

# **Valbal Trajectory Planning**

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Stanford Student Space Initiative

December 7, 2018

# Outline

ValBal

Trajectory Planning  
Background

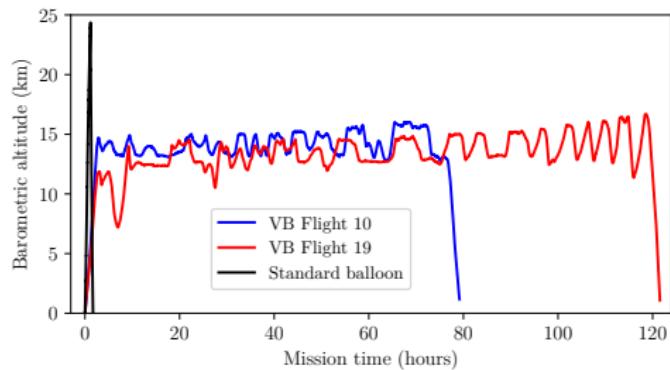
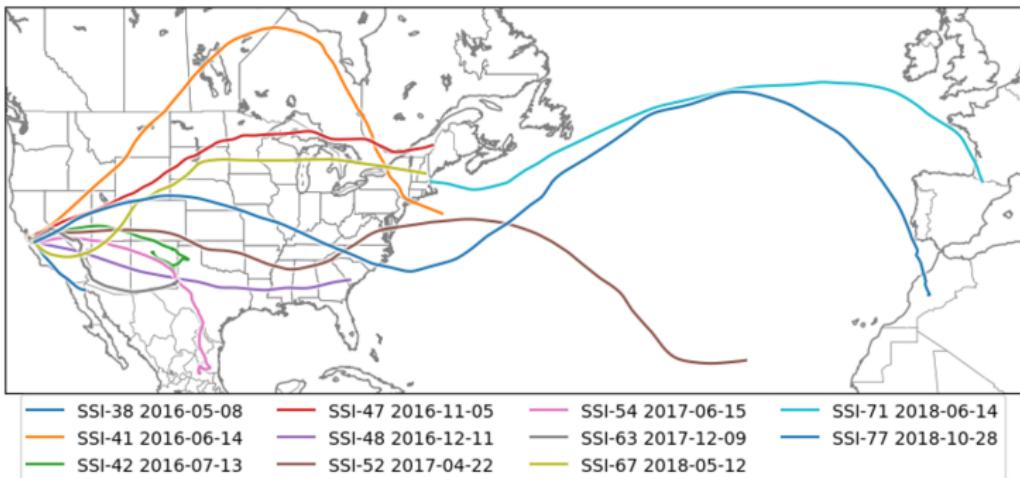
Flight Test

Altitude Control  
System Dynamics

# ValBal

- ▶ Research project by the Stanford Space Initiative (undergrad student club).
  - ▶ High altitude latex balloon platform that controls its altitude by venting lifting gas and dropping ballast mass.
  - ▶ Very cheap (sub thousand dollars), long endurance (5 days demonstrated).
  - ▶ Potential applications: hurricane data collection, radar probing of Greenland ice, lightning research, data relay...
  - ▶ Control: in altitude (remain between bounds while minimizing control effort), in space (pick altitude to get good winds).
1. A. Sushko, A. Tedjarati, J. Creus-Costa, S. Maldonado, K. Marshland and M. Pavone, "Low cost, high endurance, altitude-controlled latex balloon for near-space research (ValBal)," 2017 IEEE Aerospace Conference, Big Sky, MT, 2017, pp. 1-9.
  2. A. Sushko et al., "Advancements in low-cost, long endurance, altitude controlled latex balloons (ValBal)," 2018 IEEE Aerospace Conference, Big Sky, MT, 2018, pp. 1-10.





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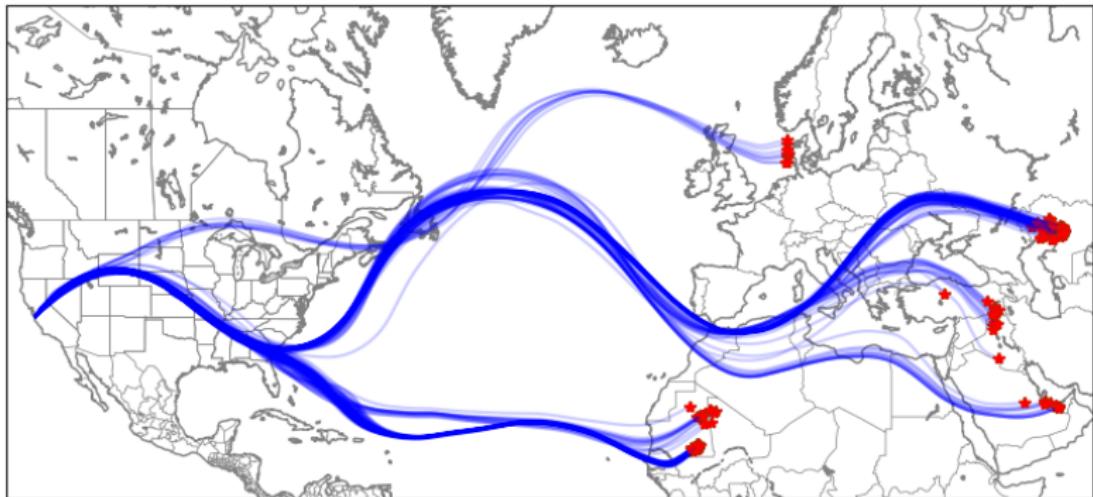
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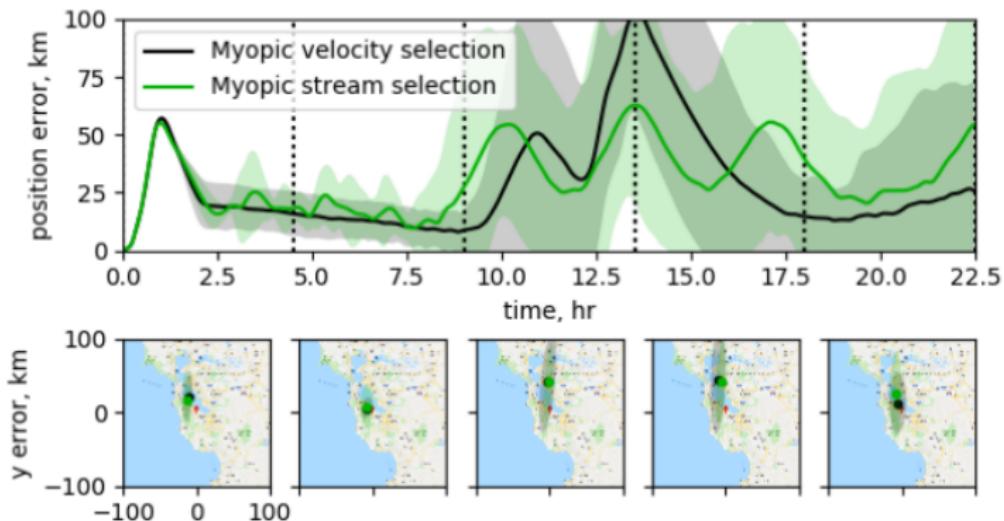
Trajectory Planning

# Trajectory Planning



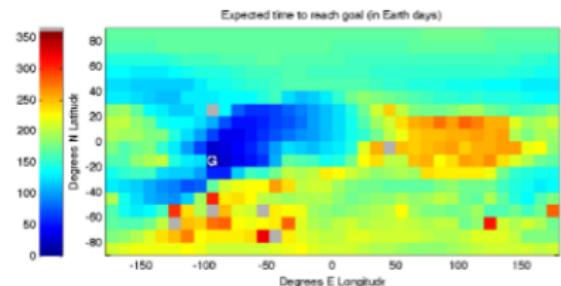
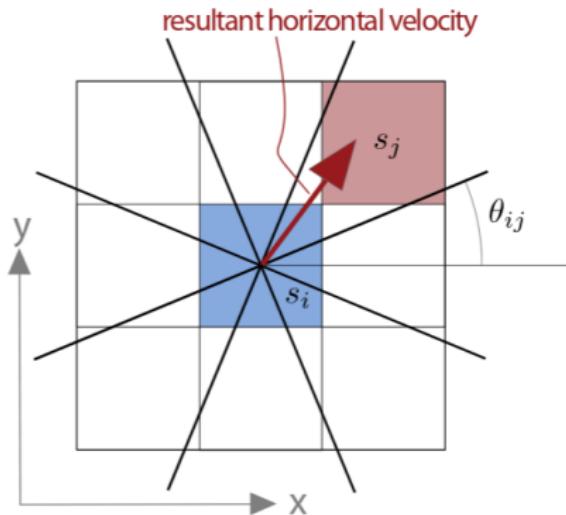
## Tree search for station keeping

- ▶ Born and Schwager, "Riding an Uncertain Wind Field: Receding Horizon Tree Search Planning with Opportunistic Sampling for an Autonomous Weather Balloon" (2019)

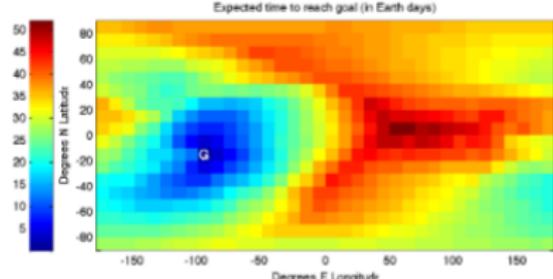


# MDP

- ▶ Wolf et al., "Probabilistic motion planning of balloons in strong, uncertain wind fields" (2010)



(a) No horizontal actuation ( $u_h \max = 0$ )



## Formulation

- ▶ System represented by states  $s \in \mathcal{S}$
- ▶  $\mathcal{S} = \mathcal{H} \times \Lambda \times \Phi \times \mathcal{T}$  (Time, Altitude, Longitude, Latitude)
  - Physically intuitive to keep majority of state continuous—curse of dimensionality as we discretize.
    - ▶  $h \in \mathcal{H}$ : altitudes ([0 km, 20 km])
    - ▶  $\lambda \in \Lambda$ : longitudes ([0,  $2\pi$ ])
    - ▶  $\phi \in \Phi$ : latitudes ( $[-\pi/2, \pi/2]$ )
  - $t \in \mathcal{T}$ : time, defined in discrete steps of 10 min. Allows us to use simple Euler integration spatially to trace out wind field (altitude handled differently).
- ▶ Atmospheric winds act on the balloon  $w(h, \lambda, \phi, t) \rightarrow (u, v)$ .  $w$  given by NOAA on  $0.25^\circ$  grid at various altitudes; interpolate in each variable.
- ▶ Control policies  $\theta(t) = (h_{\text{cmd}}, e_{\text{tol}})$  command the altitude of the balloon and error tolerance around set altitude

## Formulation

- ▶ Goal: formulate value function  $V$  as a differentiable function of a (small) set of policy parameters  $\theta$ .
  - Avoids having to discretize a huge state space as in most MDP formulations.
- ▶ Optimize  $V$  via a gradient method, e.g.  $\theta^{k+1} = \theta^k + \alpha_k \nabla_{\theta} V(\theta)$ . for stepsize  $a_k$
- ▶ Allows us to preserve key properties of the spaces we're in:
  - We preserve smoothness of the value function: the wind field is not random, and has a rather small spatial frequency.
  - We preserve the continuity of our variables: altitude, latitude, longitude need small discretization to be realistic.
  - We will be able to handle stochasticity without blowing up the size of the problem.

## Formulation: example

- ▶ Suppose we want to maximize longitudinal distance of final point after  $N$  steps (say  $N = 720$ , 5 days).
- ▶ Final longitude is the result of doing a simulation rollout, using Euler integration in latitude and longitude.
- ▶  $V = \lambda_f = \lambda_0 + v_1(t_1, h_1, \phi_1, \lambda_1)\Delta t + \cdots + v_N(t_N, h_N, \phi_N, \lambda_N)\Delta t.$
- ▶ Need to parametrize  $V$ . We control altitude of the balloon (see later). Simplest formulation: define waypoints  $\theta_1, \dots, \theta_k$  at points  $T_1, \dots, T_k$ , and assume balloon goes linearly between waypoints:  
$$h_i = \theta_j + (t_i - T_j) \frac{\theta_{j+1} - \theta_j}{T_{j+1} - T_j}.$$
- ▶ However each velocity depends on altitude, which means that each successive longitude depends on all previous altitudes... OH GOD THE BLOCK IS REAL

$$s_{k+1} = a(s_k, \theta(t_k))$$

$$s_{k+1} = a(\dots a(a(s_0, \theta(t_0)), \theta(t_1)) \dots) \theta(t_k))$$

$$\frac{ds_{k+1}}{d\theta(t_k)} = a(\dots a(a(s_0, \theta(t_0)), \theta(t_1)) \dots), \theta(t_k))$$

## algorithm

```
1: procedure STOCASTICMPC( $S_1, S_2$ )
2:    $s$  : intial sim state
3:   while not converged do
4:      $obj$  : objective object
5:     for  $i \in \{0, 1, \dots, N - 1\}$  do
6:       Sim : simulation object
7:     end for
8:     check convergence
9:   end while
9: end procedure
```

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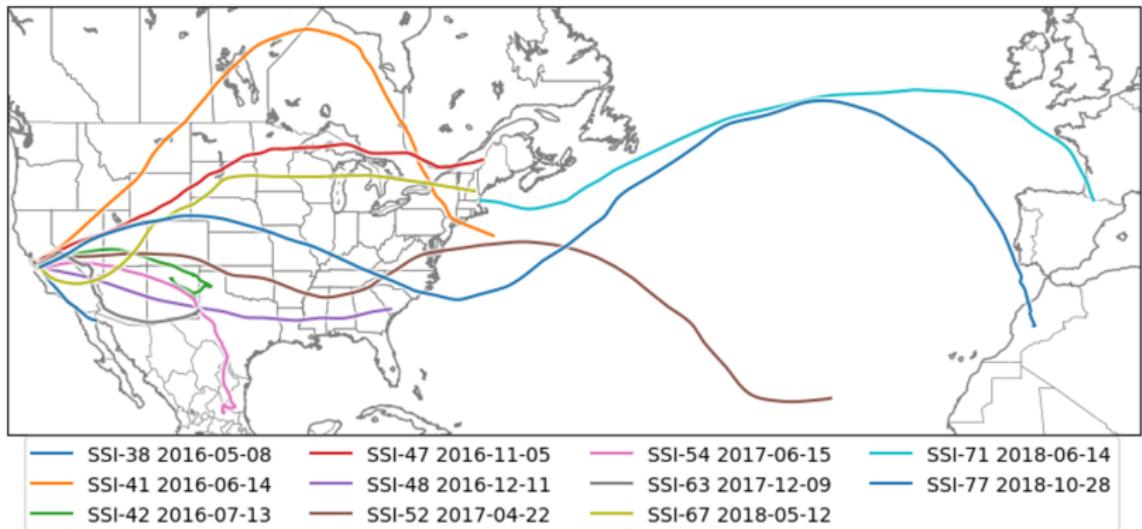
Flight Test

Altitude Control  
System Dynamics

Flight Test

15

# Valbal Flights



## SSI-77 Launch (Oct 28)



# Mission Control

habmc  
SS-77

Mission Clock 4:23:42:07  
Logged in as John Luns Dean | Logout

Primary Controls

Dashboard

Full Map

Flight Status

Communications

Transmissions

Last Transmission

SPOT

Iridium

Utilities

Predictor

Footprint

Charts & Graphs

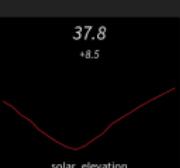
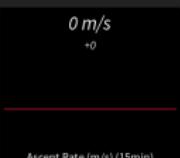
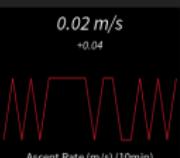
Historical Logs

Settings

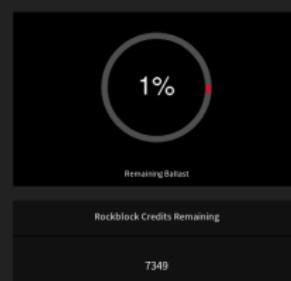
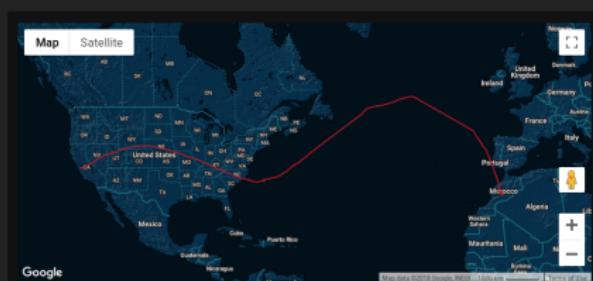
Configuration

Admin

Preferences



Remaining Battery



Rockblock Credits Remaining

7349

Click to add a new command constant variable

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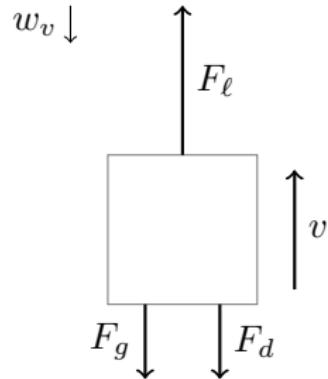
# System Dynamics

## ► Assumptions

- $F_d \propto v$  i.e. drag is linear.
- $F_l - F_g = F_d$  i.e. the balloon is always at terminal velocity

## ► Equations of motion

- let  $\ell = F_\ell - F_g$  be the net lift on the balloon
- $\dot{\ell}$  is commanded by controller
- $\dot{v}(t) = k_d(\dot{\ell}(t) + w_v(t))$
- $\dot{h}(t) = v(t) + w_v(t)$
- $\mathcal{L}\{h(t)/\dot{\ell}(t)\} = k_d/s^2$



$F_d$ : Force of drag

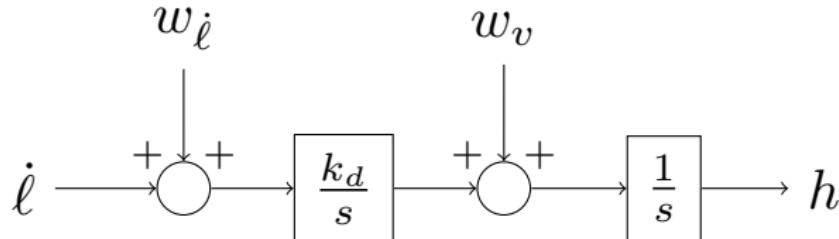
$F_g$ : Gravity

$F_\ell$ : Buoyant force

$v$ : vertical velocity of balloon

$w_v$ : vertical velocity of surrounding air

## Plant Block Diagram



$\dot{\ell}$ : commanded change in lift (valve and ballast actions)

$w_{\dot{\ell}}$ : atmospheric lift disturbance

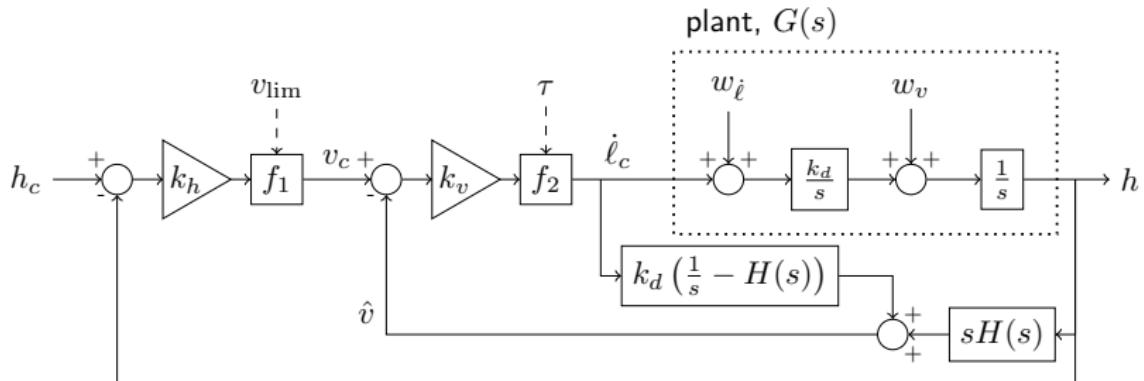
$w_v$ : atmospheric velocity disturbance

$h$ : altitude

$$x = \begin{bmatrix} h \\ v \end{bmatrix} \quad u = \dot{\ell}$$

$$\dot{x} = \begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix} x + \begin{bmatrix} 0 \\ k_d \end{bmatrix} u + \begin{bmatrix} w_v \\ k_d w_{\dot{\ell}} \end{bmatrix}$$

# Controller Block Diagram



$H(s)$  low-pass filter

$f_1(v; v_{\lim})$  clamp on the velocity commanded by the altitude loop set by  $v_{\lim}$

$f_2(\dot{l}; \tau)$  deadband on the controller effort set by  $\tau$

$h_c$  commanded altitude (set by Flight Controller)

$v_c$  commanded velocity (output of position loop)

$\dot{l}_c$  commanded change in lift per unit time (output of velocity loop)

$w_{\ell}$  atmospheric disturbances that change balloon lift (heating/cooling)

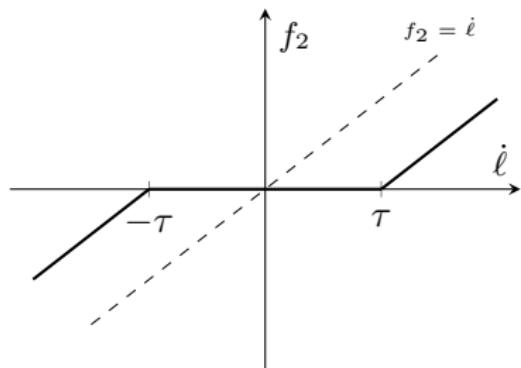
$w_v$  atmospheric disturbances that change balloon velocity (turbulence)

$h$  balloon altitude

$\hat{v}$  estimate of velocity

## Controller Deadband

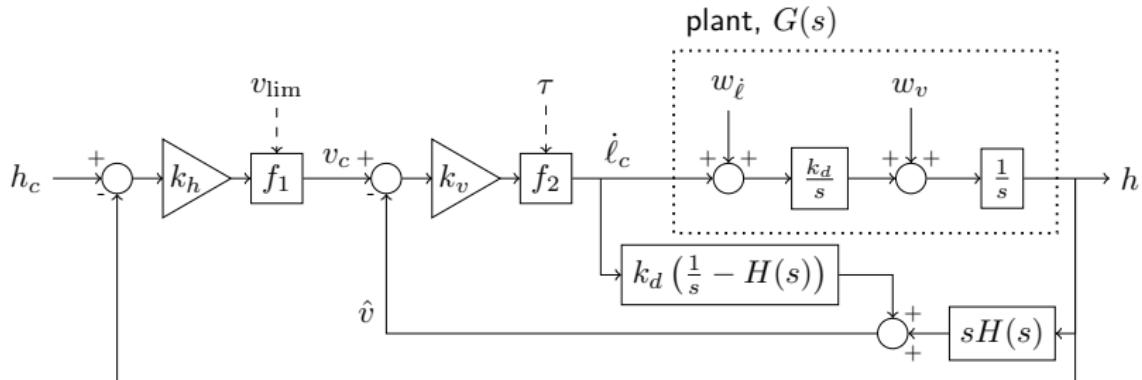
Since we typically command a target altitude and an allowable region, we add a deadband to the controller output. Let  $\dot{\ell}_o$  be the output of the nonlinearity. Deadband:



$$f_2(\dot{\ell}; \tau) = \begin{cases} 0 & |\dot{\ell}| < \tau \\ \text{sign}(\dot{\ell})(|\dot{\ell}| - \tau) & |\dot{\ell}| > \tau \end{cases}$$

To set bounds on the altitude, we set  $\tau = e_{\text{tol}} k_v k_h$ , where  $e_{\text{tol}}$  is the allowable distance from the altitude command.

# Controller Block Diagram



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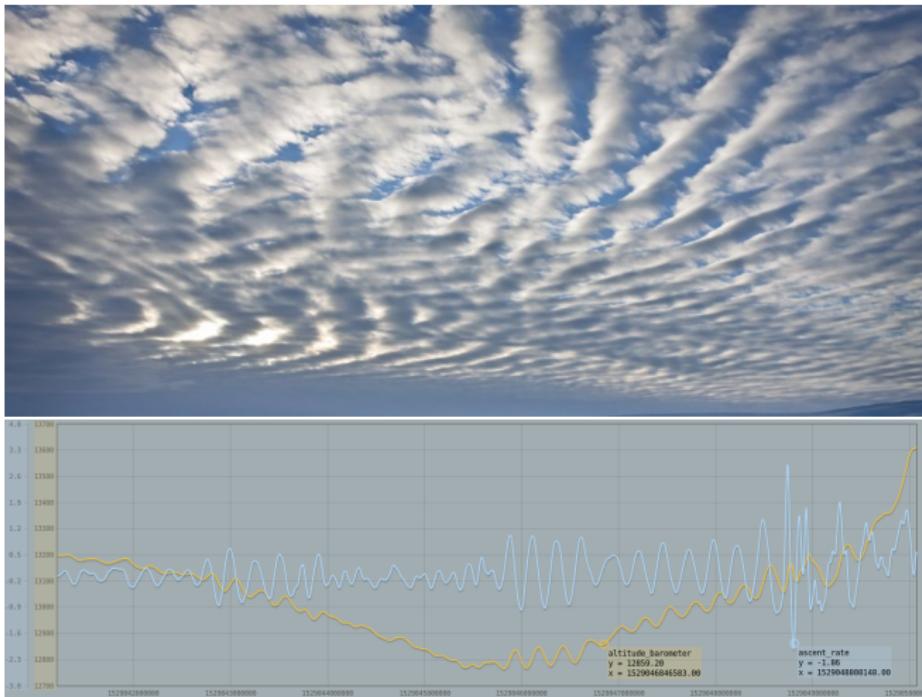
$w_\ell$  atmospheric disturbances that change balloon lift (heating/cooling)

$w_v$  atmospheric disturbances that change balloon velocity (turbulence)

$h$  balloon altitude

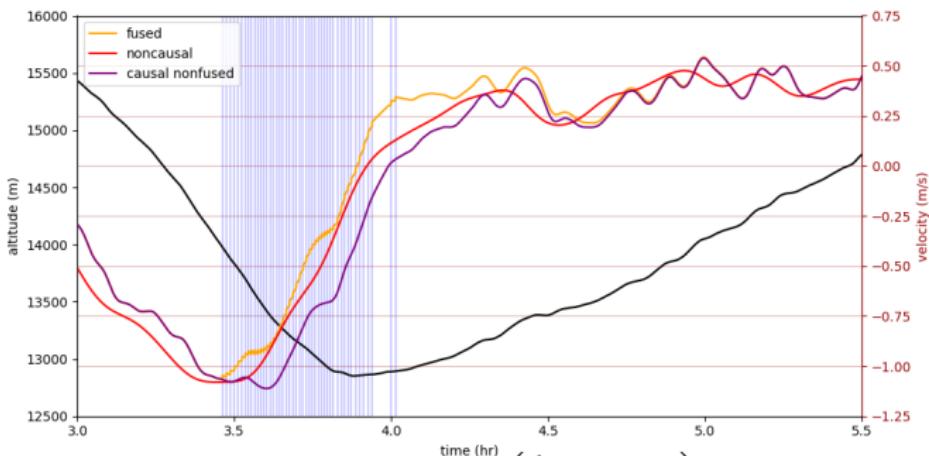
$\hat{v}$  estimate of velocity

# Atmosphere Waves



## Velocity Estimator

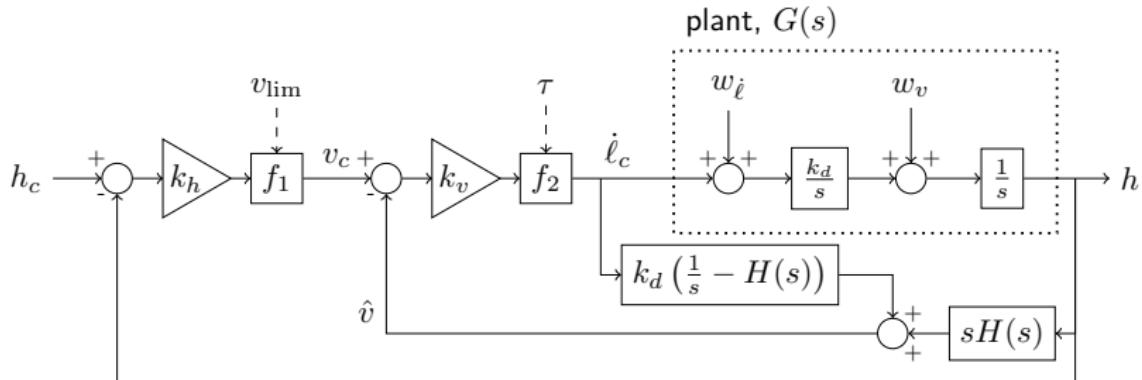
Low pass filtered velocity estimate uses a 2nd order filter to remove the effect of atmospheric waves



$$\mathcal{L}\{\hat{v}\} = sH(s)\mathcal{L}\{h\} + \left(\frac{1}{s} - H(s)\right)\mathcal{L}\{i_c\}$$

$H(s)$  a 2nd order lowpass filter

# Controller Block Diagram



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$h$  balloon altitude

$\hat{v}$  estimate of velocity

## Picking gains

*note:* while the deadband makes the controller non-linear, it still piecewise linear, thus linear analysis can be used.

Transfer function for the linear system is

$$T(s) = \frac{k_h k_v k_d}{s^2 + k_v k_d s + k_h k_v k_d}.$$

So damping ratio is  $\zeta = \frac{1}{2} \sqrt{\frac{k_d k_v}{k_h}}$ .

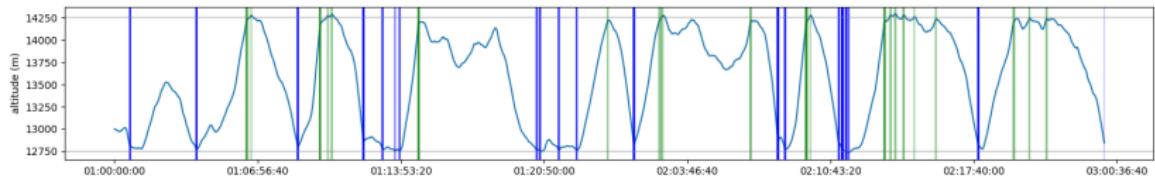
- ▶ We choose gains such that  $\zeta > 1$  and we have over damping.
- ▶ This gives ratio between  $k_v$  and  $k_h$ , but what about magnitude?
- ▶ high gain  $\rightarrow$  controller waits and acts aggressively near  $e_{\text{tol}}$
- ▶ low gain  $\rightarrow$  controller acts cautiously before  $e_{\text{tol}}$

demonstrated on next slide

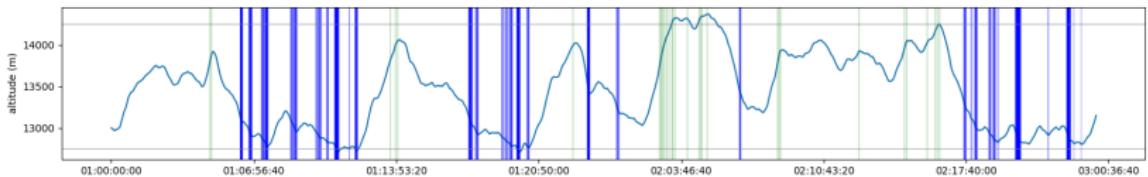
# High vs Low Gain

Plots of simulation shown

high gain

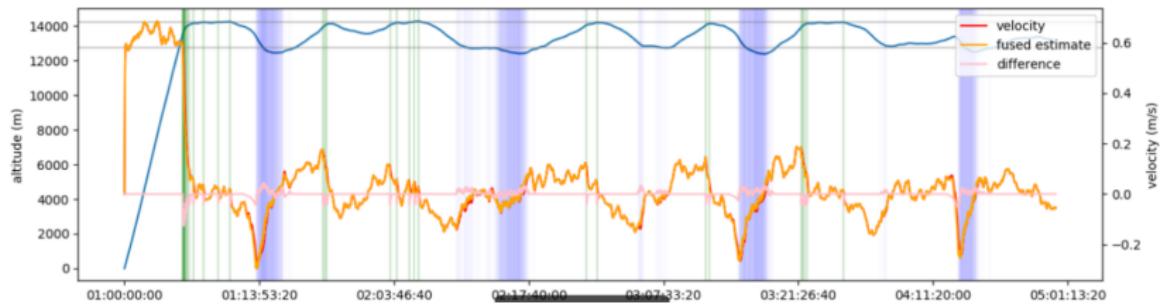


low gain

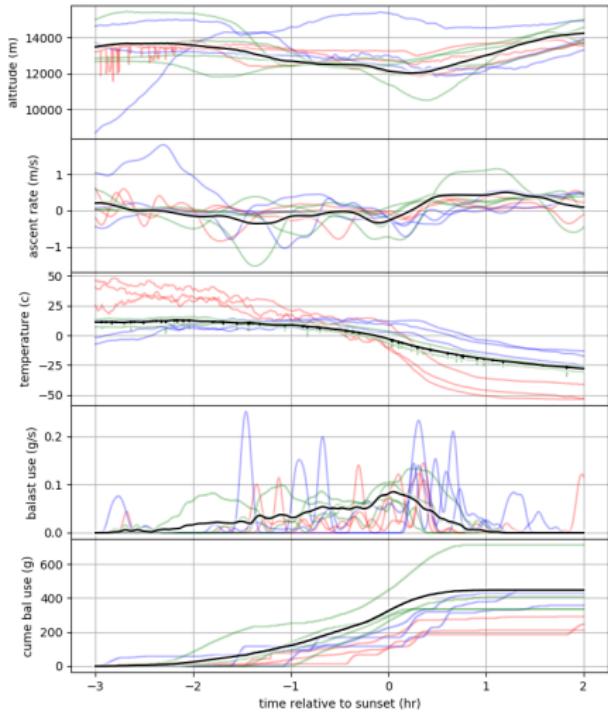


High gain performs better but can't tolerate uncertainty, low gain is worse but performs better under uncertainty

# Simulations



# Nightfall



- ▶ Left plot shows 10 sunsets across various flights (each flight different color).
- ▶ plot blow shows a fit to the data using convex regularization and constraints

