

DSP Assignment-7 Solutions

1.

The ideal frequency response of the filter shown in Fig. 6.12. We know

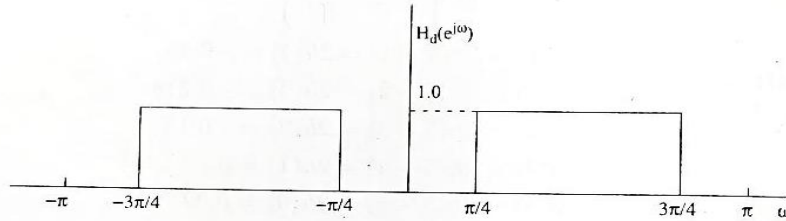


Fig. 6.12 Ideal frequency response of Bandpass filter of example 6.7.

$$\begin{aligned}
 h_d(n) &= \frac{1}{2\pi} \int_{-\pi}^{\pi} H_d(e^{j\omega}) e^{j\omega n} d\omega \\
 &= \frac{1}{2\pi} \left[\int_{-3\pi/4}^{-\pi/4} e^{j\omega n} d\omega + \int_{\pi/4}^{3\pi/4} e^{j\omega n} d\omega \right] \\
 &= \frac{1}{2\pi j n} \left[e^{-j\pi n/4} - e^{-j3\pi n/4} + e^{j3\pi n/4} - e^{j\pi n/4} \right] \\
 &= \frac{1}{\pi n} \left[\sin \frac{3\pi}{4} n - \sin \frac{\pi}{4} n \right] \quad -\infty \leq n \leq \infty \quad (6.63)
 \end{aligned}$$

Truncating $h_d(n)$ to 11 samples, we have

$$\begin{aligned}
 h(n) &= h_d(n) \quad \text{for } |n| \leq 5 \\
 &= 0 \quad \text{otherwise}
 \end{aligned}$$

The filter coefficients are symmetrical about $n = 0$ satisfying the condition $h(n) = h(-n)$.

For $n = 0$

$$\begin{aligned}
 h(0) &= \frac{1}{2\pi} \left[\int_{-3\pi/4}^{-\pi/4} d\omega + \int_{\pi/4}^{3\pi/4} d\omega \right] \\
 &= \frac{1}{2\pi} \left[-\frac{\pi}{4} + \frac{3\pi}{4} + \frac{3\pi}{4} - \frac{\pi}{4} \right] = \frac{1}{2} = 0.5
 \end{aligned}$$

$$\begin{aligned}
 h(1) &= h(-1) = \frac{\sin \frac{3\pi}{4} - \sin \frac{\pi}{4}}{\pi} = 0 \\
 h(2) &= h(-2) = \frac{\sin \frac{3\pi}{2} - \sin \frac{\pi}{2}}{2\pi} = \frac{-2}{2\pi} = -0.3183 \\
 h(3) &= h(-3) = \frac{\sin \frac{9\pi}{4} - \sin \frac{3\pi}{4}}{3\pi} = 0 \\
 h(4) &= h(-4) = \frac{\sin 3\pi - \sin \pi}{4\pi} = 0 \\
 h(5) &= h(-5) = \frac{\sin \frac{15\pi}{4} - \sin \frac{5\pi}{4}}{5\pi} = 0
 \end{aligned}$$

The transfer function of the filter is

$$\begin{aligned}
 H(z) &= h(0) + \sum_{n=1}^{\frac{N-1}{2}} [h(n)(z^n + z^{-n})] \\
 &= 0.5 - 0.3183(z^2 + z^{-2})
 \end{aligned}$$

The transfer function of the realizable filter is

$$\begin{aligned}
 H'(z) &= z^{-5} [0.5 - 0.3183(z^2 + z^{-2})] \\
 &= -0.3183z^{-3} + 0.5z^{-5} - 0.3183z^{-7}
 \end{aligned}$$

The filter coefficients of the causal filters are

$$\begin{aligned}
 h(0) &= h(10) = h(1) = h(9) = h(2) = h(8) = h(4) = h(6) = 0 \\
 h(3) &= h(7) = -0.3183 \\
 h(5) &= 0.5 \\
 \bar{H}(e^{j\omega}) &= \sum_{n=1}^{\frac{N-1}{2}} a(n) \cos \omega n \\
 a(0) &= h\left(\frac{N-1}{2}\right) = h(5) = 0.5 \\
 a(n) &= 2h\left(\frac{N-1}{2} - n\right) \\
 a(1) &= 2h(5-1) = 2h(4) = 0 \\
 a(2) &= 2h(5-2) = 2h(3) = -0.6366 \\
 a(3) &= 2h(5-3) = 2h(2) = 0 \\
 a(4) &= 2h(5-4) = 2h(1) = 0 \\
 a(5) &= 2h(5-5) = 2h(0) = 0 \\
 \bar{H}(e^{j\omega}) &= 0.5 - 0.6366 \cos 2\omega
 \end{aligned}$$

ω (in degrees)	0	20	30	45	60	75	90
$\bar{H}(e^{j\omega})$	-0.1366	0.012	0.1817	0.5	0.818	1.05	1.1366
$ H(e^{j\omega}) _{dB}$	-17.3	-38.17	-14.8	-6.02	-1.74	0.4346	1.11

	105	120	135	150	160	180
	1.05	0.818	0.5	0.1817	0.012	-0.1366
	0.4346	-1.74	-6.02	-14.8	-38.17	-17.3

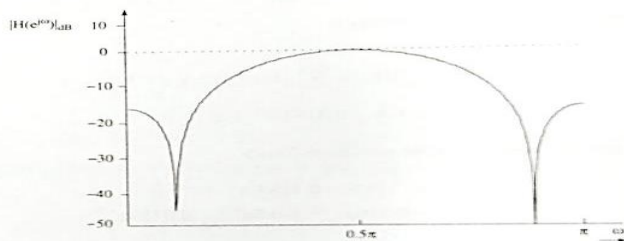


Fig. 6.13 Frequency response of Bandpass filter of example 6.7.

2.

Given $H_d(e^{j\omega}) = e^{-j3\omega}$

The frequency response is having a term $e^{-j\omega(N-1)/2}$ which gives $h(n)$ symmetrical about $n = \frac{N-1}{2} = 3$, i.e., we get a causal sequence.

We have

$$\begin{aligned} h_d(n) &= \frac{1}{2\pi} \int_{-\pi/4}^{\pi/4} e^{-j3\omega} e^{j\omega n} d\omega \\ &= \frac{1}{2\pi} \int_{-\pi/4}^{\pi/4} e^{j(n-3)\omega} d\omega \\ &= \frac{\sin \frac{\pi}{4}(n-3)}{\pi(n-3)} \end{aligned}$$

For $N = 7$ we have

$$h_d(0) = h_d(6) = 0.075$$

$$h_d(1) = h_d(5) = 0.159$$

$$h_d(2) = h_d(4) = 0.22$$

$$h_d(3) = 0.25$$

The non-causal window sequence is

$$\begin{aligned} w_{Hn}(n) &= 0.5 + 0.5 \cos \frac{2\pi n}{N-1} \quad \text{for } -(N-1)/2 \leq n \leq (N-1)/2 \\ &= 0 \quad \text{otherwise} \end{aligned}$$

For $N = 7$

$$\begin{aligned} w_{Hn}(n) &= 0.5 + 0.5 \cos \frac{2\pi n}{N-1} \quad \text{for } -3 \leq n \leq 3 \\ &= 0 \quad \text{otherwise} \end{aligned}$$

$$w_{Hn}(0) = 0.5 + 0.5 = 1$$

$$w_{Hn}(-1) = w_{Hn}(1) = 0.5 + 0.5 \cos \frac{\pi}{3} = 0.75$$

$$w_{Hn}(-2) = w_{Hn}(2) = 0.5 + 0.5 \cos \frac{2\pi}{3} = 0.25$$

$$w_{Hn}(-3) = 0.5 + 0.5 \cos \pi = 0$$

The causal window sequence can be obtained by shifting the sequence $w_{Hn}(n)$ to right by 3 samples, i.e.,

$$w_{Hn}(0) = w_{Hn}(6) = 0; w_{Hn}(1) = w_{Hn}(5) = 0.25$$

$$w_{Hn}(2) = w_{Hn}(4) = 0.75 \text{ \& } w_{Hn}(3) = 1$$

The filter coefficients using Hanning window are

$$h(n) = h_d(n)w_{Hn}(n) \quad \text{for } 0 \leq n \leq 6$$

$$h(0) = h(6) = h_d(0)w_{Hn}(0) = (0.075)(0) = 0$$

$$h(1) = h(5) = h_d(1)w_{Hn}(1) = (0.159)(0.25) = 0.03975$$

$$h(2) = h(4) = h_d(2)w_{Hn}(2) = (0.22)(0.75) = 0.165$$

$$h(3) = h_d(3)w_{Hn}(3) = (0.25)(1) = 0.25$$

3.

Given

$$y(n) = 0.25x(n) + x(n-1) + 0.25x(n-2)$$

Taking Fourier transform on both sides

$$Y(e^{j\omega}) = 0.25X(e^{j\omega}) + e^{-j\omega}X(e^{j\omega}) + 0.25e^{-2j\omega}X(e^{j\omega})$$

$$H(e^{j\omega}) = \frac{Y(e^{j\omega})}{X(e^{j\omega})} = 0.25 + e^{-j\omega} + 0.25e^{-2j\omega}$$

$$= e^{-j\omega}(0.25e^{j\omega} + 1 + 0.25e^{-j\omega}) = e^{-j\omega}(1 + 0.5 \cos \omega)$$

$$= e^{-j\omega} \bar{H}(e^{j\omega}) \quad (6.4)$$

Comparing Eq. (6.41a) with Eq. (6.25) we get $\theta(\omega) = -\omega$.

$$\text{The phase delay } \tau_p = \frac{-\theta(\omega)}{\omega} = \frac{\omega}{\omega} = 1.$$

$$\text{The group delay} = -\frac{d\theta(\omega)}{d\omega} = \frac{-d}{d\omega}(-\omega) = 1.$$

4.

Solution If $z_2 = 2$ is a zero for a linear phase filter, then $z'_2 = 1/2$ is also a zero.

If $z_1 = \frac{1}{\sqrt{2}} + \frac{j}{\sqrt{2}}$, whose $|z| = 1$ is a zero, then $z'_1 = z_1^*$ is also a zero.

The total number of zeros are four

$$z_1 = \frac{1}{\sqrt{2}} + \frac{j}{\sqrt{2}}, z_1^* = \frac{1}{\sqrt{2}} - \frac{j}{\sqrt{2}}; z_2 = 2; z'_2 = \frac{1}{2}$$

$$H(z) = (1 - 2z^{-1}) \left(1 - \frac{1}{2}z^{-1}\right) \left[1 - \left(\frac{1+j}{\sqrt{2}}\right)z^{-1}\right] \left[1 - \left(\frac{1-j}{\sqrt{2}}\right)z^{-1}\right]$$

$$= \left(1 - \frac{5}{2}z^{-1} + z^{-2}\right) (1 - \sqrt{2}z^{-1} + z^{-2})$$

5.

The ideal magnitude response with samples for the given specification is shown in Fig. 6.59.

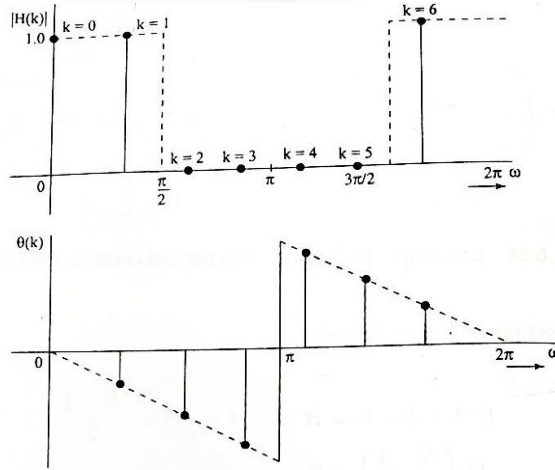


Fig. 6.59 Ideal magnitude and phase response with samples for example 6.15

Given $N = 7$

$$H(k) = H_d(e^{j\omega}) \Big|_{\omega=\frac{2\pi k}{7}} \quad k = 0, 1, 2, \dots, 6$$

From Fig. 6.59 we have

$$\begin{aligned} |H(k)| &= 1 \quad \text{for } k = 0, 1, 6 \\ &= 0 \quad \text{for } k = 2, 3, 4, 5 \end{aligned} \quad (6.140)$$

Using Eq.(6.126) we have

$$\begin{aligned} \theta(k) &= - \left(\frac{N-1}{N} \right) \pi k = -\frac{6}{7} \pi k \quad \text{for } k = 0, 1, 2, 3 \\ &= (N-1)\pi - \left(\frac{N-1}{N} \right) \pi k = 6\pi - \frac{6\pi k}{7} = \frac{6\pi}{7} (7-k) \quad \text{for } k = 4, 5, 6 \end{aligned} \quad (6.141)$$

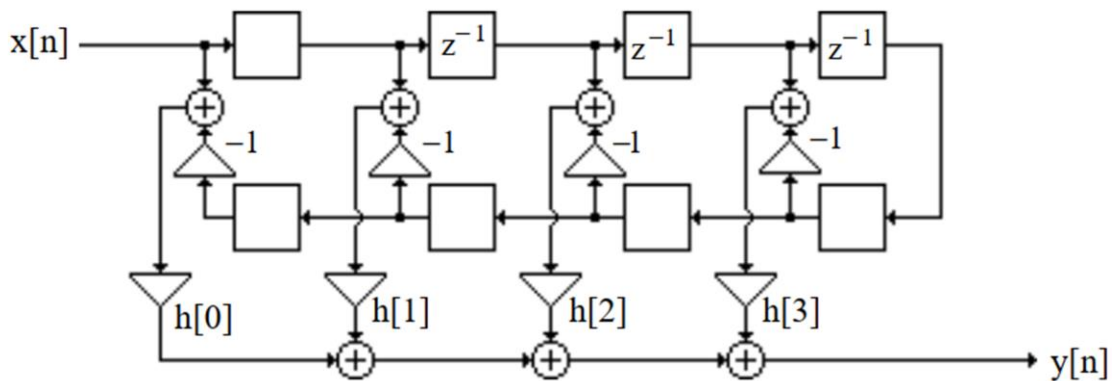
Now the frequency response of the linear phase filter can be written by substituting Eq.(6.140) and Eq.(6.141) in Eq.(6.120)

$$\begin{aligned} H(k) &= e^{-j6\pi k/7} \quad k = 0, 1 \\ &= 0 \quad \text{for } k = 2, 3, 4, 5 \\ &= e^{-j6\pi(k-7)/7} \quad \text{for } k = 6 \end{aligned}$$

The filter coefficients for N odd are given by

$$\begin{aligned}
 h(n) &= \frac{1}{N} \left\{ H(0) + 2 \sum_{k=1}^{\frac{N-1}{2}} \operatorname{Re} \left[H(k) e^{j2\pi kn/7} \right] \right\} \quad n = 0, 1, \dots, N-1 \\
 &= \frac{1}{7} \left\{ 1 + 2 \operatorname{Re} (e^{-j6\pi/7} e^{j2\pi kn/7}) \right\} \\
 &= \frac{1}{7} \left\{ 1 + 2 \operatorname{Re} (e^{j2\pi(n-3)/7}) \right\} \\
 &= \frac{1}{7} \left\{ 1 + 2 \cos \frac{2\pi}{7} (n-3) \right\} \\
 h(0) = h(6) &= \frac{1}{7} \left(1 + 2 \cos \frac{6\pi}{7} \right) = -0.11456 \\
 h(1) = h(5) &= \frac{1}{7} \left(1 + 2 \cos \frac{4\pi}{7} \right) = 0.07928 \\
 h(2) = h(4) &= \frac{1}{7} \left(1 + 2 \cos \frac{2\pi}{7} \right) = 0.321 \\
 h(3) &= \frac{1}{7} (1 + 2) = 0.42857
 \end{aligned}$$

6.



(all square boxes = z^{-1})

7. A. a) The filter is stable since its transfer function $H(z) = 1/(1-0.99z^{-1})$ has a pole $z=0.99$.

b) It is a low pass filter since it has a pole close to $z=1$ i.e. $\omega=0$.

B.

The passband ripple is given by $20 \log_{10} (1.05) = 0.42$ dB, and the attenuation in the stopband $-20 \log_{10} 0.005 = 46$ dB. The analog passband frequency is $0.3 \pi F_s / 2 \pi = 1.2$ kHz and the stopband $0.4 \pi F_s / 2 \pi = 1.6$ kHz

8.

Type 1: symmetric, odd

Type 2: symmetric, even

Type 3: antisymmetric, odd

Type 4: antisymmetric, even

The positions of zeros in the complex plane are as follows:

Type 1: Either an even number or no zeros at $z = 1$ and $z = -1$

Type 2: Either an even number or no zeros at $z = 1$, and an odd number of zeros at $z = -1$

Type 3: An odd number of zeros at $z = 1$ and $z = -1$

Type 4: An odd number of zeros at $z = 1$, and either an even number or no zeros at $z = -1$

9.

$$M = 15. H_r\left(\frac{2\pi k}{15}\right) = \begin{cases} 1, & k = 0, 1, 2, 3 \\ 0.4, & k = 4 \\ 0, & k = 5, 6, 7 \end{cases}$$

$$H_r(w) = h\left(\frac{M-1}{2}\right) + 2 \sum_{n=0}^{\frac{M-3}{2}} h(n) \cos w\left(\frac{M-1}{2} - n\right)$$

$$h(n) = h(M-1-n)$$

$$h(n) = h(14-n)$$

$$H_r(w) = h(7) + 2 \sum_{n=0}^6 h(n) \cos w(7-n)$$

Solving the above eqn yields,

$$h(n) = \{0.3133, -0.0181, -0.0914, 0.0122, 0.0400, -0.0019, -0.0141, 0.52, 0.52, -0.0141, -0.0019, 0.0400, 0.0122, -0.0914, -0.0181, 0.3133\}$$

10.

(a) There are only zeros, thus $H(z)$ is FIR.

(b)

$$\begin{aligned}\text{Zeros: } z_1 &= -\frac{4}{3}, \\ z_2 &= -\frac{3}{4}, \\ z_{3,4} &= \frac{3}{4}e^{\pm j\frac{\pi}{3}} \\ z_{5,6} &= \frac{4}{3}e^{\pm j\frac{\pi}{3}}\end{aligned}$$

$$\begin{aligned}z_7 &= 1 \\ \text{Hence, } z_2 &= \frac{1}{z_1^*} \\ z_4 &= z_3^* \\ z_5 &= \frac{1}{z_3^*} \\ z_6 &= z_5^* \\ z_1 &= \frac{1}{z_7} = 1 \\ \text{and } H(z) &= z^{-6}H(z^{-1})\end{aligned}$$

Therefore, $H(w)$ is linear phase.