not a global phenomenon with good agreement in the 2-norm for the calculations. Based on the good agreement between MCSA and GMRES for the relative difference of the flux and the eigenvalue results presented here, the MCSA results should be deemed correct for the fuel assembly problem for serial calculations with multiple energy groups.

Solver	Number of Groups	Iterations	Eigenvalue
BiCGStab-ILUT	1	25	1.105987
GMRES-ILUT	1	25	1.105987
MCSA-ILUT-R-C	1	25	1.105987
MCSA-ILUT-MR-C	1	25	1.105987
MCSA-ILUT-R-EV	1	25	1.105987
MCSA-ILUT-MR-EV	1	25	1.105987
Richardson-ILUT	1	25	1.105987
BiCGStab-ILUT	2	35	1.155239
GMRES-ILUT	2	35	1.155239
MCSA-ILUT-R-C	2	35	1.155239
MCSA-ILUT-MR-C	2	35	1.155239
MCSA-ILUT-R-EV	2	35	1.155239
MCSA-ILUT-MR-EV	2	35	1.155239
Richardson-ILUT	2	35	1.155239
BiCGStab-ILUT	4	31	1.175850
GMRES-ILUT	4	31	1.175850
MCSA-ILUT-R-C	4	31	1.175850
MCSA-ILUT-MR-C	4	31	1.175850
MCSA-ILUT-R-EV	4	31	1.175850
MCSA-ILUT-MR-EV	4	31	1.175850
Richardson-ILUT	4	31	1.175850

Table 3.11: **Serial eigensolver verification results for the fuel assembly problem.** *Each calculation was converged with the same eigensolver and linear solver tolerances. Table 3.9 gives the description for each solver type presented.*

Solver	Group	$\|\|\cdot\|\|_{inf}$	$\|\|\cdot\|\|_2$
GMRES-ILUT	0	4.562×10^{-6}	6.746×10^{-5}
MCSA-ILUT-R-C	0	2.099×10^{-5}	2.541×10^{-4}
MCSA-ILUT-MR-C	0	4.812×10^{-5}	4.672×10^{-4}
MCSA-ILUT-R-EV	0	2.371×10^{-5}	2.740×10^{-4}
MCSA-ILUT-MR-EV	0	3.605×10^{-5}	2.554×10^{-4}
Richardson-ILUT	0	1.531×10^{-5}	2.771×10^{-4}

Table 3.12: **Serial scalar flux verification results for the 1-group fuel assembly problem.** *The infinity norm and 2-norm of the relative flux vector in each group is given with BiCGStab is used as the reference. Each calculation was converged with the same eigensolver and linear solver tolerances. Table 3.9 gives the description for each solver type presented.*

Solver	Group	$\|\cdot\|_{inf}$	$\|\cdot\|_2$
GMRES-ILUT	0	7.590×10^{-6}	1.234×10^{-4}
MCSA-ILUT-R-C	0	5.308×10^{-6}	1.066×10^{-4}
MCSA-ILUT-MR-C	0	6.388×10^{-5}	2.233×10^{-4}
MCSA-ILUT-R-EV	0	4.197×10^{-5}	2.168×10^{-4}
MCSA-ILUT-MR-EV	0	2.736×10^{-5}	8.160×10^{-5}
Richardson-ILUT	0	3.976×10^{-6}	7.059×10^{-5}
GMRES-ILUT	1	7.579×10^{-6}	1.246×10^{-4}
MCSA-ILUT-R-C	1	1.645×10^{-5}	1.210×10^{-4}
MCSA-ILUT-MR-C	1	6.635×10^{-4}	9.435×10^{-4}
MCSA-ILUT-R-EV	1	1.797×10^{-4}	2.983×10^{-4}
MCSA-ILUT-MR-EV	1	1.556×10^{-4}	2.055×10^{-4}
Richardson-ILUT	1	4.031×10^{-6}	7.110×10^{-5}

Table 3.13: **Serial scalar flux verification results for the 2-group fuel assembly problem.** *The infinity norm and 2-norm of the relative flux vector in each group is given with BiCGStab is used as the reference. Each calculation was converged with the same eigensolver and linear solver tolerances. Table 3.9 gives the description for each solver type presented.*

Solver	Group	$\lVert \cdot \rVert_{inf}$	$\lVert \cdot \rVert_2$
GMRES-ILUT	0	2.376×10^{-5}	4.043×10^{-4}
MCSA-ILUT-R-C	0	2.639×10^{-5}	3.950×10^{-4}
MCSA-ILUT-MR-C	0	3.958×10^{-5}	4.635×10^{-4}
MCSA-ILUT-R-EV	0	2.749×10^{-5}	3.975×10^{-4}
MCSA-ILUT-MR-EV	0	2.969×10^{-5}	4.054×10^{-4}
Richardson-ILUT	0	2.189×10^{-5}	3.791×10^{-4}
GMRES-ILUT	1	2.271×10^{-5}	3.952×10^{-4}
MCSA-ILUT-R-C	1	3.701×10^{-5}	3.933×10^{-4}
MCSA-ILUT-MR-C	1	3.803×10^{-5}	3.933×10^{-4}
MCSA-ILUT-R-EV	1	4.142×10^{-5}	4.011×10^{-4}
MCSA-ILUT-MR-EV	1	2.723×10^{-5}	4.030×10^{-4}
Richardson-ILUT	1	2.137×10^{-5}	3.768×10^{-4}
GMRES-ILUT	2	2.310×10^{-5}	4.021×10^{-4}
MCSA-ILUT-R-C	2	2.490×10^{-5}	3.956×10^{-4}
MCSA-ILUT-MR-C	2	2.214×10^{-5}	3.608×10^{-4}
MCSA-ILUT-R-EV	2	4.456×10^{-5}	3.833×10^{-4}
MCSA-ILUT-MR-EV	2	3.366×10^{-5}	3.797×10^{-4}
Richardson-ILUT	2	2.143×10^{-5}	3.767×10^{-4}
GMRES-ILUT	3	2.335×10^{-5}	4.029×10^{-4}
MCSA-ILUT-R-C	3	3.045×10^{-5}	3.963×10^{-4}
MCSA-ILUT-MR-C	3	2.696×10^{-5}	3.606×10^{-4}
MCSA-ILUT-R-EV	3	1.947×10^{-5}	4.283×10^{-4}
MCSA-ILUT-MR-EV	3	3.295×10^{-5}	3.837×10^{-4}
Richardson-ILUT	3	2.161×10^{-5}	3.772×10^{-4}

Table 3.14: **Serial scalar flux verification results for the 4-group fuel assembly problem.** *The infinity norm and 2-norm of the relative flux vector in each group is given with BiCGStab is used as the reference. Each calculation was converged with the same eigensolver and linear solver tolerances. Table 3.9 gives the description for each solver type presented.*

3.7   MCSA Performance Comparison to Conventional Methods

In the previous section, numerical results using MCSA for the fuel assembly calculation were directly compared with production Krylov methods in order to verify their correctness. Deemed correct, performance of the algorithm for serial computations will now be addressed. With the same set of solver parameters used for verification, MCSA will now be directly compared to the same production Krylov solvers in terms of both iterative performance and CPU timing for solutions to the fuel assembly problem. The iterative performance will also be compared to using a Richardson iteration preconditioned in the same way for all calculations in order to assess the acceleration provided by the residual Monte Carlo component of MCSA. This performance comparison is necessary in order to assess the feasibility of the method and identify areas that require further research and development.

To compare iterative performance, the number of linear solver iterations required to converge each eigenvalue iteration was recorded and then averaged over all eigenvalue iterations for each solver. Table 3.15 gives the average number of linear solver iterations required to converge a single eigenvalue iteration of the fuel assembly problem as a function of the number of energy groups. In general, the iterative performance of all the solvers tested is comparable with BiCGStab performing the best. We expect this because not only are the multigroup SP_N equations elliptic and positive-definite, but they are also nearly symmetric and therefore we expect the conjugate gradient-based methods to perform well due to the structure of the projection scheme. It important to note that the iterative performance of each solver is not a strong function of the number of energy groups in the problem (and therefore the problem size). Even more important, although BiCGStab produced the best iterative results, MCSA did perform better than GMRES in many cases with the Richardson iteration accelerated with Monte Carlo using the collision estimator performing best. When compared to the preconditioned Richardson iteration, the acceleration provided by MCSA is

clear with 3-4 times fewer iterations required for convergence.

For MCSA, we are linearly increasing the number of stochastic histories used to compute the correction at each iteration as the number of energy groups are increased and therefore the work performed for the problem is of $O(N)$. It is also important to note the reduced domain approximation parameters, particularly the fill level, were fixed as the number of energy groups was increased. By fixing the fill level, we are effectively fixing the amount of information contained in the composite linear operator available for the Monte Carlo problem. Limiting this information to 100 entries per row in the preconditioned system did not appear to have a significant effect on the iterative performance of the solver. For larger numbers of energy groups (and therefore DOFs) this may be an issue and this number may need to be increased to maintain iterative performance. Currently, memory restrictions arising from the explicit preconditioning strategy prevent larger numbers of energy groups to be analyzed using an appropriate preconditioner for the fuel assembly problem.

Solver	1 Group	2 Groups	4 Groups
BiCGStab-ILUT	11.6	11.6	12.4
GMRES-ILUT	18.1	17.9	18.9
MCSA-ILUT-R-C	14.6	15.4	17.6
MCSA-ILUT-MR-C	16.0	17.1	23.7
MCSA-ILUT-R-EV	18.3	19.4	16.8
MCSA-ILUT-MR-EV	19.6	22.4	17.5
Richardson-ILUT	60.9	60.4	63.4

Table 3.15: **Average number of linear solver iterations iterations required to converge the fixed source SP_N problem at each eigenvalue iteration for the fuel assembly problem for 1, 2 and 4 energy groups.** *Values are rounded to the first decimal place. Table 3.9 gives the description for each solver type presented.*

Although iterative performance for MCSA was comparable to that observed for production Krylov implementations using exactly the same preconditioning scheme, timing performance is not as competitive. For this comparison, the amount of time to perform each linear solver iteration in every eigenvalue iteration was recorded and then averaged over all linear solver iterations. Figure 3.29 gives the average CPU time per linear solver iteration required

to converge the fuel assembly problem with all linear solver iterations over all eigenvalue iterations used to compute the average. The production Krylov solver implementations are approximately an order of magnitude faster than the MCSA implementations presented here. We expect these results for several reasons. First, even when the reduced domain approximation is used there are $O(100)$ elements in each row of the system and each of those elements must be processed during a transition in the Monte Carlo random walk sequence. In addition, although the preconditioned fixed point iterations used in the MCSA sequence do not use the composite linear operator but rather a sequence of matrix vector multiplies to achieve the same preconditioning effect, they do use the explicitly extracted inverse of the preconditioning matrices which themselves are dense, leading to exceedingly slow computation times even in the fixed point iteration.

For the production Krylov methods, the ILUT preconditioners are applied to a vector with two triangular solves, one for each triangular factor. Also, the original linear operator has $O(10)$ elements in each row of the system, an order of magnitude less than that used in the reduced domain composite operator. Second, the implementation presented here has not been optimized and it is likely that several components of the algorithm can be implemented in a more desirable time complexity. The production Krylov solvers presented here have enjoyed decades of professional development and optimization. However, it is most important to note here that the CPU timing data presented in Figure 3.29 shows that all methods have the same time complexity; their differences are merely the manifestation of a large time constant due to the effects of the explicit preconditioning scheme. For transport systems where this is not a problem, the literature explicitly shows that MCSA can be competitive with these production Krylov methods using CPU time as a measure [75].

Finally, not considered in Figure 3.29 is the time required to actually form the explicit inverse preconditioner matrices and the composite operator through matrix-matrix multiplication. The timing numbers reported were simply to perform the MCSA iteration procedure with the composite operator already formed. Figure 3.30 additionally presents the CPU times
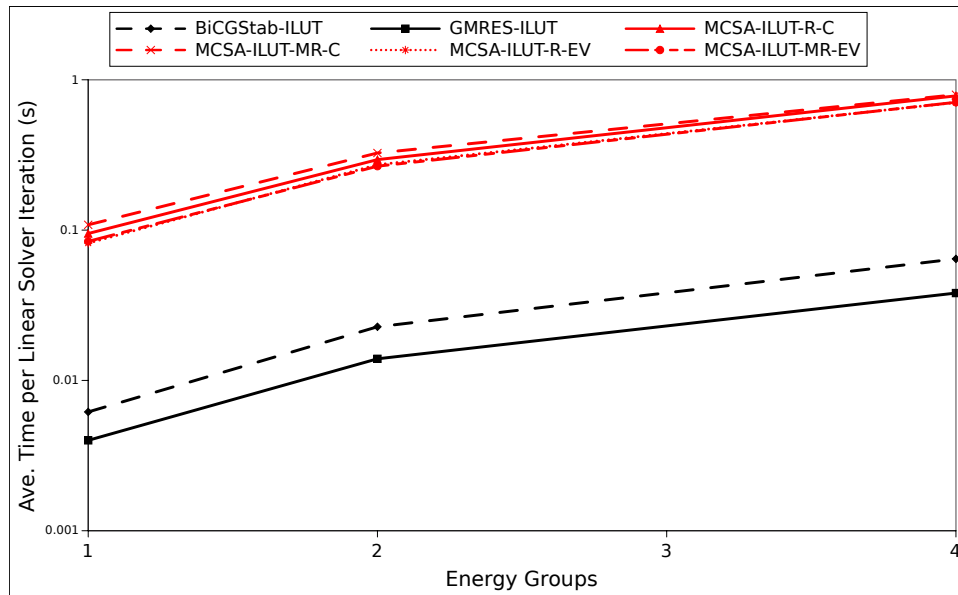
Figure 3.29: **Average CPU time per linear solver iteration in seconds for the fuel assembly problem as a function of energy groups.** *All linear solver iterations over all eigenvalue iterations were used to compute the average. Table 3.9 gives the description for each solver type presented in the legend with the Krylov solvers represented in black and the MCSA solvers represented in red.*

for MCSA convergence with the time to form the inverse of the preconditioners and the composite linear operator through matrix-matrix multiplication amortized over all iterations. As is readily observed, including the costs of these operations increases the MCSA computation time by another order of magnitude.

Based on the performance results in this section, MCSA shows promise as a competitive and perhaps even superior method for solutions to the neutron transport problem discretized with the SP_N approximation. Not only are the correct answers produced when compared to production linear solvers, but the iterative performance is comparable to production Krylov methods with identical preconditioning that would typically be used every-day calculations. From a CPU timing perspective, the methods yield the same time complexity as a function of the number of energy groups in the problem when compared to the production Krylov methods. Here, a large time constant is generated due to the explicit preconditioning strategy and the generation of dense linear operators as a result. To improve these results and put
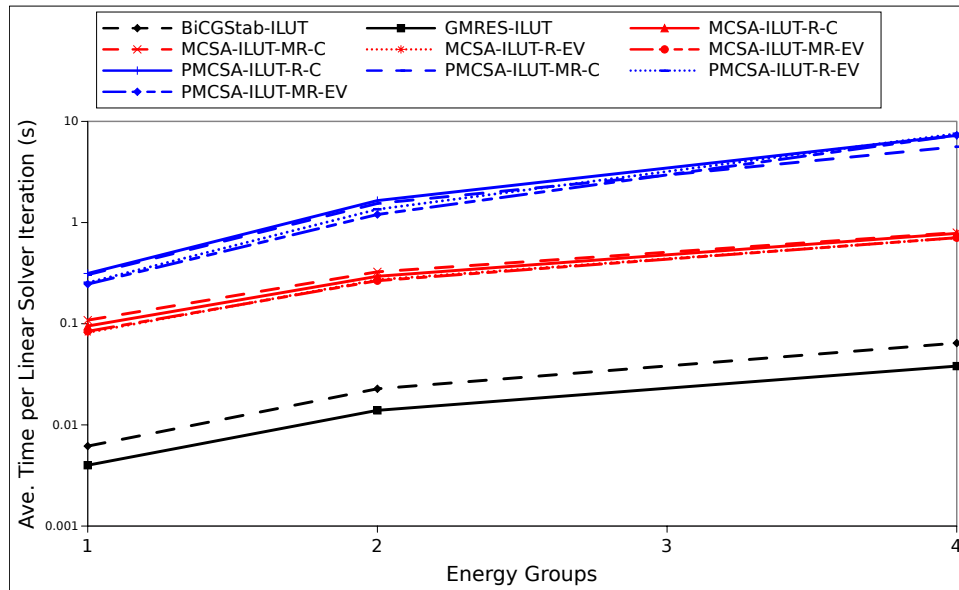
Figure 3.30: **Average CPU time per iteration in seconds for the fuel assembly problem as a function of energy groups with preconditioning time included for the MCSA methods.** *All linear solver iterations over all eigenvalue iterations were used to compute the average. Table 3.9 gives the description for each solver type presented in the legend. Data labeled starting with PMCSA and shown in blue is identical to those labeled with MCSA except that they additionally include the cost of generating the inverse of the preconditioners and composite linear operator.*

general MCSA schemes into a performance regime where they are competitive with Krylov methods for neutron transport problems, significant research will be required to improve upon the explicit preconditioning scheme presented here.

3.8 Summary

In this chapter, the Monte Carlo Synthetic Acceleration method has been applied to the SP_N discretization of the neutron transport equation and explored in the context of a difficult nuclear fuel assembly criticality problem. The following are the significant observations and findings.

- MCSA can solve the asymmetric system generated by the SP_N equations

- MCSA has been incorporated into the Exnihilo neutronics production code base developed at Oak Ridge National Laboratory

- Simple Jacobi-based preconditioning reduces the spectral radius of the SP_N system below unity, however, this alone is not sufficient for MCSA convergence

- As the spectral radius approaches unity, MCSA was demonstrated to break down with more stochastic histories required for convergence and more CPU time required per history

- Light water reactor problems are difficult to solve with MCSA as they have large spectral radii due to the neutron scattering in the moderator

- Advanced algebraic preconditioning strategies were applied to the SP_N equations to obtain convergence with ILUT chosen for subsequent investigations

- The reduced domain approximation was required to mitigate the memory and performance constraints of the explicit preconditioning strategy although both remain significant obstacles

- MCSA relaxation parameters were developed and observed to enhance the time to solution for the fuel assembly criticality problem

- MCSA was verified to produce the same flux distribution and k-eigenvalue for the fuel assembly as production Krylov methods

- MCSA was observed to converge in fewer iterations per eigenvalue iteration than GMRES for the fuel assembly criticality problem and more than Bi-CGStab using the same preconditioning

- The explicit preconditioning strategy required to overcome the MCSA spectral radius restriction creates runtimes $O(100)$ larger than the production Krylov methods for the fuel assembly criticality problem

Chapter 4

Monte Carlo Synthetic Acceleration Methods for the Navier-Stokes Equations

In this chapter the fundamentals of Newton's method will be presented along with a brief discussion of inexact Newton methods. Newton-Krylov methods, a variant of inexact Newton methods, will be outlined including two techniques for numerically representing the Jacobian commonly used in today's applications. Following this, a new algorithm utilizing Monte Carlo Synthetic Acceleration will be presented and implementation details will be discussed. Using the new algorithm and a production fluid physics code, a group of challenging nonlinear benchmark problems for the Navier-Stokes equations will be used to verify the correctness of the method relative to solutions obtained using conventional methods in various flow regimes and geometries. Finally, we will compare the performance of the new method against contemporary Newton-Krylov methods for the same benchmark problems.

4.1 Preliminaries

We formulate the *nonlinear problem* as follows [91]:

$$\mathbf{F}(\mathbf{u}) = \mathbf{0} \,, \tag{4.1}$$

where $\mathbf{u} \in \mathbb{R}^n$ is the solution vector and $\mathbf{F} : \mathbb{R}^N \to \mathbb{R}^N$ is the function of nonlinear residuals. We write the nonlinear system in this form so that when an exact solution for $\mathbf{u}$ is achieved,

all residuals evaluate to zero. *Newton's method* is a root finding algorithm and therefore we can use it to solve Eq (4.1) if we interpret the exact solution $\mathbf{u}$ to be the roots of $\mathbf{F}(\mathbf{u})$. Newton's method is also an iterative scheme, and we can generate this procedure by building the Taylor expansion of the $k+1$ iterate, $\mathbf{F}(\mathbf{u}^k)$, of the nonlinear residuals about the previous k iterate, $\mathbf{F}(\mathbf{u}^{k+1})$:

$$\mathbf{F}(\mathbf{u}^{k+1}) = \mathbf{F}(\mathbf{u}^k) + \mathbf{F}'(\mathbf{u}^k)(\mathbf{u}^{k+1} - \mathbf{u}^k) + \frac{\mathbf{F}''(\mathbf{u}^k)}{2}(\mathbf{u}^{k+1} - \mathbf{u}^k)^2 + \cdots . \qquad (4.2)$$

If we ignore the nonlinear terms in the expansion and assert that at the $k+1$ iterate $\mathbf{u}^{k+1}$ is the exact solution such that $\mathbf{F}(\mathbf{u}^{k+1}) = \mathbf{0}$, then we are left with the following equality:

$$-\mathbf{F}(\mathbf{u}^k) = \mathbf{F}'(\mathbf{u}^k)(\mathbf{u}^{k+1} - \mathbf{u}^k) . \qquad (4.3)$$

We note two things of importance in Eq (4.3). The first is that $\mathbf{F}'(\mathbf{u}^k)$ is in fact the *Jacobian*, $\mathbf{J}(\mathbf{u})$, of the set of nonlinear residuals and is defined element-wise as:

$$J_{ij} = \frac{\partial F_i(\mathbf{u})}{\partial u_j} . \qquad (4.4)$$

Second, we note that $(\mathbf{u}^{k+1} - \mathbf{u}^k)$ is simply the solution update from the k iterate to the $k+1$ iterate. We will define this update as the *Newton correction* at the k iterate, $\delta\mathbf{u}^k$. To finish, we can then rearrange Eq (4.3) to define the Newton iteration scheme for nonlinear problems:

$$\mathbf{J}(\mathbf{u})\delta\mathbf{u}^k = -\mathbf{F}(\mathbf{u}^k) \qquad (4.5a)$$

$$\mathbf{u}^{k+1} = \mathbf{u}^k + \delta\mathbf{u}^k . \qquad (4.5b)$$

There are then three distinct steps to perform: evaluation of the nonlinear residuals

using the solution at the k iterate, the solution of a linear system to compute the Newton correction where the Jacobian matrix of the nonlinear equation set is the linear operator, and the application of the correction to the previous iterate's solution to arrive at the next iterate's solution. In the asymptotic limit, the iterations of Newton's method will converge the nonlinear residual quadratically [78]. Convergence criteria is set for stopping the iteration sequence based on the nonlinear residual. Commonly, the following criteria is used:

$$||\mathbf{F}(\mathbf{u}^k)|| < \epsilon ||\mathbf{F}(\mathbf{u}^0)|| \, , \tag{4.6}$$

where ϵ is a user defined tolerance parameter.

Newton's method is *consistent* in that all components of the nonlinear functions that describe the physics we are modeling are updated simultaneously in the iteration sequence with respect to one another. This is in comparison to *inconsistent* strategies, such as a pressure correction strategy for solving the Navier-Stokes equations [55], where the components of $\mathbf{u}$ are updated in a staggered fashion depending on the particular equations that they are associated with.

4.1.1 Inexact Newton Methods

Inexact Newton methods arise when the Jacobian operator is not exactly inverted, resulting in an inexact Newton correction as initially described by Dembo and others [20]. For common sparse nonlinear systems, which in turn yield a sparse Jacobian matrix, this situation occurs when conventional iterative methods are applied. In their definition, Dembo formulated inexact methods such that they are independent of the linear method used to solve for the Newton correction and therefore are amenable to use with any linear solver. Furthermore, they bind the convergence of the outer nonlinear iteration to the inner linear iteration such that:

$$||\mathbf{J}(\mathbf{u}^k)\delta\mathbf{u}^k + \mathbf{F}(\mathbf{u}^k)|| \le \eta^k ||\mathbf{F}(\mathbf{u}^k)|| \, , \tag{4.7}$$

where $\eta^k \in [0, 1)$ is defined as the *forcing term* at the k iterate. Eq (4.7) then states that the residual generated by the linear solver is bound by the nonlinear residual and how tightly it is bound is defined by the forcing term. This is useful in that we can vary how tightly coupled the convergence of the linear iterations used to generate the Newton correction is to the nonlinear iteration by relaxing or tightening the convergence properties on the linear iterative method. As a result, strategies for determining the forcing term can vary depending on the problem type and can greatly affect the convergence of the method or even prohibit convergence [19]. In addition, *globalization methods* may be used to modify the Newton correction in a more desirable direction such that convergence properties can be improved when the initial guess for **u** is poor [68].

4.1.2 Newton-Krylov Methods

A form of inexact Newton methods, *Newton-Krylov methods* are nonlinear iterative methods that leverage a Krylov subspace method as the linear solver for generating the Newton correction [78]. As outlined in Appendix A, Krylov methods are robust and enjoy efficient parallel implementations on modern architectures. Furthermore, their lack of explicit dependence on the operator make them easier to implement than other methods. Additionally, although many iterations can become memory intensive due to the need to store the Krylov subspace for the orthogonalization procedure, at each nonlinear iteration this cost is reset as the Jacobian matrix will change due to its dependence on the solution vector. This means that for every nonlinear iteration, a completely new linear system is formed for generating the Newton correction and we can modify the Krylov solver parameters accordingly to accommodate this. In most nonlinear problems, the Jacobian operator is generally non-symmetric and therefore either Krylov methods with long recurrence relations that can handle non-symmetric systems must be considered or the Newton correction system must be preconditioned such that the operator is symmetric and short recurrence relation methods can be potentially be used.

With many Krylov methods available, which to use with the Newton method is dependent

on many factors including convergence rates and memory usage. Several studies have been performed to investigate this [48, 65]. In their numerical studies in 1995, Knoll and McHugh used the set of highly nonlinear and stiff convection-diffusion-reaction equations to solve a set of tokamak plasma problems with the goal of measuring solver performance with Newton's method. They note several trade-offs in using Krylov methods with the Newton solver. The first is that the optimization condition that results from the constraints (e.g. the minimization of the GMRES residual over the Krylov space) can be relaxed by restricting the size of the subspace such that only a fixed number of subspace vectors may be maintained, thus reducing memory requirements.

We can also relax the optimization condition by instead restarting the recurrence relation with a new set of vectors once a certain number of vectors have been generated. The optimization condition is maintained over that particular set of vectors, however, Knoll and McHugh note that this ultimately slows the convergence rate as compared to keeping all vectors as the new set of vectors is not necessarily orthogonal to the previous set, and therefore not optimal over the entire iteration procedure. The orthogonality condition can be relaxed by using a recurrence relation that does not generate a strictly orthonormal basis for the Krylov subspace such as the Lanzcos biorthogonalization procedure, resulting in memory savings due to the shorter Lanzcos recurrence relation. Based on their numerical analysis, they observed GMRES to be the most robust for any given nonlinear problem and therefore used it for subsequent work in this area.

4.1.3 Jacobian-Free Approximation

In many cases, the Jacobian is difficult to form from the difference equations and costly to evaluate for large equation sets. For simple nonlinear cases such as the Navier-Stokes equations, the derivatives can be computed and coded, but due to the complexity of those derivatives and the resulting difference equations this task can be tedious, error prone, and must be repeated for every equation set. Furthermore, in their 1995 work, Knoll and McHugh

also noted that a dominating part of their computation time was the evaluation of the difference equations for building the Jacobian [65]. By recognizing that Krylov methods only need the action of the operator on a vector instead of the operator itself, the Jacobian can instead be approximated through various numerical methods including a difference-based Jacobian-free formulation.

Jacobian-Free methods, and in particular *Jacobian-Free Newton-Krylov* (JFNK) methods [91], rely on forming the action of the Jacobian on a vector as required by the Krylov solver through a forward difference scheme. In this case, the action of the Jacobian on some vector $\mathbf{v}$ is given as:

$$\mathbf{J}(\mathbf{u})\mathbf{v} = \frac{\mathbf{F}(\mathbf{u} + \epsilon\mathbf{v}) - \mathbf{F}(\mathbf{u})}{\epsilon} \, , \tag{4.8}$$

where ϵ is a small number typically on the order of machine precision. Kelley [78] points out a potential downfall of this formulation in that if the discretization error in $\mathbf{F}(\mathbf{u})$ is on the order of the perturbation parameter ϵ, then the finite difference error from Eq (4.8) pollutes the solution.

In addition, Knoll and McHugh noted that for preconditioning purposes, part of the Jacobian must still explicitly be formed periodically and that linear solver robustness issues were magnified by the matrix-free approach due to the first-order approximation. This formation frequency coupled with the numerous evaluations of the Jacobian approximation create a situation where after so many nonlinear iterations, it becomes cheaper to instead fully form the Jacobian. For simple equation sets, this may only take 5-10 Newton iterations to reach this point while over 30 may be required for larger equations sets and therefore larger Jacobians.

4.1.4   Automatic Differentiation for Jacobian Generation

If it is acceptable to store the actual Jacobian matrix, other methods are available to construct it without requiring hand-coding and evaluating derivatives, thus eliminating the associated

issues. In addition, if any additional equations are added to the system or a higher order functional approximation is desired, it would be useful to avoid regenerating and coding these derivatives. Becoming more prominent in the 1990's, *automatic differentiation* is a mechanism by which the derivatives of a function can be generated automatically by evaluating it. Automatic differentiation is built on the concept that all functions discretely represented in a computer are ultimately represented by elementary mathematical operations. If the chain rule is applied to those elementary operations, then the derivatives of those functions can be computed to the order of accuracy of their original discretization in a completely automated way [12].

The work of Bartlett and others [23] extended initial Fortran-based work in the area of automatic differentiation implementations to leverage the parametric type and operator overloading features of C++ [33]. They formulate the differentiation problem from an element viewpoint by assuming that a global Jacobian can be assembled from local element function evaluations of $e_k : \mathbb{R}^{n_k} \to \mathbb{R}^{m_k}$, similar to the finite element assembly procedure as:

$$\mathbf{J}(\mathbf{u}) = \sum_{i=1}^{N} \mathbf{Q}_i^T \mathbf{J}_k \mathbf{P}_i \,, \tag{4.9}$$

where $\mathbf{J}_{k_i} = \partial e_{k_i}/\partial P_i u$ is the kth element function Jacobian, $\mathbf{Q} \in \mathbb{R}^{n_{k_i} \times N}$ is a projector onto the element domain and $\mathbf{P} \in \mathbb{R}^{m_{k_i} \times N}$ a projector onto the element range for $\mathbf{F}(\mathbf{u}) \in \mathbb{R}^{N \times N}$. The Jacobian matrix for each element will therefore have entirely local data in a dense structure, eliminating the need for parallel communication and sparse techniques during differentiation. Only when all local differentials are computed does communication of the Jacobian occur through gather/scatter operations in order to properly assemble it.

Also of benefit is the fact that element-level computations generally consist of a smaller number of degrees of freedom, thus reducing memory requirements during evaluation as compared to a global formulation of the problem. Such a formulation is not limited to finite element formulations and is amenable to any scheme where the system is globally sparse

with degrees of freedom coupled to local domains including finite volume representations. The templating capabilities of C++ were leveraged with the element-based evaluation and assembly scheme as in Eq (4.9) by templating element function evaluation code on the evaluation type. If these functions are instantiated with standard floating point types then the residual is returned. If they are instead instantiated with the operator-overloaded automatic differentiation types, both the residual and Jacobian are returned.

Of interest to Bartlett, Averick, and the many others that have researched automatic differentiation are measures of its performance relative to hand-coded derivatives and capturing the Jacobian matrix from matrix-free approximations. Given their element-based function evaluation scheme, Bartlett's work varied the number of degrees of freedom per element and compared both the floating point operation count and CPU time for both the templated automatic differentiation method and hand-coded derivatives for Jacobian evaluations. Although they observed a 50% increase in floating point operations in the templated method over the hand-coded method, run times were observed to be over 3 times faster for the templated method due to the fact that the element-based formulation of the templated method is causing better utilization of cache and therefore faster data access. Furthermore, they observed linear scaling behavior for automatic differentiation as the number of degrees of freedom per element were increased. Based on these results, this type of automatic differentiation formulation was deemed acceptable for use in large-scale, production physics codes.

4.2 The FANM Method

In production physics codes based on nonlinear equations sets, Newton-Krylov methods are the primary means of generating a fully consistent solution scheme [86, 90, 92, 93]. It is common that for large scale simulations these problems are memory limited due to the subspaces generated by robust Krylov methods which may often build hundreds of vectors during a Newton step. Often, a matrix-free approach is chosen to relax memory requirements

over directly generating the Jacobian matrix and facilitate the implementation. However, as we observed in previous sections, these matrix-free methods suffer from poorly scaled problems and the first order error introduced by the Jacobian approximation. In addition, it was observed that the savings induced by the matrix-free approach is eventually amortized over a number of nonlinear iterations where it becomes more efficient computationally to instead form the Jacobian.

In Chapter 2, we focused our efforts on developing and improving Monte Carlo methods for inverting linear systems. These methods, when used to accelerate a stationary method in MCSA, enjoy exponential convergence rates. Although this requires more storage to represent the linear system than that of a Krylov method where the operator is not required, we do not incur any additional storage costs once the iteration sequence begins. In the context of nonlinear problems, the Jacobian matrix that we are required to generate for the Monte Carlo solvers may be generated at will from the nonlinear functions in the Newton system using automatic differentiation. Not only do we then have a simple and automated way to generate the Jacobian, but we also enjoy a Jacobian of numerical precision equivalent to that of our function evaluations.

We therefore propose the *Forward-Automated Newton-MCSA* (FANM) method that utilizes all of the above components. Presented in Algorithm 4.1, the FANM method is an inexact Newton method where MCSA is used to compute the Newton correction. In line 3, automatic differentiation is used at each iteration to build the Jacobian operator which can in turn be used to build weights and probabilities for the Monte Carlo game. In line 4, MCSA is used to solve the linear problem for the Newton correction. As with other inexact methods, any given forcing term can be used to control the convergence of the MCSA iteration at every Newton step. Finally, in line 5 the Newton correction is applied and the iteration proceeds until convergence. In addition to forcing term adjustments, other techniques for improving performance of the nonlinear iteration may be used with FANM including globalization methods.

Algorithm 4.1 FANM Algorithm

1: $k := 0$
2: **while** $||\mathbf{F}(\mathbf{u}^k)|| > \epsilon||\mathbf{F}(\mathbf{u}^0)||$ **do**
3: $\quad \mathbf{J}(\mathbf{u}^k) \leftarrow AD(\mathbf{F}(\mathbf{u}^k))$ $\qquad\qquad\qquad\qquad$ ▷ Automatic differentiation
4: $\quad \mathbf{J}(\mathbf{u}^k)\delta\mathbf{u}^k = -\mathbf{F}(\mathbf{u}^k)$ $\qquad\qquad$ ▷ Solve for the Newton correction with MCSA
5: $\quad \mathbf{u}^{k+1} \leftarrow \mathbf{u}^k + \delta\mathbf{u}^k$
6: $\quad k \leftarrow k + 1$
7: **end while**

At first glance, FANM is simply a variant of an inexact Newton method with a specific requirement of a fully formed Jacobian. However, FANM has the potential to provide value in several areas. First, if iterative or parallel performance of MCSA can be demonstrated to better than that of GMRES or similar subspace methods for asymmetric systems, FANM may outperform a Newton-Krylov method. Second, for situations where memory is a constraint, especially in situations where the Jacobian is generated often if not at every Newton iteration, not building a subspace for ill-conditioned problems will alleviate the associated cost. However, until the preconditioning issues associated with MCSA as presented in the previous chapter using the SP_N equations can be resolved, this hypothesis can unfortunately not be researched. Explicit algebraic preconditioning used in conventional solution methods will almost certainly be required to reduce the spectral radius of most Jacobian operators for MCSA to apply and therefore the current preconditioning strategy will destroy all potential memory benefits of FANM.

4.3   Navier-Stokes Benchmark Problems

To verify the FANM method for nonlinear problems, we choose benchmark solutions for the 2-dimensional, steady, incompressible Navier-Stokes equations on a rectilinear grid in much the same way as Shadid and Pawlowski's work on Newton-Krylov methods for the solution

of these equations [41, 68]. We define these equations as follows:

$$\rho \mathbf{u} \cdot \nabla \mathbf{u} - \nabla \cdot \mathbf{T} - \rho \mathbf{g} = \mathbf{0} \tag{4.10a}$$

$$\nabla \cdot \mathbf{u} = 0 \tag{4.10b}$$

$$\rho C_p \mathbf{u} \cdot \nabla T + \nabla \cdot \mathbf{q} = 0 \,, \tag{4.10c}$$

where ρ is the fluid density, $\mathbf{u}$ is the fluid velocity, C_p the specific heat capacity at constant pressure of the fluid, T the temperature of the fluid, and $\mathbf{g}$ the acceleration due to gravity. Eq (4.10a) provides momentum transport, Eq (4.10b) provides the mass balance, and Eq (4.10c) provides energy transport with viscous dissipation effects neglected. In addition, we close the system with the following equations:

$$\mathbf{T} = -P\mathbf{I} + \mu[\nabla \mathbf{u} + \nabla \mathbf{u}^T] \tag{4.11a}$$

$$\mathbf{q} = -k\nabla T \,, \tag{4.11b}$$

where $\mathbf{T}$ is the stress tensor, P is the hydrodynamic pressure, μ is the dynamic viscosity of the fluid, $\mathbf{q}$ is the heat flux in the fluid, and k is the thermal conductivity of the fluid. This set of strongly coupled equations possesses both the nonlinearities and asymmetries that we are seeking for qualification of the FANM method. Further, physical parameters within these equations can be tuned to enhance the nonlinearities. We will then apply these equations to the following three standard benchmark problems that cover convection dominated flow and flow dominated by inertial forces in two different geometries.

4.3.1 Thermal Convection Cavity Problem

In 1983 a set of benchmark solutions for the natural convection of air in a square cavity was published [21] as shown in Figure 4.1 for the solution of the energy, mass, and momentum equations.
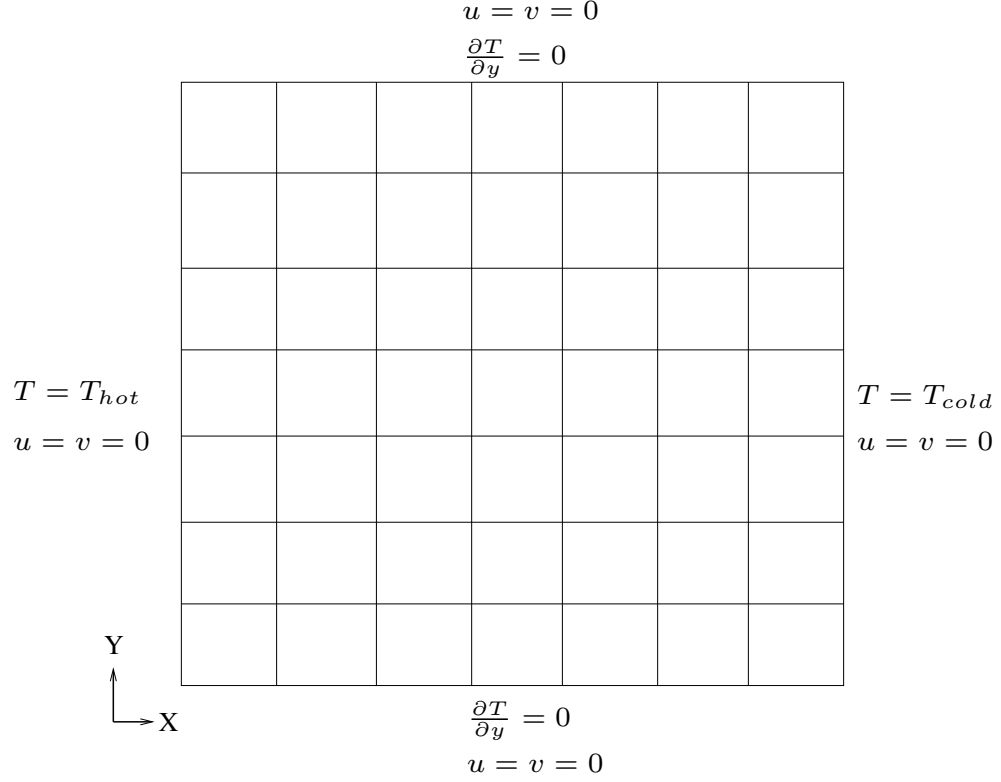
Figure 4.1: **Problem setup for the natural convection cavity benchmark.** *Dirichlet conditions are set for the temperature on the left and right while Neumann conditions are set on the top and bottom of the Cartesian grid. The temperature gradients will cause buoyancy-driven flow. Zero velocity Dirichlet conditions are set on each boundary. No thermal source was present.*

In this problem, a rectilinear grid is applied to the unit square. No heat flow is allowed out of the top and bottom of the square with a zero Neumann condition specified. Buoyancy driven flow is generated by the temperature gradient from the hot and cold Dirichlet conditions on the left and right boundaries of the box. By adjusting the Rayleigh number of the fluid (and therefore adjusting the ratio of convective to conductive heat transfer), we can adjust the influence of the nonlinear convection term in Eq (4.10a). In Shadid's work, Rayleigh numbers of up to 1×10^6 were used for this benchmark.

Isotherms of the temperature solution for these equations are given in Figure 4.2 for Rayleigh numbers of 1×10^3, 1×10^4, 1×10^5 and 1×10^6. Note that as the Rayleigh number is increased, the fluid begins to rotate in the clockwise direction. This causes the temperature
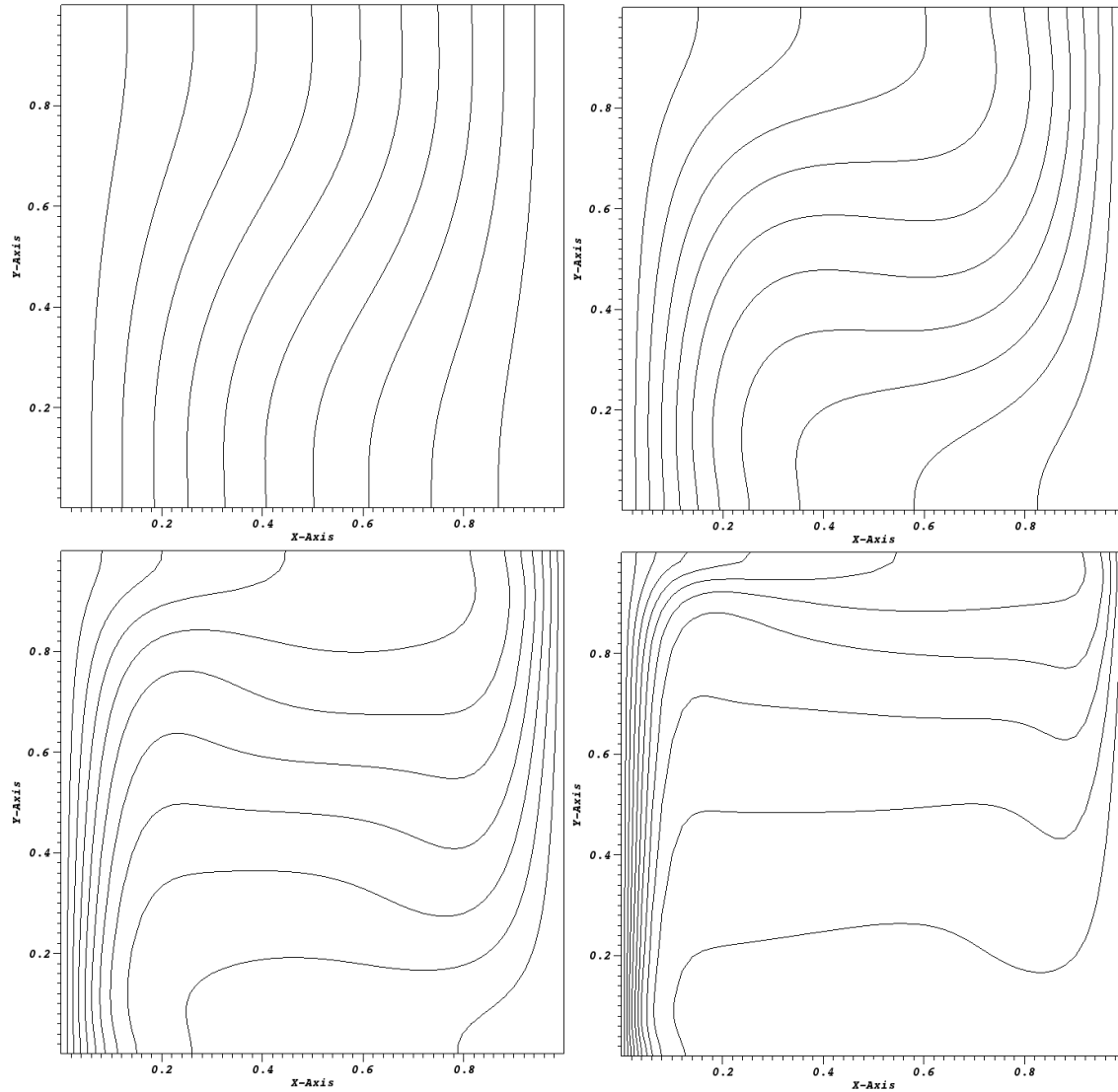
Figure 4.2: **Isotherms from solution to the thermal convection cavity problem.** *Top left: $Ra = 1 \times 10^3$; Top right: $Ra = 1 \times 10^4$; Bottom left: $Ra = 1 \times 10^5$; Bottom left: $Ra = 1 \times 10^6$. Isotherms on unit temperature scale from 0 to 1 with 10 uniformly spaced curves for each calculation.*

gradients to rotate as well with the fluid, given the increased rotation observed for the isotherms in the figure. As the Rayleigh number increases, thermal energy and momentum transport in the system become more dominated by convection rather than diffusion, causing the nonlinearities in the advective derivatives to grow.

$$u = U_0$$
$$v = 0$$

$$u = v = 0 \qquad\qquad\qquad\qquad u = v = 0$$

Y

X $\qquad\qquad u = v = 0$
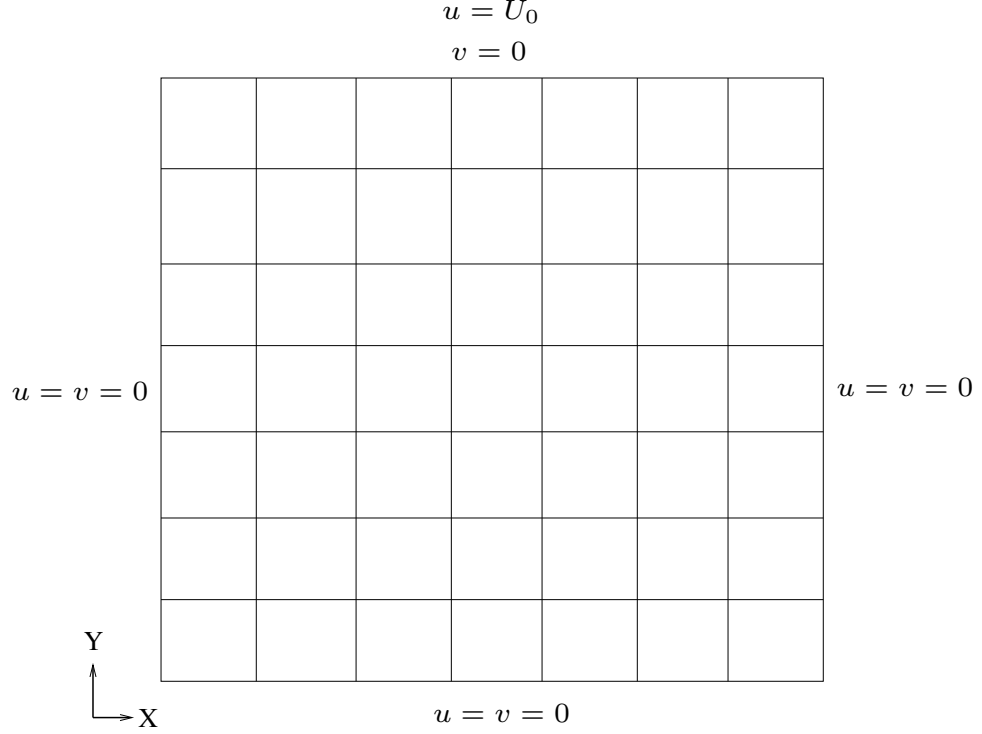
Figure 4.3: **Problem setup for the lid driven cavity benchmark.** *Dirichlet conditions of zero are set for the velocity on the left and right and bottom while the Dirichlet condition set on the top provides a driving force on the fluid.*

4.3.2   Lid Driven Cavity Problem

To study performance for flow driven by inertial forces, the second benchmark problem given by Ghia [85] incorporates a driver for the flow to introduce higher Reynolds numbers into the system, providing more inertial force to overcome the viscous forces in the fluid. The setup for this problem is equally simple, containing only the Dirichlet conditions as given in Figure 4.3 and is only applied to the mass and momentum equations on the unit square.

The top boundary condition will provide a driver for the flow and its variation will in turn vary the Reynolds number of the fluid. An increased velocity will generate more inertial forces in the fluid, which will overcome the viscous forces and again increase the influence of the nonlinear terms in Eq (4.10a). Shadid used Reynolds numbers up to 1×10^4 for this benchmark problem.
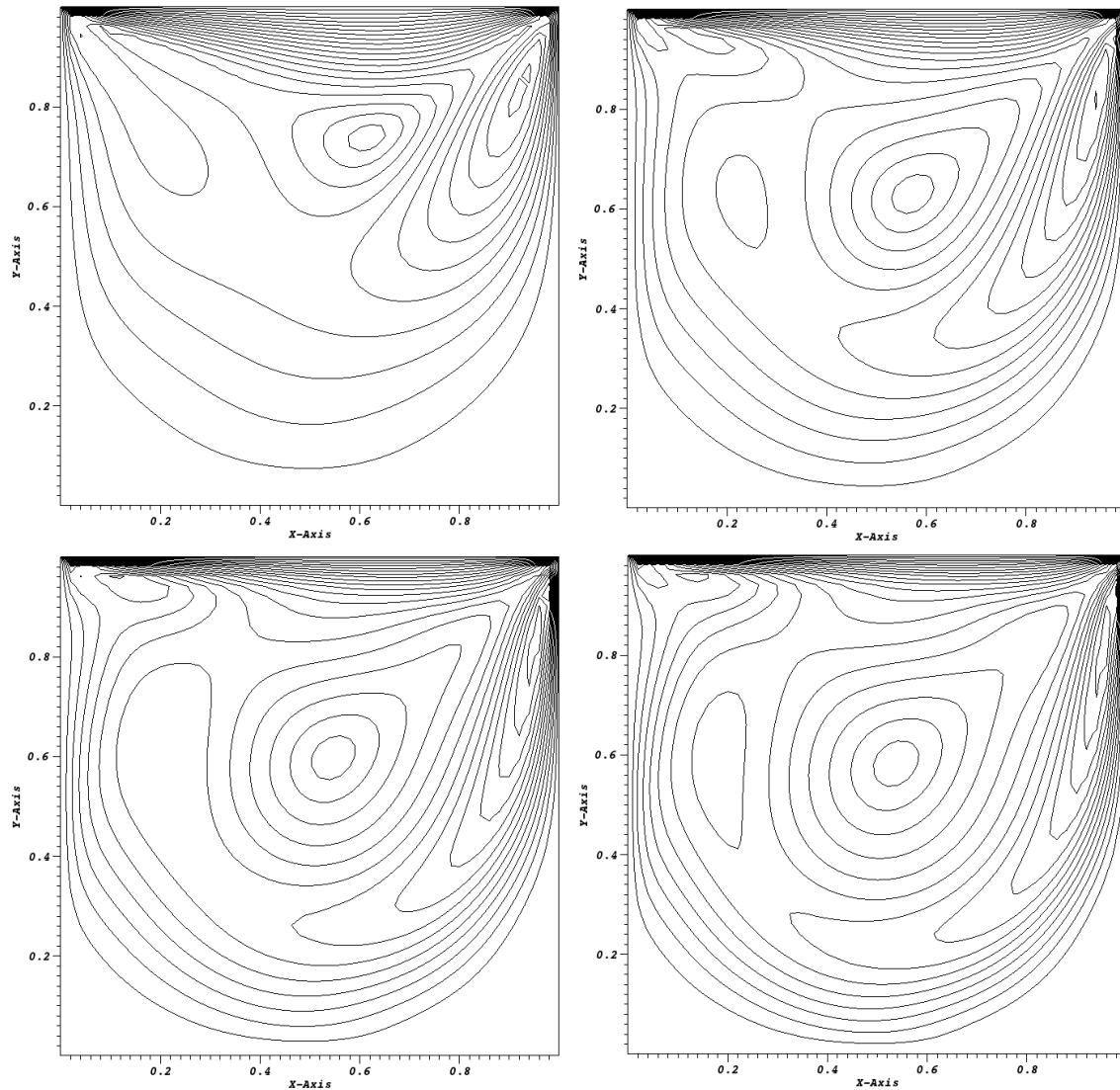
Figure 4.4: **Velocity magnitude isocurves from solution to the lid driven cavity problem.** *Top left: Re = 100; Top right: Re= 300; Bottom left: Re = 500; Bottom left: Re = 700. Isocurves on unit velocity scale from 0 to 1 with 20 uniformly spaced curves for each calculation.*

Isocurves of the velocity magnitudes are given in Figure 4.4 for solutions to the lid driven cavity problem at Reynolds numbers of 100, 300, 500 and 700. Increasing the velocity on the top boundary of the problem drives up the Reynolds number of the system making it more difficult to solve. More rotation of the fluid is induced by inertial forces and we begin to see some additional vortexes form besides the primary vortex near the center of the box.
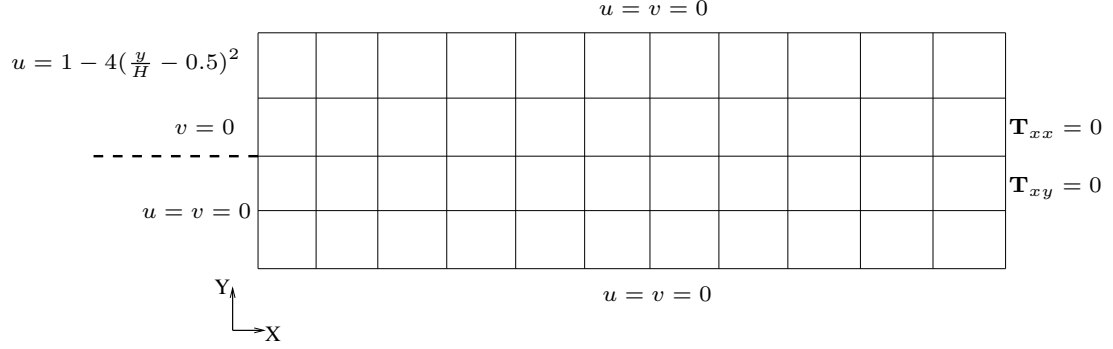
Figure 4.5: **Problem setup for the backward facing step benchmark.** *Zero velocity boundary conditions are applied at the top and bottom of the domain while the outflow boundary condition on the right boundary is represented by zero stress tensor components in the direction of the flow. For the inlet conditions, the left boundary is split such that the top half has a fully formed parabolic flow profile and the bottom half has a zero velocity condition, simulating flow over a step. The H parameter given in the parabolic inlet condition is the width of the inlet.*

4.3.2.1 Backward-Facing Step Problem

The third benchmark was generated by Gartling in 1990 and consists of both flow over a backward step and an outflow boundary condition [87]. Using the mass and momentum equations while neglecting the energy equation, this problem utilizes a longer domain with a 1/25 aspect ratio used for this work[1] with the boundary conditions as shown in Figure 4.5.

In this problem, the inflow condition is specified by a fully-formed parabolic flow profile over a zero velocity boundary representing a step. For this work, a slightly different parabolic formulation for the inlet velocities was used than in the benchmark. In the benchmark solutions, the average velocity in the parabola was 2/3 that of the maximum velocity while the formula given in Figure 4.5 produces a more plug-like flow with an average velocity 3/4 that of the maximum velocity. The flow over this step will generate a recirculating backflow under the inlet flow towards the step and at higher Reynolds numbers a recirculating zone will form farther downstream from the step. As in the lid driven cavity problem, the nonlinear

---

[1]The literature on this benchmark suggests using a domain with a 1/30 aspect ratio to reduce the effect of the outflow boundary condition on the upstream recirculation zones. Using a 1/25 aspect ratio for this work was not observed to disturb the recirculation zones and was therefore used to reduce memory pressure on the FANM solver.
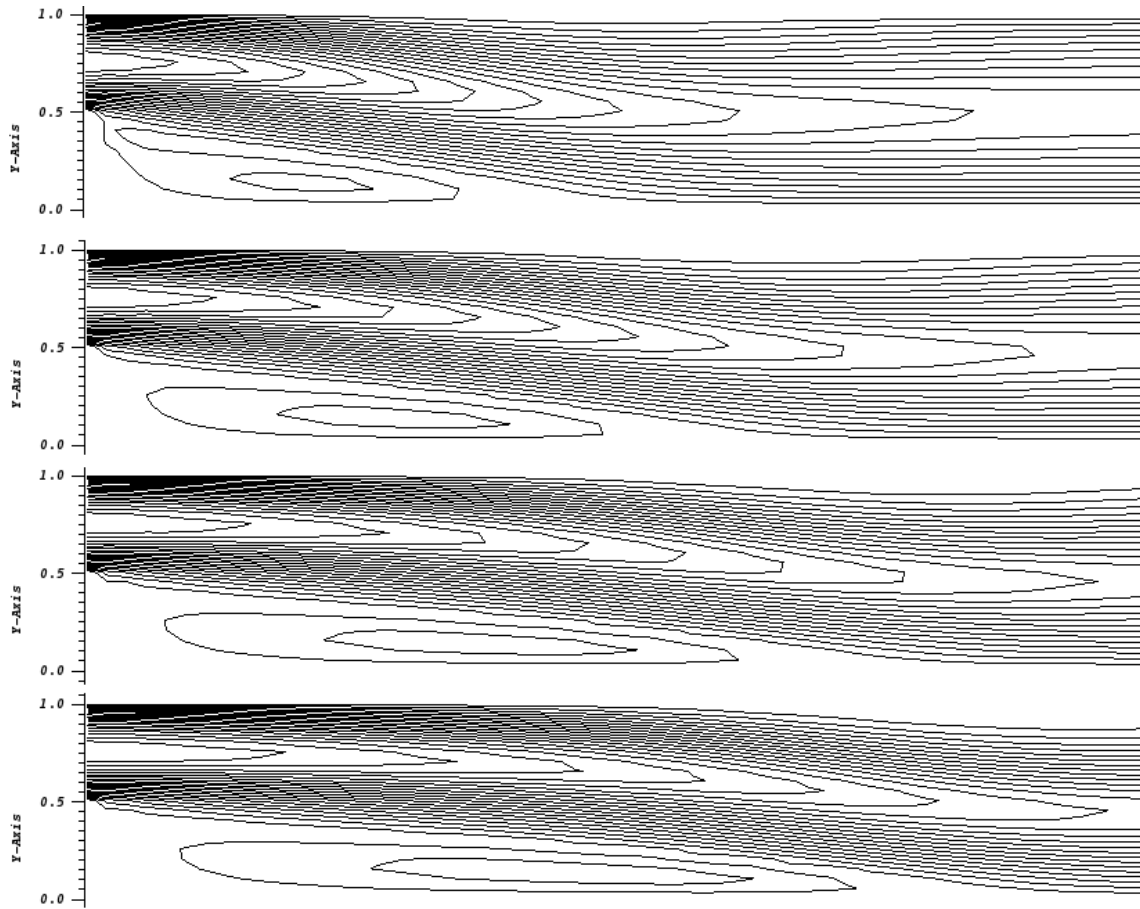
Figure 4.6: **Velocity magnitude isocurves from solution to the backward facing step problem.** *From top to bottom: Re = 200, Re = 300, Re = 400, Re = 500. Isocurves on unit velocity scale from 0 to 1 with 20 uniformly spaced curves for each calculation. The depression forming in the upper right portion of visible flow is the second vortex.*

behavior of this benchmark and the difficulty in obtaining a solution is dictated by the Reynolds number of the fluid. In Shadid's work, a Reynolds numbers up to 800 were used.

Compared to the lid driven cavity benchmark, the flow over a backward step is much more representative of flow driven by inertial forces in a nuclear reactor that may encounter several obstacles along the flow path. For example, spacer grids in fuel assemblies or mixing vanes designed to induce turbulence and improve heat transfer will create recirculation zones much like those observed for this benchmark problem. Figure 4.6 gives the velocity magnitude contours for solutions to this problem with Reynolds numbers of 200, 300, 400, and 500.

4.4 FANM Verification

For each of the benchmark problems, we will present the results of computations using FANM and directly compare them to results using a Newton-Krylov method in order to verify the correctness of FANM and its applicability to fluid problems. For each case, we will compare the global minimum, maximum, and average values for fluid velocity and pressure for all benchmarks and additionally temperature for the thermal convection cavity problem. If the values for these quantities computed using FANM match those computed using a production Newton-Krylov method, the implementation will be deemed correct and the method deemed valid for the purposes of this work. In addition, we will report the tolerance to which the nonlinear residual was converged as an additional means of comparison for correctness.

Given the difficulty of these benchmark problems, the linear solve at each Newton step was preconditioned with an algebraic multigrid method[2], a common technique for preconditioning these equations [85, 92] with the preconditioner reconstructed at every Newton step for the new Jacobian. Without multigrid preconditioning, the residual in MCSA was observed to stagnate. Typically this happens because the Richardson iteration and Neumann series on which the Monte Carlo method is based will quickly damp the higher order error modes on the scale of the computational grid used to solve the problem but will reduce lower order error modes at a considerably lower rate. In terms of Monte Carlo, this stagnation manifests itself in histories that simply do no terminate and therefore no solution is acquired. For many of the problems presented here, it is likely that a more physics-based preconditioning strategy such as those presented in [92, 93] will yield better results for more difficult problems. However, the explicit preconditioning strategy used here currently limits us to algebraic preconditioning.

For every benchmark calculation, both FANM and Newton-Krylov were preconditioned with the same multigrid parameters such that the conditioning of the system would not be

---

[2]The ML algebraic multigrid library in the Trilinos scientific computing libraries [77] was used for all problems.

a factor in the verification of the method or the performance comparison in the following section. With FANM, this preconditioning was required to reduce the spectral radius of the Jacobian operators generated at each Newton step. This preconditioning was also required to obtain good convergence properties for the Newton-Krylov solutions although it was not necessary for their convergence. In addition, the same nonlinear solver parameters including globalization and forcing term strategies were used with both methods. As with the radiation transport calculations in the previous chapter, algebraic preconditioning with the multigrid method results in dense linear systems. To mitigate this, the reduced domain approximation was again applied to the Monte Carlo solution within the MCSA solve occurring at each nonlinear iteration. The values used for the approximation will be given for each benchmark problem.

Results in this and the following section were produced by the Drekar multiphysics code base being developed at Sandia National Laboratories for fluid flow and other multiple physics simulations [46]. Drekar is a massively parallel physics framework that utilizes Newton-Krylov methods to generate a fully consistent solution scheme for the Navier-Stokes equations among other systems with Jacobian generation through automatic differentiation. To achieve these results, a Monte Carlo solver generated for this work was injected into the nonlinear tool chain within Drekar to form an implementation of the FANM method. For the Newton-Krylov solutions, the same production implementation of GMRES from the Trilinos scientific computing library Aztec [77] used for the verification of MCSA for the SP_N solutions in the previous chapter was also used here as a means of comparison and FANM benchmarking.

4.4.1   Thermal Convection Cavity Results

A Drekar model of thermal convection cavity problem was solved using both the Newton-Krylov solver and the FANM solver for Rayleigh numbers of 1×10^3, 1×10^4, 1×10^5 and 1×10^6 on a 50×50 square grid. Table 4.1 gives the physical parameters of the problem and

Table 4.2 gives the MCSA solver parameters used within the FANM method. Variation in the Rayleigh number of the system was achieved by keeping the parameters given in Table 4.1 constant and varying temperature of the hot side of the cavity. In addition to multigrid preconditioning for the linear solution at each Newton step, backtracking as outlined in Shadid's work [41] was used as a means of globalization to assist the Newton correction computation while the forcing term at all Rayleigh numbers but 1×10^6 was computed at each Newton step using method 2 from Shadid's work. In this forcing term method, nonlinear residuals from the two previous Newton steps are used to inform the choice of the forcing term for the next step. At a Rayleigh number of 1×10^6, a constant forcing term of 1×10^{-4} was use to give better convergence properties.

Parameter	Value	Units
x_{min}	0.0	m
x_{max}	1.0	m
y_{min}	0.0	m
y_{max}	1.0	m
N_x	50	-
N_y	50	-
$DOFs$	10404	-
Initial Temperature	0.0	K
Density	1.0	kg/m^3
Specific Heat	1.0	J / $(kg \times K)$
Dynamic Viscosity	0.71	$(N \times s)/m^2$
Thermal Conductivity	1.0	$W/(m \times K)$
Thermal Expansion Coefficient	1000	$1/K$
Thermal Diffusivity	1.0	m^2/s
Kinematic Viscosity	0.71	m^2/s
Gravitational Acceleration	10	m/s^2
Cavity Characteristic Length	1.0	m
Prandtl Number	0.71	-

Table 4.1: **Thermal convection cavity FANM verification model problem parameters.** *The Navier-Stokes equations in 2 dimensions are used for the model problem. The Rayleigh number is varied by modifying the hot boundary temperature to induce larger temperature gradients and buoyancy-driven flow.*

For the verification calculations, at each Rayleigh number the global minimum, maximum,

Parameter	Value
Histories	500,000 per iteration
Weight Cutoff	1×10^{-2}
Fixed Point Iteration	Richardson
Estimator	Adjoint Collision
Reduced Domain Fill Level	200

Table 4.2: **Thermal convection cavity FANM verification MCSA solver parameters.** *No relaxation parameters or variance reduction techniques were used with MCSA other than the reduced domain approximation.*

and average values were recorded for fluid velocity in the x and y directions, fluid pressure, and fluid temperature. Tables 4.3, 4.4, 4.5, and 4.6 give the results of these computations. It should be noted that the negative pressures computed are due to a relative pressure being reported. For each of the data points presented, both Newton-Krylov solutions and FANM solutions computed identical numerical results for all of these global values. No variation in solution was noted for each of the computations larger than the tolerance of the converged nonlinear residual norms given in Table 4.7. Variations in the convergence behavior and differences in performance for these solutions will be analyzed in the following section.

Parameter	Newton-Krylov Result	FANM Result
Average U	-1.288835730E-05	-1.288835730E-05
Minimum U	-3.677243960E+00	-3.677243960E+00
Maximum U	3.688908550E+00	3.688908550E+00
Average V	3.403670530E-02	3.403670530E-02
Minimum V	-3.721178580E+00	-3.721178580E+00
Maximum V	3.791483420E+00	3.791483420E+00
Average P	2.345554770E+02	2.345554770E+02
Minimum P	-5.509779180E+00	-5.509779180E+00
Maximum P	4.994885560E+02	4.994885560E+02
Average T	3.595148700E-02	3.595148700E-02
Minimum T	2.092448340E-04	2.092448340E-04
Maximum T	7.178874510E-02	7.178874510E-02

Table 4.3: **Thermal convection cavity FANM verification for a Rayleigh number of 1×10^3.** *The values reported are global minima, maxima, and averages for each variable in the problem. The velocity is given in components in the x and y directions.*

Parameter	Newton-Krylov Result	FANM Result
Average U	-7.489201240E-04	-7.489201240E-04
Minimum U	-1.607318000E+01	-1.607318000E+01
Maximum U	1.669098270E+01	1.669098270E+01
Average V	3.377624420E-01	3.377624420E-01
Minimum V	-1.932174800E+01	-1.932174800E+01
Maximum V	2.047326820E+01	2.047326820E+01
Average P	1.861894950E+03	1.861894950E+03
Minimum P	-3.353416240E+01	-3.353416240E+01
Maximum P	4.440642810E+03	4.440642810E+03
Average T	3.510568440E-01	3.510568440E-01
Minimum T	2.092448340E-04	2.092448340E-04
Maximum T	7.178874510E-02	7.178874510E-02

Table 4.4: **Thermal convection cavity FANM verification for a Rayleigh number of 1×10^4.** *The values reported are global minima, maxima, and averages for each variable in the problem. The velocity is given in components in the x and y directions.*

Parameter	Newton-Krylov Result	FANM Result
Average U	-2.043639370E-02	-2.043639370E-02
Minimum U	-3.814922470E+01	-3.814922470E+01
Maximum U	-3.814922470E+01	-3.814922470E+01
Average V	2.774864300E+00	2.774864300E+00
Minimum V	-6.038682990E+01	-6.038682990E+01
Maximum V	7.873873560E+01	7.873873560E+01
Average P	1.324208380E+04	1.324208380E+04
Minimum P	-1.390235490E+02	-1.390235490E+02
Maximum P	3.559215530E+04	3.559215530E+04
Average T	3.027827770E+00	3.027827770E+00
Minimum T	1.626405740E-02	1.626405740E-02
Maximum T	7.162571130E+00	7.162571130E+00

Table 4.5: **Thermal convection cavity FANM verification for a Rayleigh number of 1×10^5.** *The values reported are global minima, maxima, and averages for each variable in the problem. The velocity is given in components in the x and y directions.*

Parameter	Newton-Krylov Result	FANM Result
Average U	-1.802569840E-01	-1.802569840E-01
Minimum U	-6.292084130E+01	-6.292084130E+01
Maximum U	2.951113240E+02	2.951113240E+02
Average V	1.336398550E+01	1.336398550E+01
Minimum V	-1.345663290E+02	-1.345663290E+02
Maximum V	3.227873890E+02	3.227873890E+02
Average P	6.354313840E+04	6.354313840E+04
Minimum P	-1.356309630E+02	-1.356309630E+02
Maximum P	2.316308730E+05	2.316308730E+05
Average T	1.780727610E+01	1.780727610E+01
Minimum T	8.265788890E-02	8.265788890E-02
Maximum T	7.098873170E+01	7.098873170E+01

Table 4.6: **Thermal convection cavity FANM verification for a Rayleigh number of** 1×10^6**.** *The values reported are global minima, maxima, and averages for each variable in the problem. The velocity is given in components in the x and y directions.*

Rayleigh Number	Newton Krylov $||\mathbf{F}(\mathbf{u})||$	FANM $||\mathbf{F}(\mathbf{u})||$
1×10^3	4.542×10^{-14}	1.208×10^{-14}
1×10^4	1.045×10^{-12}	7.012×10^{-13}
1×10^5	1.784×10^{-12}	1.059×10^{-12}
1×10^6	3.404×10^{-12}	3.479×10^{-12}

Table 4.7: **Thermal convection cavity nonlinear residual norm achieved convergence.** *The results presented here were obtained from the benchmark verification calculations.*

4.4.2   Lid Driven Cavity Results

A Drekar model of thermal convection cavity problem was solved using both the Newton-Krylov solver and the FANM solver for Reynolds numbers of 100, 300, 500, and 700 on a 50×50 square grid. Table 4.8 gives the physical parameters of the problem and Table 4.9 gives the MCSA solver parameters used within the FANM method. Variation in the Reynolds number of the system was achieved by keeping the parameters given in Table 4.8 fixed and varying the fluid velocity in the x direction on the top boundary. In addition to multigrid preconditioning for the linear solution at each Newton step, a polynomial line search method was used as a means of globalization, assisting the Newton correction computation as outlined by Pawlowski in [68] while the forcing term was again computed using method 2 from Shadid's work [41] at all Reynolds numbers.

Parameter	Value	Units
x_{min}	0.0	m
x_{max}	1.0	m
y_{min}	0.0	m
y_{max}	1.0	m
N_x	50	-
N_y	50	-
$DOFs$	7803	-
Density	1.0	kg/m^3
Dynamic Viscosity	0.71	$(N \times s)/m^2$
Kinematic Viscosity	0.71	m^2/s
Cavity Characteristic Length	1.0	m

Table 4.8: **Lid driven cavity FANM verification model problem parameters.** *The Navier-Stokes equations in 2 dimensions are used for the model problem. The Reynolds number is varied by modifying the velocity magnitude on the upper boundary to induce flow driven by inertial forces.*

In the literature on this benchmark, solutions at Reynolds numbers of up to 1×10^4 were achieved using a variety of nonlinear solution techniques. With the FANM method, at Reynolds numbers above 700 convergence of the linear iterations could not be achieved regardless of how aggressive the multigrid preconditioner was set. In these cases, the Jacobian

Parameter	Value
Weight Cutoff	1×10^{-2}
Fixed Point Iteration	Richardson
Estimator	Adjoint Collision
Histories, Re=100	500,000 per iteration
Histories, Re=300	500,000 per iteration
Histories, Re=500	500,000 per iteration
Histories, Re=700	1,000,000 per iteration
Reduced Domain Fill Level, Re=100	200
Reduced Domain Fill Level, Re=300	200
Reduced Domain Fill Level, Re=500	200
Reduced Domain Fill Level, Re=700	300

Table 4.9: **Lid driven cavity FANM verification MCSA solver parameters.** *No relaxation parameters or variance reduction techniques were used with MCSA other than the reduced domain approximation. Different values of fill level for the reduced domain approximation and histories per iteration were used at different Reynolds numbers due to convergence requirements.*

operators are ill-conditioned enough that even GMRES converges slowly relative to the thermal convection cavity benchmark. Therefore, the spectral radius limitation on MCSA is extremely prohibitive in this case and others where transport driven by inertial forces is dominant. Because of this, only solutions to the lid driven cavity benchmark at Reynolds numbers of up to 700 are presented.

For the verification calculations, at each Reynolds number the global minimum, maximum, and average values were recorded for the fluid velocity in the x and y directions and the fluid pressure. Tables 4.10, 4.11, 4.12, and 4.13 give the results of these computations. As with the thermal convection problem, the negative pressures computed are due to a relative pressure being reported. For each of the data points given, both Newton-Krylov solutions and FANM solutions computed identical numerical results for all of these global values. The norm of the converged nonlinear residual for the calculations is given in Table 4.14. All computed global values were within these tolerances.

Parameter	Newton-Krylov Result	FANM Result
Average U	1.165632320E-01	1.165632320E-01
Minimum U	-2.423642920E+01	-2.423642920E+01
Maximum U	9.742670880E+01	9.742670880E+01
Average V	2.038480420E-02	2.038480420E-02
Minimum V	-5.266315430E+01	-5.266315430E+01
Maximum V	2.720044160E+01	2.720044160E+01
Average P	-1.656193900E+02	-1.656193900E+02
Minimum P	-9.635479370E+03	-9.635479370E+03
Maximum P	1.854517020E+04	1.854517020E+04

Table 4.10: **Lid driven cavity FANM verification for a Reynolds number of 100.** *The values reported are global minima, maxima, and averages for each variable in the problem. The velocity is given in components in the x and y directions.*

Parameter	Newton-Krylov Result	FANM Result
Average U	3.382078040E-01	3.382078040E-01
Minimum U	-9.467140360E+01	-9.467140360E+01
Maximum U	2.895885380E+02	2.895885380E+02
Average V	8.780242440E-02	8.780242440E-02
Minimum V	-1.830156060E+02	-1.830156060E+02
Maximum V	8.827373340E+01	8.827373340E+01
Average P	-2.830380160E+03	-2.830380160E+03
Minimum P	-2.352177540E+04	-2.352177540E+04
Maximum P	9.254997120E+04	9.254997120E+04

Table 4.11: **Lid driven cavity FANM verification for a Reynolds number of 300.** *The values reported are global minima, maxima, and averages for each variable in the problem. The velocity is given in components in the x and y directions.*

Parameter	Newton-Krylov Result	FANM Result
Average U	5.098921320E-01	5.098921320E-01
Minimum U	-1.731861690E+02	-1.731861690E+02
Maximum U	4.789146040E+02	4.789146040E+02
Average V	1.365493140E-01	1.365493140E-01
Minimum V	-3.170930360E+02	-3.170930360E+02
Maximum V	1.655401440E+02	1.655401440E+02
Average P	-9.378317550E+03	-9.378317550E+03
Minimum P	-4.155215280E+04	-4.155215280E+04
Maximum P	2.058742010E+05	2.058742010E+05

Table 4.12: **Lid driven cavity FANM verification for a Reynolds number of 500.** *The values reported are global minima, maxima, and averages for each variable in the problem. The velocity is given in components in the x and y directions.*

Parameter	Newton-Krylov Result	FANM Result
Average U	6.479541170E-01	6.479541170E-01
Minimum U	-2.550685400E+02	-2.550685400E+02
Maximum U	6.663054900E+02	6.663054900E+02
Average V	1.833690840E-01	1.833690840E-01
Minimum V	-4.491052980E+02	-4.491052980E+02
Maximum V	2.474376340E+02	2.474376340E+02
Average P	1.833690840E-01	1.833690840E-01
Minimum P	-6.241704500E+04	-6.241704500E+04
Maximum P	3.518174810E+05	3.518174810E+05

Table 4.13: **Lid driven cavity FANM verification for a Reynolds number of 700.** *The values reported are global minima, maxima, and averages for each variable in the problem. The velocity is given in components in the x and y directions.*

Reynolds Number	Newton Krylov $||\mathbf{F}(\mathbf{u})||$	FANM $||\mathbf{F}(\mathbf{u})||$
100	5.453×10^{-14}	6.577×10^{-14}
300	2.537×10^{-13}	2.779×10^{-13}
500	6.367×10^{-13}	6.252×10^{-13}
700	9.159×10^{-13}	1.282×10^{-12}

Table 4.14: **Lid driven cavity nonlinear residual norm achieved convergence.** *The results presented here were obtained from the benchmark verification calculations.*

4.4.3   Backward Facing Step Results

A Drekar model of the backward facing step problem was solved using both the Newton-Krylov solver and the FANM solver for Reynolds numbers of 200, 300, 400, and 500 on a 20×250 rectangular grid. Table 4.15 gives the physical parameters of the problem and Table 4.16 gives the MCSA solver parameters used within the FANM method. Variation in the Reynolds number of the system was achieved by keeping the parameters given in Table 4.15 fixed and varying the maximum fluid velocity in the parabolic inlet condition. In addition to multigrid preconditioning for the linear solution at each Newton step, a polynomial line search method was used as a means of globalization while the forcing term was again computed using method 2 from Shadid's work [41].

Parameter	Value	Units
x_{min}	0.0	m
x_{max}	25.0	m
y_{min}	0.0	m
y_{max}	1.0	m
N_x	20	-
N_y	250	-
$DOFs$	15813	-
Density	1.0	kg/m^3
Dynamic Viscosity	1.0	$(N \times s)/m^2$
Kinematic Viscosity	1.0	m^2/s
Channel Width	1.0	m
Step Height	0.5	m

Table 4.15: **Backward facing step FANM verification model problem parameters.** *The Navier-Stokes equations in 2 dimensions are used for the model problem. The Reynolds number is varied by modifying the maximum velocity magnitude in the parabolic inlet condition.*

In the literature on this benchmark, solutions at Reynolds numbers of up to 800 were achieved using a variety of nonlinear solution techniques. In identical fashion to the lid driven cavity problem, at Reynolds numbers above 500 convergence of the linear iterations could not be achieved with FANM regardless of how aggressive the multigrid preconditioner was set. In these cases, the Jacobian operators are again ill-conditioned enough that a spectral

Parameter	Value
Weight Cutoff	1×10^{-2}
Fixed Point Iteration	Richardson
Estimator	Adjoint Collision
Histories, Re=200	500,000 per iteration
Histories, Re=300	500,000 per iteration
Histories, Re=400	500,000 per iteration
Histories, Re=500	1,000,000 per iteration
Reduced Domain Fill Level, All Re	200

Table 4.16: **Backward facing step FANM verification MCSA solver parameters.** *No relaxation parameters or variance reduction techniques were used with MCSA other than the reduced domain approximation. The same fill level for the reduced domain approximation was used at every Reynolds numbers and different histories per iteration were used at different Reynolds numbers due to convergence requirements.*

radius of less than one could not be achieved with multigrid preconditioning and several cycle applications. Therefore, the spectral radius limitation on MCSA is extremely prohibitive in this case as well and even more so than the lid driven cavity problem where solutions at higher Reynolds numbers were achieved. Because of this, only solutions to the backward facing step benchmark at Reynolds numbers of up to 500 are presented.

For the verification calculations, at each Reynolds number the global minimum, maximum, and average values were recorded for the fluid velocity in the x and y directions and the fluid pressure. Tables 4.17, 4.18, 4.19, and 4.20 give the results of these computations. The norm of the converged nonlinear residual for the calculations is given in Table 4.21. The Newton-Krylov solutions and FANM solutions computed identical numerical results for all of these global values within converged tolerances.

Parameter	Newton-Krylov Result	FANM Result
Average U	8.776187720E+01	8.776187720E+01
Minimum U	-2.796828970E+01	-2.796828970E+01
Maximum U	2.639993990E+02	2.639993990E+02
Average V	-8.870766180E-01	-8.870766180E-01
Minimum V	-2.636357380E+01	-2.636357380E+01
Maximum V	1.330345700E+01	1.330345700E+01
Average P	1.226960220E+04	1.226960220E+04
Minimum P	2.953808400E+01	2.953808400E+01
Maximum P	2.202121190E+04	2.202121190E+04

Table 4.17: **Backward facing step FANM verification for a Reynolds number of 200.** *The values reported are global minima, maxima, and averages for each variable in the problem. The velocity is given in components in the x and y directions.*

Parameter	Newton-Krylov Result	FANM Result
Average U	1.316701890E+02	1.316701890E+02
Minimum U	-4.357431070E+01	-4.357431070E+01
Maximum U	3.958553050E+02	3.958553050E+02
Average V	-1.330267460E+00	-1.330267460E+00
Minimum V	-3.467114630E+01	-3.467114630E+01
Maximum V	1.694243270E+01	1.694243270E+01
Average P	1.681552980E+04	1.681552980E+04
Minimum P	4.129311640E+01	4.129311640E+01
Maximum P	2.940820620E+04	2.940820620E+04

Table 4.18: **Backward facing step FANM verification for a Reynolds number of 300.** *The values reported are global minima, maxima, and averages for each variable in the problem. The velocity is given in components in the x and y directions.*

Parameter	Newton-Krylov Result	FANM Result
Average U	1.759720450E+02	1.759720450E+02
Minimum U	-5.941731260E+01	-5.941731260E+01
Maximum U	5.287146290E+02	5.287146290E+02
Average V	-1.776706740E+00	-1.776706740E+00
Minimum V	-4.497362670E+01	-4.497362670E+01
Maximum V	1.973372840E+01	1.973372840E+01
Average P	1.954352940E+04	1.954352940E+04
Minimum P	5.294095080E+01	5.294095080E+01
Maximum P	3.457969480E+04	3.457969480E+04

Table 4.19: **Backward facing step FANM verification for a Reynolds number of 400.** *The values reported are global minima, maxima, and averages for each variable in the problem. The velocity is given in components in the x and y directions.*

Parameter	Newton-Krylov Result	FANM Result
Average U	2.199858290E+02	2.199858290E+02
Minimum U	-7.549221730E+01	-7.549221730E+01
Maximum U	6.605863330E+02	6.605863330E+02
Average V	-2.220108250E+00	-2.220108250E+00
Minimum V	-5.888473080E+01	-5.888473080E+01
Maximum V	2.201938360E+01	2.201938360E+01
Average P	1.983947940E+04	1.983947940E+04
Minimum P	-9.707913370E+03	-9.707913370E+03
Maximum P	3.771193860E+04	3.771193860E+04

Table 4.20: **Backward facing step FANM verification for a Reynolds number of 500.** *The values reported are global minima, maxima, and averages for each variable in the problem. The velocity is given in components in the x and y directions.*

Reynolds Number	Newton Krylov $||\mathbf{F}(\mathbf{u})||$	FANM $||\mathbf{F}(\mathbf{u})||$
200	1.939E-11	1.975E-11
300	2.786E-11	2.751E-11
400	3.360E-11	3.597E-11
500	5.824E-11	4.062E-11

Table 4.21: **Backward facing step nonlinear residual norm achieved convergence.** *The results presented here were obtained from the benchmark verification calculations.*

4.5 FANM Performance Comparison to Conventional Methods

Using the benchmarks from the verification, we now compare the performance of the FANM method against a conventional Newton-Krylov (NK) method. For each benchmark, we will analyze the iterative performance of both the nonlinear Newton solver and the linear solver used to compute the Newton correction vector at each step. Limiting the number of nonlinear iterations required for solution is critical for efficiency as nonlinear function evaluations, Jacobian generation, and preconditioner construction are typically required at every Newton iteration. In addition, timing results will also be discussed. To quantify the acceleration provided by the residual Monte Carlo component of MCSA, each calculation was also performed using the same Newton method but with a plain preconditioned Richardson iteration as the linear solution technique to give a Newton-Richardson (NR) scheme. For all cases the Richardson iteration was preconditioned in the same way as GMRES and MCSA.

4.5.1 Thermal Convection Cavity Results

At each Rayleigh number used for the thermal convection cavity problem, Table 4.22 gives the number of Newton iterations required for convergence for each method. For all Rayleigh numbers except 1×10^5 the number of Newton iterations required to converge is the same while the 1×10^5 result required an extra FANM iteration. This is due to the fact that the convergence of the linear residual has a strong effect on the convergence of the nonlinear residual. For nonlinear calculations, this is much stronger than the effect on the convergence of the eigenvalue in the SP_N computations where we always observed that identical numbers of k-eigenvalue iterations were required to converge each variation of the problem.

As outlined in our discussion on inexact Newton methods, depending on how converged the linear residual is at each step, it is possible to throw off the nonlinear iteration and

decrease iterative performance. Although the same preconditioner was used with both the Newton-Krylov and FANM calculations, the convergence properties of MCSA and GMRES are different and we therefore expect them to produce different results at each nonlinear iteration which will in turn affect the forcing term calculation. If they are different enough, it is possible that another Newton iteration may be required. Even considering the extra Newton iteration, the solutions are converged to effectively the same residual norm tolerance and produce the same results as provided by the verification.

Figure 4.7 gives the nonlinear residual behavior for the 1×10^5 Rayleigh number case that required the extra FANM iteration. We see that the extra iteration comes from slightly slower quadratic convergence with FANM for this particular case. The difference in convergence of the nonlinear problem comes from the fact that the same multigrid preconditioner parameters are used for this case as for the 1×10^3 and 1×10^4 Rayleigh number cases for the linear solutions. Using the same preconditioner for the harder 1×10^5 case means that the problem is still growing in difficulty even though it is preconditioned in an identical manner. This means that the GMRES solver at each Newton step is converging the linear residual to a smaller tolerance than the MCSA solver as the forcing terms adapt to the convergence of the method over the course of nonlinear iterations. For this problem, tighter convergence of the linear model at later Newton steps also improved convergence of nonlinear model, resulting in the extra FANM iteration.

As the Rayleigh number increases, the problem becomes more difficult to solve and therefore a more aggressive preconditioner should maintain iterative performance of the nonlinear method. This was observed to be true for the 1×10^6 Rayleigh number case. For this calculation, the number of multigrid cycle applications was bumped up to 3 from 1 and FANM converged in the same number of nonlinear iterations as the Newton-Krylov method.

In addition to nonlinear iterative performance, performance of the inner linear solves is also of interest. Here, we seek to maintain a minimum number of total linear solver iterations over the course of all nonlinear iterations in order to limit matrix-vector multiplies and

Rayleigh Number	NK Iterations	FANM Iterations	NR Iterations
1×10^3	5	5	5
1×10^4	7	7	7
1×10^5	9	10	9
1×10^6	11	11	11

Table 4.22: **Thermal convection cavity nonlinear iteration results for the performance comparison.** *The results presented here were obtained from the benchmark verification calculations.*
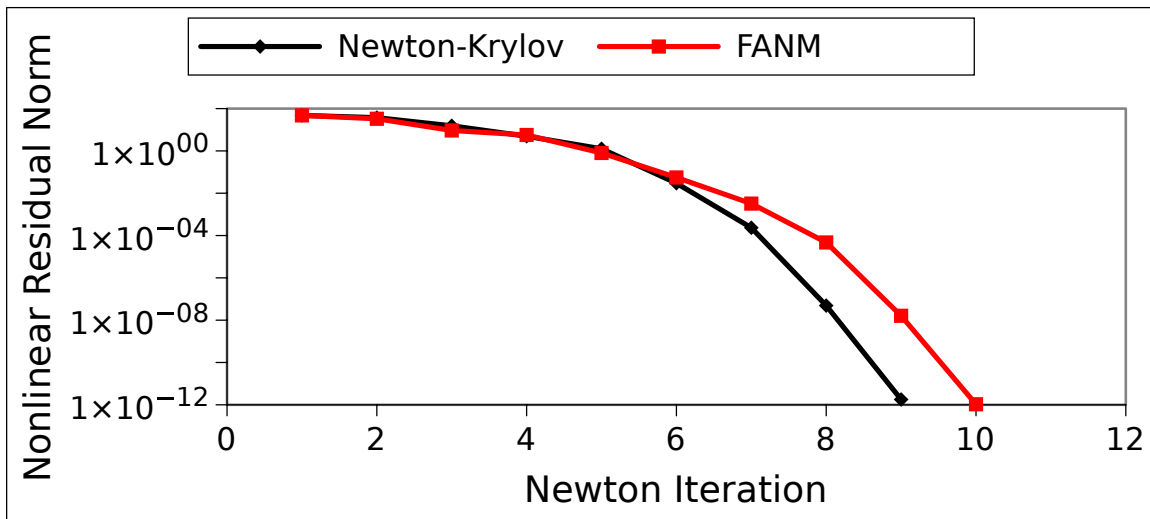
Figure 4.7: **Thermal convection cavity nonlinear residual norm as a function of Newton iteration for the 1×10^5 Rayleigh number case.** *The FANM calculation required an additional nonlinear iteration to converge.*

other costly operations. Table 4.23 gives the total number of GMRES iterations required to converge the problem for the Newton-Krylov method and the total number of MCSA iterations for the FANM method at each Rayleigh number used. For all cases, fewer MCSA iterations were required than GMRES iterations to converge the problem even with both solvers preconditioned with the same multigrid package and the same parameters. For the 1×10^6 Rayleigh number case where a constant forcing term of 1×10^{-4} was kept, this difference is most drastic with FANM requiring only 64% of the linear iterations required by the Newton-Krylov scheme with the linear solver per nonlinear iteration given for this case
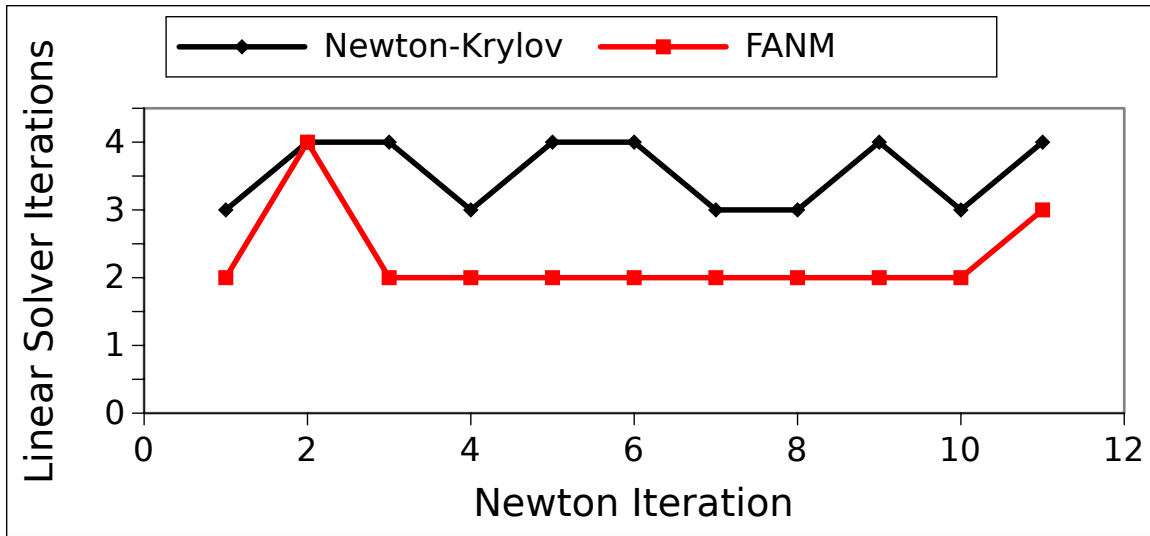
Figure 4.8: **Thermal convection cavity linear solver iterations as a function of Newton iteration for the 1×10^6 Rayleigh number case.** *MCSA shows better iterative performance than GMRES at all but the second nonlinear iteration and MCSA always accelerated the Richardson iteration. The forcing term was fixed at 1×10^{-4} at all nonlinear iterations.*

in Figure 4.8. Even the 1×10^5 Rayleigh number case that required more Newton iterations required 5 fewer MCSA iterations to converge than GMRES iterations. In all cases, MCSA improved on the iterative performance of using only the Richardson iteration through the residual Monte Carlo acceleration. If the performance of the MCSA implementation used here were to be potentially optimized in the future, this improved iterative performance could also mean improved time to solution.

Rayleigh Number	GMRES Iterations	MCSA Iterations	Richardson Iterations
1×10^3	23	18	38
1×10^4	23	17	34
1×10^5	25	20	34
1×10^6	39	25	48

Table 4.23: **Thermal convection cavity total sum of linear iterations for all nonlinear iterations.** *The results presented here were obtained from the benchmark verification calculations.*

Although the iterative performance of FANM is excellent for the thermal convection cavity

problem, the explicit preconditioning strategy causes the same issues as was observed for the SP_N equations in the previous chapter. Table 4.24 gives the speedup of the Newton-Krylov method over FANM. For all Rayleigh numbers, we see a fairly constant speedup of O(400) when using Newton-Krylov over FANM meaning that the implementation of the FANM method used here is significantly slower. As the inexact Newton scheme in Drekar was modified by simply swapping out the linear solver used at each Newton step, this increased compute time is coming directly from using MCSA as the linear solver and the overhead due to preconditioning. When preconditioning overhead for the SP_N equations was considered as shown by the data in Figure 3.30, a similar speedup of approximately two orders of magnitude was noted between the Krylov methods and MCSA showing consistency between those results and the convection cavity benchmark results presented. In addition, the fairly constant speedup values as a function of the primary problem parameter show that FANM has effectively the same time complexity as a Newton-Krylov method and the implementation timings simply differ by a constant value, also consistent with the SP_N observations.

Rayleigh Number	Newton-Krylov Speedup
1×10^3	338
1×10^4	336
1×10^5	346
1×10^6	465

Table 4.24: **Thermal convection cavity Newton-Krylov speedup over FANM method.** *Speedup values are rounded to the nearest integer. The results presented here were obtained from the benchmark verification calculations.*

4.5.2 Lid Driven Cavity Results

For the lid driven cavity benchmark, performance results were again compared between the FANM and Newton-Krylov calculations. In this case, the nonlinear iterative performance results as given by Table 4.25 show that the same number of Newton iterations were required to converge the 100, 300, and 500 Reynolds number cases while the FANM calculation with

a Reynolds number of 700 actually converged in 4 fewer iterations. The nonlinear residual norm as a function of Newton iteration for this case is given in Figure 4.9.

This result can be explained by the fact that as given by Table 4.9, although the preconditioner parameters were the same for both calculations, the MCSA iteration was pushed harder by doubling the number of histories used for the computation at each nonlinear iteration. These extra histories provided better convergence of the linear model at each iteration and did not result in oversolving, thereby increasing the convergence rate of the nonlinear model as well. This result is significant in that it shows increasing the number of histories used for each MCSA iteration can improve the performance of both linear and nonlinear convergence.

Reynolds Number	NK Iterations	FANM Iterations	NR Iterations
100	6	6	7
300	9	9	9
500	11	11	11
700	14	10	12

Table 4.25: **Lid driven cavity nonlinear iteration results for the performance comparison.** *The results presented here were obtained from the benchmark verification calculations.*

The difficulty of this benchmark problem as compared to the thermal convection cavity problem is readily apparent in the linear iteration counts as given by Table 4.26. As the opposite of what was observed for that benchmark, lid driven cavity results show that the linear models were significantly more ill-conditioned, requiring many more MCSA and GMRES iterations. For all cases except the 700 Reynolds number case, many more MCSA iterations were required to converge with the observed GMRES iteration count 64% of that observed for MCSA when looking at the 100 Reynolds number case. For the 700 Reynolds number case, fewer MCSA iterations were observed due to the fact that 4 fewer nonlinear iterations were performed. The average number of linear iterations per nonlinear iteration was still much larger for the FANM calculations. In all cases, MCSA improved on the
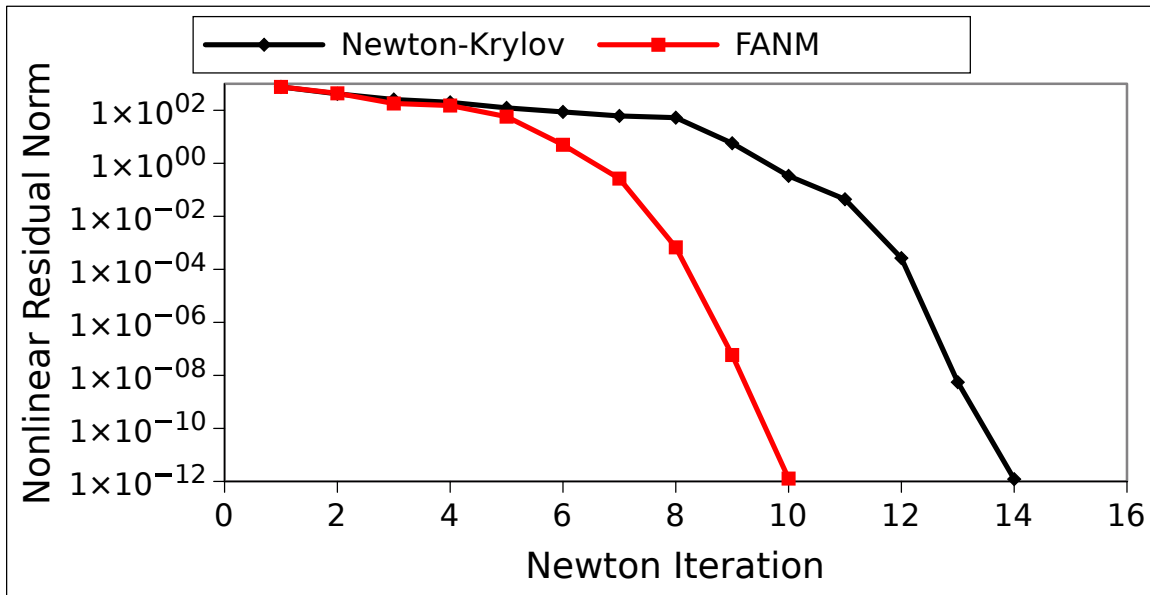
Figure 4.9: **Lid driven cavity nonlinear residual norm as a function of Newton iteration for the 700 Reynolds number case.** *The FANM calculation converged in 4 fewer iterations than the Newton-Krylov calculation.*

iterative performance of using only the Richardson iteration through the residual Monte Carlo acceleration even considering the cases with Reynolds numbers of 100 and 700 where an extra Newton-Richardson iteration was required to converge the nonlinear model.

As an additional means of analysis for the linear solver iteration results, we will look at a case where MCSA performed poorly compared to GMRES. Consider the linear iterations as a function of nonlinear iteration given in Figure 4.10 and the forcing term as a function of nonlinear iteration given in Figure 4.11 for the 500 Reynolds number case. At the later Newton iterations where the region of fast quadratic convergence is reached, we see that MCSA required many more iterations to converge than GMRES, accounting for the majority of the extra iterations. However, we see in the forcing term data that forcing terms at later Newton iterations for MCSA were much smaller than those for GMRES. This means that MCSA was converged to a tighter tolerance at these iterations and therefore required the extra iterations.

As a final comparison, the timing of both methods was again compared with the speedup
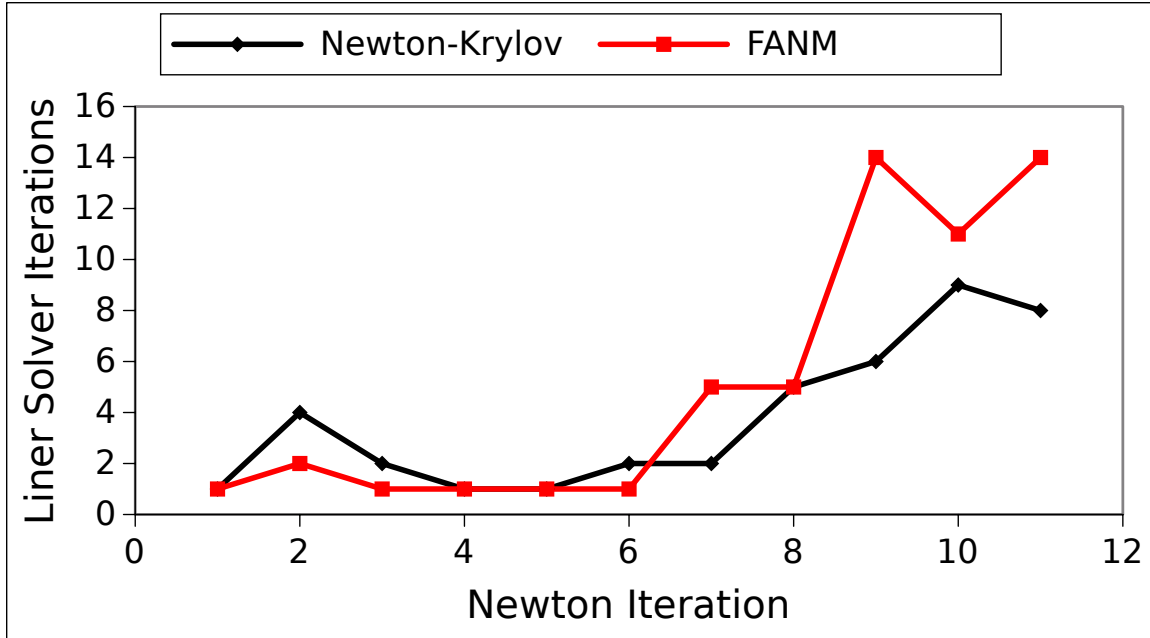
Figure 4.10: **Lid driven cavity linear solver iterations as a function of Newton iteration for the 500 Reynolds number case.** *More MCSA iterations were required to converge the linear models at later Newton iterations due to smaller forcing terms.*

Reynolds Number	GMRES Iterations	MCSA Iterations	Richardson Iterations
100	27	42	151
300	35	52	133
500	41	56	154
700	21	14	32

Table 4.26: **Lid driven cavity total sum of linear iterations for all nonlinear iterations.** *The results presented here were obtained from the benchmark verification calculations. MCSA always accelerated the Richardson iteration.*

of using the Newton-Krylov solver over FANM reported in Table 4.27. The speedup values reported here are of the same magnitude as those reported for the thermal convection cavity problem and again in agreement with those observed for the SP_N calculations. Lack of significant variation in these timing results also point to a qualitatively similar time complexity for the FANM method as a function of primary problem parameter relative to the Newton-Krylov method. In all cases, the preconditioning strategy must be significantly improved along with implementation optimization to avoid these large overheads.
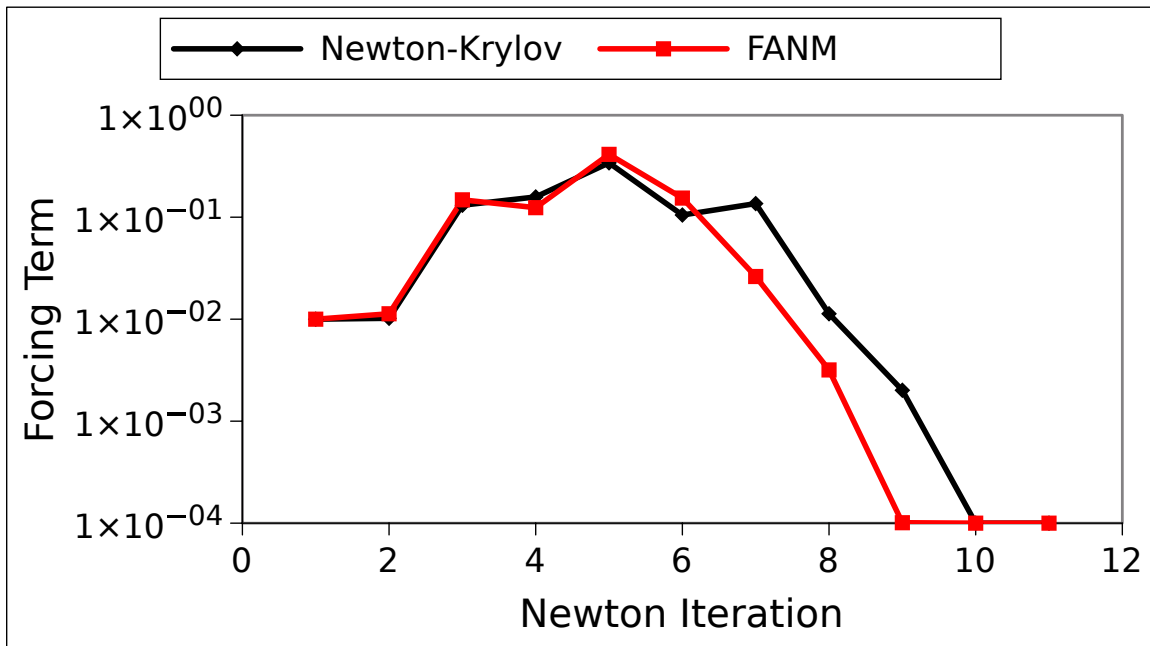
Figure 4.11: **Lid driven cavity forcing terms as a function of Newton iteration for the 500 Reynolds number case.** *Once the region of fast quadratic convergence is reached, MCSA forcing terms were much smaller.*

Reynolds Number	Newton-Krylov Speedup
100	299
300	322
500	288
700	488

Table 4.27: **Lid driven cavity Newton-Krylov speedup over FANM method.** *Speedup values are rounded to the nearest integer. The results presented here were obtained from the benchmark verification calculations.*

4.5.3 Backward Facing Step Results

The backward step problem exhibited different performance characteristics than the other two benchmark problems, likely due to the different geometry and boundary conditions. Table 4.28 gives the nonlinear iteration results for this benchmark. At low Reynolds numbers, FANM converges in fewer nonlinear iterations than the Newton-Krylov solver. However, as the problem becomes more difficult to solver at higher rates of flow, the Newton-Krylov solver eventually converges in fewer nonlinear iterations. We see the same behavior as well in the linear solver iteration data given by Table 4.29. At the 3 lowest Reynolds numbers, FANM required significantly fewer linear solver iterations to converge the problem while the ill-conditioned case at a Reynolds number of 500 is observed to use many more MCSA iterations. For Reynolds numbers of both 200 and 500, FANM also reduced the number of Newton steps need when compared to the Newton-Richardson scheme.

Reynolds Number	NK Iterations	FANM Iterations	NR Iterations
200	10	9	10
300	15	14	15
400	10	10	10
500	19	20	21

Table 4.28: **Backward facing step nonlinear iteration results for the performance comparison.** *The results presented here were obtained from the benchmark verification calculations.*

Reynolds Number	GMRES Iterations	MCSA Iterations	Richardson Iterations
200	24	13	21
300	23	17	21
400	18	12	14
500	30	52	98

Table 4.29: **Backward facing step total sum of linear iterations for all nonlinear iterations.** *The results presented here were obtained from the benchmark verification calculations.MCSA always accelerated the Richardson iteration.*

Unlike the lid driven cavity benchmark, the extra linear solver iterations are not due to the smaller forcing terms but are rather truly a function of the ill-conditioning of the Jacobian matrices produced at each Newton step. We see this by comparing the results at Reynolds numbers of 400 where FANM outperformed Newton-Krylov and 500 where Newton-Krylov outperformed FANM. Linear iterations as a function of nonlinear iteration given in Figure 4.12 and the forcing term as a function of nonlinear iteration given in Figure 4.13 for the 400 Reynolds number case and the same data is given in Figure 4.14 and Figure 4.15 for the 500 Reynolds number case. For both cases, FANM always has larger forcing terms and should therefore use fewer MCSA iterations at each Newton step to converge the linear model if the iterative performance is comparable. This is indeed the case for the 400 Reynolds number case where the linear model is better conditioned and FANM used fewer total linear solver iterations to converge the nonlinear residual. However, at a Reynolds number of 500 FANM has larger forcing terms but requires many more MCSA iterations to converge the last 2 Newton steps. Therefore, these extra iterations in this case must come from ill-conditioning.

We additionally see the effects of ill-conditioned Jacobians when looking at the acceleration provided by MCSA over using a preconditioned Richardson iteration. For the first 3 cases, the acceleration was not as significant as for the other benchmark problems. In this case, this means that the Richardson iteration and its acceleration by a stochastic realization of a Richardson iteration are not doing the bulk of the work in this problem. Rather, the algebraic multigrid preconditioning is performing more work at each iteration and therefore the acceleration is smaller. When the system becomes even more ill-conditioned in the 500 Reynolds number case the acceleration has more of an impact.

The ill-conditioning of the 500 Reynolds number case is also apparent in the timing data given in Table 4.30. For the first two cases, we see qualitatively similar speedup values for the Newton-Krylov solver relative to the observations for the first two benchmark problems of $O(100)$. However, the we expect the ill-conditioning to cause the Monte Carlo histories in the MCSA solver to have longer random walk lengths based on our MCSA breakdown
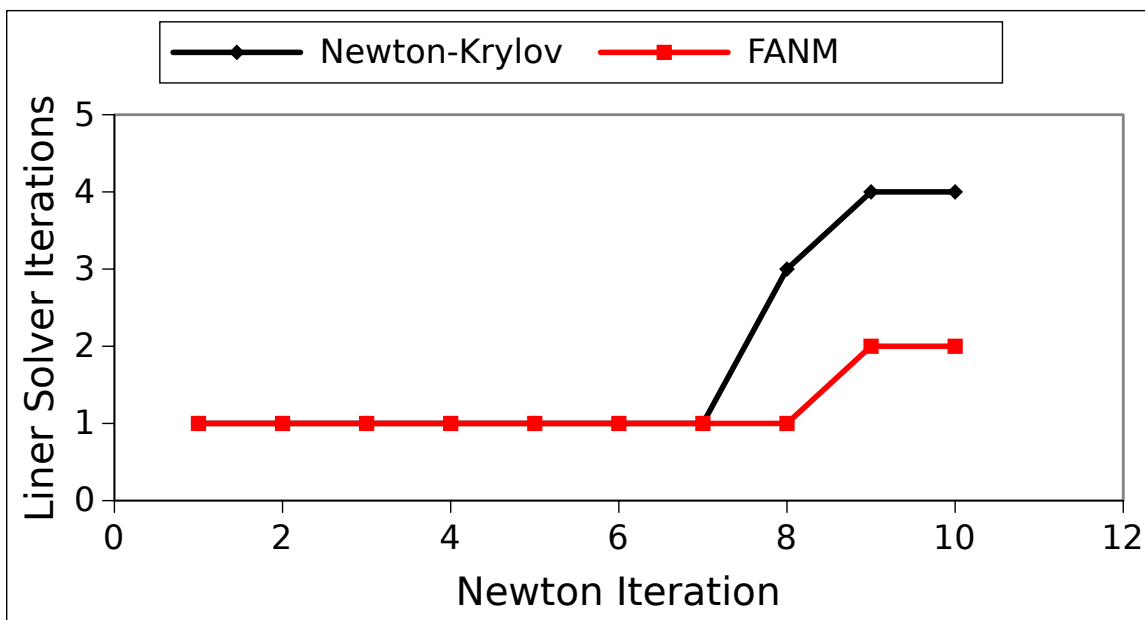
Figure 4.12: **Backward facing step linear solver iterations as a function of Newton iteration for the 400 Reynolds number case.** *More MCSA iterations were required to converge the linear models at later Newton iterations due to ill-conditioning of the Jacobian matrices.*
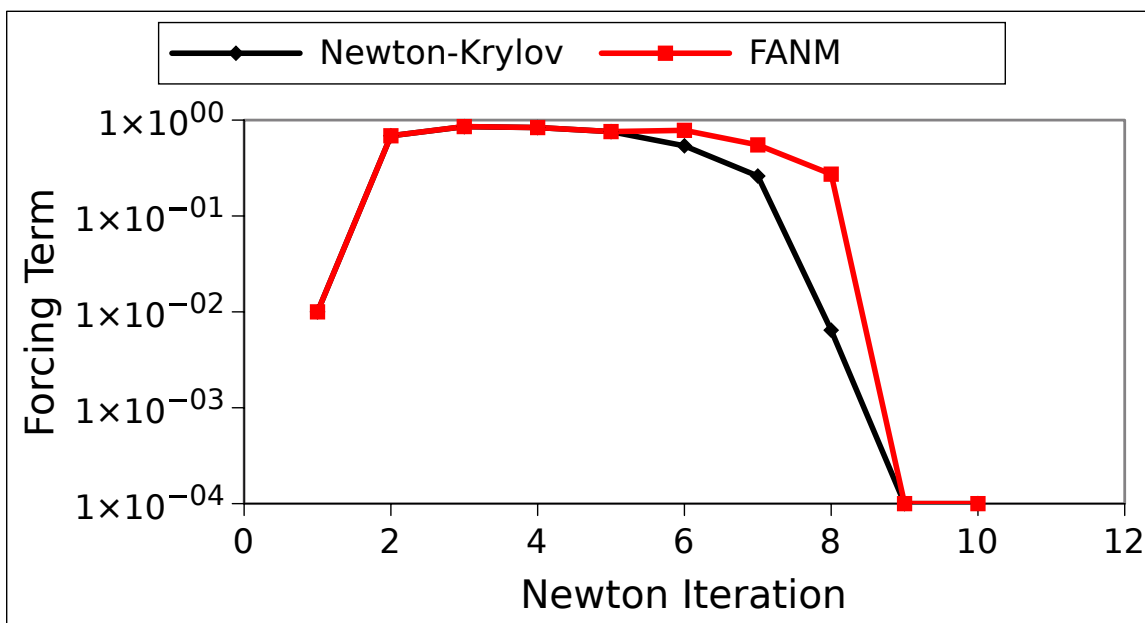
Figure 4.13: **Backward facing step forcing terms as a function of Newton iteration for the 400 Reynolds number case.** *FANM forcing terms were always larger.*

Figure 4.14: **Backward facing step linear solver iterations as a function of Newton iteration for the 500 Reynolds number case.** *More MCSA iterations were required to converge the linear models at later Newton iterations due to ill-conditioning of the Jacobian matrices.*
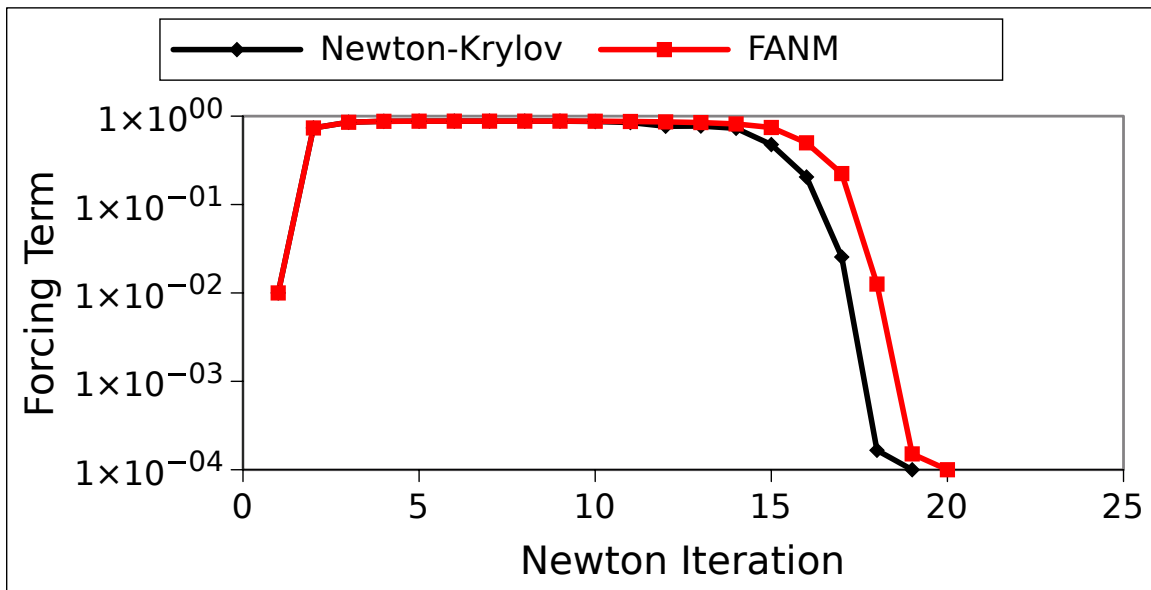
Figure 4.15: **Backward facing step forcing terms as a function of Newton iteration for the 500 Reynolds number case.** *More MCSA iterations were required to converge the linear models at later Newton iterations due to ill-conditioning of the Jacobian matrices.*

analysis in the previous chapter. In addition, we observed that the linear model required many more MCSA iterations to converge. These longer random walks and more iterations manifest themselves in the longer CPU time values and therefore the larger Newton Krylov speedup value of O(1,000) for the 500 Reynolds number case.

Reynolds Number	Newton-Krylov Speedup
200	400
300	593
400	825
500	1057

Table 4.30: **Backward facing step Newton-Krylov speedup over FANM method.** *Speedup values are rounded to the nearest integer. The results presented here were obtained from the benchmark verification calculations.*

4.5.4   Overall Performance Comparison

As a final overall comparison, we tabulate the results from the benchmark calculations over the three performance metrics: nonlinear iterations, linear iterations, and CPU time. Tables 4.31, 4.32, and 4.33 give the results. In these tables, the calculations that produced the best performing results are tallied. In the case of a tie, both are tallied. Looking at the tabulated results, we see marginally better performance for FANM in terms of nonlinear iterations with 1 extra case outperforming the Newton-Krylov method. As observed for each benchmark, the timing results were always in favor of the Newton-Krylov method due to the effects of the explicit preconditioning strategy.

For the total linear solver iterations given in Table 4.32, the difference is more dramatic with FANM converging the nonlinear residual in fewer linear solver iterations for twice as many cases as the Newton-Krylov method keeping in mind that for all cases both GMRES and MCSA were preconditioned with identical multigrid parameters using the same multigrid preconditioning library. This shows that when properly preconditioned, we can expect performance improvements in terms of total linear solver iterations required to converge the

nonlinear residual. With future optimization of MCSA implementations, this may also mean improved time to solution for FANM when compared to Newton-Krylov methods.

Benchmark	Newton-Krylov	FANM
Convection, Ra=1×10^3	$\times$	$\times$
Convection, Ra=1×10^4	$\times$	$\times$
Convection, Ra=1×10^5	$\times$	
Convection, Ra=1×10^6	$\times$	$\times$
Lid Driven, Re=100	$\times$	$\times$
Lid Driven, Re=300	$\times$	$\times$
Lid Driven, Re=500	$\times$	$\times$
Lid Driven, Re=700		$\times$
Backward Step, Re=200		$\times$
Backward Step, Re=300		$\times$
Backward Step, Re=400	$\times$	$\times$
Backward Step, Re=500	$\times$	

Table 4.31: **Navier-Stokes benchmark comparison for nonlinear iterations.** *Over all benchmarks, FANM performed better in terms of nonlinear iterations for 1 more case than the Newton-Krylov method.*

Benchmark	Newton-Krylov	FANM
Convection, Ra=1×10^3		$\times$
Convection, Ra=1×10^4		$\times$
Convection, Ra=1×10^5		$\times$
Convection, Ra=1×10^6		$\times$
Lid Driven, Re=100	$\times$	
Lid Driven, Re=300	$\times$	
Lid Driven, Re=500	$\times$	
Lid Driven, Re=700		$\times$
Backward Step, Re=200		$\times$
Backward Step, Re=300		$\times$
Backward Step, Re=400		$\times$
Backward Step, Re=500	$\times$	

Table 4.32: **Navier-Stokes benchmark comparison for total linear solver iterations.** *Over all benchmarks, FANM performed better in terms of linear solver iterations for twice as many cases as the Newton-Krylov method.*

Benchmark	Newton-Krylov	FANM
Convection, Ra=1×10^3	$\times$	
Convection, Ra=1×10^4	$\times$	
Convection, Ra=1×10^5	$\times$	
Convection, Ra=1×10^6	$\times$	
Lid Driven, Re=100	$\times$	
Lid Driven, Re=300	$\times$	
Lid Driven, Re=500	$\times$	
Lid Driven, Re=700	$\times$	
Backward Step, Re=200	$\times$	
Backward Step, Re=300	$\times$	
Backward Step, Re=400	$\times$	
Backward Step, Re=500	$\times$	

Table 4.33: **Navier-Stokes benchmark comparison for CPU time.** *For all benchmarks the explicit MCSA preconditioning strategy caused significantly larger CPU times for FANM when compared to the Newton-Krylov solutions.*

4.6 Summary

In this chapter we have developed and explored Monte Carlo Synthetic Acceleration methods in the context of solutions to the Navier-Stokes equations. The following are the significant observations and findings.

- Forward-Automated Newton-MCSA (FANM), a new inexact Newton method leveraging Monte Carlo Synthetic Acceleration, has been developed

- The FANM method has been incorporated into the Drekar multiphysics production code base developed at Sandia National Laboratories

- The FANM method has been verified to produce the same solutions as a production Newton-Krylov method for three difficult benchmark problems for the Navier-Stokes equations in different flow regimes and geometries

- The FANM method has better iterative performance than the Newton-Krylov method for convection dominated problems, converging in fewer linear solver iterations with the same preconditioning for high and low Rayleigh numbers

- The Newton-Krylov method has better iterative performance than the FANM method for flow dominated by inertial forces, converging in fewer linear solver iterations with the same preconditioning for high Reynolds numbers

- The spectral radius convergence restriction on MCSA was observed to be a significant hindrance by preventing solutions to forced flow problems at high Reynolds numbers

- Explicit algebraic preconditioning used to overcome the spectral radius restriction of MCSA creates FANM run times $O(100)$-$O(1,000)$ slower than the Newton-Krylov solver

- More Monte Carlo histories at every FANM iteration can reduce the number of linear and nonlinear iterations required to converge the problem

- With future optimization and improved preconditioning, reactor accident analyses that rely on convection dominated transport or steady state calculations requiring driven flow could experience improved time to solution with FANM given the improved iterative performance observed for problems of these types

Chapter 5

Parallel Monte Carlo Synthetic Acceleration Methods

In this chapter we briefly review particle transport methods for domain decomposed Monte Carlo. Considering a domain decomposed Neumann-Ulam method, we derive an analytic framework based on algebraic quantities from which to estimate aspects of its performance when applied to neutron transport systems. We then devise a parallel algorithm for the Neumann-Ulam method based on the multiple-set overlapping-domain decomposition algorithm and a parallel algorithm for the MCSA iteration that leverages the parallel Monte Carlo algorithm and general parallel matrix-vector operations. Using parallel solutions for the neutron diffusion problem, we verify the correctness of the parallel algorithm and implementation by comparing the numerical results against production Krylov methods. With the verified implementation of the algorithm, we perform parallel scaling studies to test its performance on a leadership class machine and compare this performance to the production Krylov methods.

5.1   Domain Decomposed Monte Carlo

Large-scale problems will for reasons typically related to memory restrictions or performance have their data partitioned such that each parallel process owns a subset of the equations in the linear system. Given this convention, the Neumann-Ulam Monte Carlo algorithm must perform random walks over a domain that is decomposed and must remain decomposed to avoid the same performance and memory restrictions that required the domain to be decomposed. To parallelize this algorithm, we then seek parallel Monte Carlo algorithms that

handle domain decomposition.

To motivate this problem, consider the square domain presented in Figure 5.1 and on this domain we imagine a Monte Carlo particle transport problem. If the domain were decomposed into 9 subdomains as shown, each of those subdomains and their associated data (i.e. cross sections) could be owned by a different parallel process in the computation. In Figure 5.1, the tracks of 3 particles that are born in the center subdomain are shown. In this example, particle A is first transported from the center domain to the domain directly to the left. Before the scattering event in the new domain may be processed, particle A must be communicated between between the two parallel processes that own those domains. For any given particle in the transport simulation, this communication event may hardly occur during the lifetime of the particle (particle B), or may occur many times (particle C) depending on the problem parameters and the random path in phase space taken by the particle. Scalable parallel algorithms for domain decomposed Monte Carlo are those that handle this domain-to-domain communication of particles effectively and balance it with the on-process computations for particle interactions, tallies, response calculations, and other simulation requirements.

For a domain decomposed Neumann-Ulam method, the situation is very much the same where instead the transport process is now discrete and the "physics" of the transport process is the Monte Carlo game with probabilities and weights described by Eq (2.13) for the given linear problem. Figure 5.2 gives the domain decomposed Neumann-Ulam analog of particle transport problem in Figure 5.1. Imagine in this problem that we are solving for the monoenergetic scalar neutron flux as in the model diffusion problem presented in Appendix C. In this problem, the solution has only a spatial dependence and therefore each point in the mesh corresponds to an equation in the resulting linear system. In Figure 5.2, the domain has now been discretized by this mesh and again decomposed into 9 subdomains, each owning a piece of the mesh and therefore the corresponding equations in the linear system. As we play the Monte Carlo game presented in Chapter 2, the discretization and resulting
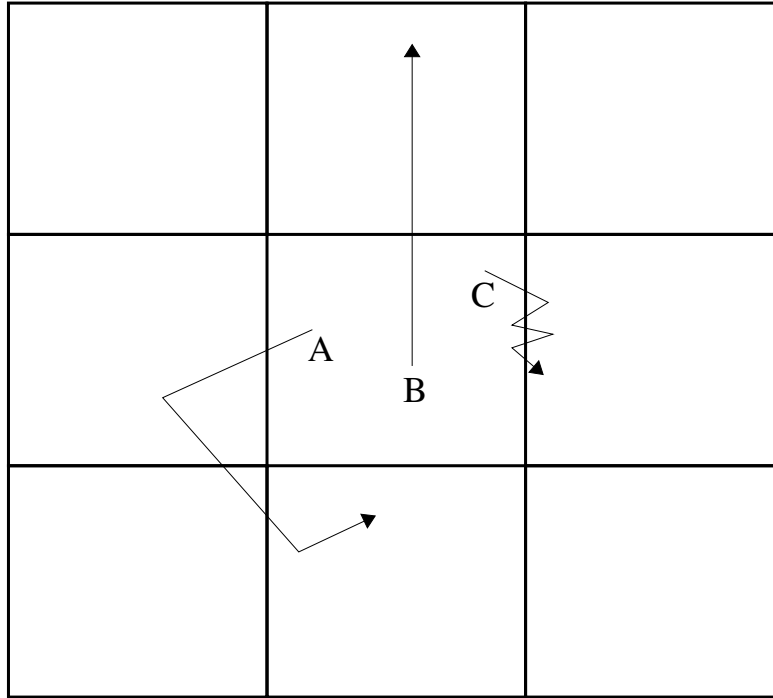
Figure 5.1: **Domain decomposed Monte Carlo transport example illustrating how domain decomposition requires parallel communication of particles.** *If a particle crosses a domain boundary it must be communicated to the next domain in its path.*

Neumann-Ulam decomposition of the problem describes how each state in the system is coupled to the other states in the system through the set of equations that form the linear system. This coupling is then responsible for the discrete random walk that each history takes as shown in this example. As discrete states (or rows in the linear system) that do not exist in the local domain are reached during the random walk by stochastic histories, the histories must be communicated to the subdomain that does own the discrete state in an analogous fashion to the particles in the previous example.

To further motivate using a parallel algorithm similar to particle transport methods, again consider history A in Figure 5.2. This history begins in the center subdomain and through the course of transitioning through states in the system arrives at a state that exists in the subdomain directly to the left of the center subdomain. History A must then be communicated from the center subdomain to the subdomain immediately to the left
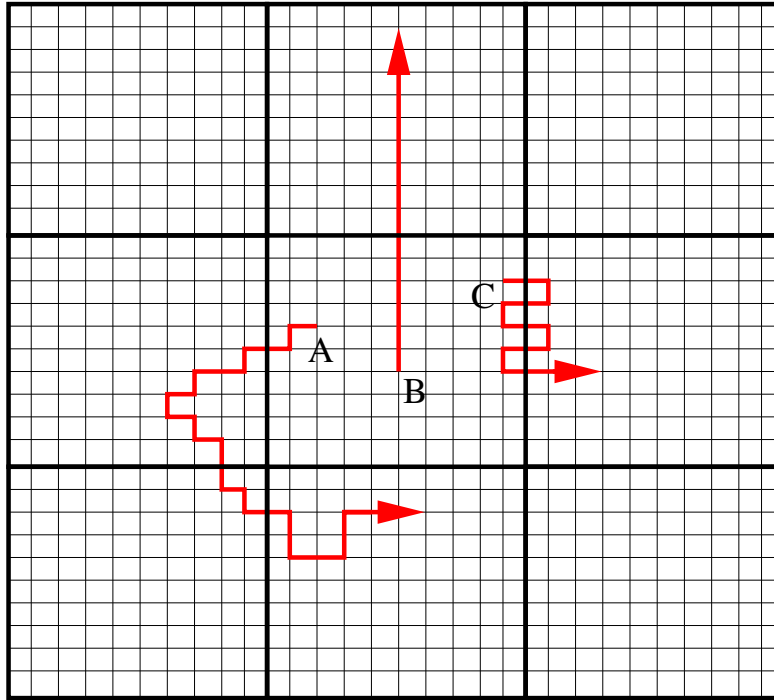
Figure 5.2: **Domain decomposed Neumann-Ulam example illustrating how domain decomposition requires parallel communication of histories.** *Each mesh point corresponds to an equation in the linear system and the coupling among equations is described by the discretization of the problem.*

to continue the random walk. As with the particle transport system, we may find that histories in a domain decomposed Neumann-Ulam method are only communicated a few times (history B) if at all, or they may be communicated many times (history C) depending on the discretization and the outcome of the Monte Carlo game. In identical fashion to the particle transport problem, a domain decomposed Neumann-Ulam method has the same communication requirements with all histories in both examples requiring the same parallel operations. The amount of communication of histories from domain to domain will be the primary factor in the parallel scalability of the algorithm. In the next section, the number of histories communicated in a given problem will be quantified analytically for a simple model problem.

5.2 Analytic Framework for Domain-Decomposed Monte Carlo

To date, parallel Neumann-Ulam methods have been limited to full domain replication with parallelism exploited through individual histories [5] and in this chapter we will exploit particle transport algorithms to alleviate this. To accomplish this, we recognize from the literature that stochastic histories must be transported from domain to domain as the simulation progresses and they transition to states that are not in the local domain. Because we have chosen a domain decomposition strategy in a parallel environment, this means that communication of these histories must occur between compute nodes owning neighboring pieces of the global domain. We wish to characterize this communication not only because communication is in general expensive, but also because these nearest-neighbor communication sequences, specifically, have poor algorithmic strong scaling [84] in much the same way as a parallel matrix-vector multiply operation. Therefore, we desire a framework to provide a simple, analytic theory based on the properties of the transport system that will allow for estimates of the domain decomposed behavior of the Neumann-Ulam method in terms of the amount of information that must be communicated.

When solving problems where the linear operator is symmetric, a host of analytic techniques exist based on the eigenvalue spectrum of the operator that characterize their behavior in the context of deterministic linear solvers. Using past work, these techniques are adapted to the domain decomposed Neumann-Ulam method using the one-speed, two-dimensional neutron diffusion equation and spatial discretization presented in Appendix C as a model transport problem. Using the linear system generated by the discretization of the model problem, we use a spectral analysis to generate analytic relations for the eigenvalues of the operator based on system parameters. Using the eigenvalue spectra, we then build relationships to characterize the transport of stochastic histories in a decomposed domain and the fraction of histories that leak from a domain and will therefore have to be communicated.

Finally, we compare these analytic results to numerical experiments conducted with the model transport problem.

5.2.1 Spectral Analysis

The convergence of the Neumann series in Eq (2.38) approximated by the Monte Carlo solver is dependent on the eigenvalues of the iteration matrix. We will compute these eigenvalues by assuming eigenfunctions of the form [63]:

$$\Phi_{p,q}(x,y) = e^{2\pi\iota px} e^{2\pi\iota qy} , \tag{5.1}$$

where different combinations of p and q represent the different eigenmodes of the solution. As these are valid forms of the solution, then the action of the linear operator on these eigenfunctions will yield the eigenvalues of the matrix as they exist on the unit circle in the complex plane.

For the model problem, we first compute the eigenvalues for the diffusion operator $\mathbf{D}$ by applying the operator to the eigenfunctions and noting that $x = ih$ and $y = jh$:

$$\mathbf{D}\Phi_{p,q}(x,y) = \lambda_{p,q}(\mathbf{D}) =$$
$$-\frac{D}{6h^2}\Big[4e^{-2\pi\iota ph} + 4e^{2\pi\iota ph} + 4e^{-2\pi\iota qh} + 4e^{2\pi\iota qh} + e^{-2\pi\iota ph}e^{-2\pi\iota qh}$$
$$+ e^{-2\pi\iota ph}e^{2\pi\iota qh} + e^{2\pi\iota ph}e^{-2\pi\iota qh} + e^{2\pi\iota ph}e^{2\pi\iota qh} - 20\Big] + \Sigma_a . \tag{5.2}$$

Using Euler's formula, we can collapse the exponentials to trigonometric functions:

$$\lambda_{p,q}(\mathbf{D}) = -\frac{D}{6h^2}[8\cos(\pi ph) + 8\cos(\pi qh) + 4\cos(\pi ph)\cos(\pi qh) - 20] + \Sigma_a . \tag{5.3}$$

As Eq (C.1) is diagonally dominant, point Jacobi preconditioning as outlined in § 2.6.2 is sufficient to reduce the spectral radius of the iteration matrix below unity and therefore

ensure convergence of the Neumann series. Applying this preconditioner, we are then solving the following diffusion system:

$$\mathbf{M}^{-1}\mathbf{D}\boldsymbol{\phi} = \mathbf{M}^{-1}\mathbf{s} \,. \tag{5.4}$$

The operator $\mathbf{M}^{-1}\mathbf{D}$ is merely the original diffusion operator with each row scaled by the diagonal component. As we have defined a homogeneous domain, the scaling factor, α, is the same for all rows in the operator and defined as the $\phi_{i,j}$ coefficient from Eq (C.5):

$$\alpha = \left[\frac{10D}{3h^2} + \Sigma_a \right]^{-1} \,. \tag{5.5}$$

Using this coefficient, we then have the following spectrum of preconditioned eigenvalues:

$$\lambda_{p,q}(\mathbf{M}^{-1}\mathbf{D}) = \alpha\lambda_{p,q}(\mathbf{D}) \,. \tag{5.6}$$

The spectral radius of the iteration matrix is obtained by seeking its largest eigenvalue. As with the diffusion operator, we can use the same analysis techniques to find the eigenvalues for the iteration matrix. We use a few simplifications by noting that if the Jacobi preconditioned iteration matrix is $\mathbf{H} = \mathbf{I} - \mathbf{M}^{-1}\mathbf{D}$, the we except all terms on the diagonal of the iteration matrix to be zero such that we have the following stencil:

$$\mathbf{H}\boldsymbol{\phi} = \frac{\alpha D}{6h^2}\Big[4\phi_{i-1,j} + 4\phi_{i+1,j} + 4\phi_{i,j-1} + 4\phi_{i,j+1} +$$
$$\phi_{i-1,j-1} + \phi_{i-1,j+1} + \phi_{i+1,j-1} + \phi_{i+1,j+1} \Big] \,. \tag{5.7}$$

Inserting the eigenfunctions defined by Eq (5.1) we get:

$$\lambda_{p,q}(\mathbf{H}) = \frac{\alpha D}{6h^2}\Big[4e^{-2\pi\imath ph} + 4e^{2\pi\imath ph} + 4e^{-2\pi\imath qh} + 4e^{2\pi\imath qh} + e^{-2\pi\imath ph}e^{-2\pi\imath qh}$$
$$+ e^{-2\pi\imath ph}e^{2\pi\imath qq} + e^{2\pi\imath ph}e^{-2\pi\imath qh} + e^{2\pi\imath ph}e^{2\pi\imath qh} \Big] \,, \tag{5.8}$$

which simplifies to:

$$\lambda_{p,q}(\mathbf{H}) = \frac{\alpha D}{6h^2}\left[8\cos(\pi ph) + 8\cos(\pi qh) + 4\cos(\pi ph)\cos(\pi qh)\right], \tag{5.9}$$

giving the eigenvalue spectrum for the Jacobi preconditioned iteration matrix. We find that the maximum eigenvalue exists when $p = q = 0$, giving the following for the spectral radius of the Jacobi preconditioned iteration matrix:

$$\rho(\mathbf{H}) = \frac{10\alpha D}{3h^2}. \tag{5.10}$$

5.2.2   Neumann Series Convergence

As outlined in §2.2, the adjoint Monte Carlo method is effectively an approximation to a stationary method. In the adjoint Neumann-Ulam method, k iterations, equivalent to k applications of the iteration matrix, are approximated by a random walk of average length k to yield the summation in Eq (2.39) [7, 17]. This random walk length, or the number of transitions before the termination of a history (either by the weight cutoff, absorption, or exiting the global domain) is therefore approximately the number of stationary iterations required to converge to the specified tolerance. In the case of the adjoint Neumann-Ulam method, no such tolerance exists, however, we have specified a weight cutoff, W_c, that determines when low-weight histories will be prematurely terminated as their contributions are deemed minute. After k iterations, a stationary method is terminated as the error has reached some fraction, ϵ, of the initial error:

$$||\mathbf{e}^k||_2 = \epsilon||\mathbf{e}^0||_2. \tag{5.11}$$

Per Eq (A.10), we see that this fraction is equivalent to $\epsilon = \rho(\mathbf{H})^k$. For the adjoint Neumann-Ulam method, if we take this fraction to be the weight cutoff, a measure of how accurately the contributions of a particular history to the solution are tallied, we then have the following

relationship for k:

$$k = \frac{\log(W_c)}{\log(\rho(\mathbf{H}))} \ .$$

(5.12)

This then gives us a means to estimate the length of the random walks that will be generated from a particular linear operator based on the eigenvalues of its iteration matrix (independent of the linear operator splitting chosen) and based on the weight cutoff parameter used in the Neumann-Ulam method.

5.2.3   Domain Leakage Approximations

In a domain decomposed situation, not all histories will remain within the domain they started in and must instead be communicated. This communication, expected to be expensive, was analyzed by Siegel and colleagues for idealized, load balanced situations for full nuclear reactor core Monte Carlo neutral particle simulations [34]. To quantify the number of particles that leak out of the local domain they define a leakage fraction, Λ, as:

$$\Lambda = \frac{average \ \# \ of \ particles \ leaving \ local \ domain}{total \ of \ \# \ of \ particles \ starting \ in \ local \ domain} \ .$$

(5.13)

For their studies, Siegel and colleagues assumed that the value of Λ was dependent on the total cross section of the system via the Wigner rational approximation. Outlined more thoroughly by Hwang's chapter in [10], we will use both the Wigner rational approximation and the mean chord approximation as a means to estimate the leakage fraction.

In the case of domain decomposed linear systems, we can use diffusion theory to estimate the optical thickness of a domain in the decomposition and the corresponding leakage fraction in terms of properties of the linear operator and the discretization. To begin we must first calculate the mean distance a Monte Carlo history will move in the grid by computing the mean squared distance of its movement along the chord of length l defined across the domain.

After a single transition a history will have moved a mean squared distance of:

$$\langle \overline{r_1^2} \rangle = (n_s h)^2 \,, \tag{5.14}$$

where h is the size of the discrete grid elements along the chord and n_s is the number of grid elements a history will move on average every transition. For our diffusion model problem, n_s would equate to the expected number of states in the i (or j as the problem is symmetric) direction that a history will move in a single transition and is dependent on the stencil used for the discretization. After k transitions in the random walk, the history will have moved a mean squared distance of:

$$\langle \overline{r_k^2} \rangle = k(n_s h)^2 \,. \tag{5.15}$$

If our chord is of length l and there are n_i grid elements (or states to which a history may transition) along that chord, then $h = l/n_i$ giving:

$$\langle \overline{r_k^2} \rangle = k\left(\frac{n_s l}{n_i}\right)^2 \,. \tag{5.16}$$

From diffusion theory, we expect the average number of interactions along the chord to be:

$$\tau = \frac{l}{2d\sqrt{\langle \overline{r_k^2} \rangle}} \,, \tag{5.17}$$

where d is the dimensionality of the problem and $\sqrt{\langle \overline{r_k^2} \rangle}$ is effectively the mean free path of the Monte Carlo history in the domain. We can readily interpret τ to be the *effective optical thickness* of a domain of length l. Inserting Eq (5.16) we arrive at:

$$\tau = \frac{n_i}{2 d n_s \sqrt{k}} \,, \tag{5.18}$$

which if expanded with Eq (5.12) gives us the final relation for the effective optical thickness:

$$\tau = \frac{n_i}{2dn_s}\sqrt{\frac{\log(\rho(\mathbf{H}))}{\log(W_c)}} \ .$$

(5.19)

For optically thin domains, we expect that most histories will be communicated, while optically thick domains will leak the fraction of histories that did not interact within. Using the optical thickness defined in Eq (5.19), we can then complete the leakage approximations by defining the bounds of $\tau \to 0, \Lambda \to 1$ and $\tau \to \infty, \Lambda \to \tau^{-1}$. With these bounds we can then define the leakage fraction out of a domain for the adjoint Neumann-Ulam method using the Wigner rational approximation:

$$\Lambda = \frac{1}{1+\tau} \ ,$$

(5.20)

and using the mean-chord approximation:

$$\Lambda = \frac{1 - e^{-\tau}}{\tau} \ .$$

(5.21)

Here, the leakage fraction is explicitly bound to the eigenvalues of the iteration matrix, the size of the domain, the content of the discretization stencil, and the weight cutoff selected to terminate low weight histories.

5.2.4 Numerical Experiments

To test the relationships developed by the spectral analysis, we form two simple numerical experiments using the diffusion model problem: one to measure the length of the random walks as a function of the iteration matrix eigenvalues, and one to measure the domain leakage fraction as a function of the iteration matrix eigenvalues and the discretization properties. Before doing this, we verify our computation of the spectral radius of the iteration matrix by numerically computing the largest eigenvalue of the diffusion operator using an iterative
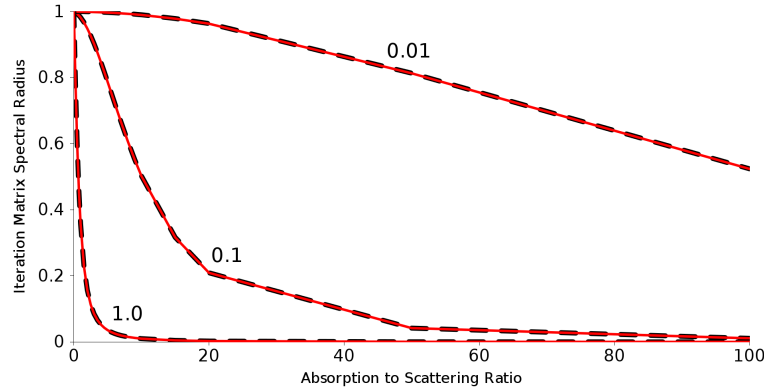
Figure 5.3: **Measured and analytic preconditioned diffusion operator spectral radius as a function of the absorption cross section to scattering cross section ratio.** *Values of $h = 0.01$, $h = 0.1$, and $h = 1.0$ were used. The red data was computed numerically by an eigensolver while the black dashed data was generated by Eq (5.10).*

eigenvalue solver. For this verification, a 100×100 square grid with $h = 0.01$, $h = 0.1$, and $h = 1.0$ and the absorption cross varied from 0 to 100 while the scattering cross section was fixed at unity. Figure 5.3 gives the measured spectral radius of the iteration matrix and the computed spectral radius for the preconditioned diffusion operator using Eq (5.10) as function of the absorption to scattering ratio (Σ_a / Σ_s). Excellent agreement was observed between the analytic and numerical results with all data points computed within the tolerance of the iterative eigenvalue solver.

5.2.4.1 Random Walk Length

With the eigenvalue derivations verified, we can go about setting up an experiment to measure the length of the random walks generated by the adjoint Neumann-Ulam solver. To do this, we again use a 100×100 square grid with $h = 0.1$ and the absorption cross varied from 0 to 100 while the scattering cross section was fixed at unity. Three weight cutoff values of 1×10^{-2}, 1×10^{-4}, and 1×10^{-8} were used with 10,000 histories generated by a point source of strength 1 in the center of the domain. For each of the histories, the number of transitions made was tallied to provide an effective value of k for each history. This value was then
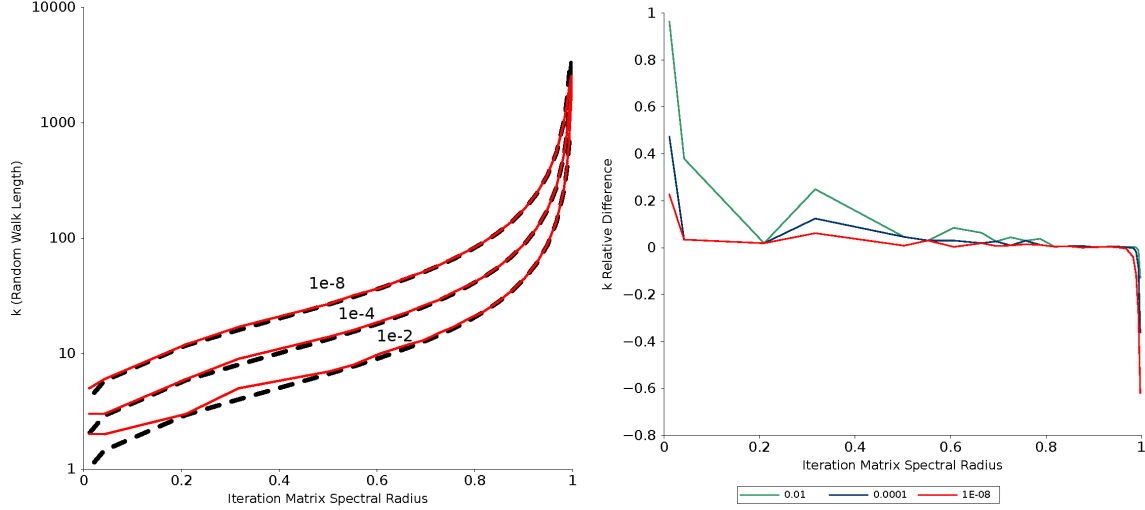
Figure 5.4: **Measured and analytic random walk length as a function of the iteration matrix spectral radius.** *The weight cutoff was varied with 1×10^{-2}, 1×10^{-4}, and 1×10^{-8}. In the left plot, the red data was computed numerically by an adjoint Neumann-Ulam implementation while the black dashed data was generated by Eq (5.12). In the right plot, the relative difference between the predicted and measured results is presented for each weight cutoff.*

averaged over all histories to get a measured value of k for the particular operator. On the left, Figure 5.4 presents these measurements as well as the analytic result computed by Eq (5.12) as a function of the iteration matrix spectral radius, $\rho(\mathbf{H})$. On the right, Figure 5.4 gives the relative difference between the predicted and observed results. We note good qualitative agreement between the measured and analytic results. However, we observe a larger relative difference for both long and short random walks.

5.2.4.2 Domain Leakage

Finally, we seek to measure the leakage from a domain in a domain decomposed Monte Carlo calculation and assess the quality of our analytic relation for the optical thickness of a domain and the associated leakage approximations. For this experiment, a square grid with $h = 0.1$ was decomposed into 9 square domains, 3 in each cardinal direction with measurements occurring in the central domain without boundary grid points. For the cross sections, the

absorption cross section was varied from 1 to 100 while the scattering cross section was set to zero to create a purely absorbing environment with weight cutoff of 1×10^{-4}. The optical thickness of these domains will vary as a function of the absorption cross section if the other parameters are fixed.

To compute the optical thickness, along with the spectral radius as given by Eq (5.10), we also need the parameters n_i and n_s which respectively describe the typical domain length and the average number of states moved along that typical length per history transition. For our grid above, the domains are varied in size with 50×50, 100×100, and 200×200 cells giving $n_i = 50$, $n_i = 100$, and $n_i = 200$ grid points or states along the typical length of the domain respectively. Looking at the Laplacian stencil in Eq (C.4), we see that all history transitions will only move a single state in either the i or j directions due to the symmetry of the problem. Furthermore, if we choose the i direction, not all states we will transition to will move the history in that direction. Therefore, we look to the definition of the iteration matrix in Eq (5.7) and the definition of the adjoint probability matrix in Eq (2.46) to estimate the n_s parameter. For a particular transition starting at state (i, j), 6 of the 8 possible new states in the stencil move the history in i direction with relative coefficients of 4 for moving in the $(\pm i, 0)$ direction and of 1 for moving in the $(\pm i, \pm j)$. These coefficients dictate the frequency those states are visited relative to the others. For those 6 states we can visit along the typical length, their sum is 12 out of the total 20 for the coefficients for all possible states with their ratio giving $n_s = \frac{3}{5}$.

To compute the leakage fraction numerically, 3×10^5 histories were sampled from a uniform source of strength unity over the global domain. At the start of a stage of histories, the number of histories starting in the center domain was computed and as the stage progressed, the number of histories that exited that domain was tallied with the ratio of the two numbers providing a numerical measure for the leakage fraction. Figure 5.5 gives the domain leakage measurements for the domain in the center of the global grid as well as the analytic result computed by Eqs (5.20) and (5.21) as a function of the iteration matrix spectral radius.
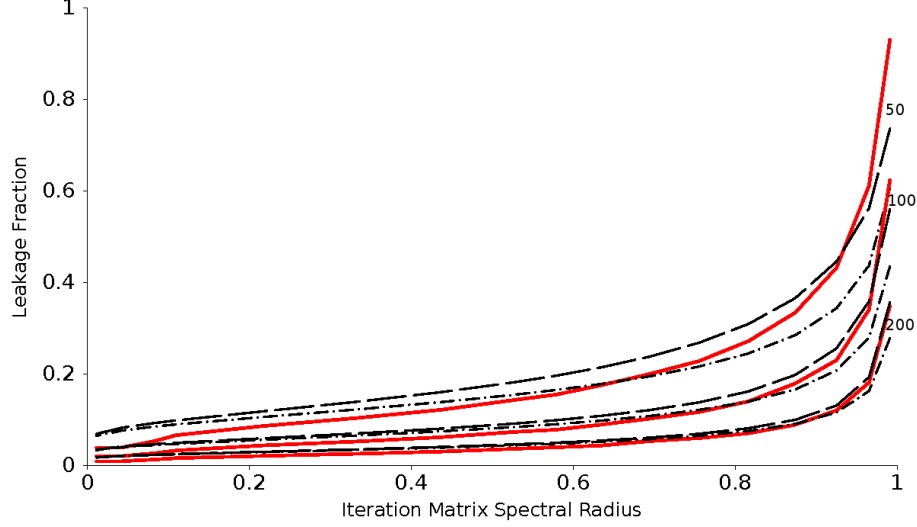
Figure 5.5: **Measured and analytic domain leakage as a function of the iteration matrix spectral radius.** *To test the behavior with respect to domain size, $n_i = 50$, $n_i = 100$, and $n_i = 200$ were used. The red data was computed numerically by a domain-decomposed adjoint Neumann-Ulam implementation, the black dashed data was generated by Eq (5.21) using the mean-chord approximation, and the dashed-dotted black data was generated by Eq (5.20) using the Wigner rational approximation.*

Again, we note good qualitative agreement between the measured and analytic quantities but we begin to see the limits of the leakage approximations.

To compare the quality of the two approximations, the absolute difference between the computed leakage fraction and that generated by the Wigner rational and mean chord approximations is plotted in Figure 5.6 for all domain sizes tested. From these difference results, the mean chord approximation is shown to have a lower difference for ill-conditioned systems as compared to the Wigner approximation while the Wigner approximation produces less difference for more well-conditioned systems. We also note that for the optically thick domains, the difference is likely corresponded to that observed in Figure 5.4 for the k parameter while the large relative difference in k for optically thin domains does not affect the approximation significantly. In general, the mean chord approximation is a better choice to estimate the leakage fraction in a domain from the adjoint Neumann-Ulam method and except for a single data point with $n_i = 50$, the mean chord approximation yielded leakage
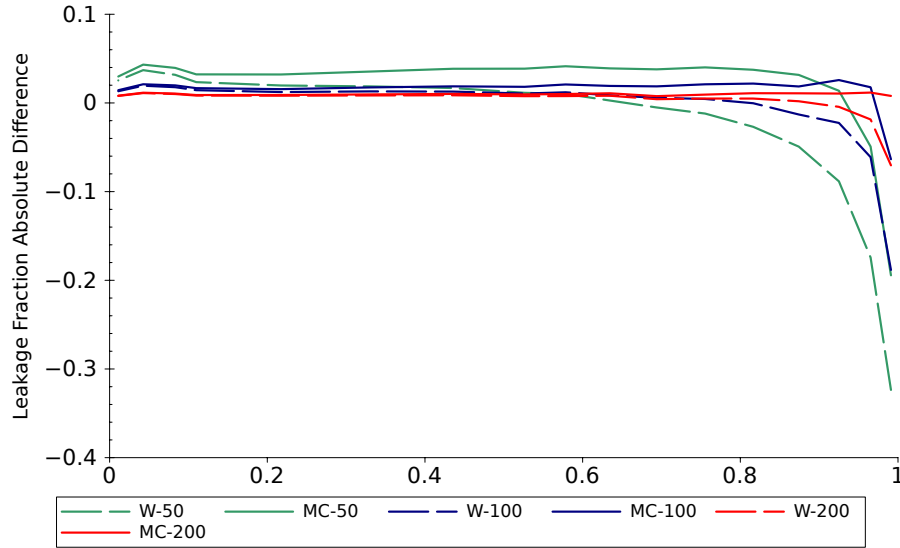
Figure 5.6: **Measured and analytic domain leakage absolute difference as a function of the iteration matrix spectral radius.** *To test the behavior with respect to domain size, $n_i = 50$ (green), $n_i = 100$ (blue), and $n_i = 200$ (red) were used. The dashed lines represent the difference using the Wigner rational approximation while the solid lines represent the difference using the mean-chord approximation.*

fractions within 0.05 of the measured results. As the domain becomes more optically thick (with both increasing n_i and decreasing $\rho(\mathbf{H})$), the approximations are more accurate.

5.3   Domain Decomposed Neumann-Ulam Algorithm

In the context of radiation transport, in 2009 Brunner and colleagues provided a fully asynchronous domain decomposed parallel algorithm as implemented in production implicit Monte Carlo codes [13]. We will adapt their algorithm and directly apply it to a parallel formulation of the Neumann-Ulam method. Direct analogs can be derived from their works by noting that the primary difference between solving a linear transport system with Monte Carlo methods and traditional fixed source Monte Carlo transport problems is the content of the Markov chains that are generated.

The transitions represented by these chains are bound by probabilities and weights and are initiated by the sampling of a discrete source. In the context of transport problems, those

transitions represent events such as particle scattering and absorption with probabilities that are determined by physical data in the form of cross sections. For stochastic matrix inversion, those transitions represent moving between the equations of the linear system (and therefore the components of phase space which they represent) and their probabilities are defined by the coefficients of those equations. Ultimately, we tally the contributions to generate expectation values in the desired states as we progress through the chains. Therefore, parallel methods for Monte Carlo radiation transport can be abstracted and we can use those concepts that apply to matrix inversion methods as an initial means of developing a parallel Neumann-Ulam-type solver.

In this section Brunner and Brantley's fully asynchronous algorithm, which was effectively implemented verbatim for this work, is presented along with its application to the Neumann-Ulam method. For considerably more detail, the algorithm presented can be found in [13]. In their work they identify two data sets that are required to be communicated: the sharing of particles that are transported from one domain to another and therefore from one processor to another and a global communication that signals if particle transport has been completed on all processors. Both of these communication sequences will be addressed at a high level along with how the Monte Carlo data structures they require are constructed in parallel.

5.3.1 Parallel Transport Domain and Source

To utilize a parallel transport algorithm, we must generate the required data with the correct parallel decomposition. For the Neumann-Ulam method, the transport domain consists of all states in the system that are local, and the probabilities and weights for all state transitions possible in the local domain. At the core of this representation is the Neumann-Ulam decomposition of the linear operator as given by Eq 2.13. Given an input decomposition for the linear operator, by definition the Neumann-Ulam decomposition will have the same parallel decomposition. In addition, any modification made to the linear operator through preconditioning or relaxation parameters will also modify the Neumann-Ulam decomposition.

All possible transitions are described by the local graph of the sparse input matrix. In addition, any left preconditioning or relaxation parameters will modify the right hand side of the linear system and therefore the fixed source in the Monte Carlo calculation. This source vector will have the same parallel decomposition as the input matrix and therefore all of the birth states for the histories will exist for at least a single transition event within the local domain.

Compared to the serial construction of the Neumann-Ulam decomposition, data for all states that is required to be on process must be collected in parallel. For the pure domain decomposition case, given an input parallel decomposition for the Neumann-Ulam decomposition, for all local states m we require access to P_{mn} and W_{mn} (or P_{mn}^T and W_{mn}^T) for the adjoint method for all possible states n. Given by Figure 5.7, consider the adjacency graph of a single state in the neutron diffusion matrix for the model problem presented in Appendix C.

In this example, we currently reside in state m of the system, directly correlating to physical location (i, j) in the mesh (the center node). The discretization stencil of the diffusion problem dictates the structure of this graph and the states to which a history may transition. If we play the Monte Carlo game to move to a new state n, then we may move to any of the nodes in this graph, including the node at which we started. If grid point (i, j) in this example is on the right of the local domain boundary and we transition to the right to state n corresponding to mesh point $(i + 1, j)$, we are now in a state that is owned by the adjacent domain. We must then gather the data in the Neumann-Ulam decomposition from the neighboring process that owns grid point $(i + 1, j)$. Doing this provides us with the data required by the estimators permitting P_{mn} and W_{mn} to be computed locally for this particular boundary transition. In addition, we also collect the identification number for the process that owns this state such that we have an address to send all histories that leave the local domain boundary for this state. For the parallel source, these adjacent states are not required as histories may only be born in states in the local domain. Once the local Neumann-Ulam
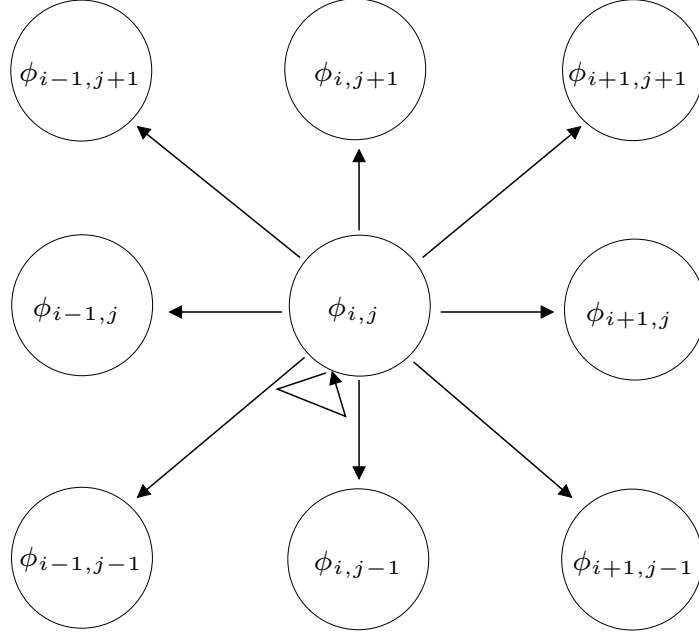
Figure 5.7: **Neutron diffusion equation state adjacency graph.** *The structure of the graph comes from the discretization of the Laplacian operator describing the diffusion physics. Adjacent boundary states are collected by traversing the graph one step for all local boundary states and collecting the equations for those states that are not local. For a given transition in the random walk for the diffusion problem, a history at mesh point (i, j) may transition to all adjacent mesh points including itself, corresponding to a global state transition from m to n in the linear system.*

decomposition has been generated with the proper data collected from adjacent domains, Monte Carlo transport may proceed in parallel.

5.3.2 Domain Decomposed Algorithm

Here we present in detail Brunner and Brantley's 2009 algorithm in detail and discuss how it is adapted to parallelize the Neumann Ulam method. Presented in Algorithm 5.1, the top level sequence performs the task of managing history transport through the local domain, communication of histories to adjacent domains, and the completion of transport. For each of these specific tasks, additional algorithms, shown in bold in Algorithm 5.1 (e.g. **LocalHistoryTransport()**), are presented for additional detail in the same manner as Brunner and Brantley.

Algorithm 5.1 Parallel Neumann-Ulam Algorithm

1: get list of neighbor processors   ▷ Each neighbor owns an adjacent subdomain
2: **for all** neighbors **do**
3:      post nonblocking receive for maximum history buffer size
4:      allocate history buffer
5: **end for**
6: *historiesCompleted* = 0   ▷ local+child finished histories
7: *localProcessed* = 0   ▷ local trajectories computed (not necessarily finished)
8: calculate parent and children processor ID numbers in binary tree
9: **for all** child processes **do**
10:      post nonblocking receive for *historiesCompleted* tally
11: **end for**
12: post nonblocking receive for stop message from parent
13: **while** stop flag not set **do**
14:      **if** any local histories in source or stack **then**
15:          **LocalHistoryTransport()**
16:          *++localProcessed*
17:      **end if**
18:      **if** message check period == *localProcessed* || no local histories **then**
19:          **ProcessMessages()**
20:          *localProcessed* = 0
21:      **end if**
22:      **if** no local histories **then**
23:          **ControlTermination()**
24:      **end if**
25: **end while**
26: cancel outstanding nonblocking requests
27: free all history buffers

Successful execution of this algorithm requires construction of the parallel Neumann-Ulam decomposition as described in the preceding section. This data is used to begin Algorithm 5.1 where lines 1-5 use the collected list of neighboring processors generated while building the Neumann-Ulam decomposition to setup the set of asynchronous messages required for domain-to-domain communication. Again, consider this communication pattern for the 9 subdomain example given by Figure 5.8. In this pattern, each boundary domain has two neighbors and the center domain four neighbors with which they will communicate parallel histories and this communication goes both ways as represented by the adjacent arrows in the figure. For each set of neighbors, a non-blocking send and receive is required with data
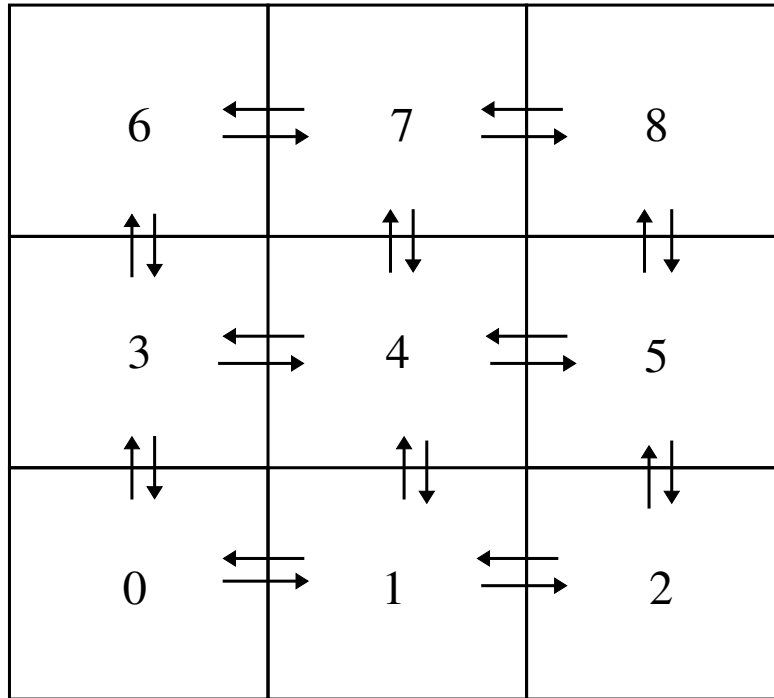
Figure 5.8: **Nearest neighbor history communication sequence.** *Each subdomain in the system has a set of nearest neighbors determined by the parallel adjacency graph of the input matrix. The subdomains are indexed by an integer.*

buffers allocated with a user-defined size prepared for incoming and outgoing histories. This nonblocking structure is critical to the performance of the algorithm in that it permits local history transport to continue while new histories to transport are being collected in the buffers. When a given process is ready to do more work, it can check these data buffers for incoming histories requiring further transport. In this way there is a maximum amount of overlap between communication and transport of histories.

Once the nearest-neighbor communication sequence has been prepared, the completion of transport sequence is readied in lines 6 and 8-12 in Algorithm 5.1. In these lines we are setting up an asynchronous binary communication tree as presented for the same 9 subdomain example in Figure 5.3.2. In this communication pattern, each process has one parent process (except for the MASTER process 0) to which it will nonblocking send the number of histories that terminated their transport procedure by weight cutoff in the local domain. Equivalently,

each process has up to two child processes from which it will receive their completed number of histories with a nonblocking receive operation. Setting up a tree in this manner lets the completed history tally (*historiesCompleted* in the algorithm) be updated incrementally and funneled to the root process. Because we are solving fixed source problems with the Neumann-Ulam algorithm without any type of variance reduction that may generate more histories that we started with, once the root process completion sum tallies to the number of histories in the source, transport is complete. Once this occurs, the root process nonblocking sends a process to its children and each process nonblocking receives a stop message from its parent as shown in Figure 5.3.2. The stop message is then propagated up the tree in the same manner.

With these communication structures prepared, we can now enter the main transport loop at line 13 of Algorithm 5.1. In this loop, a set of mutually exclusive tasks enabled by the fully asynchronous communication patterns are executed until the stop signal is received from the parent process in the binary tree. In this case, mutually exclusivity permits all local operations to occur independently of other processes in the system and their current state. For each process, there are two data structures from which histories may be obtained for the transport procedure. The first is the local source and the second is a LIFO (last in first out) stack of histories transported to the local domain from the adjacent domain. In lines 14-17, if histories exist in either of these data structures, then they are transported through the local domain using Algorithm 5.2. If the history is terminated by weight cutoff the *historiesCompleted* tally is updated. If it hits the boundary of the domain it is added to the outgoing history buffer for the neighboring domain and if the buffer is full, it is sent to the neighboring domain with a nonblocking operation and the memory associated with that buffer reallocated. In all instances that Algorithm 5.2 is executed, *localProcessed* is incremented to account for histories that have been processed locally.

Continuing in the transport loop, if there are no local histories to transport or the *localProcessed* count has reached some user-defined check frequency, lines 18-21 in Algorithm 5.2
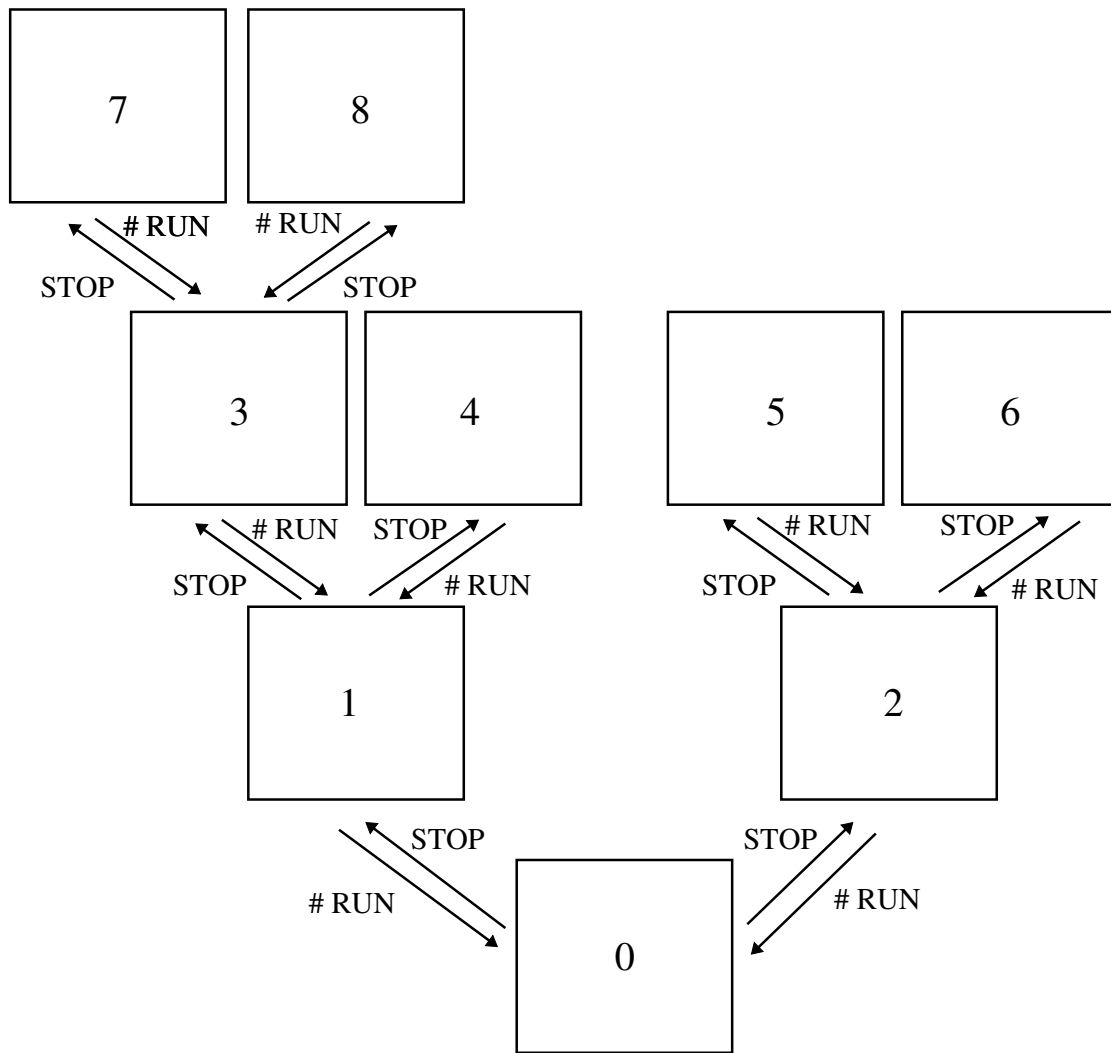
Figure 5.9: **Binary communication tree for coordinating the end of a parallel Neumann-Ulam solve.** *Each child process reports to its parents how many histories completed within its domain. When the root process sums all complete histories, it forwards the stop signal to its children which in turn forward the message up the tree. The subdomains are indexed by an integer.*

check for more histories to transport in the incoming data buffers by calling Algorithm 5.3. For each neighboring domain in the problem, if there are histories in those data buffers then they are added to the stack from processing and the nonblocking receive operation re-instantiated. In addition, the terminated histories count is updated with those values received from the child processes.

Finally, the transport loop finishes in lines 22-24 of Algorithm 5.2 by calling Algorithm 5.4

Algorithm 5.2 LocalHistoryTransport()

1: transport history through the domain until termination
2: **if** history is in neighbor boundary state **then**
3:     add history to neighbor buffer
4:     **if** neighbor buffer is full **then**
5:         nonblocking send history buffer to neighbor
6:         allocate new history buffer for neighbor
7:     **end if**
8: **else**
9:     **if** history terminated by weight cutoff **then**
10:         post-process history
11:         $++historiesCompleted$
12:     **end if**
13: **end if**

Algorithm 5.3 ProcessMessages()

1: **for all** received history buffers from neighbor **do**
2:     unpack number of histories in buffer
3:     add the histories to the running stack
4:     repost nonblocking receive with neighbor
5: **end for**
6: **for all** *historiesCompleted* messages from children **do**
7:     *historiesCompleted* += message value
8:     repost nonblocking receive with child
9: **end for**

---

if there are no local histories to transport in the stack or the source. In Algorithm 5.4, we continue to forward the terminated history tally down to the parent in the binary tree and send all history buffers to our neighbors, even if they are not full. If Algorithm 5.4 is called by the MASTER process, it checks for completion of the problem and if it is complete, forwards to stop flag onto its children as in Figure 5.3.2. If the process is not the MASTER, then we check for a stop signal from the parent and forward to the child processes if transport is complete.

In this manner the transport loop continues until all process have received the stop signal from their parents. Older versions of this algorithm, particularly some of those presented in [14], use a master/slave approach as given by Figure 5.3.2 for the completion of a transport stage instead of the binary tree scheme. In this approach, the root process still manages

---

Algorithm 5.4 ControlTermination()

 1: nonblocking send an partially full history buffers
 2: **for all** *historiesCompleted* messages from children **do**
 3:     *historiesCompleted* += message *historiesCompleted*
 4:     repost nonblocking receive with child
 5: **end for**
 6: **if** MASTER processor **then**
 7:     **if** *historiesCompleted* == global # of source histories **then**
 8:         set stop flag
 9:         **for all** children **do**
10:             nonblocking send stop message to child
11:         **end for**
12:     **end if**
13: **else**
14:     nonblocking send *historiesCompleted* to parent
15:     *historiesCompleted* = 0
16:     check for stop signal from parent
17:     **if** stop signal from parent **then**
18:         **for all** children **do**
19:             nonblocking send stop message to child
20:         **end for**
21:     **end if**
22: **end if**

---

the final summation of the completion tally, it directly receives completed tally results from all other processes in the problem instead of from just its children. Although this implementation is potentially simpler to understand than the binary tree approach, the authors of [14] observed that this type of termination pattern, even when implemented in a fully asynchronous manner, was a major scalability bottleneck. This bottleneck is due to the fact that the master process falls behind the others, creating a load imbalance even with the addition of a few integer addition operations. We will explicitly demonstrate in scaling studies how this bottleneck also occurs within a Neumann-Ulam implementation of this algorithm thus requiring the implementation of a binary communication tree.

There is an additional advantage to Brunner and Brantley's work that although not immediately applicable to this work has the potential to provide value in the future. In addition to a robust fully asynchronous communication pattern, this algorithm may also
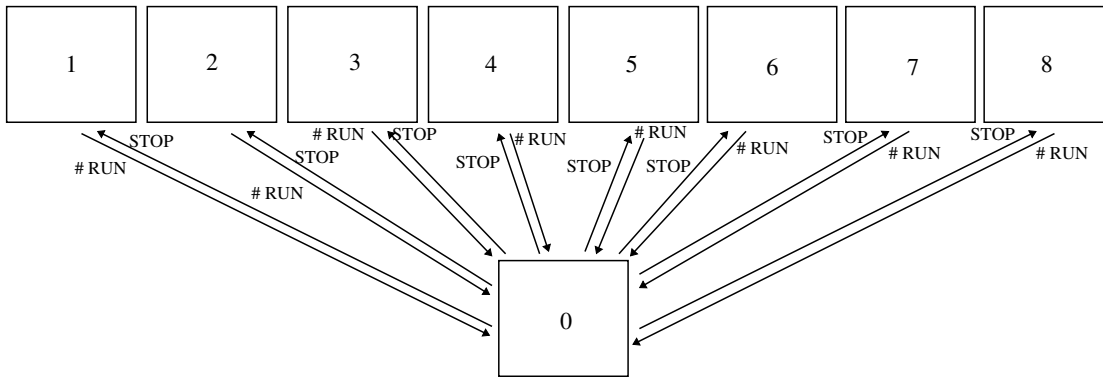
Figure 5.10: **Master/slave scheme for coordinating the end of a parallel Neumann-Ulam solve.** *Each slave process reports to the master how many histories completed within its domain. When the master process sums all complete histories, it sends the stop signal to all slave processes. The subdomains are indexed by an integer.*

be modified to account for situations where the total number of histories in a given stage are not known before starting transport. From a physics perspective, we might expect this for situations where perhaps an (n,2n) interaction occurs in a neutronics problem. In this case, the algorithm is modified to account for both histories terminated and created and several mechanisms are introduced to determine completion of the transport stage. For future variations of this work, certain variance reduction techniques which create histories, such as splitting, have the potential to be successfully employed as a means of accelerating the time to solution for a given problem using MCSA. The parallel Neumann-Ulam algorithm presented here may be adapted to account for these additional techniques.

5.4 Multiple-Set Overlapping-Domain Algorithm

Although the implementation presented in the previous section was observed by Brunner and Brantley to be robust and allowed for scaling to large numbers of processors, performance issues were still noted with parallel efficiency improvements needed in both the weak and strong scaling cases for unbalanced problems. These results led them to conclude that a combination of domain decomposition and domain replication could be used to solve some of

these issues. In 2010, Wagner and colleagues developed the *multiple-set overlapping-domain* (MSOD) decomposition for parallel Monte Carlo applications for full-core light water reactor analysis [37]. In their work, an extension of Brunner's, their scheme employed similar parallel algorithms for particle transport but a certain amount of overlap between adjacent domains was used to decrease the number of particles leaving the local domain. In addition, Wagner utilized a level of replication of the domain such that the domain was only decomposed on $O(100)$ processors and if replicated $O(1,000)$ times potentially achieves efficient simulation on $O(100,000)$ processors, thus providing both spatial and particle parallelism.

Each collection of processors that constitutes a representation of the entire domain is referred to as a set, and within a set overlap occurs among its sub-domains. The original motivation was to decompose the domain in a way that it remained in a physical cabinet in a large distributed machine, thus reducing latency costs during communication. A multiple set scheme is also motivated by the fact that communication during particle transport only occurs within a set, limiting communications during the transport procedure to a group of $O(100)$ processors, a number that was shown to have excellent parallel efficiencies in Brunner's work and therefore will scale well in this algorithm. The overlapping domains within each set also demonstrated reduced communication costs. On each processor, the source is sampled in the local domain that would exist if no overlap was used while tallies can be made over the entire overlapping domain.

To demonstrate this, consider the example adapted from Mervin's work with Wagner and others in the same area [53] and presented in Figure 5.11. In this example, 3 particle histories are presented emanating from the blue region of interest. Starting with particle A, if no domain overlap is used then the only the blue domain exists on the starting processor. Particle A is then transported through 3 other domains before the history ends, therefore requiring three communications to occur in Brunner's algorithm. If a 0.5 domain overlap is permitted as shown by the dashed line, then the starting process owns enough of the domain such that no communications must occur in order to complete the particle A transport process.
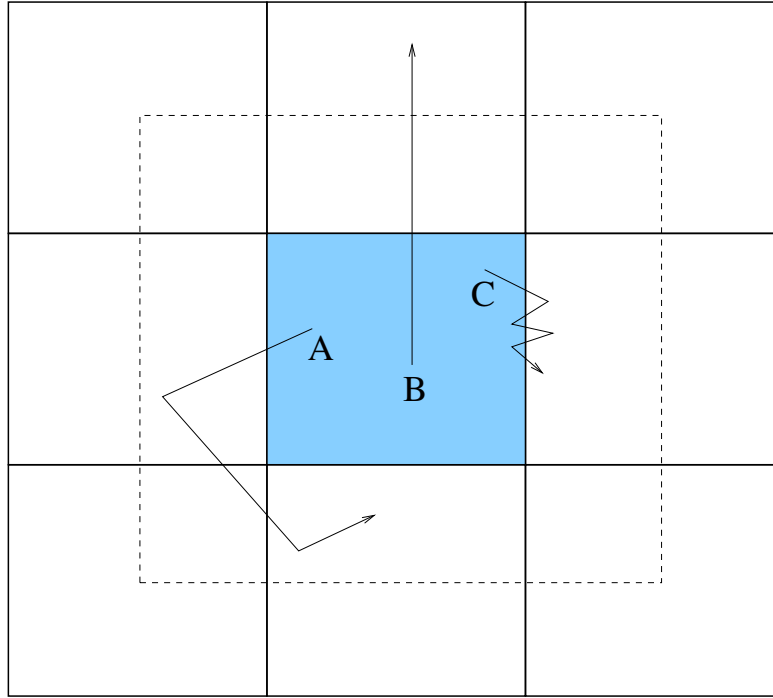
Figure 5.11: **Overlapping domain example illustrating how domain overlap can reduce communication costs.** *All particles start in the blue region of interest. The dashed line represents 0.5 domain overlap between domains.*

Using 0.5 domain overlap also easily eliminates cases such as that represented by the path of particle C. In this case, particle C is scattering between two adjacent domains, incurring a large latency cost for a single particle. Finally, with particle B we observe that 0.5 domain overlap will still not eliminate all communications. However, if 1 domain overlap were used, the entire geometry shown in Figure 5.11 would be contained on the source processor and therefore transport of all 3 particles without communication would occur.

Wagner and colleagues used this methodology for a 2-dimensional calculation of a pressurized water reactor core and varied the domain overlap from 0 to 3 domain overlap (a 7×7 box in the context of our example) where a domain contained an entire fuel assembly. For the fully domain decomposed case, they observed that 76.12% of all source particles leave the domain. At 1.5 domain overlap, the percentage of source particles born in the center assembly leaving the processor domain dropped to 1.05% and even further for 0.02% for the 3 domain

overlap. Based on their results, we hypothesize that the overlap approach coupled with the multiple sets paradigm that will enhance the scalability of the pure domain-decomposition algorithm for Neumann-Ulam presented in the previous section.

5.4.1 Generating the MSOD Decomposition

In § 5.3.1 we discussed how we generated the parallel transport domain from the Neumann-Ulam decomposition of a domain decomposed linear operator. We can readily adapt those data structures to account for the extra information required by an implementation of the MSOD algorithm. First, we consider the generation of overlap. Conveniently, this is identical to the neighboring states discovery problem discussed in conjunction with Figure 5.7. To generate the boundary for the local transport domain, we needed to gather all data from the immediately adjacent states in the system that did not already exist in the local domain. We solved this problem by traversing the graph of the matrix for each of the boundary states and determining which processes owned those adjacent states.

To generate overlap, we use the identical algorithm but in this case we perform as many graph level traversals as the specified amount of overlap. For example, consider the analytic relations derived in § 5.2 for the length of random walks in a Neumann-Ulam method and the amount of leakage from a domain considering a neutron diffusion problem. From these relations we might determine that, for our particular problem, if we can grow the domain by 10 additional discrete state transitions, we can reduce the number of histories that must be communicated by a significant fraction. We determine the information we must gather from neighboring domains to build the overlap by traversing the graph of the matrix outward from the boundary 10 levels. At each step, we find the data in the adjacent domain that we require and make that data local, incrementing the size of the overlap. Once the overlap has been gathered, one extra graph traversal on the boundary states is performed to get the new neighboring states and their owning processes.

Once overlap has been generated, the transport domain for a single set is complete.
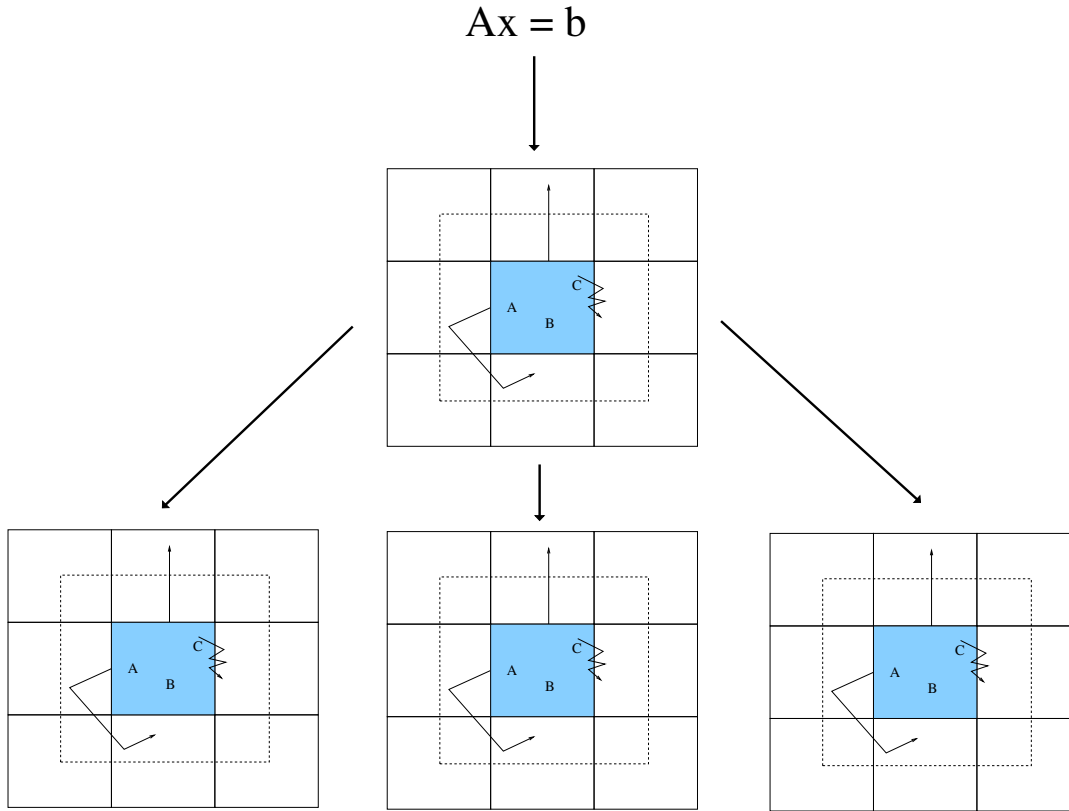
Figure 5.12: **MSOD construction for 4 sets with overlap.** *The linear system is used to construct the Monte Carlo transport domain on the primary set. The Monte Carlo data structures are then broadcast among the blocks to all sets in the system.*

However, if multiple sets are to be used, an additional set of parallel procedures is required to generate the necessary data structures. Figure 5.12 gives a schematic representation of the MSOD construction process using 4 sets. For a problem where P parallel processors are available and S sets are to be used, each set is allocated P/S processors for computation. On the first P/S processors, the linear problem is generated. From the linear problem, the linear operator is used to construct the transport domain, the solution vector used to construct the tallies, and the forcing term vector used to construct the fixed source. Once these Monte Carlo data structures have been generated, they are broadcast to the remaining sets in the problem as shown in Figure 5.12 such that we have S replications of the Monte Carlo problem for a single instance of the original linear problem.

5.4.2 MSOD Neumann Ulam Algorithm

With the ability to generate the transport domain within an MSOD decomposition as well as the source and tally structures, we can now define how to perform a Neumann-Ulam solve using MSOD. Given by Algorithm 5.5, we begin by constructing the Monte Carlo data structures for each set including the transport domain, the source, and the tallies. Next, in line 4 we perform the asynchronous transport algorithm presented in § 5.3 for each of the individual sets. Adding overlap to Algorithm 5.1 in this case simply modifies the set of local states and the set of neighboring states to additional states gathered during overlap generation.

Algorithm 5.5 MSOD Transport Sequence
___
 1: build MSOD domain
 2: build Monte Carlo source
 3: build Monte Carlo tally
 4: perform parallel Neumann-Ulam transport in each set
 5: combine set tallies
 6: combine block tallies
___

Once Monte Carlo transport is complete complete, the tallies for each individual computation must be gathered to the original set in order to build the correction vector within an MCSA sequence. To do this, we perform two parallel vector operations. First, overlap not only creates additional states in the local transport domain but also additional states in the local tally vector such that any events that occur in the local domain may be tallied in a local vector. Because of this, the tally vector in a single set will share local states with other domains and a parallel sum reduction operation is required to transform the tally into the original Neumann-Ulam parallel decomposition. Second, the tallies in individual sets must be combined and applied to the primary set in the problem that shares the processor space with the original linear problem. For this operation, we employ the concept of blocks as a subdivision of parallel space complementary to the concept of sets.

Consider the schematic representation of the final parallel reduction presented in Fig-

ure 5.13. For this operation, the tally vectors in each set must be summed together and applied to the primary set. As each set is an exact replica of the others, the parallel decomposition of the tally vector is the same within all sets. We can take advantage of this by building a processor space that encapsulates each identical domain in each set. We can then use this processor space for the reduction. For the schematic in Figure 5.13, the upper-left domain in each set creates a single block, giving 9 total blocks for this example problem. The processor space that encapsulates each of the upper-left domains is then used for the parallel reduction operation. This reduction will happen in a mutually exclusive manner for each of the blocks in the system. One benefit of this approach is that this reduction occurs only over a subset of the processors in the problem, providing better scalability than a reduction operation over all processors in the problem.
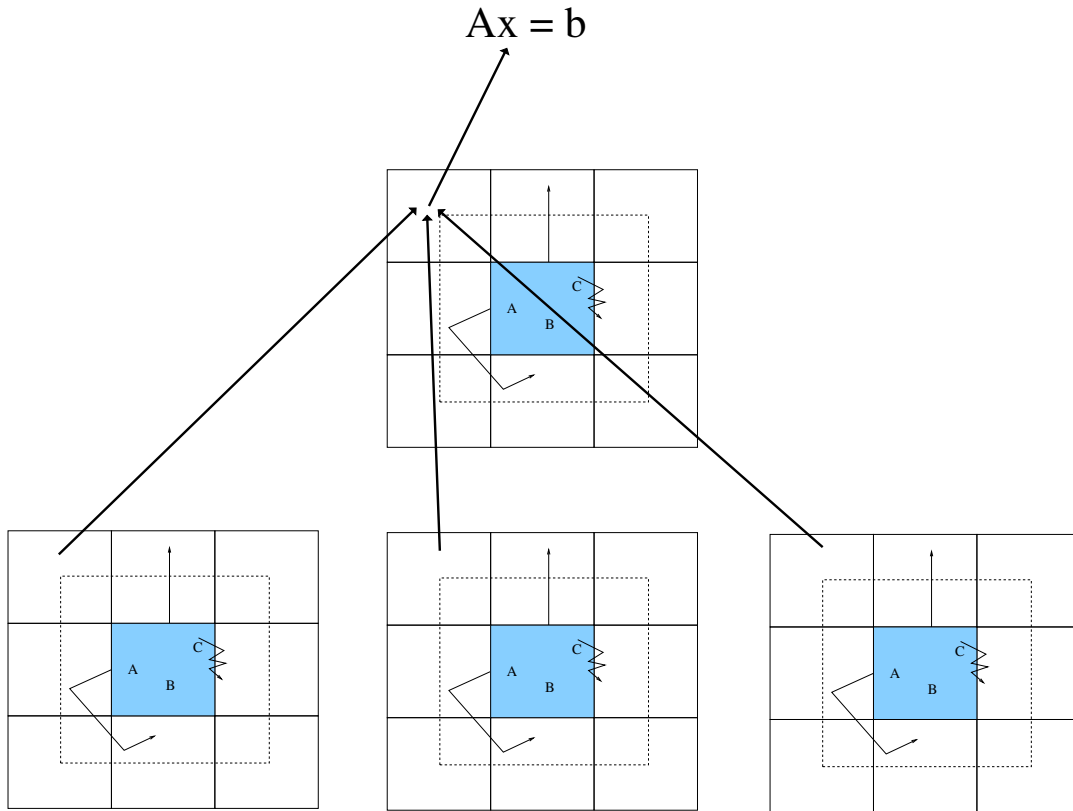
Figure 5.13: **MSOD tally reduction over blocks.** *The tally computed independently in each set is reduced across the blocks to the primary set. The linear system vector is updated on the primary set. In this example the tally vector in the block containing upper-left subdomains is combined. Identical reduction operations occur for all other blocks simultaneously.*

5.5   Parallel MCSA

With the parallel adjoint Neumann-Ulam solver implementation described above, the parallel implementation of an MCSA iteration is trivial. Recall the MCSA iteration procedure presented again here for clarity:

$$\mathbf{x}^{k+1/2} = \mathbf{x}^k + \mathbf{r}^k \,, \tag{5.22a}$$

$$\mathbf{r}^{k+1/2} = \mathbf{b} - \mathbf{A}\mathbf{x}^{k+1/2} \,, \tag{5.22b}$$

$$\mathbf{A}\delta\mathbf{x}^{k+1/2} = \mathbf{r}^{k+1/2} \,, \tag{5.22c}$$

$$\mathbf{x}^{k+1} = \mathbf{x}^{k+1/2} + \delta\mathbf{x}^{k+1/2} \,, \tag{5.22d}$$

$$\mathbf{r}^{k+1} = \mathbf{b} - \mathbf{A}\mathbf{x}^{k+1} \,. \tag{5.22e}$$

In §A.3 we discuss parallel matrix and vector operations as utilized in conventional projection methods. We utilize these here for the parallel MCSA implementation for the computations required in Eqs (5.22a), (5.22b), (5.22d), and (5.22e). In the first step, a parallel matrix-vector multiply is used to apply the split operator to the previous iterate's solution. A parallel vector update is then performed with the source vector to arrive at the initial iteration guess. In the next step, the residual is computed by the same operations where now the operator is applied to the solution guess with a parallel matrix-vector multiply and then a parallel vector update with the source vector is performed. Once the correction is computed with a parallel adjoint Neumann-Ulam solve, this correction is applied to the guess with a parallel vector update to get the new iteration solution. Additionally, as given by Eq (2.68), 2 parallel vector reductions will be required to check the stopping criteria: one initially to compute the infinity norm of the source vector, and another at every iteration to compute the infinity norm of the residual vector.

To parallelize the solution of Eq (5.22c), we apply the MSOD Neumann-Ulam algorithm presented in the previous section. The problem is potentially replicated with overlap and the

Monte Carlo procedure returns a correction vector, $\delta\mathbf{x}$, with the same parallel decomposition as the input linear problem. As was the case for generating the replications required for a multiple set implementation, the explicit matrix and vector operations required for the rest of an MCSA iteration occur only on the subset of processors containing the primary set. Only the Monte Carlo data structures exist on the rest of the processors in the problem as replication of the other operations does not generate any more information that could be used to accelerate the time to solution.

5.5.1   Parallel FANM Implementation

Here we briefly comment on how a FANM method may be implemented in parallel. A parallel FANM method relies on a basic set of parallel matrix-vector operations outlined in § A.3 as well as the global residual and Jacobian assembly procedure described in § 4.1.4. Consider the FANM iteration scheme in Algorithm 4.1. We must first assemble the linear system in parallel through the element-wise function evaluations to generate both the global Jacobian operator and the global residual vector on the right hand side. Per Bartlett's work on automatic differentiation, efficient and automated parallel mechanisms are available to do this through a sequence of scatter/gather operations. With these tools available for residual and Jacobian generation, the remainder of the parallel procedure is simple. The linear Newton correction system is solved using the parallel MCSA method as described in the previous section and the Newton correction applied to the previous iterate's solution through a parallel vector update.

5.6   Parallel MCSA Verification

Before we consider the parallel performance of the MCSA algorithm, we must first verify that the algorithm generates the correct solution in parallel with respect to reference solutions provided by production Krylov methods. To verify correctness, we use solutions to the

neutron diffusion system presented in Appendix C. As the reference computation, serial results will be used from the conjugate gradient solver in Belos, a linear solvers package in the Trilinos scientific computing libraries [77]. In identical fashion to the verification for the SP_N equations performed in § 3.6, we will solve the neutron diffusion problem in parallel using multiple cores on a desktop machine. For each parallel solution, then the solution at each grid point in the system will be compared to the solution at the same grid point in the serial reference case with the minimum and maximum absolute differences of these values reported.

GMRES and conjugate gradient solvers from the Belos package were used on 4 cores as a means of both assuring the Krylov solvers produce the same results on multiple cores and as a means of providing an acceptable range of minimum and maximum values in the comparison. For MCSA, a range of MSOD parameters will be used such that problems with multiple sets and multiple blocks may be tested along with overlap. For all MCSA calculations, a single history was used for every DOF in the problem to compute the correction vector. For all solvers, the flux was converged to a tolerance of 1×10^{-8} and therefore if the comparisons agree within this tolerance the solutions will be deemed correct. Table 5.1 gives the parameters for the verification problem and Table 5.3 gives the results of the calculations. Solver parameters used for MCSA are given in Table 5.2.

Parameter	Value
dx	0.1
dy	0.1
N_x	400
N_y	400
N	160,000
Σ_a	5.0
Σ_s	1.0
Boundary Type	Vacuum
Linear Solver Tolerance	1×10^{-8}

Table 5.1: **Parallel MCSA verification model problem parameters.** *The neutron diffusion equation in 2 dimensions is used for the model problem.*

Parameter	Value
Histories	1 per DOF
Weight Cutoff	1×10^{-2}
Fixed Point Iteration	Richardson
Estimator	Adjoint Collision

Table 5.2: **Parallel MCSA verification solver parameters.** *No relaxation parameters or variance reduction techniques were used with MCSA.*

From the data we see that for all solvers, the parallel results agree with the reference serial results within the solution tolerance for all DOF in the system. In addition, we do not notice any systematic differences in the results as a function of number of blocks, number of sets, or amount of overlap. In addition, the parallel GMRES results have maximum absolute differences of the same magnitude as all MCSA results and a larger minimum absolute difference than all MCSA results by three orders of magnitude. Based on these results, MCSA parallelized with the MSOD algorithm, and in particular the implementation used here, generates the correct results with respect to the serial conjugate gradient reference computation.

Solver	Blocks	Sets	Cores	Overlap	Min Difference	Max Difference
Conjugate Gradient	-	-	4	-	0.0	1.11022×10^{-16}
GMRES	-	-	4	-	5.64215×10^{-13}	3.83348×10^{-9}
MCSA	2	1	2	0	8.60423×10^{-16}	7.6806×10^{-9}
MCSA	3	1	3	0	6.41154×10^{-15}	7.65397×10^{-9}
MCSA	4	1	4	0	2.66454×10^{-15}	7.62623×10^{-9}
MCSA	2	2	4	0	1.52656×10^{-15}	7.57108×10^{-9}
MCSA	1	4	4	0	5.55112×10^{-16}	7.61631×10^{-9}
MCSA	8	1	8	0	6.13398×10^{-15}	7.51744×10^{-9}
MCSA	4	2	8	0	1.03251×10^{-14}	7.62601×10^{-9}
MCSA	2	4	8	0	5.13478×10^{-15}	7.60777×10^{-9}
MCSA	1	8	8	0	1.80411×10^{-15}	7.60651×10^{-9}
MCSA	2	1	2	5	2.47025×10^{-15}	7.58882×10^{-9}
MCSA	3	1	3	5	2.44249×10^{-15}	7.6326×10^{-9}
MCSA	4	1	4	5	7.49401×10^{-16}	7.49014×10^{-9}
MCSA	2	2	4	5	1.19349×10^{-15}	7.61814×10^{-9}
MCSA	1	4	4	5	5.55112×10^{-16}	7.61631×10^{-9}
MCSA	8	1	8	5	2.05391×10^{-15}	7.63955×10^{-9}
MCSA	4	2	8	5	9.57567×10^{-15}	7.61313×10^{-9}
MCSA	2	4	8	5	5.7454×10^{-15}	7.60767×10^{-9}
MCSA	1	8	8	5	1.80411×10^{-15}	7.60651×10^{-9}
MCSA	2	1	2	10	1.08247×10^{-15}	7.63231×10^{-9}
MCSA	3	1	3	10	3.27516×10^{-15}	7.60211×10^{-9}
MCSA	4	1	4	10	4.996×10^{-16}	7.64756×10^{-9}
MCSA	2	2	4	10	4.13558×10^{-15}	7.60259×10^{-9}
MCSA	1	4	4	10	5.55112×10^{-16}	7.61631×10^{-9}
MCSA	8	1	8	10	9.71445×10^{-16}	7.58535×10^{-9}
MCSA	4	2	8	10	7.77156×10^{-16}	7.65978×10^{-9}
MCSA	2	4	8	10	4.16334×10^{-16}	7.63191×10^{-9}
MCSA	1	8	8	10	1.80411×10^{-15}	7.60651×10^{-9}

Table 5.3: **Parallel MCSA verification results.** *Difference values given are absolute values. The neutron diffusion equation in 2 dimensions is used for the model problem with the parameters given in Table 5.1. A serial conjugate gradient calculation is used as the reference computation and neutron fluxes are compared element-wise. Parameters used for the MCSA solver are given in Table 5.2. All solvers including the reference computation were converged to tolerance of 1×10^{-8}.*

5.7 Parallel Performance Metrics

How effectively the presented algorithms parallelize MCSA will be determined by several performance measures. For this work, these measures will come directly from Keyes' primer on the scalability of domain decomposed methods and specifically his discussion on how to measure their parallel performance [72]. All of these metrics are derived from two measured quantities: the number of iterations required for convergence and the total wall time required for convergence. Each of these quantities are then measured in varying parameter studies by changing the number of processes in a simulation and by varying the local or global problem size. Using the notation of Keyes, we will define *parallel efficiency* as $\eta(N, P)$ where the efficiency is a function of the global problem size, N, and the number of processes in the calculation, P. There are several types of efficiencies that will be useful in our analysis of scalability with different definitions depending on the type of parametric scaling study performed. For all efficiencies, a value of 100% is considered perfect while a value of 0% signals the worst possible performance. Often, as was observed in this work, it is the case that efficiencies above 100% are computed in certain scaling studies. For the data presented in the following sections, an explanation of each observed case of super-unitary efficiencies will be provided.

Of primary interest to the nuclear engineer is the *strong scaling* performance of an algorithm [34]. In this type of scaling study, the global problem size is fixed and the local problem size changes with the number of processes in the calculation. In this case, as P increases, N is fixed, thus reducing the local problem size and performance by having a larger ratio of communication to computational work. This type of scaling is important because typically the global problem size is fixed due to the problem of interest. Consider the desire for a high fidelity neutronics simulation of the entire core of a nuclear reactor. In this case, the global problem is known from the geometry definition including the number of fuel assemblies and the geometry of those assemblies all the way down to the resolution of

the space, angle, and energy discretizations required in order to capture physical phenomena of interest. Because the global problem size is known a priori, strong scaling is an important measure of how useful a solution technique is when larger and larger values of P are used to solve the problem. Ideally, the time to solution for the the problem will decrease linearly as a function of P, permitting a faster time to solution using the maximum available resources and thus making sure all P are positively affecting the runtime of the problem.

For strong scaling, the objective is to then decrease the runtime of a fixed size global problem as a linear function of P. Based on this, we can define the strong scaling *absolute efficiency* as:

$$\eta_{strong}(N, P) = \frac{1}{P} \frac{T(N, 1)}{T(N, P)} , \tag{5.23}$$

where $T(N, P)$ is the wall time for a computation of global size N using P processes. Note here that this particular definition is measured with respect to a serial computation. On leadership class machines, it is often the case that a problem size large enough to effectively execute on $O(10,000)$ cores or larger is significantly larger than any problem that may be solved by a single core due to memory restrictions. Therefore, we consider absolute scaling for a base case where Q processes are used instead of a serial computation:

$$\eta_{strong}(N, P|Q) = \frac{Q}{P} \frac{T(N, Q)}{T(N, P)} . \tag{5.24}$$

The absolute efficiency measure presented here only considers the total time to solution. Often, that total time to solution may be changing for an iterative method due to the fact that the number of iterations required to converge may be changing as a function of P. This will often happen in cases where modifying N changes the spectral character of the problem, often making it stiffer and therefore more difficult to solve when N increases. Therefore we also consider *algorithmic efficiency* from Keyes' work which considers this potential change in iteration count:

$$\eta_{alg}(N, P|Q) = \frac{I(N, Q)}{I(N, P)} , \tag{5.25}$$

where $I(N, P)$ is the number of iterations required to converge a problem of global size N computed using P processes. We can then adjust the absolute efficiency using this new algorithmic efficiency in order to compute the parallel scalability of a single iteration such that algorithmic effects may be neglected. We define the *implementation efficiency* as:

$$\eta_{impl}(N, P|Q) = \frac{\eta}{\eta_{alg}} , \qquad (5.26)$$

using the absolute efficiency in the numerator, giving an effective measure of scalability of a single iteration of the algorithm.

In addition to strong scaling, in certain cases it is useful to consider the *weak scaling* of an iterative method. In this case, the ratio N/P is fixed such that the local problem size remains the same for all values of P. In this case, the objective is to maintain a constant wall time while both N and P grow as a fixed ratio. In this case, we define the absolute efficiency as:

$$\eta_{weak}(M|N, P|Q) = \frac{T(M, Q)}{T(N, P)} , \qquad (5.27)$$

subject to the constraint $M/Q = N/P$. The scaling is perfect if the runtime is static for all P when N/P is fixed.

Often, weak scaling is of interest to the nuclear engineer due to the fact that the computational resources available are fixed and may not be able to contain the entire global problem of interest. In this case, an algorithm with good weak scaling performance permits all of the computational resources available to be used effectively to allow for the highest fidelity problem possible to be solved. In addition, for the resources available, the memory to processor ratio on a distributed machine is often fixed, giving an exercise in fixed N/P to solve the highest fidelity problem possible. Therefore, good weak scaling should not be viewed as an enhancement of time to solution for the engineer but rather permitting a higher fidelity problem to be solved within a given time constraint. For problems where increasing fidelity increases the stiffness of the system, there is often a trade-off between the absolute

efficiencies computed for a given method and the degrading algorithmic efficiencies that arise when increasing the fidelity. Both time and hardware constraints should be considered when preparing a parallel calculation.

5.8   Leadership-Class Parallel Scaling Studies

Using the parallel performance metrics presented in the previous section, we will next measure performance in various scaling studies using an implementation of the parallel MCSA algorithm to assess its quality using the neutron diffusion problem presented in Appendix C. For these scaling studies, large problems at high levels of concurrency will be solved at a leadership-class computing facility. In this section, we will outline the parallel machine on which the calculations were performed and then present a series of numerical studies that identify both strengths and weaknesses of the parallel algorithm. Both pure domain decomposition and MSOD parallel performance will be explored and compared to performance results for the same problems using a set of production parallel Krylov solvers.

For the scaling results presented here, all parallel MCSA results were computed using the Monte Carlo Linear Solvers[1] (MCLS) library generated specifically for this work while the conjugate gradient and GMRES Krylov solvers used are part of the Belos linear solver package within the Trilinos framework [77]. In general, the Belos package produces solutions to the neutron diffusion problem nearly two orders of magnitude faster than the MCLS library for serial computations using the conjugate gradient solver. Therefore, when we directly compare these two codes, the MCLS parallel efficiencies will appear artificially inflated relative to the Belos efficiencies due to the fact that the MCLS ratio of work to communication will be much larger than that for the Belos calculations. For every scaling study presented, the calculations were performed 3 times with the average values reported for wall time and those average values used for the efficiency computations. In addition, it should be noted that in

---

[1]MCLS is an open source C++ library built on the Trilinos framework and can be downloaded at `https://github.com/sslattery/MCLS`

practice, symmetric positive-definite problems like the neutron diffusion problem solved here would never be solved using GMRES. Instead, a method such as conjugate gradient would typically be used due to the enhanced performance. We use GMRES here simply as a means of providing an additional comparison for MCSA performance.

5.8.1 Titan

All parallel scaling studies presented in this work were performed on the Titan Cray XK7 machine at the Oak Ridge Leadership Computing Facility located at Oak Ridge National Laboratory. Titan is a heterogeneous architecture machine combining both CPU and GPU components to achieve a theoretical peak performance of more than 20 petaflops. The technical specifications for Titan for only the CPU portion of the machine are given in Table 5.4.

Processor	16 core AMD
Nodes	18,688 AMD Opterons
Cores/Node	16
Total Cores	299,008
Memory/Node	32 GB
Memory/Core	2 GB
Interconnect	Gemini

Table 5.4: **Titan Cray XK7 hardware specifications.** *Specifications presented for Titan in this table were gathered from the Oak Ridge Leadership Computing Facility at* `http://www.olcf.ornl.gov/computing-resources/titan-cray-xk7/`

For the scaling studies presented in this work, only the CPU components of Titan specified in Table 5.4 were utilized. This is due to the fact that the implementations of the parallel MCSA algorithm in the MCLS library utilized code written only with the Message Passing Interface (MPI) and therefore could not take advantage of the GPU accelerators. Even considering just the CPU portion of Titan, nearly 300,000 CPUs are available to test the parallel performance of the MCSA algorithm at high levels of concurrency.

For each parallel performance metric presented in the previous section, a reference case is required to compute efficiencies for all other cases. For smaller machines, often a serial computation can be performed and used as the base case to get a true measure of speed-up for a particular problem. For our scaling studies, we will always use as a reference case a calculation which uses 16 cores, filling an entire node of the machine. We fill an entire node so that we may ignore the effects on scalability measures that arise from using only a subset of cores in a node. Typically this results in a large drop in efficiency from a serial computation to a calculation that fills the entire node. Once a node is filled, adding subsequent nodes has less of an effect on the scaling, providing a more stable region of analysis.

5.8.2   Communication Parameters

In our description of Brunner and Brantley's algorithm as applied to the Neumann-Ulam method, we noted two free parameters that are user-defined at runtime. The first is the static data buffer size for communicating histories between neighboring domains and the second is the frequency by which a domain checks for incoming information from neighboring domain, both of which may potentially affect latency and load balancing. Changing the static history buffer size parameter affects the scalability of the algorithm in two ways. If the buffer size is increased, the buffer takes longer to fill and is therefore sent less frequently, potentially causing load balancing bottlenecks where a neighboring domain is idle and waiting for more work to do but is waiting for another domain to complete work. In addition, if the buffer size is too large, the network may become saturated with these very large data packets, slowing down performance. If the buffer size is too small, too many history messages are sent, not providing enough data for a neighboring process to work on to make up for the time spent communicating. Considering the second parameter, when the message check frequency period is increased, more histories are processed locally before looking to do work elsewhere. If this value becomes too large, incoming data buffers may not be cleared frequently enough and cause decreased performance in the domain-to-domain communications. If this value is too

small, too much time is spent looking for work instead of actually performing it.

To assess how these parameters affect the performance of the parallel Monte Carlo algorithm on the Titan machine, a parameter study was performed using the neutron diffusion problem on 64 cores (4 nodes). This problem had a reasonably well conditioned spectral radius of 0.78 with a global problem size of 1.6×10^7 DOFs with one stochastic history used per DOF in the MCSA Neumann-Ulam used to compute the correction for the acceleration. Each parameter was varied between 16 and 4096 and the time to solve the problem recorded. The results of this study are presented in Figure 5.14. Compared to the results of Brunner and Brantley for the same type of study, we note qualitatively similar results with the general observation that a larger history buffer check period is better than a shorter one. The larger the check period, the more on-process work is done before checking messages. Second, there was not a significant variation observed in the history buffer size parameter for a given check frequency.

Compared to the reference work, there was also not a significant change in the runtime over the values of parameters tested with all runtimes reported within 6.5% of the fastest case observed. For this work, a history buffer size of 4096 and a buffer check period of 128 performed best for the initial calculations. However, most values in the range tested will give good performance. Brunner and Brantley found that a value of 1024 was best for both parameters. For the results observed here, these parameters were only 0.7% slower than the fastest case. It may be best practice to fix these parameters internally at 1024 as both this work and the reference found these to perform well several years apart on both different parallel machines and for different transport sequences. Therefore, for the scaling studies presented in the following sections, values of 1024 for both the history buffer size and message check frequency will be used.
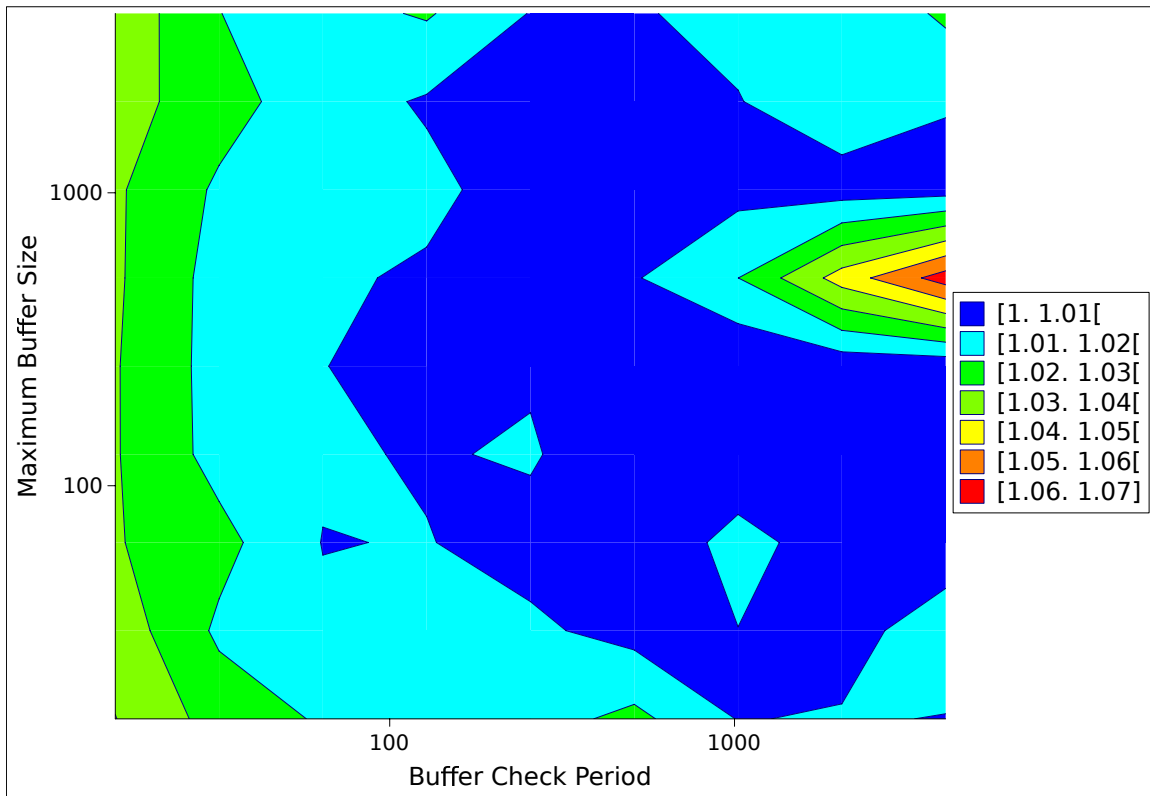
Figure 5.14: **Neumann Ulam parallel algorithm history buffer check period vs. history buffer size sensitivity.** *The color scale represents the ratio of the runtime of a particular parameter variation with the runtime from the faster parameter variation. A value of 1.02 on the color scale corresponds to a runtime 2% longer than the faster time. All runtimes were within 6.5% of the fastest observed case.*

5.8.3   Pure Domain Decomposition Scaling

For the first set of scaling studies, we consider the parallel MCSA algorithm where MSOD has not been used in the parallel Neumann-Ulam algorithm. We refer to this case as pure domain decomposition where no overlap or replication has been leveraged. Such a test will isolate specifically the performance of Brunner and Brantley's algorithm as applied to the Neumann-Ulam algorithm. For the strong scaling study, the global diffusion problem size was fixed at 1.6×10^7 DOFs for all solvers and the 16 core run used as the base case. MCSA was used again with one stochastic history used per DOF in the Neumann-Ulam solve to compute the correction for the acceleration with the remainder of the problems and solver parameters the same as those for the verification calculation given in Table 5.1 and Table 5.2. As with all of the scaling studies, 3 calculations for all data points were performed with the average wall time reported and used for the efficiency calculations. Figure 5.15 gives the wall time per iteration for these calculations while Figure 5.16 gives the results of the this study with the given absolute efficiencies computed using Eq (5.23). We report wall time per iteration due to the fact that MCSA converged on the solution in 22 iterations while the Krylov solvers converged in 19 iterations.

There are several key features of Figure 5.15 and Figure 5.16 worth noting. First, up to around 5,000 cores, all methods experience a super-linear improvement in parallel efficiencies. For all methods, this increase is not a function of the algorithmic efficiency as those computed using Eq (5.25) remained at unity, meaning that all computations converged in the same number of iterations relative to the base case[2]. Instead, what is happening here and was observed by Brunner and Brantley in their work is that the large problem used to scale to O(10,000) cores was large enough that memory thrashing was occurring in the 16 core base case. As the number of cores in the strong scaling study was increased and the local problem size decreased, more of the local problem fit into the cache of the system, thus causing

---

[2]When the algorithmic efficiency remains at unity for all calculations, the implementation efficiency is equivalent to the absolute efficiency and therefore is not presented here.
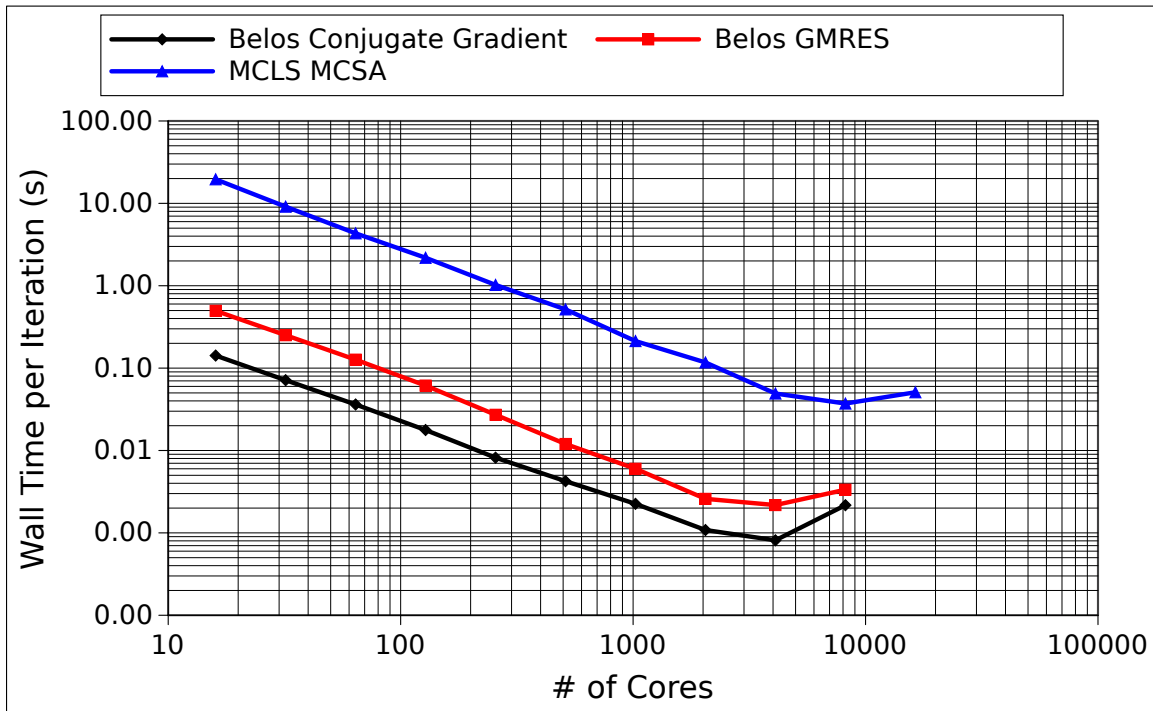
Figure 5.15: **Pure domain decomposition strong scaling wall time per iteration.** *Wall time is reported per iteration because the methods converged in different numbers of iterations. MCLS is over an order of magnitude slower arithmetically than the Krylov solvers. GMRES executes more operations than conjugate gradient and is therefore slower as well.*

improved serial performance and therefore enhanced runtimes. In this region of super-linear efficiencies, we also observe larger efficiencies for GMRES as compared to conjugate gradient. This occurs due to the fact that conjugate gradient has a static set of operations performed at every iteration while GMRES operates on a continually growing subspace. In addition, the orthogonalization operations required to generate that subspace consume much more time than the basic conjugate gradient operations, causing a larger serial runtime and subsequently higher efficiencies. For the same reasons, we also observe higher efficiencies for the MCSA implementation due to the serial performance of the implementation.

Beyond around 5,000 cores, the global problem size selected for this strong scaling study causes the local problem size to shrink enough that parallel communication costs begin to overtake arithmetic costs on process. This takeover causes this effective strong scaling wall
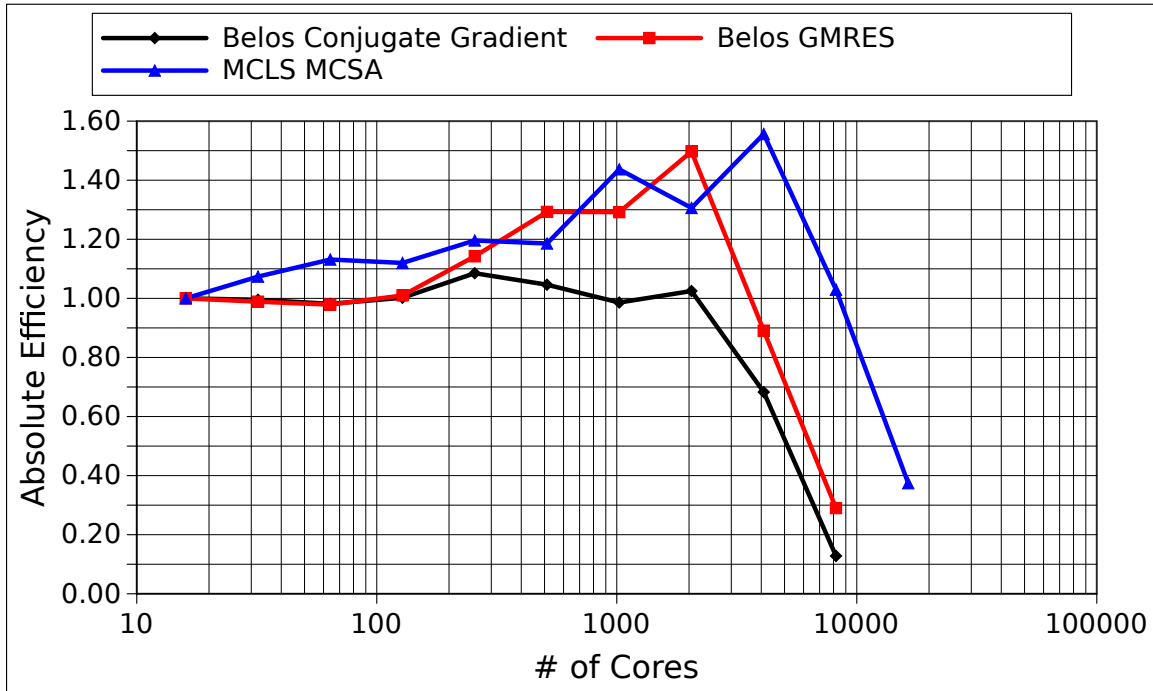
Figure 5.16: **Pure domain decomposition strong scaling absolute efficiency.** *Super-linear speed-up is from memory thrashing in the base case. MCLS is over an order of magnitude slower arithmetically, causing the higher efficiency. GMRES executes more operations than conjugate gradient, also creating a higher efficiency.*

that is observed in all methods. Using any more cores to solve this particular global problem is not an efficient use of those parallel resources. Furthermore, the fact that we see a very similar trends in efficiencies for all methods means that they are bound by the same parallel performance limitations in a strong scaling environment. This is important as we can expect the same qualitative scaling performance from MCSA if arithmetic optimization has been performed to improve the serial performance of the implementation. In addition, these results are valuable in that they show MCSA, when properly parallelized, has the ability to be competitive on leadership-class computing platforms with conventional subspace methods with good strong scaling observed in the pure domain decomposition case to O(10,000) cores.

Next, we consider the weak scaling performance of the algorithm. In this case, we fix the local problem size at 4×10^4 DOFs and increase the number of processors used in the simulation. Figure 5.17 gives the wall time per iteration and Figure 5.18 gives the weak
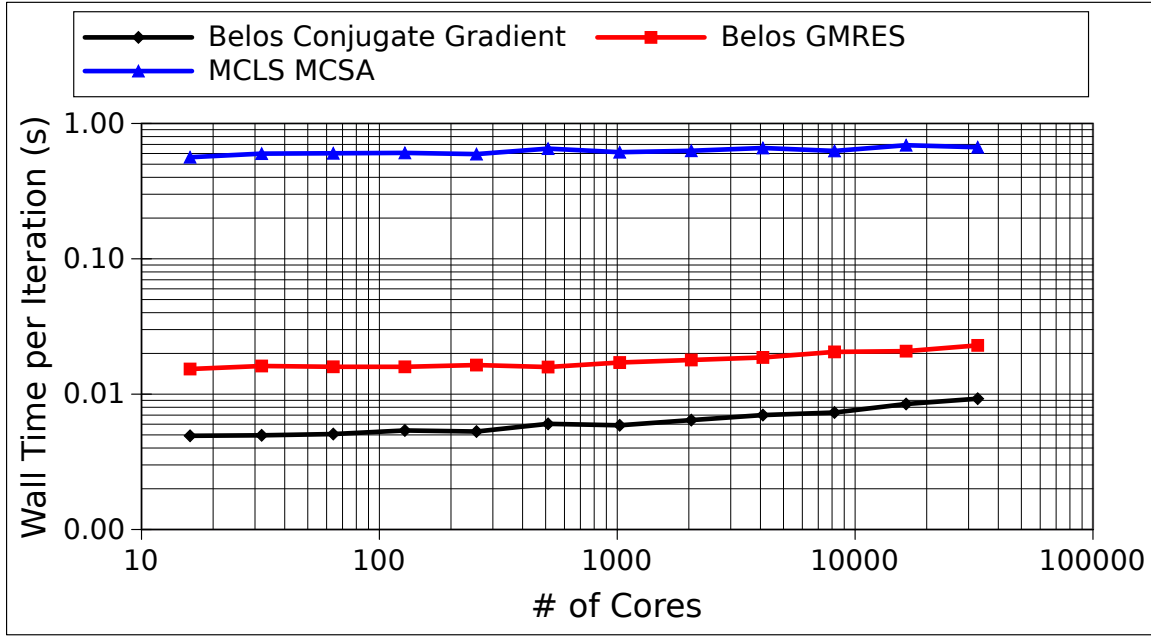
Figure 5.17: **Pure domain decomposition weak scaling wall time per iteration.** *Wall time is reported per iteration because the methods converged in different numbers of iterations. MCLS is over an order of magnitude slower arithmetically than the Krylov solvers. GMRES executes more operations than conjugate gradient and is therefore slower as well.*

scaling absolute efficiencies for this problem as computed by Eq (5.27). In general, the relative trends when comparing MCSA to the Krylov methods are the same with MCSA and GMRES scaling better than the conjugate gradient method due to the increased amount of arithmetic work on-process. In addition, it is important to note that the weak scaling of MCSA when properly parallelized remains competitive with the Krylov methods keeping in mind the artificial inflation of efficiencies.

As an additional means of comparison between MCSA and the Krylov methods, we compute the algorithmic efficiencies of the calculations using Eq (5.25). As shown in Figure 5.19, the algorithm efficiency of the Krylov algorithm improves as a function of the number of cores in the problem due to the fact that the number of iterations required to converge decreased from 20 in the base case to 19 and then to 18 for the final set of weak scaling computations. When this reduction in iterations is used to account for the observed runtimes and computed absolute efficiencies for weak scaling we end up with the
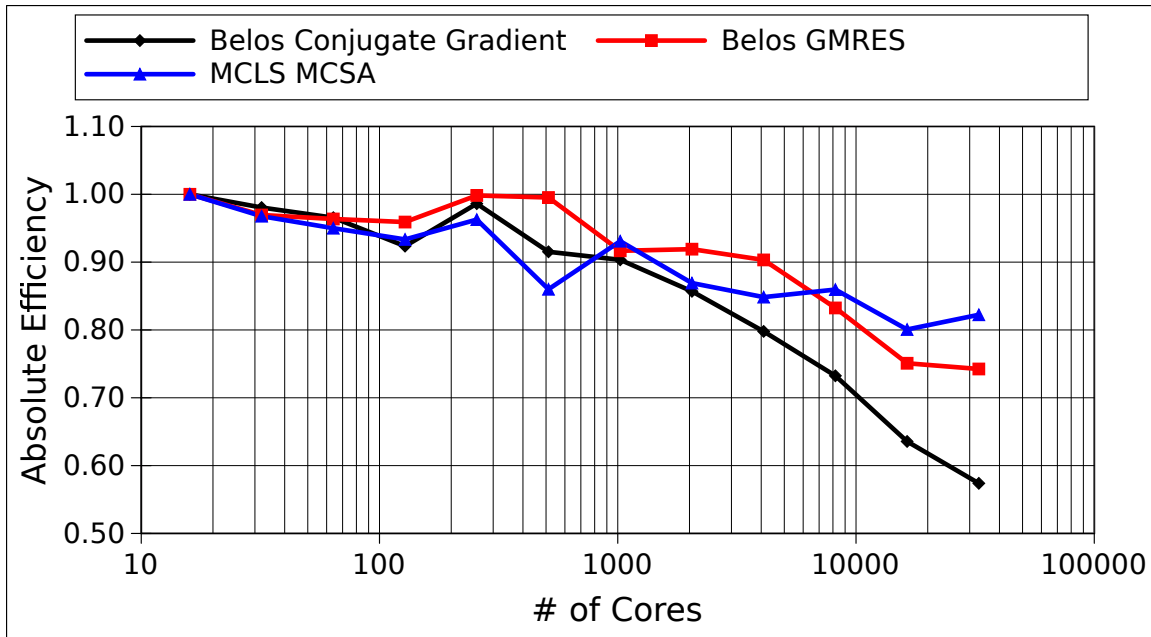
Figure 5.18: **Pure domain decomposition weak scaling absolute efficiency.** *MCLS is an over order of magnitude slower arithmetically, causing the higher efficiency. GMRES executes more operations than conjugate gradient, also creating a higher efficiency.*

implementation efficiencies computed using Eq (5.26) given in Figure 5.20. Because MCSA maintains the same iterative performance as a function of global problem size in the weak scaling study, the implementation efficiencies compare more favorably to the Krylov methods. Using the implementation efficiency, we are effectively measuring the parallel performance of a single iteration for each method by looking at these implementation efficiencies. As the global problem size increases, MCSA is less prone to a drop in parallel efficiency. If optimization has been performed and runtimes potentially approach those of the Krylov methods, this comparison may not be as favorable. Overall, weak scaling performance of the parallel MCSA algorithm is excellent for the pure domain decomposition case with absolute parallel efficiencies of over 80% observed at over 32,000 cores.

In addition to comparing MCSA scaling to conventional methods, we also motivate avoiding any type of master/slave algorithms at these high levels of concurrency by comparing the binary communication tree implementation used in the previous results with a parallel
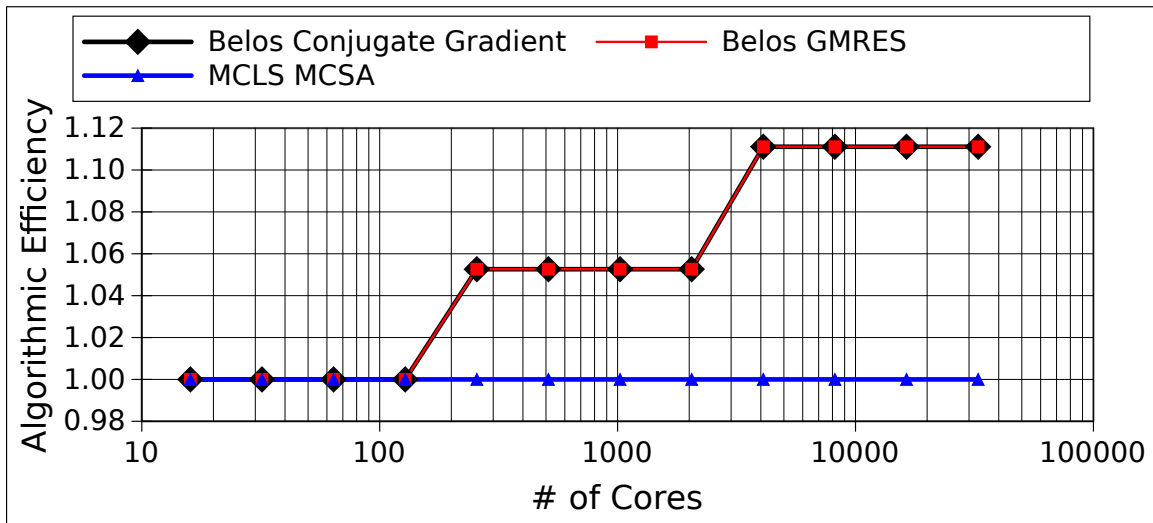
Figure 5.19: **Pure domain decomposition weak scaling algorithmic efficiency.** *As the global problem size was increased in the weak scaling study, both conjugate gradient and GMRES converged in fewer iterations, causing the rise in algorithmic efficiency.*
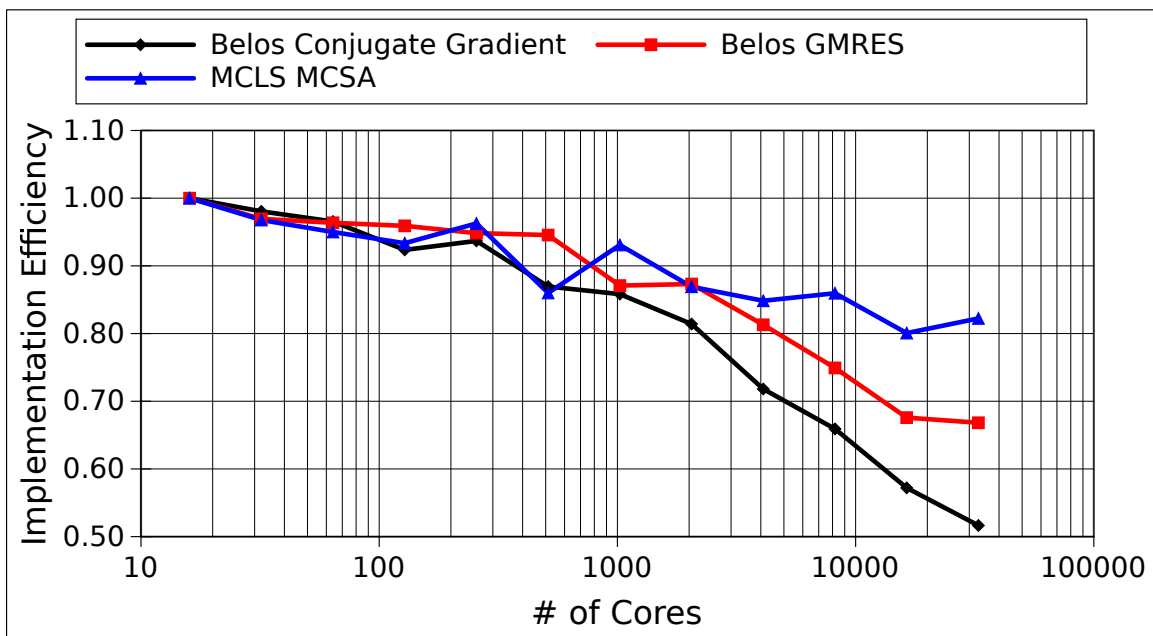
Figure 5.20: **Pure domain decomposition weak scaling implementation efficiency.** *Considering the scalability of a single iteration of the implementation, the inflated efficiencies of the MCLS MCSA implementation become more obvious. Implementation optimization will likely reduce the MCSA values to a level more comparable to the Belos values.*
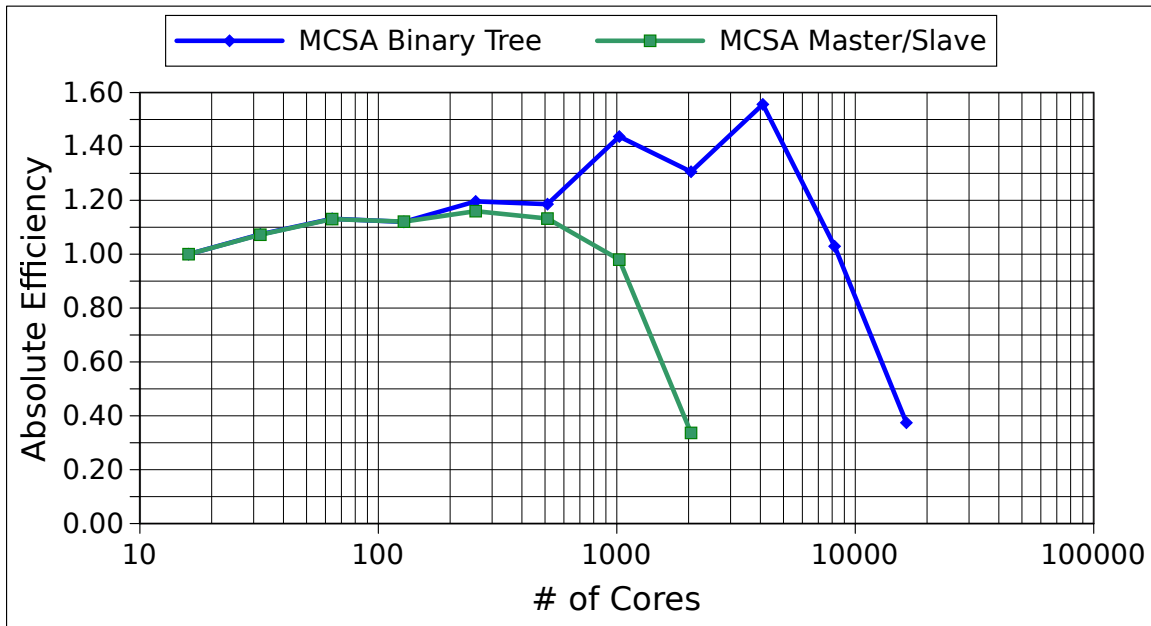
Figure 5.21: **Binary tree vs. master/slave communication scheme strong scaling absolute efficiency.** *The master/slave scheme will not scale beyond $O(1,000)$ cores due to load imbalance.*

MCSA implementation that uses the master/slave scheme to determine the end of a history transport stage as shown in Figure 5.3.2 instead. Figure 5.21 provides this comparison using the strong scaling study while Figure 5.22 gives the results of the comparison for the weak scaling study. In both cases, the deficiencies caused by using the master/slave scheme for transport completion are obvious. At around 1,000 cores, both the strong and weak scaling performance seriously degrades while the binary tree pattern maintains excellent performance. At this number of cores, any extra work given to the master process, even if it amounts to summing a handful of integers and checking for a few extra messages as in this algorithm, grows enough to create serious load imbalance and reduce performance.
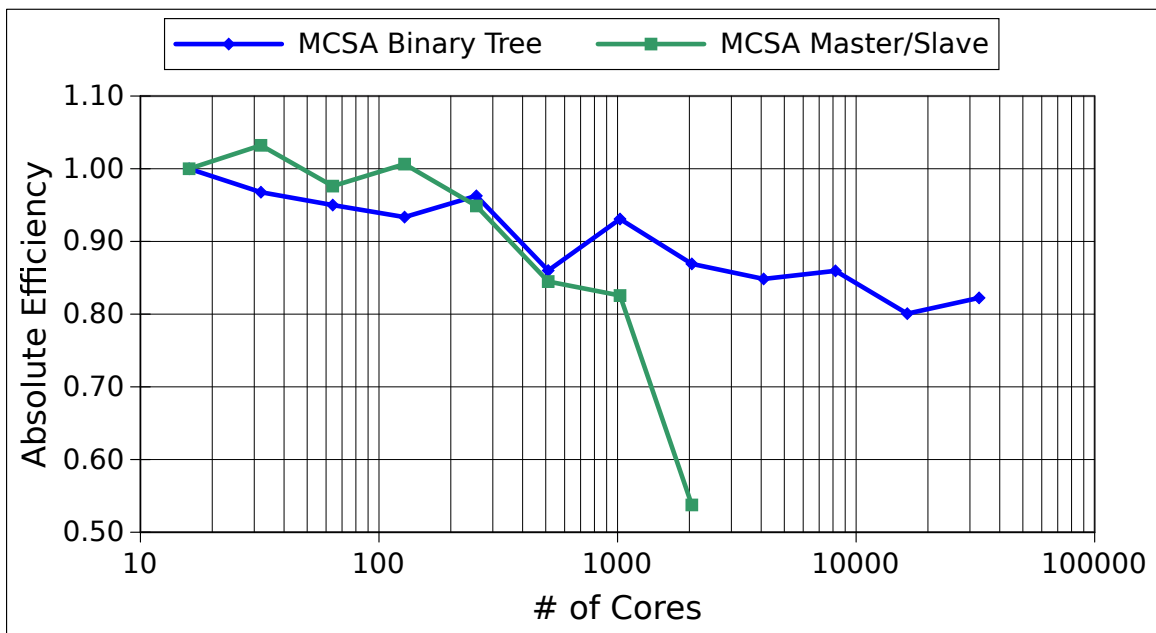
Figure 5.22: **Binary tree vs. master/slave communication scheme weak scaling absolute efficiency.** *The master/slave scheme will not scale beyond* $O(1,000)$ *cores due to load imbalance.*

5.8.4 Overlapping Domain Decomposition

In the next set of scaling studies, we will explore how adding overlap to the subdomains in the problem affects runtimes and parallel performance as compared to the case with pure domain decomposition. To do this, we utilize the set of analytic relations developed in § 5.2 to design these numerical experiments. For the neutron diffusion problem used in these scaling studies, the linear operator had a spectral radius of 0.787 and a weight cutoff of 1×10^{-2} was used with the Neumann-Ulam solver. Using Eq (5.12) gives an expected random walk length of 19.22 transitions for any given history in the problem. Using the mean-chord approximation given by Eq (5.21), we then expect approximately 5.3% of the histories born in a particular domain to leak out after the first transport stage. By adding overlap, we aim to reduce this fraction of communicated histories and therefore boost the parallel performance of the algorithm.

To determine the amount of overlap to test for the scaling studies, we use a variation of Eq (5.15) to determine how many discrete states a history will move on average from its birth site. We modify Eq (5.15) to only account for discrete movements:

$$\sqrt{\overline{n_k^2}} = n_s \sqrt{k} \, , \tag{5.28}$$

where $\sqrt{\overline{n_k^2}}$ is now the root-mean-squared number of discrete states a history will move from its birth site. For our diffusion problem used in these scaling studies, we compute a value of 2.63 states per history for any of the dimensions of the system. This means that we can expect to end up on average 2.63 states in both the i and j dimensions away from the starting state. Therefore, we will use the overlap generation algorithm outlined in § 5.4.1 such that we parametrically grow the local domain using 1, 2, 3, and 5 levels to measure how scalability is affected when this root-mean-squared number of states is considered. For example, using 3 levels of overlap should keep over 50% of the histories that would be communicated in the pure domain decomposition case on-process as this is greater than the root-mean-squared

number of states we would expect a history to travel.

For the performance metrics, we may use the same weak and strong scaling efficiency metrics that we used for the pure domain decomposition case. As we are comparing to the case without overlap and are looking to boost performance relative to the case without overlap, for both weak and strong scaling calculations we will use the 16-core case without overlap as the reference computation for all efficiency measures reported.

The absolute efficiency results from the strong scaling exercise are given in Figure 5.23. Aside from the boosting of efficiencies at 2,048 cores, little evidence of strong scaling improvement is evident for all levels of overlap tested. To further explore any potential benefits of adding overlap into the system, Figure 5.24 gives the difference in the efficiencies between all overlap cases and the reference case without overlap at each core count. At smaller numbers of cores, there is no observed benefit to using overlap to improve strong scaling. The improvements noted at 2,048 cores are also present here and account for the best efficiency improvements for all core counts tested. at 16,384 cores, using 2 levels of overlap did give a 6.4% boost in efficiency while at 1,024 cores this same amount of overlap actually reduced the efficiency. Beyond 2 levels of overlap, efficiency levels begin to fall with 5 levels of overlap performing the worst for all cases. From this, we don't expect adding any more overlap will improve the scalability of the algorithm and the best strong scaling performance was observed when the number of overlap levels is approximately equal to the root-mean-squared number of states we expect a history to move from its starting point as computed by Eq (5.28). We will defer an explanation of the drop in efficiencies for levels of overlap beyond this value until we have analyzed the weak scaling data.

For weak scaling, the same study as in the pure domain decomposition case was performed again with 1, 2, 3, and 5 levels of overlap. The absolute parallel efficiencies from these calculations are given in Figure 5.25 and the differences in efficiencies from the calculations without overlap. The results here are much the same in that there is not a dramatic improvement in scalability relative to the case without overlap. Opposite the strong scaling
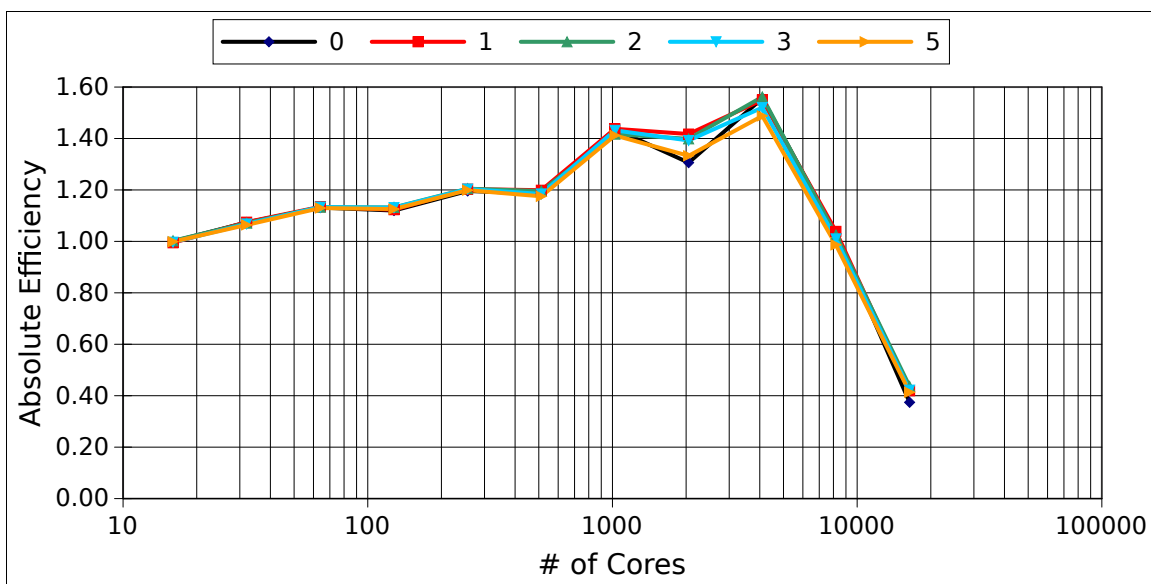
Figure 5.23: **Strong scaling absolute efficiency with varying levels of overlap.** *Values of 0, 1, 2, 3, and 5 levels of overlap were used as the problem had a root-mean-squared number of states of 2.63 for each history.*
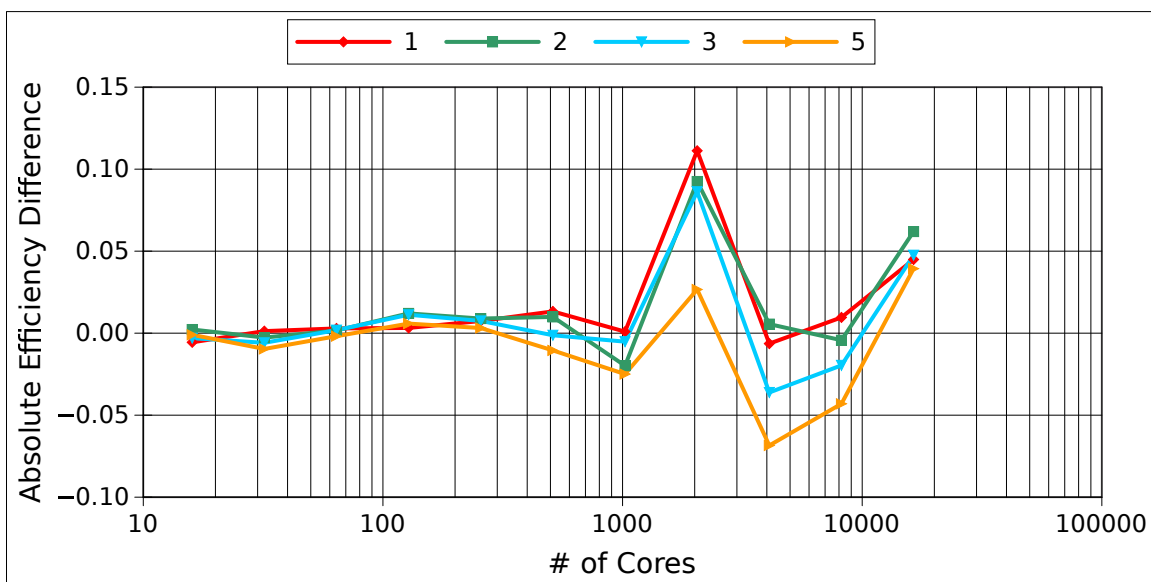
Figure 5.24: **Strong scaling absolute efficiency difference with respect to the 0 overlap base case.** *Values of 1, 2, 3, and 5 levels of overlap are compared here with the absolute difference of the absolute efficiencies presented.*
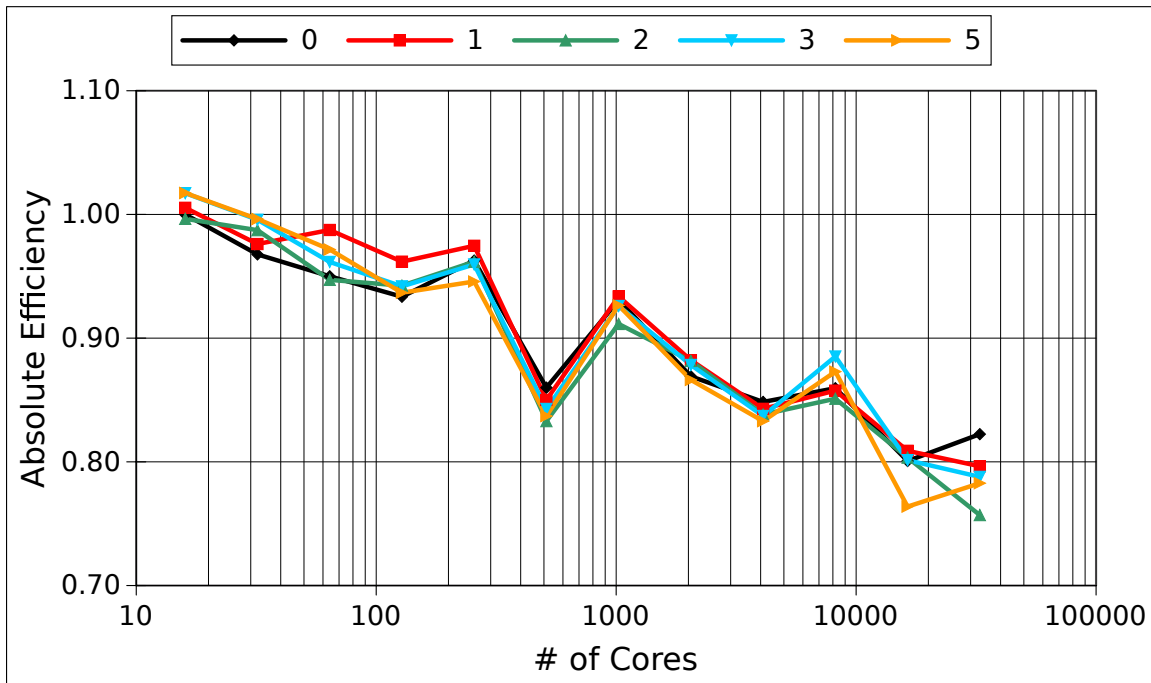
Figure 5.25: **Weak scaling absolute efficiency with varying levels of overlap.** *Values of 0, 1, 2, 3, and 5 levels of overlap were used as the problem had a root-mean-squared number of states of 2.63 for each history.*

calculation, overlap enhances weak scaling efficiencies at lower core counts and degrades the efficiencies at higher core counts. In addition, 1 level of overlap provided the best enhancement of scalability when overlap was beneficial.

For both the strong and weak scaling studies, the parallel performance of the algorithm was either marginally improved or not improved at all. We would always expect an improvement in performance for using overlap to prevent the transport of histories from domain to domain during execution of the Neumann-Ulam algorithm. The reduction in transport means a reduction in parallel communication and therefore should never degrade the performance of the algorithm. It is true that doing so in fact enhances Monte Carlo performance. However, the Neumann-Ulam algorithm is not representative of the entire MCSA algorithm. When overlap is used, an overlapping tally vector is constructed in parallel such that multiple cores may own multiple states in the system. When this occurs, the tally data associated with these
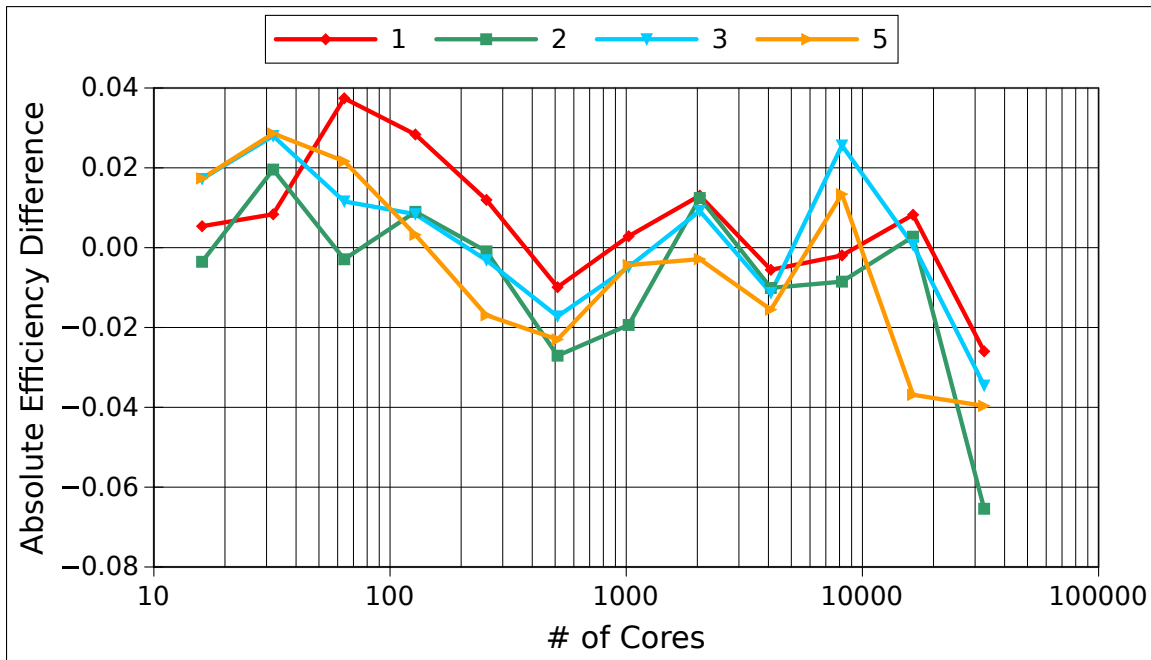
Figure 5.26: **Weak scaling absolute efficiency difference with respect to the 0 overlap base case.** *Values of 1, 2, 3, and 5 levels of overlap are compared here with the absolute difference of the absolute efficiencies presented.*

shared states must be communicated after the Neumann-Ulam solve as outlined in § 5.4.2. This reduction operation then builds the full MCSA correction vector in the decomposition of the solution vector.

Therefore, by building overlap we are in fact reducing parallel communication during the Neumann-Ulam solve but we are simply deferring that communication until after Monte Carlo transport when the overlapping tally vector must be reduced. When overlap becomes large enough (i.e. larger than the root-mean-squared number of discrete states a history will travel), then the savings in communication during the Neumann-Ulam solve start to become smaller than the communication created in the overlapping tally vector reduction. We see this in both the strong and weak scaling cases at larger levels of overlap. For the strong scaling case, we see better performance improvement at higher core counts because the total number of overlapping states on each core is smaller from the local problem size shrinking. For weak scaling, we see better performance improvement at lower numbers of cores because

although the local overlap size is fixed, the global amount of overlap is growing with core count and therefore reducing the performance of the tally reduction operation.

Based on this data, a few levels of overlap within the expected distance of travel for a history may offer some marginal improvement in scalability, however, it is not as effective as one might think given its improvement to reactor physics calculations as observed in the literature. This is largely due to the density of states in the system that creates the described performance bottlenecks in the overlapping tally vector reduction operation. In a Monte Carlo particle simulation, these overlapping tally reduction operations are not expected to be performed at the speed they are required in MCSA. For example, in a criticality calculation with overlapping domains, we would expect to perform as many parallel tally vector reduction in a particle transport simulation as there are particle stages required for convergence of the eigenvalue. However, these particle stages will likely be much more costly in terms of wall time relative to a Neumann-Ulam solve in an MCSA iteration due to the more extensive particle physics and logic structure that must be evaluated. Therefore, we can expect this overlapping tally reduction to be less significant to scalability in those operations. We do not have as complicated a logic structure in a history random walk for the Neumann-Ulam method and therefore overlap can inhibit scalability if too large.

5.8.5 Multiple Set Domain Decomposition

We next look to apply replication to the problem in the form of multiple sets. As the previous analysis showed overlap to be of little assistance in improving scalability, we only apply multiple sets to the problem with pure domain decomposition within the sets for these scaling studies. Before performing parallel scaling studies using multiple sets, several aspects of the replicated parallel problem must be considered in order to effectively craft the studies and interpret their results. First is the question of how many stochastic histories to use to generate the correction vector in the MCSA iteration. For this work we consider two choices; the split case and the fully replicated case. As an example of these cases, consider a single set problem where 20,000 histories are used in the Monte Carlo solve. If we choose the split case, then solving the same problem with 2 sets would give 10,000 histories in each set and 4 sets would give 5,000 histories in each set. Splitting the histories in this way provides the same global number of histories used to compute the correction in the single set problem. We expect to reduce the time to solution by doing this as each individual set solve will occur faster in an almost linear fashion with the reduced number of histories. For the replicated history case, each additional set in the problem will use just as many histories as the single set case. Using 2 sets with fully replicated histories for our example problem then has each set computing 20,000 histories with 40,000 global histories in the computation. For the 4 set case, the number of global histories is increased to 80,000. We also expect this type of replication to reduce the time to solution as the extra global histories should reduce the stochastic uncertainty in the correction vector and reduce the overall number of MCSA iterations required to converge.

5.8.5.1 Strong Scaling with Multiple Sets

For the strong scaling study, we apply the additional sets as follows. Using the same problems as the pure domain decomposition scaling study, the multiple sets are used to replicate those

problems and boost the core count. For example, for the 4 set case, the data point at 64 cores has the same N/P ratio in one set as the single set problem with 16 cores. This is due to the fact that N is fixed for the strong scaling study and 4 replications gives a set size of 16 cores. For the 2 set case, the 32 core data point is solving the same N/P problem in a set as the 16 core base case.

In addition to considering the replicated domain, we must also consider how to modify the efficiencies we will compute. For the strong scaling case, recall that the objective is to decrease the time to solution for a given global problem size N by increasing P. Therefore, we may use Eqs (5.24), (5.25), and (5.26) to compute the various strong scaling efficiencies, but we must modify the reference computation in each of these formulas to reflect our objective. For all efficiency computations, the 16 core single set computation will be used as the reference case. By adding more cores to the problem, either by replicating with multiple sets, or decreasing the local problem size, any computational resources added to the problem should aim to result in speedup of this reference case. If this speedup for one technique of adding cores is less than another, then that technique is deemed a less efficient use of those computational resources.

For the multiple sets problem, the single set strong scaling study from the pure domain decomposition base case was repeated for multiple sets with both splitting of histories across sets and full replication of histories across sets using both 2 and 4 sets. Figure 5.27 gives the actual wall times for these computations. There are two important features to note in the wall time data. First, splitting the histories among sets instead of replicating them is faster due to the fact that cutting the number of histories in half reduces the time of an iteration by a factor that is nearly linear while increasing linearly the number of histories through replication does not decrease the iterations required to converge by a linear factor. Second, until the strong scaling wall is hit starting at around 10,000 cores, the single set case actually performs the fastest with only marginal improvement in runtimes at higher numbers of cores with more sets. At these larger numbers of cores, however, the improvements are so modest
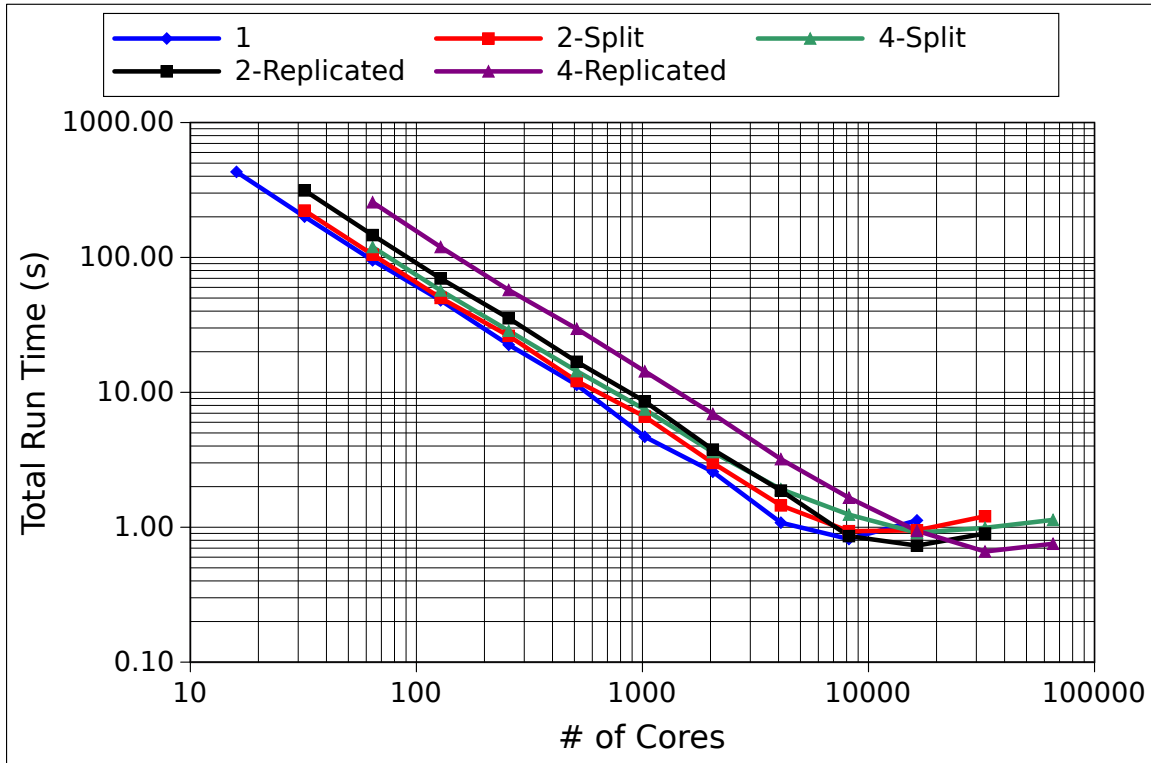
Figure 5.27: **Wall time in seconds to solution for each case for the strong scaling study with multiple sets.** *Until the strong scaling wall is reached at O(10,000) cores, the single set case performs the best. For the multiple set cases, it is faster to split histories among sets and maintain iterative performance rather than replicate histories to improve iterative performance.*

that one is better off running the same problem using a single set at lower core counts to conserve computational resources while maintaining a good time to solution.

From this timing data we then compute the absolute efficiencies for strong scaling as given in Figure 5.28 using the 16-core single set calculation as the reference case. As observed in the timing data, because the single set case had the fastest run times up to the strong scaling wall it also has the best observed efficiencies. For the 2 set case with history splitting, although the time to perform an iteration was nearly cut in half, the extra parallel overhead associated with reducing the tally across the blocks to combine the set results increases run times and reduces efficiencies. This reduction across blocks is even more obvious for the 4 set case. For the replicated cases, we do observe a flat region of parallel efficiencies at larger core counts

(up to around 32,000 for the 4 set case with history replication) showing improved scaling within context of not considering the single set calculation. Unfortunately, the additional cores do not reduce the runtime of the global problem as efficiently as expected. Ultimately, all cases effectively hit the strong scaling wall at the same time at around O(10,000) cores.

We expect this if we consider the fact that adding sets to the problem is in itself effectively a form of strong scaling. For any given problem of fixed size N, adding extra sets to the computation decreases the global ratio of N/P as P will grow with the addition of sets (although N/P is constant within a set). For the split history case, the splitting further exacerbates this situation by further decreasing the amount of histories that will be computed in the local domain, giving a larger ratio of communication to work in the Monte Carlo solve. As with with single set results, we also observe some efficiencies greater than unity for the multiple set cases also due to improved cache utilization.

Although not as dramatic as one might originally expect from introducing replication, there are some modest gains in efficiencies at high core counts by using multiple sets. Of interest here is where the multiple set cases perform better than the single set case after the single set case has hit the strong scaling wall. In Figure 5.28, at 16,384 cores the single set case operates at 38% efficiency while at the same number of cores, the 2 set case with history replication operates at 58% efficiency. This is reasonable improvement in the use of those computational resources, gained by replicating the problem. Beyond 16,384 cores, there is not a compelling reason to use more computational resources for the this problem.

Also of interest here is the effect of splitting histories among sets versus replicating them on the iterative performance of the method. Table 5.5 gives the iterations required to converge and computed algorithmic efficiencies for each of the cases presented in the strong scaling data. As expected, splitting histories maintains a fixed global number of histories and therefore maintained the number of iterations required to converge relative to the single set base case. When histories were replicated, adding sets decreased the number of iterations required to converge in a nonlinear fashion. Therefore, increasing the number of histories
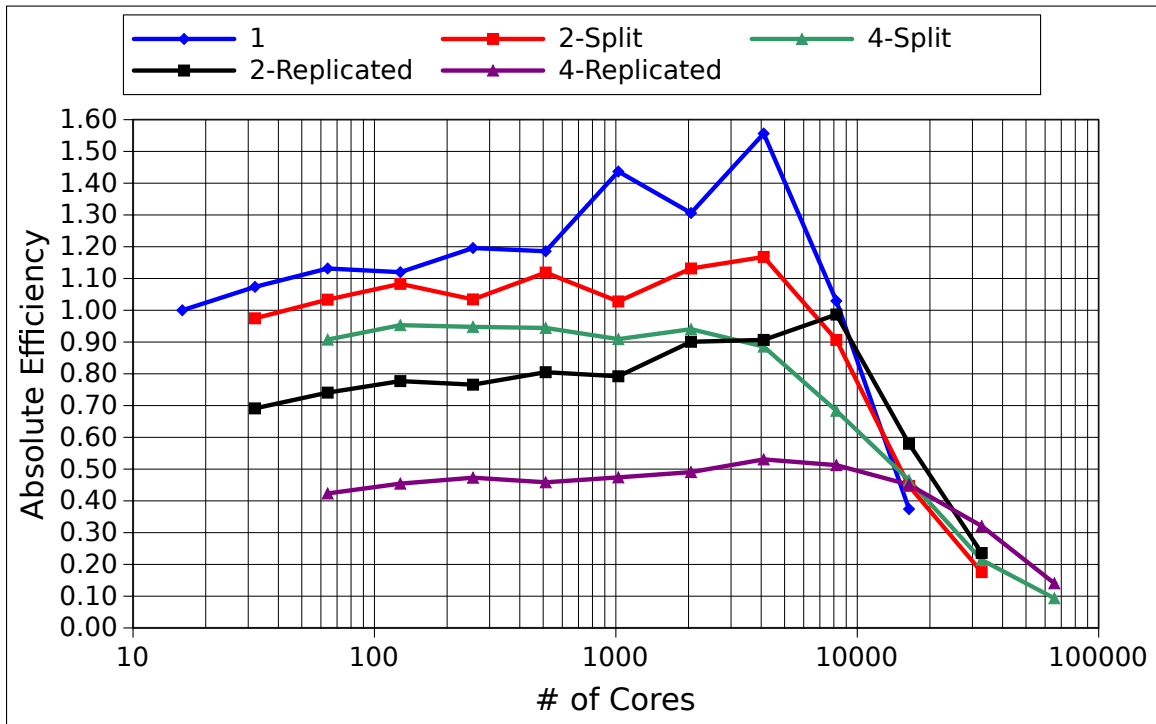
Figure 5.28: **Multiple set absolute parallel efficiency.** *Computed relative to the 16-core 1-set base case. Using a single set is the best means by which to improve strong scaling up to the strong scaling wall. At higher core counts past where the single set case hits the strong scaling wall adding sets can provide some improvements in efficiencies.*

per MCSA iteration improves algorithmic efficiency. Using these algorithmic efficiencies, the implementation efficiencies for the multiple set cases were computed and are given in Figure 5.29. From these results, we see that the replicated history cases are even less efficient than in the absolute case with respect to the performance of a single iteration. Not only do we have the additional parallel overhead of doing the block level reduction, but we also have additional histories that increase the time to solution for a single iteration.

Case	Iterations	η_{alg}
1	22	1.0
2-split	22	1.0
2-replicated	16	1.375
4-split	22	1.0
4-replicated	13	1.692

Table 5.5: **Strong scaling algorithmic efficiency using multiple sets.** *Replicating histories improves algorithmic efficiency by converging in fewer iterations.*
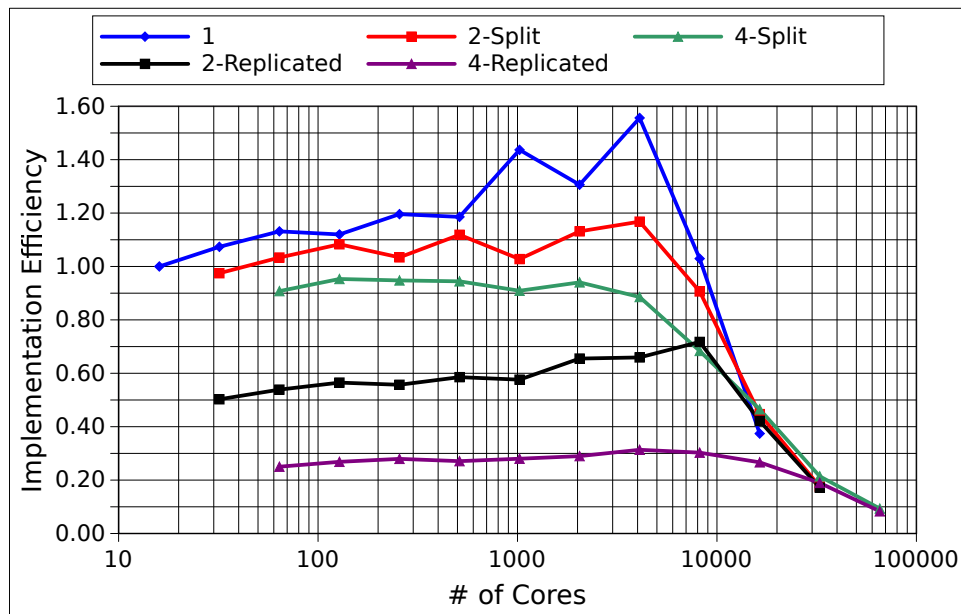
Figure 5.29: **Multiple set strong scaling implementation efficiency.** *Computed relative to the 16-core 1-set base case. Considering iterations required to converge, the performance of the split history cases at much better than the cases with history replication.*

5.8.5.2   Weak Scaling with Multiple Sets

Next, we continue to a weak scaling study of the multiple sets problem. In the same way as the strong scaling study, we will modify the pure domain decomposition study to account for the additional replication. For each calculation in the single set study, that problem will be replicated either 2 or 4 times with both split and replicated histories to assess the effects on scalability and runtime. Figure 5.30 gives the wall times from the multiple sets weak scaling study. Of primary importance here is the fact that adding sets to the problem with both split and replicated histories actually decreases the time to solution. This was not observed in the strong scaling case until much larger core counts as the multiple set computations hit the strong scaling wall after the single set computation.

This result is significant in that it shows a solution technique in which the linear problem can actually be replicated and enhance time to solution, something that cannot be achieved with conventional methods. At larger core counts, however, this reduction in compute time is not as large as at lower core counts due to the fact that the tally reduction across blocks requires more resources and those resources are clearly growing with core count (most obviously in the 4 set case with split histories). In addition, at 131,072 cores for the largest 4 set computation, load balance is likely becoming an issue due to the linear system and subsequent parallel matrix and vector operations only occurring on a subset of the entire processor space of the problem while the Monte Carlo calculation is occurring on all processors.

For a multiple set analysis of the weak scaling timing results, we again have to consider that adding sets to the problem is actually a form of strong scaling. Consider a single set problem ($S = 1$) for a given P and N. When that problem is now solved using 2 sets we have $S = 2$, N and $2P$. For any number of sets we then have a global problem size of N while the number of processors is SP where P is the number of processors in the single set case. Therefore, N/P is no longer fixed in the weak scaling study but rather $N/(SP)$ is fixed. As
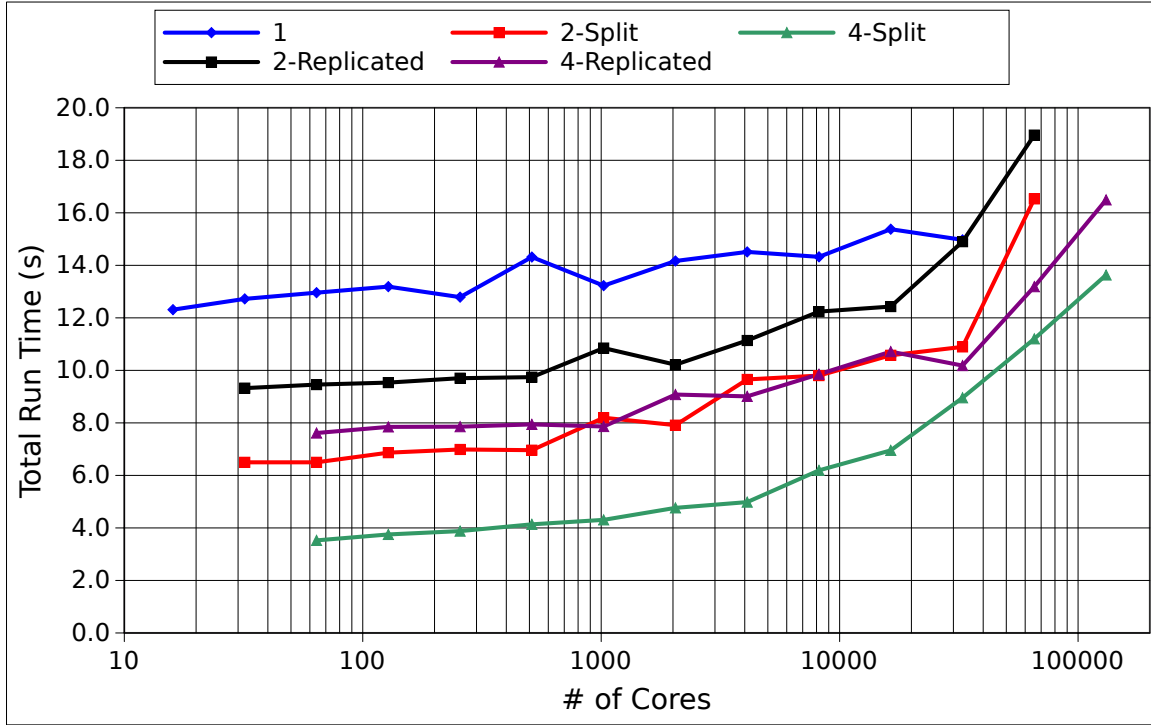
Figure 5.30: **Wall time in seconds to solution for each case for the weak scaling study with multiple sets.**

a result, we modify the weak scaling absolute efficiency relationship to account for this fact:

$$\eta_{weak}(M|N, P|Q, S) = \frac{T(M,Q)}{S \times T(N,P)} \,, \tag{5.29}$$

where now the absolute efficiency is a function of the number of sets in the problem and again $M/Q = N/P$. As with the strong scaling study, we will use the 16-core single set case as the reference computation for efficiencies. Interestingly, Eq (5.29) has a very similar form to the strong scaling efficiency given by Eq (5.23), representative of the strong scaling nature of adding additional sets. For problems where adding sets improves time to solution, this new weak scaling formulation accounts for how efficiently those extra resources are incorporated into the problem. Without such a modification, the largest case run for the split 4 set case would have a computed weak scaling efficiency of nearly 100% using the standard formula for absolute efficiency. However, using 4 times as many cores as the single set case increased the
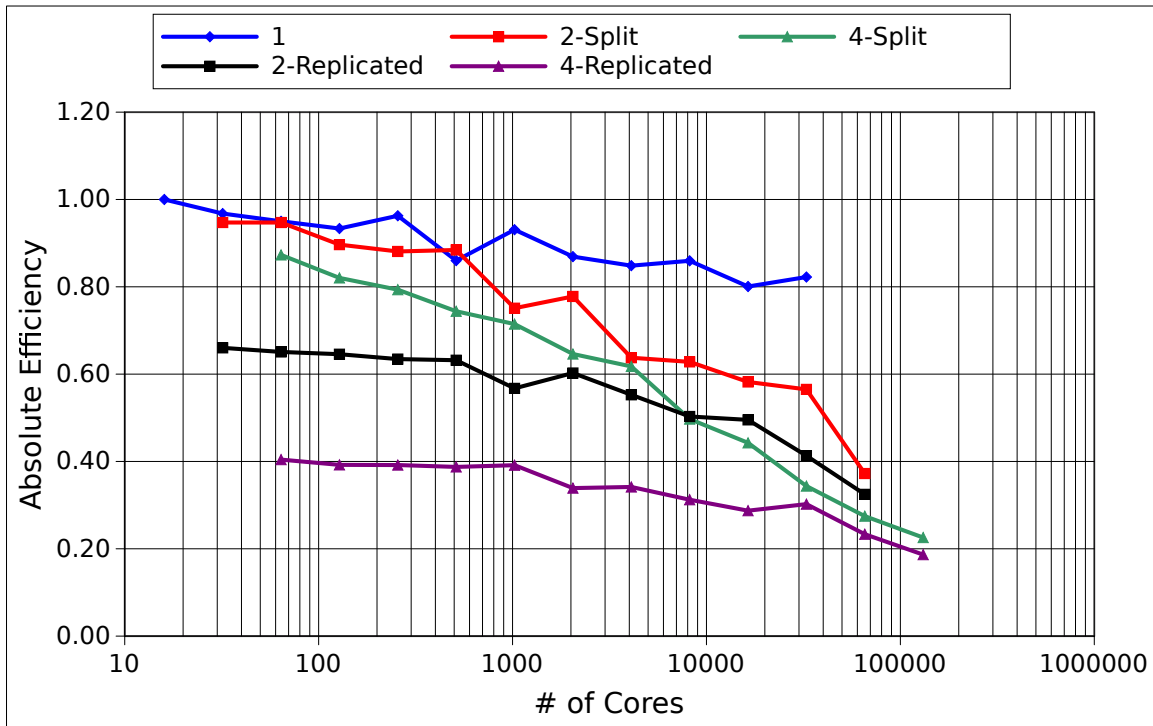
Figure 5.31: **Weak scaling absolute efficiency relative to 16-core 1-set base case.**

runtime for a fixed global problem size and therefore we would actually expect to compute a very low efficiency that shows this very poor use of resources.

Figure 5.31 gives the results of the weak scaling efficiency computations using the multiple set metric given by Eq (5.29). Although we do reduce the time to solution over the base cases for nearly all data points, the observation here is that the reduction in time to solution is still not large enough to efficiently use all resources. For example, for the 2 set case to be a perfect use of resources with either split or replicated histories, the runtime of that calculation must be half of that for the single set case. For the 4 set case, this run time should be a quarter of the single set case for perfect scaling. This was not the observation for the runtimes in Figure 5.30 and therefore the single set case is still the most efficient use of computational resources in this scaling study.

As in the strong scaling case, splitting and replicating histories across sets had effectively the same results for the weak scaling study with the iterations to converge and computed

algorithmic efficiencies given by Table 5.6. Again, when the implementation efficiencies are computed, we see in Figure 5.32 that splitting histories among sets is still a more efficient manner of introducing multiple sets rather than replicating histories in an attempt to reduce the number of iterations required to converge. Here we also note that this is not a true weak scaling study as indicated by Eq (5.29) but rather an odd combination of both weak and strong scaling. Regardless of this, although multiple sets are not the most efficient use of resources in this analysis, they do enhance the time to solution through replication and do so significantly at core counts of O(1,000) and lower. In both the weak and strong scaling cases, due to the additional computational and communication overhead of adding sets to the system, one should never expect to seriously boost parallel efficiencies for MCSA using this technique except for certain instances past the strong scaling wall in a purely strong scaling environment. In a weak scaling environment, although no efficiency increase will be noted, one can expect an enhancement of time to convergence by replicating.

Case	Iterations	η_{alg}
1	22	1.0
2-split	22	1.0
2-replicated	16	1.375
4-split	22	1.0
4-replicated	13	1.692

Table 5.6: **Weak scaling algorithmic efficiency using multiple sets.** *Replicating histories improves algorithmic efficiency by converging in fewer iterations.*
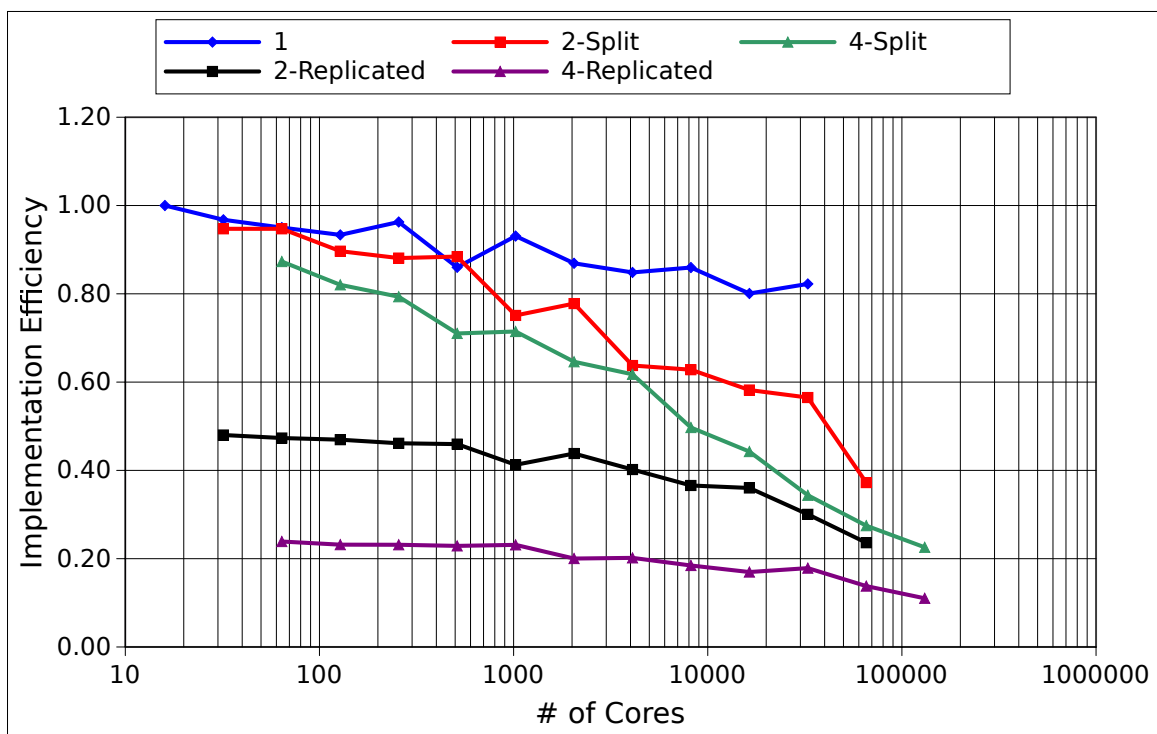
Figure 5.32: **Implementation parallel efficiency relative to 16-core 1-set base case.**

5.8.6 Subdomain Neumann-Ulam

Based on the analysis of the pure domain decomposed MCSA algorithm and subsequently the multiple sets and overlapping domain implementation, one may ask then ask if there is any need to communicate histories from domain-to-domain at all. Overlap was not as successful because because the additional communication required to reduce the overlapping tally vector eventually becomes larger than the communication savings during Monte Carlo transport. In addition, for local domains that are large enough to get good performance (e.g. those used in the weak scaling studies), then our analytic relationships for domain leakage, and in particular Eq (5.21), tell us that only about 5% of the histories in this diffusion problem will leave the domain in the first place. If that is true, then perhaps without any overlap or communication, just doing local Monte Carlo transport such that histories are terminated upon reaching the domain boundary may be satisfactory for accelerating the MCSA iteration. In this case, histories near the boundaries of the domain may be truncated before reaching the weight cutoff if they reach the domain boundary first. This truncation has the potential to increase the stochastic uncertainty of the Neumann-Ulam result and therefore increase the number of MCSA iterations required to converge. In addition, the scalability of the method will then be purely limited by the parallel matrix and vector operations required to implement the remainder of the algorithm on the subset of processors containing the linear problem.

Considering using MCSA in this way such that the Monte Carlo solve occurs only in the subdomains casts the method as more of a true domain decomposition as outlined by Chapter 14 of Saad's text on iterative methods [56]. Compared to traditional domain decomposition methods we see many similarities including the potential to overlap the subdomains to improve the results. By building the boundary data as outlined in § 5.3.1, we are effectively gathering one level of the adjacent domains, albeit in this case to satisfy the data requirements of the Monte Carlo estimators. Furthermore, the fact that we are using residual Monte Carlo to compute the correction vector casts MCSA as a stochastic realization of an additive Schwarz

method with a fixed point iteration used as a relaxation step[3]. Both the fixed point iteration and the computation of the residual propagate the solution from individual subdomains to the others through the matrix-vector multiply operation after all subdomain Monte Carlo solves have been completed. Perhaps an even more important consequence of viewing MCSA as a stochastic additive Schwarz procedure is that it has the potential to more readily fit as an accelerator into other linear solver techniques including GMRES or potentially as a preconditioner.

Using the Neumann-Ulam solver to compute the MCSA correction only in the subdomains, the strong and weak scaling studies were repeated to assess the performance gains made by eliminating communication in the Monte Carlo solver. For each scaling study, the 16-core base case with Monte Carlo communication was used as the reference point for efficiency computations in order to measure how eliminating communication boosts efficiencies. Figure 5.33 gives the results of the strong scaling study and Figure 5.34 gives the results of the the weak scaling study in terms of absolute efficiencies. In both cases, the benefits to parallel performance of using MCSA as a subdomain solver are obvious. In the strong scaling case we make the important observation that we hit the strong scaling wall at the same time with and without the additional Monte Carlo communication. Although the Monte Carlo communication did contribute to the efficiency decrease, it is clear that the remaining matrix and vector operations are the primary impediment to scalability. Furthermore, we see an even greater rise above unity in efficiencies because there is less communication overhead hiding the better cache utilization as the local problem size shrinks. At 16,384 cores, performing the subdomain solves boost the absolute efficiency from 38% to 67% relative to the reference case.

In the weak scaling study, we do not have the scaling wall to contend with and eliminating Monte Carlo communication through subdomain solves provides an effectively linear boost in the weak scaling absolute efficiency. We still see a small reduction in weak scaling efficiency

---

[3]See section 14.3.3 in [56] for a full definition of the additive Schwarz method.
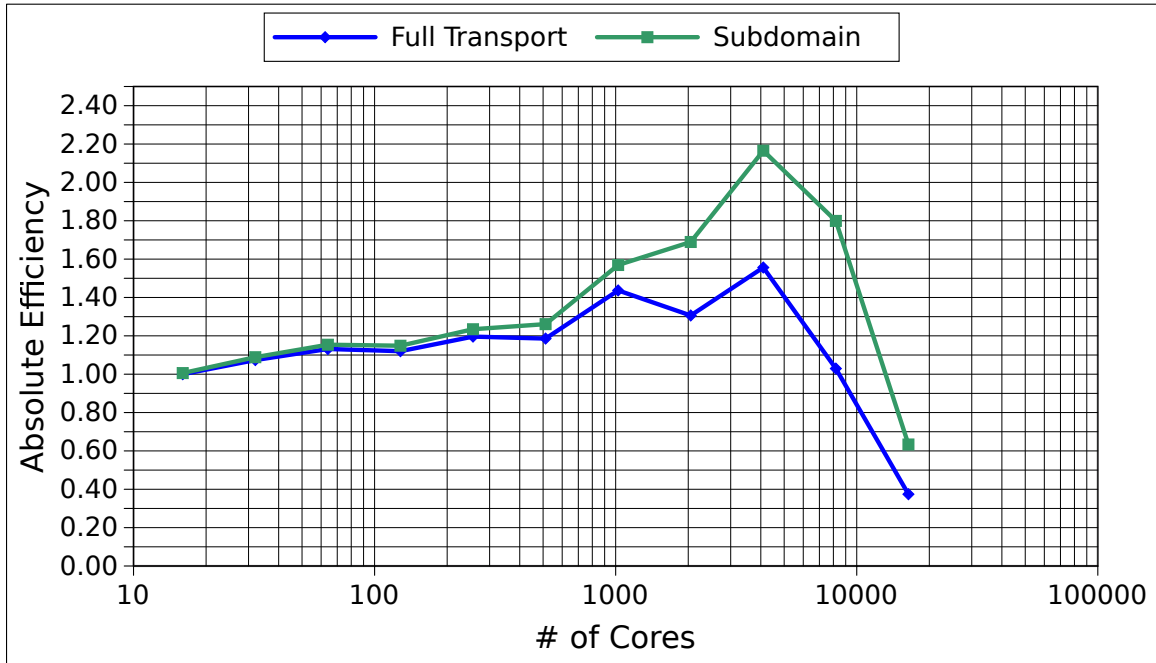
Figure 5.33: **Strong scaling absolute efficiency for pure domain decomposition.** *The subdomain Monte Carlo solver improves the parallel efficiency and therefore time to solution by eliminating all parallel communication during the Monte Carlo solve.*

as a function of core count due to the communication overhead for the parallel matrix and vector operations. Here we observe super unitary efficiencies for the subdomain case as there was a substantial improvement in runtimes relative to the 16-core base case with Monte Carlo communication.

Of additional concern for the subdomain method is the potential decrease in iterative performance due to the fact that histories near the boundary will potentially have their random walk truncated, thus decreasing the information available to compute the correction vector. For both the weak and strong scaling study, all calculations with split histories converged in 22 or in only a few cases 21 iterations for both the subdomain solve and the solve with communication giving an algorithmic efficiency of 1.048 for all cases. This small improvement in iteration count was not observed to be a function of problem size, number of processors, or whether the subdomain method was used. For the replicated history cases, the algorithmic efficiency improvement was not as good as when communication was allowed
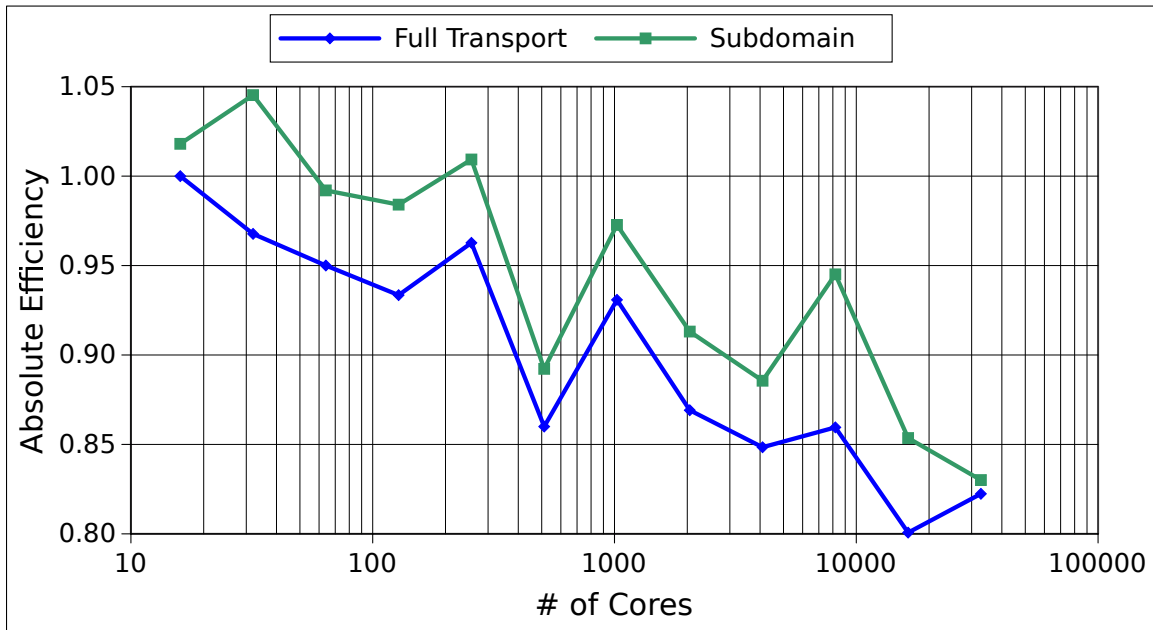
Figure 5.34: **Weak scaling absolute efficiency for pure domain decomposition.** *The subdomain Monte Carlo solver improves the parallel efficiency and therefore time to solution by eliminating all parallel communication during the Monte Carlo solve.*

for the Monte Carlo algorithm. For these calculations, the number of iterations to converge was reduced to 18 or 19 in both the strong and weak scaling studies with lower core counts converging in fewer iterations.

Therefore, there is no reason to expect overlap to improve the iterative or scaling performance of the method as iterative performance is maintained without it for this particular problem. Overlap is not as effective because histories relinquish most of their useful information within the first few steps (which is why we can use such a large weight cutoff and there is an insensitivity to weight cutoff as shown in Figure 2.13). Keeping them around longer with overlap to do extra work in the local domain will not improve iterative performance and thus increase compute times.

As a final analysis of MCSA using subdomain Monte Carlo, the multiple sets scaling studies are repeated to determine if any performance benefits are made from replication by eliminating Monte Carlo communication. Figure 5.35 gives the runtimes for the strong

scaling calculation and Figure 5.36 the computed absolute efficiencies. For the weak scaling studies, Figure 5.37 gives the wall times and Figure 5.38 the efficiencies. For both scaling studies, the results are effectively the same as for the case with Monte Carlo communication. This is again due to the fact that adding sets to the problem is not only an exercise in strong scaling but it also adds additional parallel overhead in the form of the tally vector reduction across blocks.

From a parallel performance perspective, MCSA may then be best used in a mode where the Monte Carlo is performed over only the subdomains with no replication or overlap added to the system. In this mode, iterative performance is maintained relative to the solutions with communication even for more ill-conditioned problems with larger spectral radii. Furthermore, no overlap was required to maintain iterative performance be letting histories near the boundary take a few more steps in their random walks. If in the future there are ill-conditioned problems where using subdomain Monte Carlo reduces the algorithmic efficiency of MCSA due to the information lost in the correction vector, overlap would be a viable mechanism to potentially maintain that iterative performance, keeping in mind the potential impacts on scalability that were observed in this work. However, although eliminating all Monte Carlo communication was observed to be the best mode of use for MCSA, the parallel Monte Carlo methods developed for this work still provide value for cases where only a Monte Carlo solution is desired. In those cases, full transport of the Monte Carlo histories are required in order to generate the correct solution.
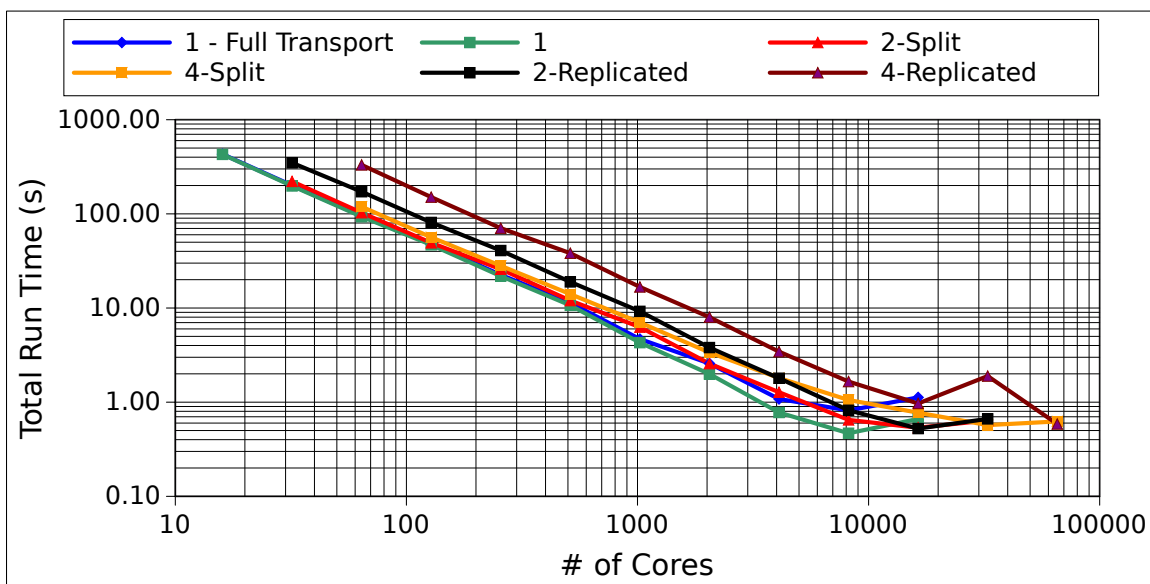
Figure 5.35: **Strong scaling total wall time with multiple sets and subdomain Monte Carlo.** *Adding multiple sets has in general a negative effect on the wall time as was observed for the case with full Monte Carlo transport.*
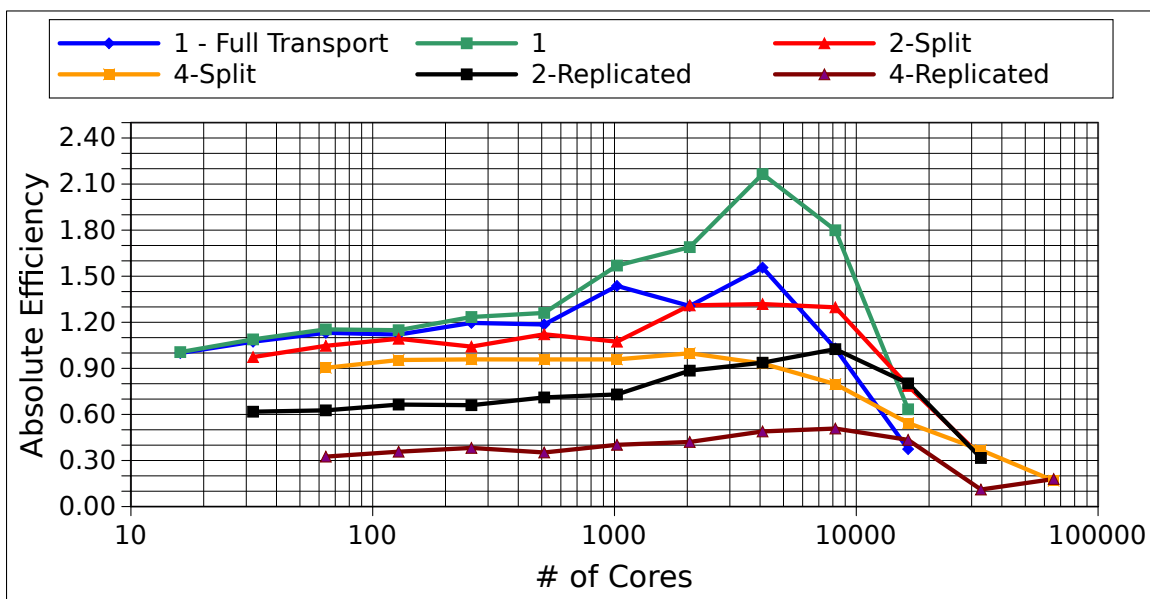
Figure 5.36: **Strong scaling absolute efficiency for with multiple sets and subdomain Monte Carlo.** *Increased wall times from adding parallel reduction operations for multiple sets reduces parallel scalability at lower core counts but gives a higher efficiency at the strong scaling wall.*
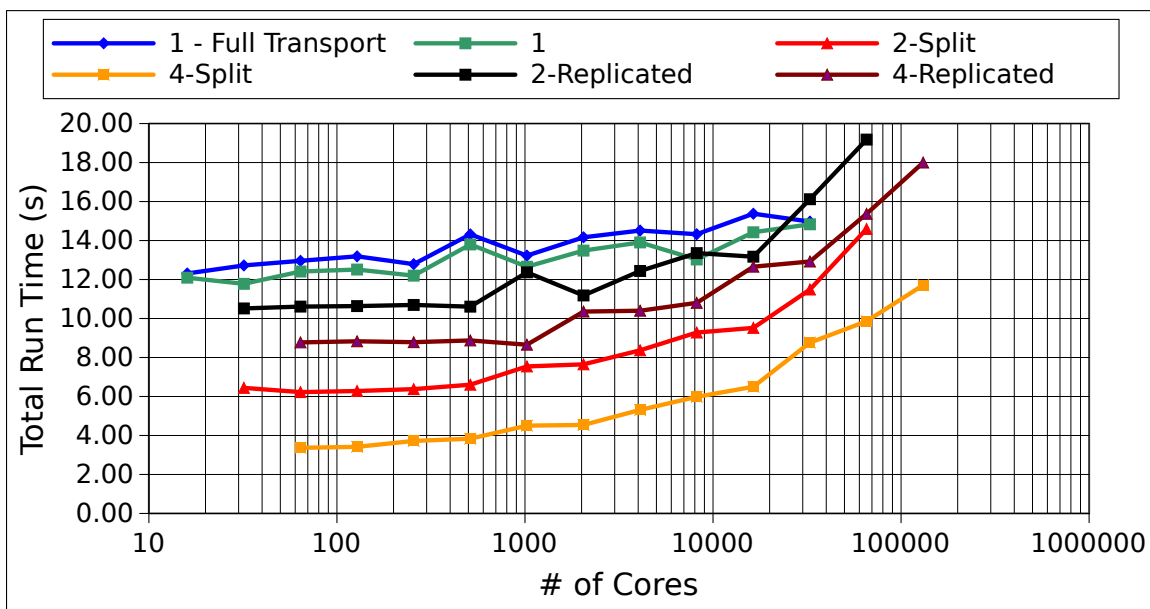
Figure 5.37: **Weak scaling total wall time with multiple sets and subdomain Monte Carlo.** *The addition of the set tally reduction is significant with cost of the reduction observed as core count grows.*
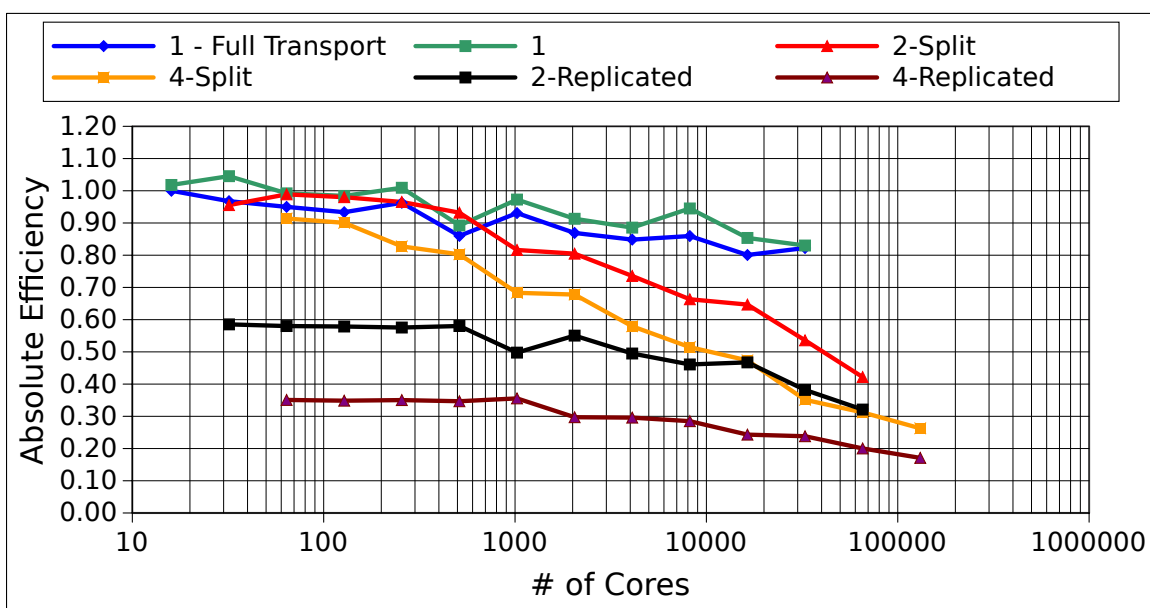
Figure 5.38: **Weak scaling absolute efficiency for with multiple sets and subdomain Monte Carlo.** *Weak scaling efficiencies are not improved at large core counts when multiple sets are added.*

5.9 Summary

In this chapter we have developed a domain-decomposed parallel algorithm for Monte Carlo Synthetic Acceleration and explored the qualities of the algorithm through parallel scaling studies. The following are the significant observations and findings.

- MCSA can be effectively parallelized using domain decomposition

- The leakage fraction of stochastic histories from a parallel subdomain can be quantified analytically using algebraic quantities

- The multiple-set overlapping-domain (MSOD) parallel algorithm for particle transport has been adapted to parallelize MCSA

- MCSA parallelized with MSOD was verified to produce the same results for solutions to the neutron diffusion equation as production Krylov methods

- Strong scaling studies were performed with up to 65,536 cores and weak scaling studies were performed with up to 131,072 cores on the Titan Cray XK7 leadership class machine at Oak Ridge National Laboratory

- MCSA scales favorably compared to production Krylov methods for both strong and weak scaling cases

- Overlap in small quantities determined analytically by random walk length can provide parallel efficiency boosts of a few percent in strong scaling cases but is ineffective in weak scaling cases

- Multiple sets will never boost parallel efficiencies in the weak scaling case due to additional communication overhead from added reduction operations but will boost efficiencies beyond the strong scaling wall

- Multiple sets offers a means to reduce time to solution by solving multiple copies of the original problem and combining the solutions using superposition

- MCSA is most efficiently used in parallel as a stochastic realization of an additive Schwarz method

- With future optimization, large scale reactor analyses in which the transport operator is fully formed (e.g. the SP_N equations) could experience improved time to solution on leadership-class machines with MCSA given the improved scaling performance

Chapter 6

Conclusions and Analysis

For high fidelity simulations of nuclear reactors, physics solutions are required with speed and accuracy. When the problems become large enough, such as the simulation of an entire reactor core, leadership-class computing facilities must be leveraged on the grounds of requirements for both time to solution and the amount of memory required to contain the description of the entire problem and the solution. Looking forward to the next generation of machines, concurrency will go up and available memory will go down, putting pressure on physics application developers to research and develop solution techniques that can efficiently leverage this hardware. In nuclear reactor simulation, both neutron transport and fluid flow calculations consume a vast amount of computational time in order to properly characterize both steady state operational characteristics and transient accident scenarios. In both cases, we desire solution techniques that are aware of coming changes in hardware.

In this work, we have presented Monte Carlo Synthetic Acceleration as a viable solution technique for both neutron transport and fluid flow problems on future hardware. To do this, we carried out three research and development activities. First, we applied MCSA to the SP_N form of the neutron transport equation and analyzed the preconditioning requirements and subsequent performance of the method when compared to conventional practices. Second, we used the knowledge gained from the research on neutron transport to develop the FANM method for nonlinear problems and studied its performance on three different benchmarks for the Navier-Stokes equations to demonstrate its applicability. Finally, we parallelized MCSA such that it may be applied to physics problems on leadership-class computing platforms.

In this chapter, we review the work presented in this document and describe how this work met the goals of the research. We then reiterate the important issues discovered during

the course of this work and develop a strategy for future work to potentially alleviate them. Finally, we close with some final remarks regarding Monte Carlo Synthetic Acceleration.

6.1 Monte Carlo Synthetic Acceleration Solutions for the SP_N Equations

This work demonstrates the first application of MCSA to the neutron transport problem. To do this, we used the SP_N form of the Boltzmann transport equation. In this form, the transport equation takes on a diffusion-like form where the angular character of the flux is accounted for in moment terms much like those found in the P_N equations. To meet the goals of this work and drive the research and development of MCSA for application to light water reactor problems, a difficult nuclear fuel assembly criticality calculation was used in a set of numerical experiments. These calculations were enabled by incorporating MCSA as a solution scheme into the k-eigenvalue solver in the Exnihilo production neutronics code base at Oak Ridge National Laboratory.

When applying the new technique to the fuel assembly problem, it was initially found that MCSA could not converge the problem with basic Jacobi-based preconditioning. This was discovered to be due to the fact that the transport operator generated in the eigenvalue calculation was very ill-conditioned due to the large amount of neutron scattering in the light water moderator. The more scattering present in the system, the longer a random walk will take and thus a spectral radius approaching unity was observed. A simpler neutron diffusion problem was used to demonstrate the breakdown of MCSA when spectral radii this large are generated.

As a result of the breakdown observation, a suite of advanced preconditioning techniques was applied to MCSA for the fuel assembly problem in order to reduce the spectral radius to a level below where breakdown occurs. From the results of this analysis, ILUT preconditioning was chosen for subsequent investigations. Using this preconditioning, it was verified that

MCSA is indeed general enough to solve the asymmetric system generated by the SP_N equations. However, the explicit MCSA preconditioning strategy developed for this work generated very dense systems that consumed tremendous amounts of memory to store and compute time to generate. The memory problem was partially alleviated by applying the reduced domain approximation, however a significant memory overhead remained along with prohibitive time for construction.

Using the developed preconditioners and the reduced domain approximation, a set of SP_N calculations using up to 4 energy groups was enabled for the fuel assembly problem. To verify MCSA, the fuel assembly problem was solved with different energy groups using both MCSA and two production Krylov methods. MCSA was observed to produce the same scalar flux in all groups at all spatial locations and generate the same k-eigenvalue in the same number of eigenvalue iterations when used in conjuction with an eigenvalue solver.

For the same calculations, MCSA had qualitatively similar iterative performance to the production Krylov methods, showing improved performance over GMRES while a Conjugate Gradient-based method performed better using the same preconditioning. Improved performance over GMRES meets the goal of improving iterative performance to a certain extent but this was not the true for the Conjugate Gradient-based method. However, although the SP_N equations are asymmetric for multigroup calculations, they are symmetric at the block level and therefore we expect the Conjugate Gradient-based method to perform better as this structure can be more readily leveraged to improve performance than with the more general GMRES and MCSA methods. In terms of CPU time, MCSA was observed to perform $O(100)$ times slower than the Krylov methods due to both lack of optimization in the random walk sequence and the explicit preconditioning strategy.

6.2 Monte Carlo Synthetic Acceleration Solutions for Navier-Stokes Equations

This work presents the FANM method, a new nonlinear solution scheme based on an inexact Newton method. To meet the goals of this work the FANM method was characterized by applying it to the Navier-Stokes equations. This research was enabled by implementing the FANM method within the nonlinear solver sequence leveraged by the Drekar production multiphysics code base being developed at Sandia National Laboratories. In both convection and driven flow regimes we solved three difficult benchmark problems for the Navier-Stokes equations. Using the work in preconditioning from the research on the SP_N equations, it was found that the same preconditioning strategy could be used to achieve convergence of the linear models generated at each FANM iteration by applying an algebraic multigrid method.

For each benchmark problem, FANM solutions were verified against Newton-Krylov solutions leveraging GMRES as the linear solver. The FANM solutions were observed to be numerically identical to those generated by the Newton-Krylov method. In addition, the benchmark problems also served as a vehicle to compare the performance of FANM with the Newton-Krylov method. For the thermal convection cavity problem, FANM was observed to converge in fewer linear solver iterations than Newton-Krylov at all Rayleigh numbers tested when the same preconditioning was applied to both methods. This means that FANM demonstrated superior iterative performance for problems dominated by natural convection, meeting the goal of improved iterative performance in this case.

Iterative performance for the problems dominated by inertial driven flow varied depending on the situation. For the lid driven cavity problem, FANM converged in more linear solver iterations for 3 out of 4 cases. However, for each of these cases it was observed that the extra MCSA iterations were generated by a smaller forcing term at each Newton iteration when compared to the Newton-Krylov solver. Given that a smaller forcing term is equivalent to requesting convergence of the linear solver to a smaller residual, we expect these

extra iterations. For the lid driven cavity case where FANM converged in fewer iterations, it was observed that increasing the number of stochastic histories used at every MCSA iteration enabled convergence in fewer iterations, again meeting the goal of improved iterative performance.

The backward facing step problem at low Reynolds number gave better performance with FANM converging in fewer linear solver iterations. However, as the Reynolds number was increased so did the number of MCSA iterations required to converge the linear model at each FANM iteration. Unlike the lid driven cavity problem, this was discovered to occur due to the inability of MCSA to quickly converge the ill-conditioned linear model rather than the introduction of smaller forcing terms.

Timing performance for all benchmarks favored the Newton-Krylov solver with FANM observed to be $O(100)$ slower for the thermal convection cavity and lid driven cavity problems and $O(1,000)$ times for the backward facing step problem. For the first two cases, the timing differences were observed to be qualitatively the same as those observed for the SP_N performance analysis. Again, this comes from both lack of optimization of the Monte Carlo sequence and the introduction of explicit preconditioning. For the backward facing step problem, the ill-conditioning of the system adds the extra order of magnitude slow down.

6.3   Parallel Monte Carlo Synthetic Acceleration

A new parallel MCSA algorithm was developed for this work to meet the goal of demonstrating the improved scalability of MCSA on leadership-class hardware. It was found the MCSA can indeed be effectively parallelized using the multiple-set overlapping-domain decomposition algorithm borrowed from the reactor physics community. Using a neutron diffusion problem, the parallel algorithm was verified to produce the same results as two production Krylov methods.

The new algorithm was tested in a wide variety of parallel scaling studies on the Titan

Cray XK7 machine at the Oak Ridge Leadership Computing Facility. To test the algorithm at high levels of concurrency, up to 65,356 cores were used in strong scaling exercises and 131,072 cores used in weak scaling exercises using the neutron diffusion problem. In general, the new parallel MCSA algorithm was observed to produce better parallel scaling results when compared to a production GMRES and Conjugate Gradient method. We note here that these scaling studies should be reconsidered if arithmetic optimization of the code has been completed.

It was found that the leakage of histories from domain to domain in the parallel Monte Carlo algorithm could in fact be quantified analytically using the algebraic properties of the system. These relationships were then used to determine the amount of overlap one may require in the parallel algorithm to reduce communication costs and increase parallel efficiencies. Scaling studies showed that in the strong case overlap in small quantities on the order of the mean-free-path of a stochastic history in the simulation could boost parallel efficiencies by a few percent. However, it was found that this additional overlap was not effective in boosting strong scaling efficiencies. It was found that in general overlap was not very effective due to the fact that the parallel communication saved during the Monte Carlo transport sequence is simply deferred until after transport is complete when it manifests itself as an overlapping parallel vector reduction operation.

Applying multiple sets in the parallel algorithm was found to not enhance the weak scaling of the problem as an additional parallel overhead is introduced when the calculations from the set are combined in superposition. For the strong scaling case, improvements were not noted until after the strong scaling wall was hit. At this point, multiple sets were observed to increase parallel efficiencies from 38% to 58% at 16,384 cores. Perhaps more important here is the fact that although the parallel efficiency was reduced, multiple sets were observed to actually improve the time to solution. Unlike a traditional Krylov method that we might apply to solve a neutron transport problem, using MCSA means that we can actually make a physical copy of the problem on the machine and can combine separate Monte Carlo solutions

for each copy through superposition to enhance time to solution. Time to solution is then improved because fewer histories were run in each copy and therefore each MCSA iteration is faster or more global histories are computed and fewer MCSA iterations are required to converge.

Finally, given that overlap was not very constructive in boosting parallel efficiencies, it was postulated that very little domain-to-domain communication of histories was occurring in the first place and then subsequently verified using the analytic relationships for domain leakage. Using this idea, we implemented a subdomain Neumann-Ulam method with MCSA such that MCSA now takes the form of a stochastic realization of an additive Schwarz method. Scaling studies using this technique showed significant improvements in parallel scalability even when compared to the MCSA results when domain-to-domain communication was present, further enhancing the method and meeting the goal of improved scalability.

6.4   Future Work

Throughout this work, three salient issues were observed over all others. First, the performance of the MCSA implementation developed for this work was severely lacking in terms of time to solution when compared to production Krylov methods. In all cases, this difference was several orders of magnitude. Second, the preconditioning strategy developed by this work, although often successful in achieving convergence for difficult problems, creates many obstacles to a production implementation. These obstacles all primarily stem from the dense composite operators that are required to form the probabilities and weights for the Monte Carlo game. Third, perhaps the most restrictive and unattractive piece of MCSA as a whole is the simple fact that the spectral radius of the physics operator iteration matrix be less than one. This was demonstrated to prohibit convergence for cases where the preconditioning was considered aggressive and Krylov solvers exhibited excellent convergence properties. We will address each one of these problems in turn in this section and provide suggestions for

their solution.

6.4.1 Performance

When issues arising from preconditioning are not considered, there are two primary issues that can be resolved in the MCSA implementation developed by this work that will likely result in performance gains for serial computations. First, all random walks in the implementation have a state which changes as the random walk proceeds. These states are those given by Eq (2.12). For random walks that are traversing a domain which has been decomposed in a parallel environment, there are two sets of these states: one that represents the states over the entire global domain and one that represents them only over the local subdomain. Each state in the system gets a unique index in both of these sets that act as absolute coordinates in the random walk and permit the construction of the Monte Carlo estimates and other data needed for the solution.

A fundamental flaw of the implementation developed for this work is that those random walk states given by Eq (2.12) were formulated such that they were always represented using the indices from the global set. However, all data in the system (e.g. weights, probabilities, tallies, etc.) are stored such that they are accessed using the local indexing scheme. Because of this, each time a random walk wants to sample its current probability distribution function, get a weight for its transition, or add its estimate to a tally, a call must first be made to translate the current global state of the random walk into its local state[1]. What this then means is that we are performing orders of magnitude more operations during the Monte Carlo sequence than if the random walk sequence operated in the local index space rather than the global index space. Preliminary profiling of the implementation has shown that indeed a vast majority of the time in the Monte Carlo sequence is spent doing this index translation. Therefore, future work should perform the significant refactoring of the implementation required to achieve this.

---

[1]This is a look-up in a hash table.

A second mode of optimization to improve performance regards how discrete probability distribution functions are sampled in the implementation. At each transition in the random walk sequence, the discrete probability distribution function generated by the current row of the physics operator in which a random walk resides is sampled to get the next state in the sequence. This operation is also used when the right hand side of the system is sampled to acquire the starting state for each random walk in the problem through Eq (2.42). The current implementation uses the inverse transform method for sampling where the a random number is generated and the cumulative distribution function is queried with a binary search to find the next discrete state. This algorithm has $O(log(N))$ time complexity for sampling and $O(N)$ time complexity for construction. The alias sampling method is suggested instead as it produces $O(1)$ complexity for sampling and $O(N)$ time complexity for construction [97]. Sabelfeld outlines the use of this sampling technique in his Monte Carlo algorithms [54]. Profiling of the implementation shows that this improvement could also provide quality reductions in run time.

For the parallel MCSA algorithm, overall parallel scaling results indicated that the implementation was of good quality in both the strong and weak scaling cases. However, for the multiple set cases in the weak scaling analysis, it was noted that there was a growing parallel overhead as a function of core count. This was counter-intuitive in that the size of the parallel group over which the set reductions were occurring was fixed at all core counts and therefore we do not expect the addition of such an operation to increase parallel run times. It did, however, and therefore future research should explore why the implementation for multiple sets generated parallel overhead that increased with core count instead of remaining constant.

Nonlinear performance may also be improved by a closer relationship between MCSA and the Newton iteration. We saw in our research how the forcing term selected very tightly controls the convergence of the linear model in FANM. For MCSA, in addition to the residual tolerance that is dictated by this forcing term, convergence may also be controlled

by adjusting the number of stochastic histories computed at each MCSA iteration. As the nonlinear iteration evolves, we may find it useful to adjust the number of histories used at each MCSA iteration in the same way as we adjust the convergence tolerance of the linear model through the forcing term. Future research is suggested to analyze the effects of the number of stochastic histories on the convergence of the linear and nonlinear models and how this may be controlled by the forcing term or another parameter.

With these implementation improvements perhaps MCSA and FANM timing may approach that of production Krylov methods for equally conditioned problems. Next we discuss potential research in the area of preconditioning which may enable performance research for MCSA in the area of memory consumption.

6.4.2 Preconditioning

In general, preconditioning developments in this work enabled much of the desired research to be performed but also prevented some of it. Of primary concern is the large memory footprint induced by the explicit algebraic preconditioning strategy outlined in § 2.6.2.2. By preconditioning in this way, we were able to leverage modern algebraic preconditioning strategies used in current physics applications and enable solutions for both neutronics and fluid flow simulations. The downside is that in order to generate weights and probabilities with which to play the Monte Carlo game we must first invert each of the preconditioners which in many cases means applying their inverse over each row in the system and then perform matrix-matrix multiply operations to build the composite physics operator.

These operations were observed to substantially increase runtimes of MCSA and consume unacceptable amounts of memory, mostly due to the fact that inverting the preconditioners created dense matrices. Although a good fraction of the elements in each row of the composite operator could be eliminated through the reduced domain approximation developed by this work, memory costs still prevented higher fidelity simulations from being performed. In addition, the reduced domain approximation does not prevent the large run times incurred

for inverting the preconditioners. We therefore propose the following three developments in preconditioning for Monte Carlo methods:

Research and develop alternative sampling schemes for the general left/right preconditioned Monte Carlo method not relying on composite matrix generation. Developments that break away from matrix-matrix multiplications within the preconditioned solver framework improve scalability. This means avoiding the generation of the composite operator and instead playing the Monte Carlo game with weights and probabilities formed by considering the original linear operator and the preconditioners individually. This individual consideration may come from an alternative algebraic formulation of the general preconditioned MCSA method in Eq (2.76) or from an alternative random sampling strategy for the Monte Carlo game.

Develop Monte Carlo variance reduction based preconditioning strategies that do not rely on an algebraic preconditioner. Constructing the complete inverse of the preconditioner is the core time and scalability constraint when modern algebraic preconditioners are used. Building the inverse for preconditioners where a sparsity pattern is not enforced typically results in a dense matrix that destroys scalability for domain decomposed parallel computations. Alleviating both of these issues by stochastic preconditioning methods should be studied. Decades of research and development in Monte Carlo variance reduction for particle transport [96] may be leveraged to form similar strategies for linear systems. In the same way that this work has been able to adapt modern particle transport strategies for parallelism and apply them to linear systems, the same strategy may possibly be applied to variance reduction techniques to improve MCSA convergence by modifying the weights and probabilities of the Monte Carlo game as an effective means of preconditioning.

Study physics or PDE-based preconditioners for linear systems that produce a reduced-order model of the original system to which the Monte Carlo method

may be applied. As the Monte Carlo method serves to construct the solution correction vector in the MCSA method, the Monte Carlo method may be applied to a reduced-order physics or PDE-based system that captures the essence of the original system and still allows for acceleration of the iterative procedure. By reducing the order of the system, we are effectively generating a Monte Carlo problem within MCSA in which the linear operator is either more sparse, has a better-conditioned eigenvalue spectrum, or both. The reduced domain approximation has shown that a purely algebraic strategy for reducing the order of the Monte Carlo problem can result in improved overall timing performance due to increased sparsity at the cost of iterative performance as a result of loss of information. A more well informed strategy for order reduction via either an intelligent simplification of the PDEs that describe the system or a simplification of the physics involved may prove to be a more effective strategy.

6.4.3   Breaking Away from $\rho(H) < 1$

All numerical methods for solving linear problems require quality preconditioning. Even a Krylov method may be effectively useful without it. However, these methods typically converge eventually whereas quality preconditioning may not be enough to guarantee convergence of MCSA. We saw in our work that in many cases very aggressive preconditioning was not enough to condition the eigenvalues of the system into a regime where MCSA would apply. The limitation that the spectral radius of the physics operator iteration matrix must be less than one is by far the most prohibitive component of MCSA. The fact that the Monte Carlo sequence is based on the Richardson iteration means that without sufficient preconditioning, even if this condition is achieved convergence may be incredibly slow. Therefore, we propose two elements of future work that aim to move away from this restriction, both fundamentally based on sampling a sequence not based on the Neumann series.

6.4.3.1 Monte Carlo Methods of the Second Degree

Iterative methods of the nth degree produce solutions at each iteration of the following form:

$$\mathbf{x}^{k+1} = F(\mathbf{A}, \mathbf{b}, \mathbf{x}^k, \mathbf{x}^{k-1}, \ldots, \mathbf{x}^{k-n+1}) \,, \tag{6.1}$$

where $\mathbf{A}$ is the linear operator and $\mathbf{b}$ is the right hand side as defined by Eq (2.1). Richardson's iteration is an iterative method of the first degree such that $\mathbf{x}^{k+1} = F(\mathbf{A}, \mathbf{b}, \mathbf{x}^k)$. To move the Monte Carlo method away from the spectral radius limitation we therefore we seek higher order methods as outlined by Hallett [70] that have guaranteed convergence at all eigenvalue spectra. In his work, Hallett builds a second order method such that $\mathbf{x}^{k+1} = F(\mathbf{A}, \mathbf{b}, \mathbf{x}^k, \mathbf{x}^{k-1})$. Such a method results from mapping the original Richardson iteration onto a different set of eigenvalues in the complex plane that have a spectral radius less than one, thus guaranteeing convergence. Derived as expansions of the iteration sequence in Chebyshev polynomials, Hallett arrives at simple formulation for the second degree method that requires knowledge of the bounding curve in the complex plane of the eigenvalue spectra for good convergence properties.

As it turns out, Sabelfeld has already applied such a technique to the Monte Carlo method but arrived at the same conclusions in a different way [54][2] with this work effectively re-developed later by Dimov without citation of Sabelfeld [3, 7]. In his work, Sabelfeld formulated the random walk sequence by instead building the Neumann series from the *resolvent* of the operator. The resolvent operator is defined as that which spans all of the complex plane but has singularities at the points that are eigenvalues of the original operator. By building the Monte Carlo sequence from this operator, Sabelfeld arrived at a Monte Carlo method which in fact was equivalent to a fixed point method of the second degree and utilized effectively the same spectral mapping procedure as Hallett. Just like the deterministic case, some knowledge of the eigenvalue spectrum of the system was required to ensure convergence.

---

[2]Although the technique is outlined in this document, Sabelfeld cites his previous work in this area in 1982.

These methods should be researched and developed further in the context of MCSA as a potential means of always guaranteeing convergence of the algorithm regardless of the eigenvalue spectrum.

6.4.3.2 Stochastic Projection Methods

As a final means of improvement we consider stochastic projection methods as developed by Sabelfeld [95]. In his work, Sabelfeld claims his method is 'beyond Markov chains and von Neumann-Ulam scheme'. To a certain extent this is true; his method is based on a projection method and should always converge. In his work, he utilizes a Kaczmarz iteration:

$$\mathbf{x}^{k+1} = \mathbf{x}^k + \lambda_k \frac{b_i - \langle \mathbf{a}_i \mathbf{x}^k \rangle}{||\mathbf{a}_i||} \mathbf{a}_i \, , \tag{6.2}$$

where $\mathbf{a}_i$ is the ith row vector of the operator and λ_k is a relaxation parameter.

The stochastic nature of the algorithm comes from effectively modifying the iteration sequence such that the value of i is now selected at random. This is interesting but arguably does not serve our purposes at well. We have an interest in a fully stochastic process like a random walk sequence because of its potential benefits in terms of resiliency and the ability to use superposition to combine results from replicated problems to enhance performance. In Sabelfeld's work, the randomness is used to select which deterministic iteration step will be performed and does not meet either of these requirements. However, that does not mean there is nothing to learn from this work. If one writes Eq 6.2 in terms of applications of projection operators as that outlined in [98] we see that this actually takes a similar form as the Neumann series and could therefore be used in a random walk sequence. In addition, perhaps the above algorithm can be modified such that the randomness of the projection sequence permits improved results via the superposition principle. Research studying random walks based on projection sequences is therefore suggested as a means of moving beyond the spectral radius limitation.

6.5 Closing Remarks

This work was performed with the goal of investigating new solution techniques based on Monte Carlo Synthetic Acceleration and how they perform when applied to real problems in nuclear engineering. These methods aim to make improvements over conventional methods when looking towards the advanced computer architectures of the near future. Parallelism at high levels of concurrency, a potential reduction in memory footprint, and a natural element of resiliency deriving from the stochastic nature of the algorithm motivated us to research their strengths and weaknesses and develop solutions to further their applicability.

Before this work was performed, MCSA had yet to be applied to the neutron transport problem, asymmetric systems, and nonlinear problems including fluid flow systems. Techniques were developed by this work that enabled solutions for all of these problems using MCSA. In many cases, it was found that the iterative performance of the MCSA-based methods were superior to that of conventional solution techniques based on Krylov methods. Furthermore, with improved implementation performance, future problems may be solved in less time and more efficiently using MCSA due to this demonstrated improved iterative performance.

When this work began, the Neumann-Ulam sequence and MCSA in general had yet to be parallelized in a domain decomposed framework. This research developed a new parallel algorithm based on Monte Carlo particle transport that permitted MCSA solutions to be generated on $O(100,000)$ cores on a leadership class computing platform. The new algorithm was also demonstrated to achieve better strong and weak scaling than conventional Krylov methods at high levels of concurrency. If future work can improve the time to solution using MCSA through optimization, then this improved scaling demonstrated by the algorithm can potentially improve the time to solution for the engineer and more efficiently leverage high performance computing hardware for analysis.

With this work, a new foundation for Monte Carlo Synthetic Acceleration methods has

been laid with new theory, algorithms, and numerical experiments that demonstrate both their potential to make great contributions to nuclear engineering calculations in the future and where the research must go in order to achieve this. By advancing these techniques, we look forward to future work that will enable the improved design and analysis of nuclear systems.

Appendix A

Conventional Solution Methods for Linear Systems

The discretization of partial differential equations (*PDEs*) through common methods such as finite differences [63], finite volumes [62], and finite elements [38] ultimately generates sets of coupled equations in the form of matrix problems. In many cases, these matrices are sparse, meaning that the vast majority of their constituent elements are zero. This sparsity is due to the fact that the influence of a particular grid element only expands as far as a few of its nearest neighbors depending on the order of discretization used and therefore coupling among variables in a particular discrete equation in the system leads to a few non-zero entries. Because of the natural occurrence of sparse matrices in common numerical methods many iterative techniques have been developed to solve such systems. We discuss here conventional stationary and projection methods for solving sparse systems to provide the necessary background for the remainder of this work. Details on the parallelization of conventional methods are discussed.[1]

A.1   Stationary Methods

Stationary methods for linear systems arise from splitting the operator in Eq (2.1):

$$\mathbf{A} = \mathbf{M} - \mathbf{N}\,, \tag{A.1}$$

[1]The contents of this appendix, particularly those sections relating to projection methods and matrix analysis, are heavily based on Saad's text [56].

where the choice of $\mathbf{M}$ and $\mathbf{N}$ will be dictated by the particular method chosen. Using this split definition of the operator we can then write:

$$\mathbf{Mx} - \mathbf{Nx} = \mathbf{b} \,. \tag{A.2}$$

By rearranging, we can generate a form more useful for analysis:

$$\mathbf{x} = \mathbf{Hx} + \mathbf{c} \,, \tag{A.3}$$

where $\mathbf{H} = \mathbf{M}^{-1}\mathbf{N}$ is defined as the *iteration matrix* and $\mathbf{c} = \mathbf{M}^{-1}\mathbf{b}$. With the solution vector on both the left and right hand sides, an iterative method can then be formed:

$$\mathbf{x}^{k+1} = \mathbf{Hx}^k + \mathbf{c} \,, \tag{A.4}$$

with $k \in \mathbb{Z}^+$ defined as the *iteration index*. In general, we will define methods in the form of Eq (A.4) as *stationary methods*. Given this, we can then generate a few statements regarding the convergence of such stationary methods. Defining $\mathbf{e}^k = \mathbf{u}^k - \mathbf{u}$ as the solution error at the kth iterate, we can subtract Eq (A.3) from Eq (A.4) to arrive at an error form of the linear problem:

$$\mathbf{e}^{k+1} = \mathbf{He}^k \,. \tag{A.5}$$

Our error after k iterations is then:

$$\mathbf{e}^k = \mathbf{H}^k \mathbf{e}^0 \,. \tag{A.6}$$

In other words, successive application of the iteration matrix is the mechanism driving down the error in a stationary method. We can then place restrictions on the iteration matrix by using the tools developed in § (2.1). By assuming $\mathbf{H}$ is diagonalizable[2] [56], we then have:

$$\mathbf{e}^k = \mathbf{R\Lambda}^k\mathbf{R}^{-1}\mathbf{e}^0 \,, \tag{A.7}$$

---

[2]We may generalize this to non-diagonalizable matrices with the Jordan canonical form of $\mathbf{H}$.

where $\mathbf{\Lambda}$ contains the Eigenvalues of $\mathbf{H}$ on its diagonal and the columns of $\mathbf{R}$ contain the Eigenvectors of $\mathbf{H}$. Computing the 2-norm of the above form then gives:

$$||\mathbf{e}^k||_2 \leq ||\mathbf{\Lambda}^k||_2 \; ||\mathbf{R}||_2 \; ||\mathbf{R}^{-1}||_2 \; ||\mathbf{e}^0||_2 \,, \tag{A.8}$$

which gives:

$$||\mathbf{e}^k||_2 \leq \rho(\mathbf{H})^k \kappa(\mathbf{R}) ||\mathbf{e}^0||_2 \,. \tag{A.9}$$

For iteration matrices where the Eigenvectors are orthogonal, $\kappa(\mathbf{R}) = 1$ and the error bound reduces to:

$$||\mathbf{e}^k||_2 \leq \rho(\mathbf{H})^k ||\mathbf{e}^0||_2 \,. \tag{A.10}$$

We can now restrict $\mathbf{H}$ by asserting that $\rho(\mathbf{H}) < 1$ for a stationary method to converge such that k applications of the iteration matrix will not cause the error to grow in Eq (A.10).

A.2   Projection Methods

Among the most common iterative methods used in scientific computing today for sparse systems are of a broad class known as *projection methods*. These methods not only provide access to more powerful means of reaching a solution, but also a powerful means of encapsulating the majority of common iterative methods including the stationary methods just discussed in a common mathematical framework. All projection methods are built around a core structure where the solution to Eq (2.1) is extracted from a *search subspace* $\mathcal{K}$ and bound by a *constraint subspace* $\mathcal{L}$ that will vary in definition depending on the iterative method selected. We build the approximate solution $\tilde{\mathbf{x}}$ by starting with an initial guess $\mathbf{x}_0$ and extracting a correction $\boldsymbol{\delta}$ from $\mathcal{K}$ such that:

$$\tilde{\mathbf{x}} = \mathbf{x}_0 + \boldsymbol{\delta}, \; \boldsymbol{\delta} \in \mathcal{K} \,. \tag{A.11}$$
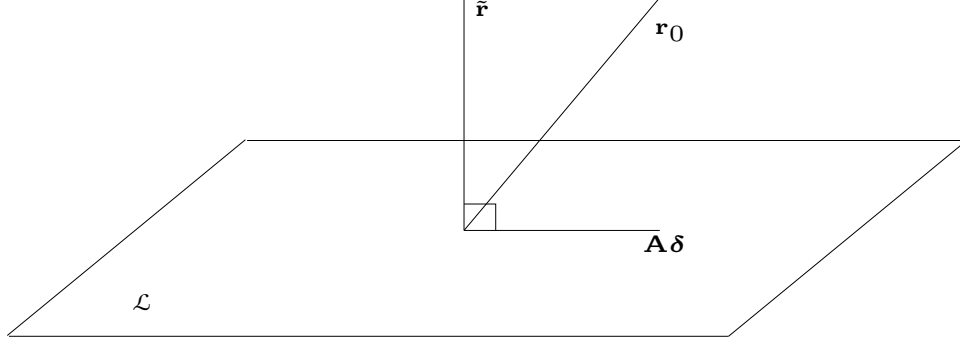
Figure A.1: **Orthogonality constraint of the new residual with respect to $\mathcal{L}$.** *By projecting $\mathbf{r}_0$ onto the constraint subspace, we minimize the new residual by removing those components.*

We bound this correction by asserting that the new residual, $\tilde{\mathbf{r}}$, be orthogonal to $\mathcal{L}$:

$$\langle \tilde{\mathbf{r}}, \mathbf{w} \rangle = 0, \ \forall \mathbf{w} \in \mathcal{L} \ . \tag{A.12}$$

We can generate a more physical and geometric-based understanding of these constraints by writing the new residual as $\tilde{\mathbf{r}} = \mathbf{r}_0 - \mathbf{A}\boldsymbol{\delta}$ and again asserting the residual must be orthogonal to $\mathcal{L}$. If $\tilde{\mathbf{r}}$ is to be orthogonal to $\mathcal{L}$, then $\mathbf{A}\boldsymbol{\delta}$ must be the projection of $\mathbf{r}_0$ onto the subspace $\mathcal{L}$ that eliminates the components of the residual that exist in $\mathcal{L}$. This situation is geometrically presented in Figure A.1.

From Figure A.1 we then note that the following geometric condition must hold:

$$||\tilde{\mathbf{r}}||_2 \leq ||\mathbf{r}_0||_2, \ \forall \mathbf{r}_0 \in \mathbb{R}^N \ , \tag{A.13}$$

meaning that the residual of the system will always be *minimized* with respect to the constraints. Given this minimization condition for the residual, we can form the outline of an iterative projection method. Consider a matrix $\mathbf{V}$ to form a basis of $\mathcal{K}$ and a matrix $\mathbf{W}$ to form a basis of $\mathcal{L}$. As $\boldsymbol{\delta} \in \mathcal{K}$ by definition in Eq (A.11), then $\boldsymbol{\delta}$ can instead be rewritten as:

$$\boldsymbol{\delta} = \mathbf{V}\mathbf{y}, \ \forall \mathbf{y} \in \mathbb{R}^N : \tag{A.14}$$

where $\mathbf{V}$ *projects* $\mathbf{y}$ onto $\mathcal{K}$. From the orthogonality constraint in Eq (A.12) it then follows that:

$$\mathbf{y} = (\mathbf{W}^T \mathbf{A} \mathbf{V})^{-1} \mathbf{W}^T \mathbf{r}_0 \,, \tag{A.15}$$

where here the projection onto $\mathcal{K}$ is constrained by the projection onto $\mathcal{L}$. Knowing this, we can then outline the following iteration scheme for a projection method:

$$\mathbf{r}^k = \mathbf{b} - \mathbf{A}\mathbf{x}^k \,, \tag{A.16a}$$

$$\mathbf{y}^k = (\mathbf{W}^T \mathbf{A} \mathbf{V})^{-1} \mathbf{W}^T \mathbf{r}^k \,, \tag{A.16b}$$

$$\mathbf{x}^{k+1} = \mathbf{x}^k + \mathbf{V}\mathbf{y}^k \,, \tag{A.16c}$$

where $\mathbf{V}$ and $\mathbf{W}$ are generated from the definitions of $\mathcal{K}$ and $\mathcal{L}$ and are updated prior to each iteration.

From an iteration standpoint, as we choose $\boldsymbol{\delta}$ from $\mathcal{K}$ and constrain it with $\mathcal{L}$, each iteration performs a projection that systematically annihilates the components of the residual that exists in $\mathcal{L}$. This then means that if our convergence criteria for an iterative method is bound to the residual of the system, then Eq (A.13) tells us that each projection step guarantees us that the norm of the new residual will never be worse than that of the previous step and will typically move us towards convergence. Depending on the qualities of the system in Eq (2.1), the selection of the subspaces $\mathcal{K}$ and $\mathcal{L}$ can serve to both guarantee convergence and optimize the rate at which the residual is decreased.

A.2.1 Krylov Subspace Methods

Among the most common projection techniques used in practice are a class of methods known as *Krylov subspace methods*. Here, the search subspace is defined as the *Krylov subspace*:

$$\mathcal{K}_m(\mathbf{A}, \mathbf{r}_0) = span\{\mathbf{r}_0, \mathbf{A}\mathbf{r}_0, \mathbf{A}^2\mathbf{r}_0, \ldots, \mathbf{A}^{m-1}\mathbf{r}_0\} \,, \tag{A.17}$$

Algorithm A.1 GMRES Iteration

$\mathbf{r}_0 := \mathbf{b} - \mathbf{A}\mathbf{x}_0$
$\beta := ||\mathbf{r}_0||_2$
$\mathbf{v}_1 := \mathbf{r}_0/\beta$ ▷ Create the orthonormal basis for the Krylov subspace
for $j = 1, 2, \cdots, m$ **do**
     $h_{ij} \leftarrow \langle w_j, v_j \rangle$
     $w_j \leftarrow w_j - h_{ij}v_i$
end for
$h_{j+1,j} \leftarrow ||w_j||_2$
$v_{j+1} \leftarrow w_j/h_{j+1,j}$ ▷ Apply the orthogonality constraints
$\mathbf{y}_m \leftarrow argmin_y||\beta\mathbf{e}_1 - \mathbf{H}_m \, \mathbf{y}||_2$
$\mathbf{x}_m \leftarrow \mathbf{x}_0 + \mathbf{V_m}\mathbf{y}_m$

---

where m denotes the dimensionality of the subspace. In order to accommodate a more general structure for the operator in Eq (2.1), we often choose an *oblique* projection method where $\mathcal{K} \neq \mathcal{L}$. If we choose $\mathcal{L} = \mathbf{A}\mathcal{K}_m(\mathbf{A}, \mathbf{r}_0)$, then we are ultimately solving the normal system $\mathbf{A}^T\mathbf{A}\mathbf{x} = \mathbf{A}^T\mathbf{b}$ where $\mathbf{A}^T\mathbf{A}$ will be symmetric positive definite if $\mathbf{A}$ is nonsingular, thereby expanding the range of operators over which these methods are valid. This choice of constraint subspace also then gives us the result via Eq (A.12) that the residual is minimized for all $\boldsymbol{\delta} \in \mathcal{K}$, forming the basis for the *generalized minimum residual method* (GMRES) [64].

Choosing GMRES as our model Krylov method, we are first tasked with finding a projector onto the subspace. We seek an orthonormal basis for $\mathcal{K}_m(\mathbf{A}, \mathbf{r}_0)$ by an orthogonalization procedure that is commonly based on, but not limited to, the *Arnoldi* recurrence relation. The Arnoldi procedure will generate an orthonormal basis, $\mathbf{V}_m \in \mathbb{R}^{N \times m}$, via a variant of the Gram-Schmidt procedure that re-applies the operator for each consecutive vector, thus forming a basis that spans the subspace in Eq (A.17). Due to its equivalent dimensionality, m, to that of the subspace, we will refer to such recurrence relations as *long recurrence relations.* Those orthogonal projection procedures that have a dimensionality less than m will be referred to as *short recurrence relations.* Once $\mathbf{V}_m$ is found, per the constraint subspace definition it then follows that its basis is defined as $\mathbf{W}_m = \mathbf{A}\mathbf{V}_m$. Knowing the projections onto the search and constraint subspaces, the GMRES iteration may be formulated as follows:

We note here several properties of this formulation and how they may facilitate or hinder the solution of large-scale, sparse linear problems, also noting that these properties are common among many Krylov methods. First, from a memory perspective GMRES is efficient in that the operator $\mathbf{A}$ need not be explicitly stored. Rather, only the ability to compute the action of that operator on a vector of valid size is required. However, these savings in memory are balanced by the fact that the long recurrence relations used in the Arnoldi procedure require all vectors that span the Krylov space to be stored. If the size of these vectors becomes prohibitive, the Arnoldi procedure can be restarted at the cost of losing information in the orthogonalization process, creating the potential to generate new search directions that are not orthogonal to all previous search directions (and therefore less than optimal). From an implementation perspective, because the operator is not required to be formed, GMRES is significantly more flexible in its usage in that there are many instances where various processes serve to provide the action of that operator (e.g. radiation transport sweeps [89]) that normally may not be amenable to its full construction. In addition, the minimization problem is a straight-forward least-squares problem where $\mathbf{H}$ is an upper-Hessenberg matrix.

A.3 Parallel Projection Methods

Modern parallel implementations of projection methods on distributed memory architectures rely heavily on capabilities provided by general linear algebra frameworks. For methods like GMRES, this arises from the fact that Krylov methods require only a handful of operation types in their implementation that can be efficiently programmed on these architectures. Per Saad's text [56] and as noted in Algorithm A.1, these operations are preconditioning, matrix-vector multiplications, vector updates, and inner products. For the last three items, linear algebra libraries such as PETSc [76] and Trilinos [77] provide efficient parallel implementations for these operations. Depending on the type of preconditioning used, efficient parallel implementations may also be available for those operations. Due to their prevalence in

modern numerical methods, parallel formulations these operations have warranted intense study [42]. In all cases, a series of scatter/gather operations are required such that global communication operations must occur. Although the relative performance of such operations is bound to the implementation, asymptotically performance should be the same across all implementations.

We will look at the three primary parallel matrix/vector operations as preconditioning is not an immediate requirement for implementing the algorithms. We note here that variants are available that reduce the number of global communications required (consider [44] as an example of reducing global operation counts using a different orthogonalization procedure than Arnoldi), however, we will only consider the basic algorithms here as this handful of operations can be generalized to fit more complicated algorithms. In all of these cases, we assume a general matrix/vector formulation that is distributed in parallel such that both local and global knowledge of their decomposition is available on request. Furthermore, it is assumed that these objects are partitioned in such a way that the parallel formulation of the operator and vectors in Eq (2.1) will be such that each parallel process contains only a subset of the global problem and that subset forms a local set of complete equations. The form of this partitioning is problem dependent and often has a geometric or graph-based aspect to its construction in order to optimize communication patterns. Libraries such as Zoltan [16], provide implementations of such algorithms.

A.3.1   Parallel Vector Update

Parallel vector update operations arise from the construction of the orthonormal basis and the application of the correction generated by the constraints to the solution vector. Vector update operations are embarrassingly parallel in that they require no communication operations to be successfully completed; all data operated on is local. These operations are globally of the form:

$$\mathbf{y}[n] \leftarrow \mathbf{y}[n] + a * \mathbf{x}[n], \ \forall n \in [1, N_g] \, , \tag{A.18}$$

and locally of the form:

$$\mathbf{y}[n] \leftarrow \mathbf{y}[n] + a * \mathbf{x}[n], \ \forall n \in [1, N_l] \, , \tag{A.19}$$

where $\mathbf{y}$ and $\mathbf{x}$ are vectors of global size N_g, local size N_l, and $a \in \mathbb{R}^N$. In order to avoid communication, the vectors $\mathbf{y}$ and $\mathbf{x}$ must have the same parallel decomposition where each parallel process owns the same pieces of each vector.

A.3.2 Parallel Vector Product

Vector product operations are used in several instances during a Krylov iteration including vector norm computations and the orthogonalization procedure. By definition, the vector product is a global operation that effectively collapses a set of vectors to a single value. Therefore, we cannot eliminate all global communications. Instead, vector product operations are formulated as *global reduction operations* that are efficiently supported by modern message passing libraries. For the dot product of two vectors $\mathbf{y}$ and $\mathbf{x}$, a single reduction is required such that:

$$d_l = \mathbf{y}_l \cdot \mathbf{x}_l, \ d_g = \sum_p d_l \, , \tag{A.20}$$

where the l subscript denotes a local quantity, d_l is the local vector dot product, and d_g is the global dot product generated by summing the local dot products over all p processes. Parallel norm operations can be conducted with the same single reduction. Consider the infinity norm operation:

$$||x||_{\infty,l} = \max_n \mathbf{y}[n], \ \forall n \in [1, N_l] \tag{A.21a}$$

$$||x||_{\infty,g} = \max_p ||x||_{\infty,l} \, . \tag{A.21b}$$

In this form, the local infinity norm is computed over the local piece of the vector. The reduction operation is then formed over all p processes such that the global max of the vector

Figure A.2: **Sparse matrix-vector multiply Ax = y operation partitioned on 3 processors.** *Each process owns a set of equations that correlates to its physical domain.*

is computed and distributed to all processes.

A.3.3   Parallel Matrix-Vector Multiplications

We finally consider parallel matrix-vector multiplication operations using sparse matrices in a compressed storage format by considering Saad's outline as well as the more formal work of Tuminaro [42]. For these operations, more complex communication patterns will be required given that the entire global vector is required in order to compute a single element of the local product vector. Fortunately, the vast majority of the global vector components will be multiplied by zero due to the sparsity of the matrix and therefore much of the vector can be neglected. Instead we only require data from a handful of other processes that can be acquired through asynchronous/synchronous communications. Consider th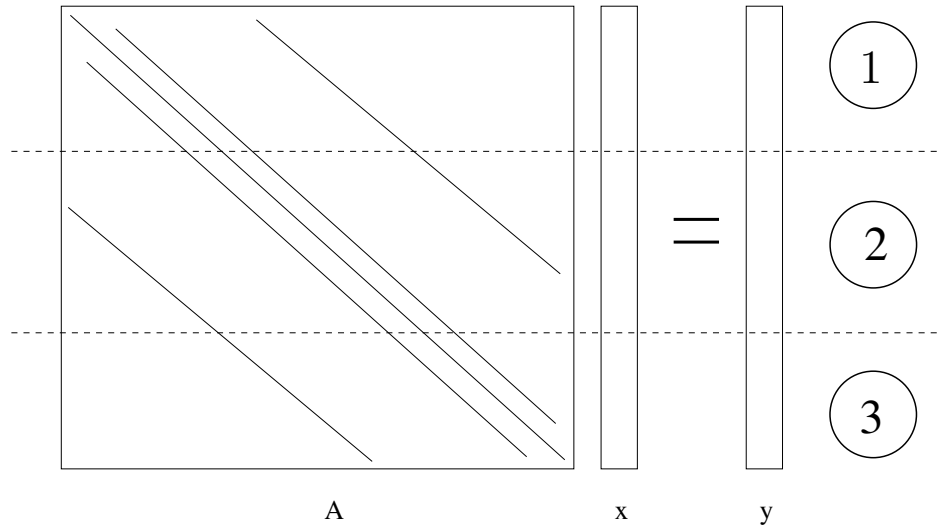e sparse matrix-vector multiply in Figure A.2 that is partitioned on 3 processors. Each process owns a set of equations that correlate to the physical domain of which it has ownership. We can break down the equations owned by each process in order to devise an efficient scheme for the multiplication. Consider the portion of the matrix-vector multiply problem owned by process
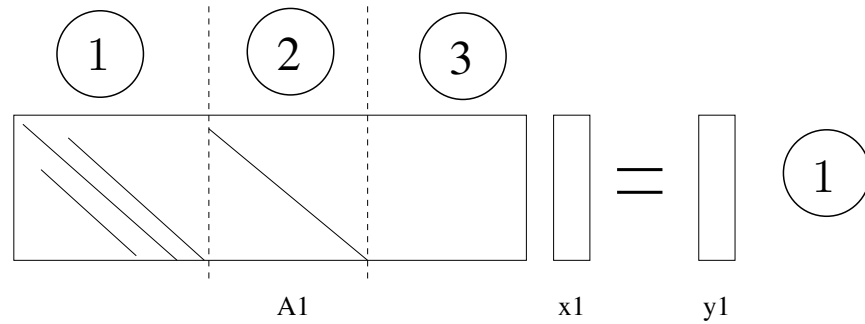
Figure A.3: **Components of sparse matrix-vector multiply operation owned by process 1.** *The numbers above the matrix columns indicate the process that owns the piece of the global vector they are acting on. In order to compute its local components of the matrix-vector product, process 1 needs its matrix elements along with all elements of the global vector owned by processes 2 and 3. The piece of the matrix shown is $\mathbf{A}_1$ and it is acting locally on $\mathbf{x}_1$ to compute the local piece of the product, $\mathbf{y}_1$.*

1 in Figure A.2. As shown in Figure A.3, the components of the matrix will be multiplied by pieces of the vector that are owned by all processors. For those pieces of the matrix that are owned by process 1 that act on the vector owned by process 1, we do these multiplications first as no communication is required. Next, process 1 gathers the components of the global vector owned by the other two processes that it requires to complete its part of the vector product. For this example, the components of matrix owned by process 1 that will operate on the global vector components owned by process 3 are zero, and therefore no vector elements are required to be scattered from process 3 to process 1. Those matrix elements owned by process 1 that will act on the piece of the vector owned by process 2 are not all non-zero, and therefore we must gather the entire process 2 vector components onto process 1 to complete the multiplication. Conversely, processes 2 and 3 must scatter their vector components that are required by other processes (such as process 1) in order to complete their pieces of the product. This then implies that these domain connections for proper gather and scatter combinations must be constructed a priori. These data structures are typically generated by a data partitioning library. Mathematically, if we are performing a global matrix-vector multiply of the form $\mathbf{A}\mathbf{x} = \mathbf{y}$, then for this example on process 1 we have a sequence of local

matrix-vector multiplications:n $\mathbf{A}_1\mathbf{x}_1 + \mathbf{A}_1\mathbf{x}_2 = \mathbf{y}_1$, with the subscripts provided by notation in Figure A.3. Here, some of the data is intrinsically local, and some must be gathered from other processes using the partitioning data structures.

A.3.4   Parallel Performance Implications for Krylov Methods

Knowing the parallel characteristics of the key operations we must perform in order to implement Krylov methods, we can make a few statements about parallel performance and implications for operation on machines of increasing size. Reconsider the matrix and vector operations required to implement Algorithm A.1. For very large distributed machines, the global reduction operations required at several levels of Krylov algorithms stand to reduce scalability and performance. In the case of GMRES, these reductions include vector norm operations and the inner products required for basis orthogonalization. Furthermore, communication between adjacent domains in matrix-vector multiply operations may also cause a bottleneck as the number of domains used in a simulation grows and the number of processors participating in the gather/scatter sequence requires a large communication bandwidth. The end result is that global data must be collected and communicated. For scaling improvement, we seek a reduction in these types of operations. In addition, these issues become more prominent as the Krylov iterations progress, causing the Krylov subspace to grow and the total number of operations needed to orthogonalize that subspace to increase.

As an example of these performance implications in practice, in a 2001 work, Gropp and colleagues presented results on fluid dynamic simulations that heavily leveraged Krylov methods in their solution schemes [84]. In this follow-on to their 1997 Bell Prize-winning work, part of their analysis included identifying parallel scalability bottlenecks generated by solver implementations in a strong scaling exercise where the number of processors was increased with respect to a fixed global problem size. Gropp's observations show that for their particular hardware, a distributed memory machine similar to modern architectures, that global reduction operations did not impede scalability, meaning that the global reduction

operation occupied approximately the same percentage of compute time independent of the number of processors used. Rather, it was the gather/scatter operations required to communicate data to neighboring processors that reduced performance with an increasing percentage of compute time consumed by these operations as processor count was increased. Furthermore, it was noted that this reduction in scaling was a product of poor algorithmic strong scaling rather than hardware or implementation related issues as the algorithm requires more data to be scattered/gathered as the number of processors and therefore computational domains increased. In the case of a weak scaling exercise, we would instead expect this percentage to exhibit a more desirable behavior of remaining constant for gather/scatter operations as problem size would be scaled with the number of processors.

Appendix B

Derivation of the Multigroup SP_N Equations

In the text, we formulated the SP_N equations for a single neutron energy. To expand these equations for multiple energies, we start by stating the multigroup neutron transport equation for a single dimension in planar geometry:

$$\mu \frac{\partial}{\partial x} \psi^g(x, \mu) + \sigma^g(x)\psi^g(x, \mu) =$$

$$\sum_{g'=0}^{G} \int \sigma_s^{gg'}(x, \hat{\Omega}' \to \hat{\Omega})\psi^{g'}(x, \hat{\Omega}')d\Omega' + \frac{q^g(x)}{4\pi} , \quad \text{(B.1)}$$

where g denotes the group index of 0 to G groups, $G = N_g - 1$, and the integration of the scattering emission term over energy has been replaced by a discrete summation. For scattering, $\sigma_s^{gg'}$ provides the probability of scattering at a particular angle from group g to g'. The result is an equation nearly identical in form to Eq (3.2) where now instead of forming the SP_N equations for a single energy group, we form them for each of the energy groups with group coupling occurring through the scattering term. The multigroup P_N equations are then:

$$\frac{1}{2n+1} \frac{\partial}{\partial x}\left[(n+1)\phi_{n+1}^g + n\phi_{n-1}^g\right] + \sum_{g'}(\sigma^g \delta_{gg'} - \sigma_{sn}^{gg'})\phi_n^g = q\delta_{n0} , \quad \text{(B.2)}$$

for $n = 0, 1, \ldots, N$ where the flux and scattering moments are defined in a group. We observe that a $N_g \times N_g$ scattering matrix is formed:

$$\mathbf{\Sigma}_n = \sum_{g'}(\sigma^g \delta_{gg'} - \sigma_{sn}^{gg'}) , \quad \text{(B.3)}$$

and when expanded gives:

$$\mathbf{\Sigma}_n = \begin{bmatrix} (\sigma^0 - \sigma_{sn}^{00}) & -\sigma_{sn}^{01} & \cdots & -\sigma_{sn}^{0G} \\ & & & \\ -\sigma_{sn}^{10} & (\sigma^1 - \sigma_{sn}^{11}) & \cdots & -\sigma_{sn}^{1G} \\ & & & \\ \vdots & \vdots & \ddots & \vdots \\ & & & \\ -\sigma_{sn}^{G0} & -\sigma_{sn}^{G1} & \cdots & (\sigma^G - \sigma_{sn}^{GG}) \end{bmatrix} . \tag{B.4}$$

It is also useful to combine the group flux moments and sources into a single vector for more compact notation:

$$\mathbf{\Phi_n} = (\phi_n^0 \ \phi_n^1 \ \cdots \phi_n^G)^T \,, \tag{B.5}$$

$$\mathbf{q} = (q^0 \ q^1 \ \cdots q^G)^T \,. \tag{B.6}$$

Next, we apply the SP_N approximation to Eq (B.2) in identical fashion to the monoenergetic case. This gives:

$$-\nabla \cdot \left[\frac{n}{2n+1} \mathbf{\Sigma_{n-1}}^{-1} \nabla \left(\frac{n-1}{2n-1} \mathbf{\Phi_{n-2}} + \frac{n}{2n-1} \mathbf{\Phi_n} \right) \right.$$
$$\left. + \frac{n+1}{2n+1} \mathbf{\Sigma_{n+1}}^{-1} \nabla \left(\frac{n+1}{2n+3} \mathbf{\Phi_n} + \frac{n+2}{2n+3} \mathbf{\Phi_{n+2}} \right) \right]$$
$$+ \mathbf{\Sigma_n} \mathbf{\Phi_n} = \mathbf{q} \delta_{n0} \qquad n = 0, 2, 4, \cdots, N \,. \tag{B.7}$$

This adds more complexity than the monoenergetic formulation in that all unknowns in this group of equations are now vector quantities and scattering relationships are contained in matrices rather than a scalar quantity. Because of this, the same sequence of variable changes

and algebra can be used to build a set of matrix equations, this time in a block formulation:

$$-\nabla \cdot \mathbb{D}_n \nabla \mathbb{U}_n + \sum_{m=1}^{4} \mathbb{A}_{nm} \mathbb{U}_m = \mathbb{Q}_n \,, \tag{B.8}$$

where the definition of all quantities are the same with internal scalar values replaced by the group-vector values. In addition, $\mathbb{A}$ is now a block matrix of $N_g \times N_g$ sub-matrices generated from the moment scattering matrices:

$$\mathbf{A} = \begin{bmatrix} (\boldsymbol{\Sigma}_0) & (-\frac{2}{3}\boldsymbol{\Sigma}_0) & (\frac{8}{15}\boldsymbol{\Sigma}_0) & (-\frac{16}{35}\boldsymbol{\Sigma}_0) \\[2em] (-\frac{2}{3}\boldsymbol{\Sigma}_0) & (\frac{4}{9}\boldsymbol{\Sigma}_0 + \frac{5}{9}\boldsymbol{\Sigma}_2) & (-\frac{16}{45}\boldsymbol{\Sigma}_0 - \frac{4}{9}\boldsymbol{\Sigma}_2) & (\frac{32}{105}\boldsymbol{\Sigma}_0 + \frac{8}{21}\boldsymbol{\Sigma}_2) \\[2em] (\frac{8}{15}\boldsymbol{\Sigma}_0) & (-\frac{16}{45}\boldsymbol{\Sigma}_0 - \frac{4}{9}\boldsymbol{\Sigma}_2) & (\frac{64}{225}\boldsymbol{\Sigma}_0 + \frac{16}{45}\boldsymbol{\Sigma}_2 + \frac{9}{25}\boldsymbol{\Sigma}_4) & (-\frac{128}{525}\boldsymbol{\Sigma}_0 - \frac{32}{105}\boldsymbol{\Sigma}_2 - \frac{54}{175}\boldsymbol{\Sigma}_4) \\[2em] (-\frac{16}{35}\boldsymbol{\Sigma}_0) & (\frac{32}{105}\boldsymbol{\Sigma}_0 + \frac{8}{21}\boldsymbol{\Sigma}_2) & (-\frac{128}{525}\boldsymbol{\Sigma}_0 - \frac{32}{105}\boldsymbol{\Sigma}_2 - \frac{54}{175}\boldsymbol{\Sigma}_4) & (\frac{256}{1225}\boldsymbol{\Sigma}_0 + \frac{64}{245}\boldsymbol{\Sigma}_2 + \frac{324}{1225}\boldsymbol{\Sigma}_4 + \frac{13}{49}\boldsymbol{\Sigma}_6) \end{bmatrix}. \tag{B.9}$$

Appendix C

Two-Dimensional One-Speed Neutron Diffusion Model Problem

For many numerical experiments in this work, we choose the one-speed, two-dimensional neutron diffusion equation as a model neutron transport problem [11]:

$$-\boldsymbol{\nabla} \cdot D\boldsymbol{\nabla}\phi + \Sigma_a\phi = S \,, \tag{C.1}$$

where ϕ is the neutron flux, Σ_a is the absorption cross section, and S is the source of neutrons. In addition, D is the diffusion coefficient defined as:

$$D = \frac{1}{3(\Sigma_t - \bar{\mu}\Sigma_s)} \,, \tag{C.2}$$

where Σ_s is the scattering cross section, $\Sigma_t = \Sigma_a + \Sigma_s$ is the total cross section, and $\bar{\mu}$ is the cosine of the average scattering angle. For simplicity, we will take $\bar{\mu} = 0$ for our analysis giving $D = (3\Sigma_t)^{-1}$. In addition, to further simplify we will assume a homogeneous domain such that the cross sections remain constant throughout. Doing this permits us to rewrite Eq (C.1) as:

$$-D\boldsymbol{\nabla}^2\phi + \Sigma_a\phi = S \,. \tag{C.3}$$

We choose a finite difference scheme on a square Cartesian grid to discretize the problem.
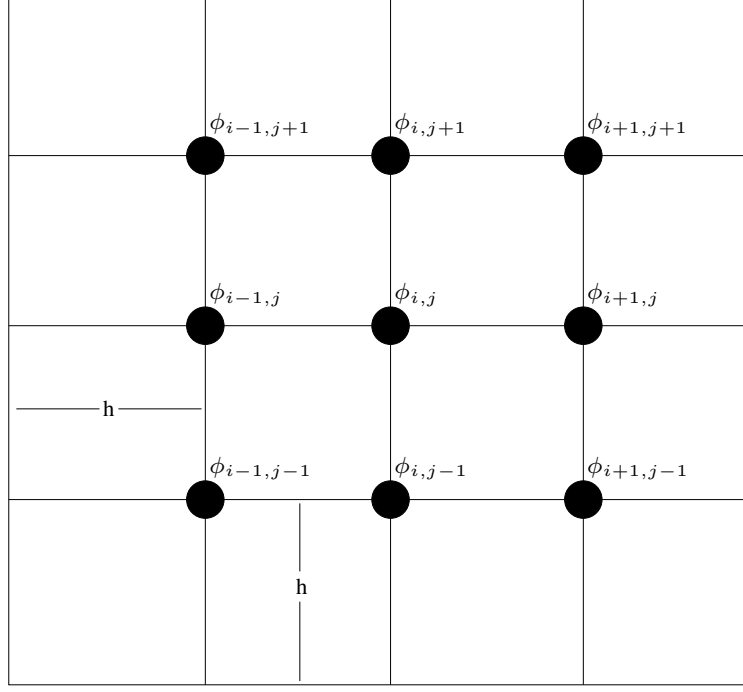
Figure C.1: **Nine-point Laplacian stencil.**

For the Laplacian, we choose the 9-point stencil shown in Figure C.1 over a grid of size h [63]:

$$\nabla_9^2\phi = \frac{1}{6h^2}[4\phi_{i-1,j} + 4\phi_{i+1,j} + 4\phi_{i,j-1} + 4\phi_{i,j+1} + \phi_{i-1,j-1}$$

$$+ \phi_{i-1,j+1} + \phi_{i+1,j-1} + \phi_{i+1,j+1} - 20\phi_{i,j}]. \quad (C.4)$$

We then have the following linear system to solve:

$$-\frac{1}{6h^2}[4\phi_{i-1,j} + 4\phi_{i+1,j} + 4\phi_{i,j-1} + 4\phi_{i,j+1} + \phi_{i-1,j-1}$$

$$+ \phi_{i-1,j+1} + \phi_{i+1,j-1} + \phi_{i+1,j+1} - 20\phi_{i,j}] + \Sigma_a\phi_{i,j} = s_{i,j}, \quad (C.5)$$

and in operator form:

$$\mathbf{D}\phi = \mathbf{s}, \quad (C.6)$$

where $\mathbf{D}$ is the diffusion operator, $\mathbf{s}$ is the source in vector form and ϕ is the vector of

unknown fluxes.

To close the system, a set of boundary conditions is required. In the case of a non-reentrant current condition applied to all global boundaries of the domain, we choose the formulation of Duderstadt by assuming the flux is zero at some ghost point beyond the grid. Consider for example the equations on the $i = 0$ boundary of the domain:

$$-\frac{1}{6h^2}[4\phi_{-1,j} + 4\phi_{1,j} + 4\phi_{0,j-1} + 4\phi_{0,j+1} + \phi_{-1,j-1}$$
$$+ \phi_{-1,j+1} + \phi_{1,j-1} + \phi_{1,j+1} - 20\phi_{0,j}] + \Sigma_a\phi_{0,j} = s_{0,j} . \quad \text{(C.7)}$$

Here we note some terms where $i = -1$ and therefore are representative of grid points beyond the boundary of the domain. We set the flux at these points to be zero, giving a valid set of equations for the $i = 0$ boundary:

$$-\frac{1}{6h^2}[4\phi_{1,j} + 4\phi_{0,j-1} + 4\phi_{0,j+1}$$
$$+ \phi_{-1,j+1} + \phi_{1,j-1} + \phi_{1,j+1} - 20\phi_{0,j}] + \Sigma_a\phi_{0,j} = s_{0,j} . \quad \text{(C.8)}$$

We repeat this procedure for the other boundaries of the domain. For reflecting boundary conditions, the net current across a boundary is zero.

Bibliography

[1] T. M. Evans, "Simplified PN methods in Denovo," Oak Ridge National Laboratory, Technical Report RNSD-00-000, Mar. 2013.

[2] P. S. Brantley and E. Larsen, "The simplified P3 approximation," *Nuclear Science and Engineering*, vol. 134, no. 1, pp. 1–21, Jan. 2000.

[3] I. Dimov, V. Alexandrov, and A. Karaivanova, "Parallel resolvent Monte Carlo algorithms for linear algebra problems," *Mathematics and Computers in Simulation*, vol. 55, no. 1-3, pp. 25–35, Feb. 2001.

[4] I. Dimov, B. Philippe, A. Karaivanova, and C. Weihrauch, "Robustness and applicability of Markov chain Monte Carlo algorithms for eigenvalue problems," *Applied Mathematical Modelling*, vol. 32, no. 8, pp. 1511–1529, Aug. 2008.

[5] V. Alexandrov, "Efficient parallel Monte Carlo methods for matrix computations," *Mathematics and Computers in Simulation*, vol. 47, no. 2-5, pp. 113–122, Aug. 1998.

[6] S. Branford, C. Sahin, A. Thandavan, C. Weihrauch, V. Alexandrov, and I. Dimov, "Monte Carlo methods for matrix computations on the grid," *Future Generation Computer Systems*, vol. 24, no. 6, pp. 605–612, 2008.

[7] I. Dimov and V. Alexandrov, "A new highly convergent Monte Carlo method for matrix computations," *Mathematics and Computers in Simulation*, vol. 47, no. 2-5, pp. 165–181, Aug. 1998.

[8] I. Dimov, V. Alexandrov, R. Papancheva, and C. Weihrauch, "Monte Carlo numerical treatment of large linear algebra problems," in *Computational Science - ICCS 2007*, ser. Lecture Notes in Computer Science, Y. Shi, G. D. v. Albada, J. Dongarra, and P. M. A. Sloot, Eds.   Springer Berlin Heidelberg, Jan. 2007, no. 4487, pp. 747–754.

[9] V. Alexandrov, E. Atanassov, and I. Dimov, "Parallel quasi-Monte Carlo methods for linear algebra problems," *Monte Carlo Methods & Applications*, vol. 10, no. 3/4, pp. 213–219, Jul. 2004.

[10] Y. Azmy and E. Sartori, *Nuclear Computational Science: A Century in Review*, 1st ed. Springer, May 2010.

[11] J. J. Duderstadt and L. J. Hamilton, *Nuclear Reactor Analysis*, 1st ed.   Wiley, Jan. 1976.

[12] B. M. Averick, J. J. More, C. H. Bischof, A. Carle, and A. Griewank, "Computing large sparse Jacobian matrices using automatic differentiation," *SIAM Journal on Scientific Computing*, vol. 15, no. 2, pp. 285–294, Mar. 1994.

[13] T. A. Brunner and P. S. Brantley, "An efficient, robust, domain-decomposition algorithm for particle Monte Carlo," *Journal of Computational Physics*, vol. 228, no. 10, pp. 3882–3890, Jun. 2009.

[14] T. A. Brunner, T. J. Urbatsch, T. M. Evans, and N. A. Gentile, "Comparison of four parallel algorithms for domain decomposed implicit Monte Carlo," *Journal of Computational Physics*, vol. 212, no. 2, pp. 527–539, Mar. 2006.

[15] I. Dimov, T. Dimov, and T. Gurov, "A new iterative Monte Carlo approach for inverse matrix problem," *Journal of Computational and Applied Mathematics*, vol. 92, no. 1, pp. 15–35, May 1998.

[16] K. Devine, E. Boman, R. Heaphy, B. Hendrickson, and C. Vaughan, "Zoltan data management services for parallel dynamic applications," *Computing in Science Engineering*, vol. 4, no. 2, pp. 90 –96, Apr. 2002.

[17] D. Danilov, S. Ermakov, and J. Halton, "Asymptotic complexity of Monte Carlo methods for solving linear systems," *Journal of Statistical Planning and Inference*, vol. 85, no. 1-2, pp. 5–18, Apr. 2000.

[18] T. Evans and S. Mosher, "A Monte Carlo synthetic acceleration method for the nonlinear, time-dependent diffusion equation," *American Nuclear Society - International Conference on Mathematics, Computational Methods and Reactor Physics 2009*, 2009.

[19] S. C. Eisenstat and H. F. Walker, "Choosing the forcing terms in an inexact Newton method," *SIAM Journal on Scientific Computing*, vol. 17, no. 1, pp. 16–32, Jan. 1996.

[20] R. S. Dembo, S. C. Eisenstat, and T. Steihaug, "Inexact Newton methods," *SIAM Journal on Numerical Analysis*, vol. 19, no. 2, pp. 400–408, Apr. 1982.

[21] G. De Vahl Davis, "Natural convection of air in a square cavity: A bench mark numerical solution," *International Journal for Numerical Methods in Fluids*, vol. 3, no. 3, pp. 249–264, 1983.

[22] X.-C. Cai and D. E. Keyes, "Nonlinearly preconditioned inexact Newton algorithms," *SIAM Journal on Scientific Computing*, vol. 24, no. 1, pp. 183–200, Jan. 2002.

[23] R. A. Bartlett, D. M. Gay, and E. T. Phipps, "Automatic differentiation of C++ codes for large-scale scientific computing," in *Computational Science - ICCS 2006*. Berlin, Heidelberg: Springer Berlin Heidelberg, 2006, vol. 3994, pp. 525–532.

[24] C. G. Baker, U. L. Hetmaniuk, R. B. Lehoucq, and H. K. Thornquist, "Anasazi software for the numerical solution of large-scale eigenvalue problems," *ACM Trans. Math. Softw.*, vol. 36, no. 3, pp. 1–23, Jul. 2009.

[25] R. N. Slaybaugh, "Acceleration methods for massively parallel deterministic transport," PhD Nuclear Engineering and Engineering Physics, University of Wisconsin-Madison, Madison, WI, Nov. 2011.

[26] Q. Wang, D. Gleich, A. Saberi, N. Etemadi, and P. Moin, "A Monte Carlo method for solving unsteady adjoint equations," *Journal of Computational Physics*, vol. 227, no. 12, pp. 6184–6205, Jun. 2008.

[27] B. F. Vajargah, "New advantages to obtain accurate matrix inversion," *Applied Mathematics and Computation*, vol. 189, no. 2, pp. 1798–1804, Jun. 2007.

[28] B. F. Vajargah and K. F. Vajargah, "Parallel Monte Carlo computations for solving SLAE with minimum communications," *Applied Mathematics and Computation*, vol. 183, no. 1, pp. 1–9, Dec. 2006.

[29] B. F. Vajargah, "Stochastic inverse matrix computation with minimum variance of errors," *Applied Mathematics and Computation*, vol. 199, no. 1, pp. 181–185, May 2008.

[30] J. Spanier and E. M. Gelbard, *Monte Carlo Principles and Neutron Transport Problems*. New York: Dover Publications, 1969.

[31] U.S. Department of Energy, "Resilient extreme-scale solvers," ASCR, Tech. Rep. LAB 12-742, 2012.

[32] ——, "CASL - a project summary," Consortium for Advanced Simulation of LWRs, CASL-U-2011-0025-000, 2011.

[33] B. Stroustrup, *The C++ Programming Language*, 3rd ed. Addison-Wesley Professional, Jun. 1997.

[34] A. Siegel, K. Smith, P. Fischer, and V. Mahadevan, "Analysis of communication costs for domain decomposed Monte Carlo methods in nuclear reactor analysis," *Journal of Computational Physics*, vol. 231, no. 8, pp. 3119–3125, Apr. 2012.

[35] A. Srinivasan, "Monte Carlo linear solvers with non-diagonal splitting," *Mathematics and Computers in Simulation*, vol. 80, no. 6, pp. 1133–1143, Feb. 2010.

[36] W. Wasow, "A note on the inversion of matrices by random walks," *Mathematical Tables and Other Aids to Computation*, vol. 6, no. 38, pp. 78–81, Apr. 1952.

[37] J. Wagner, S. Mosher, T. Evans, D. Peplow, and J. Turner, "Hybrid and parallel domain-decomposition methods development to enable Monte Carlo for reactor analyses," *Joint International Conference on Supercomputing in Nuclear Applications and Monte Carlo*, 2010.

[38] O. C. Zienkiewicz, R. L. Taylor, and J. Z. Zhu, *The Finite Element Method: Its Basis and Fundamentals, Sixth Edition*, 6th ed. Butterworth-Heinemann, May 2005.

[39] A. Siegel, K. Smith, P. Romano, B. Forget, and K. Felker, "The effect of load imbalances on the performance of Monte Carlo algorithms in LWR analysis," *Journal of Computational Physics*, 2012.

[40] L. N. Trefethen and D. B. III, *Numerical Linear Algebra*. SIAM: Society for Industrial and Applied Mathematics, Jun. 1997.

[41] J. N. Shadid, R. S. Tuminaro, and H. F. Walker, "An inexact Newton method for fully coupled solution of the Navier-Stokes equations with heat and mass transport," *Journal of Computational Physics*, vol. 137, no. 1, pp. 155–185, Oct. 1997.

[42] R. S. Tuminaro, J. N. Shadid, and S. A. Hutchinson, "Parallel sparse matrix vector multiply software for matrices with data locality," *Concurrency: Practice and Experience*, vol. 10, no. 3, pp. 229–247, 1998.

[43] J. N. Shadid and R. S. Tuminaro, "A comparison of preconditioned nonsymmetric Krylov methods on a large-scale MIMD machine," *SIAM Journal on Scientific Computing*, vol. 15, no. 2, pp. 440–459, Mar. 1994.

[44] M. Sosonkina, D. Allison, and L. Watson, "Scalable parallel implementations of the GMRES algorithm via householder reflections," in *1998 International Conference on Parallel Processing, 1998. Proceedings*, Aug. 1998, pp. 396 –404.

[45] G. Okten, "Solving linear equations by Monte Carlo simulation," *SIAM Journal on Scientific Computing*, vol. 27, no. 2, pp. 511–531, Jan. 2005.

[46] Pawlowski, J. N. Shadid, T. Smith, E. Cyr, and P. Weber, "Drekar CFD - a turbulent fluid-flow and conjugate heat transfer code: Theory manual (version 1.0)," Sandia National Laboratories, Technical Report, 2012.

[47] P. R. McHugh and D. A. Knoll, *Fully implicit solutions of the benchmark backward facing step problem using finite element discretization and inexact Newton's method*, 1992.

[48] ——, "Inexact Newton's method solutions to the incompressible Navier-Stokes and energy equations using standard and matrix-free implementations," in *AIAA 11th Computational Fluid Dynamics Conference*, vol. -1, 1993, pp. 385–393.

[49] P. Romano, B. Forget, and F. Brown, "Towards scalable parallelism in monte carlo particle transport codes using remote memory access," in *Joint International Conference on Supercomputing in Nuclear Applications and Monte Carlo 2010 (SNA+ MC2010)*, 2010, pp. 17–21.

[50] R. Procassini, M. O'Brien, and J. Taylor, "Dynamic load balancing of parallel Monte Carlo transport calculations," *Monte Carlo 2005*, 2005.

[51] D. R. Musser and A. A. Stepanov, "Algorithm-oriented generic libraries," *Software: Practice and Experience*, vol. 24, no. 7, pp. 623–642, 1994.

[52] Y. Li and M. Mascagni, "Analysis of large-scale grid-based Monte Carlo applications," *The International Journal of High Performance Computing Applications*, vol. 17, no. 4, pp. 369–382, 2003.

[53] B. Mervin, S. Mosher, T. Evans, J. Wagner, and G. Maldonado, "Variance estimation in domain decomposed Monte Carlo eigenvalue calculations," *PHYSOR 2012 - Advances in Reactor Physics*, 2012.

[54] K. Sabelfeld and N. Mozartova, "Sparsified randomization algorithms for large systems of linear equations and a new version of the random walk on boundary method," *Monte Carlo Methods & Applications*, vol. 15, no. 3, pp. 257–284, Nov. 2009.

[55] R. H. Pletcher, J. C. Tannehill, and D. Anderson, *Computational Fluid Mechanics and Heat Transfer, Second Edition*, 2nd ed. Taylor & Francis, Apr. 1997.

[56] Y. Saad, *Iterative Methods for Sparse Linear Systems.* SIAM, Apr. 2003.

[57] ——, "A flexible inner-outer preconditioned GMRES algorithm," *SIAM Journal on Scientific Computing*, vol. 14, no. 2, p. 9, Mar. 1993.

[58] P. Notz and Pawlowski, "Graph-based software design for managing complexity and enabling concurrency in multiphysics PDE software," *ACM Trans. Math. Softw.*, vol. 40, pp. 1–24, 2010.

[59] N. M. Nachtigal, S. C. Reddy, and L. N. Trefethen, "How fast are nonsymmetric matrix iterations?" *SIAM Journal on Matrix Analysis and Applications*, vol. 13, no. 3, pp. 778–795, Jul. 1992.

[60] P. R. McHugh and D. A. Knoll, "Fully coupled finite volume solutions of the incompressible Navier-Stokes and energy equations using an inexact Newton method," *International Journal for Numerical Methods in Fluids*, vol. 19, no. 5, pp. 439–455, 1994.

[61] E. E. Lewis, *Computational Methods of Neutron Transport*, J. Miller, W. F., Ed. Wiley-Interscience, Jan. 1993.

[62] R. J. LeVeque, *Finite Volume Methods for Hyperbolic Problems*, 1st ed. Cambridge University Press, Aug. 2002.

[63] R. LeVeque, *Finite Difference Methods for Ordinary and Partial Differential Equations: Steady-State and Time-Dependent Problems.* SIAM, Society for Industrial and Applied Mathematics, Jul. 2007.

[64] Y. Saad and M. H. Schultz, "GMRES: a generalized minimal residual algorithm for solving nonsymmetric linear systems," *SIAM Journal on Scientific and Statistical Computing*, vol. 7, no. 3, pp. 856–869, Jul. 1986.

[65] D. Knoll and P. McHugh, "Newton-Krylov methods applied to a system of convection-diffusion-reaction equations," *Computer Physics Communications*, vol. 88, no. 2-3, pp. 141–160, Aug. 1995.

[66] H. Rief, "Touching on a zero-variance scheme in solving linear equations by random walk processes," *Monte Carlo Methods & Applications*, vol. 5, no. 2, p. 135, Apr. 1999.

[67] M. Pernice and H. F. Walker, "NITSOL: a Newton iterative solver for nonlinear systems," *SIAM Journal on Scientific Computing*, vol. 19, no. 1, pp. 302–318, Jan. 1998.

[68] R. P. Pawlowski, J. N. Shadid, J. P. Simonis, and H. F. Walker, "Globalization techniques for Newton-Krylov methods and applications to the fully coupled solution of the Navier-Stokes equations," *SIAM Review*, vol. 48, no. 4, pp. 700–721, Jan. 2006.

[69] P. M. Kogge and T. J. Dysart, "Using the TOP500 to trace and project technology and architecture trends," in *Proceedings of 2011 International Conference for High Performance Computing, Networking, Storage and Analysis*, ser. SC '11. New York, NY, USA: ACM, 2011, pp. 28:1–28:11.

[70] A. Hughes Hallett, "Second-order iterations with guaranteed convergence," *Journal of Computational and Applied Mathematics*, vol. 10, no. 3, pp. 285–291, Jun. 1984.

[71] D. E. Keyes, D. K. Kaushik, and B. F. Smith, "Prospects for CFD on petaflops systems," Tech. Rep., Dec. 1997.

[72] D. E. Keyes, *How Scalable is Domain Decomposition in Practice?*, 1999.

[73] N. Gentile, M. Kalos, and T. A. Brunner, "Obtaining identical results on varying numbers of processors in domain decomposed particle Monte Carlo simulations," in *Computational Methods in Transport*. Berlin/Heidelberg: Springer-Verlag, 2005, vol. 48, pp. 423–433.

[74] H. Ji and Y. Li, "Reusing random walks in Monte Carlo methods for linear systems," *Procedia Computer Science*, vol. 9, pp. 383–392, 2012.

[75] T. Evans, S. Mosher, and S. Slattery, "A Monte Carlo synthetic-acceleration method for solving the thermal radiation diffusion equation," *Journal of Computational Physics*, vol. Submitted, 2012.

[76] W. Gropp and B. Smith, "Scalable, extensible, and portable numerical libraries," in *Scalable Parallel Libraries Conference, 1993., Proceedings of the*, Oct. 1993, pp. 87 –93.

[77] M. A. Heroux, R. A. Bartlett, V. E. Howle, R. J. Hoekstra, J. J. Hu, T. G. Kolda, R. B. Lehoucq, K. R. Long, R. P. Pawlowski, E. T. Phipps, A. G. Salinger, H. K. Thornquist, R. S. Tuminaro, J. M. Willenbring, A. Williams, and K. S. Stanley, "An overview of the trilinos project," *ACM Trans. Math. Softw.*, vol. 31, no. 3, pp. 397–423, Sep. 2005.

[78] C. T. Kelley, *Iterative Methods for Linear and Nonlinear Equations*, 1st ed. Society for Industrial and Applied Mathematics, 1995.

[79] J. M. Hammersley and D. C. Handscomb, *Monte Carlo Methods*. Methuen, 1964.

[80] J. H. Halton, "Sequential Monte Carlo techniques for the the solution of linear systems," *Journal of Scientific Computing*, vol. 9, pp. 213–257, 1994.

[81] ——, "Sequential Monte Carlo," *Mathematical Proceedings of the Cambridge Philosophical Society*, vol. 58, no. 01, pp. 57–78, 1962.

[82] ——, "A retrospective and prospective survey of the Monte Carlo method," *SIAM Review*, vol. 12, no. 1, pp. 1–63, Jan. 1970.

[83] ——, "Sequential Monte Carlo techniques for solving non-linear systems," *Monte Carlo Methods & Applications*, vol. 12, no. 2, pp. 113–141, Apr. 2006.

[84] W. D. Gropp, D. K. Kaushik, D. E. Keyes, and B. F. Smith, "High-performance parallel implicit CFD," *Parallel computing in aerospace*, vol. 27, no. 4, pp. 337–362, Mar. 2001.

[85] U. Ghia, K. Ghia, and C. Shin, "High-re solutions for incompressible flow using the Navier-Stokes equations and a multigrid method," *Journal of Computational Physics*, vol. 48, no. 3, pp. 387–411, Dec. 1982.

[86] D. Gaston, G. Hansen, S. Kadioglu, D. A. Knoll, C. Newman, H. Park, C. Permann, and W. Taitano, "Parallel multiphysics algorithms and software for computational nuclear engineering," *Journal of Physics: Conference Series*, vol. 180, p. 012012, Jul. 2009.

[87] D. K. Gartling, "A test problem for outflow boundary conditions - flow over a backward-facing step," *International Journal for Numerical Methods in Fluids*, vol. 11, no. 7, pp. 953 – 967, 1990.

[88] G. E. Forsythe and R. A. Leibler, "Matrix inversion by a Monte Carlo method," *Mathematical Tables and Other Aids to Computation*, vol. 4, no. 31, pp. 127–129, Jul. 1950, ArticleType: research-article / Full publication date: Jul., 1950 / Copyright 1950 American Mathematical Society.

[89] T. Evans, A. Stafford, R. Slaybaugh, and K. Clarno, "Denovo: A new three-dimensional parallel discrete ordinates code in SCALE," *Nuclear Technology*, vol. 171, no. 2, pp. 171–200, Aug. 2010.

[90] W. F. Godoy and X. Liu, "Parallel Jacobian-free Newton-Krylov solution of the discrete ordinates method with flux limiters for 3D radiative transfer," *Journal of Computational Physics*, vol. 231, no. 11, pp. 4257–4278, Jun. 2012.

[91] D. Knoll and D. Keyes, "Jacobian-free Newton-Krylov methods: a survey of approaches and applications," *Journal of Computational Physics*, vol. 193, no. 2, pp. 357–397, Jan. 2004.

[92] K. J. Evans, D. Knoll, and M. Pernice, "Enhanced algorithm efficiency for phase change convection using a multigrid preconditioner with a SIMPLE smoother," *Journal of Computational Physics*, vol. 223, no. 1, pp. 121–126, Apr. 2007.

[93] ——, "Development of a 2-d algorithm to simulate convection and phase transition efficiently," *Journal of Computational Physics*, vol. 219, no. 1, pp. 404–417, Nov. 2006.

[94] T. Evans, T. Urbatsch, H. Lichtenstein, and Morel, "A residual Monte Carlo method for discrete thermal radiative diffusion," *Journal of Computational Physics*, vol. 189, no. 2, pp. 539–556, Aug. 2003.

[95] K. Sabelfeld, "Stochastic algorithms in linear algebra - beyond the Markov chains and von Neumann - Ulam scheme," in *Numerical Methods and Applications*, D. Hutchison, T. Kanade, J. Kittler, J. M. Kleinberg, F. Mattern, J. C. Mitchell, M. Naor, O. Nierstrasz, C. Pandu Rangan, B. Steffen, M. Sudan, D. Terzopoulos, D. Tygar, M. Y. Vardi, G. Weikum, I. Dimov, S. Dimova, and N. Kolkovska, Eds. Berlin, Heidelberg: Springer Berlin Heidelberg, 2011, vol. 6046, pp. 14–28.

[96] T. Booth, "Monte Carlo variance reduction approaches for non-Boltzmann tallies," *Nuclear Science and Engineering*, vol. 116, 1994.

[97] J. C. Smith and S. H. Jacobson, "An analysis of the alias method for discrete random-variate generation," *INFORMS Journal on Computing*, vol. 17, no. 3, pp. 321–327, Jun. 2005.

[98] K. Tanabe, "Projection method for solving a singular system of linear equations and its applications," *Numerische Mathematik*, vol. 17, no. 3, pp. 203–214, Jun. 1971.

[99] E. Olbrant, E. Larsen, M. Frank, and B. Seibold, "Asymptotic derivation and numerical investigation of time-dependent simplified equations," *Journal of Computational Physics*, vol. 238, pp. 315–336, Apr. 2013.