

# Tutorial

Subject : RF and Microwave Engineering  
(EC31005)

Q1. A terminated transmission line with  $Z_0 = 60 \Omega$  has a reflection co-efficient at the load of  $0.4\angle 60^\circ$

- a) What is the load impedance?
- b) What is the reflection coefficient  $0.3\lambda$  away from the load?
- c) What is the input impedance at this point?

ANSWER:

(a)  $Z_0 = 60\Omega$

$$\Gamma_L = 0.4\angle 60^\circ$$

$$\Gamma_L = \frac{Z_L - Z_0}{Z_L + Z_0} = 0.2 + j0.346$$

Load reflection coefficient

$$Z_L = (66.43 + j54.7)\Omega$$

Load Impedance

- (b) The line reflection coefficient is

$$\Gamma_L(l) = \Gamma_L e^{-j2\beta l} = 0.4\angle -156^\circ$$

$$(c) \quad \tan \beta l = -3.07$$

$$Z_{in} = Z_o \frac{Z_L + jZ_o \tan \beta l}{Z_o + jZ_L \tan \beta l} = (26.65 - j10.24)\Omega$$

Q2. A lossless transmission line is terminated with a  $100 \Omega$  load. If the SWR on the line is 1.5, find the two possible values for the characteristic impedance of the line.

ANSWER:

$$|\Gamma| = \frac{(S-1)}{(S+1)} = \frac{0.5}{2.5} = 0.2$$

SWR is denoted as S

$$|\Gamma| = \left| \frac{Z_L - Z_o}{Z_L + Z_o} \right| = \left| \frac{100 - Z_o}{100 + Z_o} \right|$$

$$\Gamma = \pm 0.2$$

Either

$$\frac{100 - Z_o}{100 + Z_o} = 0.2 \Rightarrow Z_o = 100 * \left( \frac{1 - \Gamma}{1 + \Gamma} \right) = 66.7 \Omega$$

or

$$\frac{100 - Z_o}{100 + Z_o} = -0.2 \Rightarrow Z_o = 100 * \left( \frac{1 - \Gamma}{1 + \Gamma} \right) = 150 \Omega$$

Q3. A radio transmitter is connected to an antenna having an impedance  $80 + j40 \Omega$  with a  $50 \Omega$  coaxial cable. If the  $50 \Omega$  transmitter can deliver 30 W when connected to a  $50 \Omega$  load, how much power is delivered to the antenna?

Given: load impedance  $Z_L = 80 + j40 \Omega$ ,

Coaxial cable impedance  $Z_0 = 50 \Omega$ ,

Now the reflection coefficient is given by,  $\Gamma = \frac{Z_L - Z_0}{Z_L + Z_0}$

Substituting the values of  $Z_L$  and  $Z_0$ ,  $\Gamma = \frac{80 + j40 - 50}{80 + j40 + 50} = 0.296 + j0.215$

And  $|\Gamma| = 0.366$

Now given that the transmitter can deliver 30 W when connected to a  $50 \Omega$  load i.e. the matched load condition, It means the Incident power = 30 W.

Hence the power delivered to the antenna (Load) =  $P_{\text{incident}} - P_{\text{reflected}} = P_{\text{incident}} [1 - |\Gamma|^2]$ .....(i)

Substituting the values of  $P_{\text{incident}}$  and  $|\Gamma|$  in equation (i),

$$P_{\text{load}} = 30[1 - 0.366^2] = 25.98 \text{ W}$$

Hence Power delivered to the Antenna is = 25.98 W.

Q4. The transmission line circuit in the accompanying figure has  $V_g = 15 \text{ V rms}$ ,  $Z_g = 75 \Omega$ ,  $Z_0 = 75 \Omega$ ,  $Z_L = 60 - j40 \Omega$ , and  $l = 0.7\lambda$ . Compute the power delivered to the load using three different techniques:

a. Find  $\Gamma$  and compute

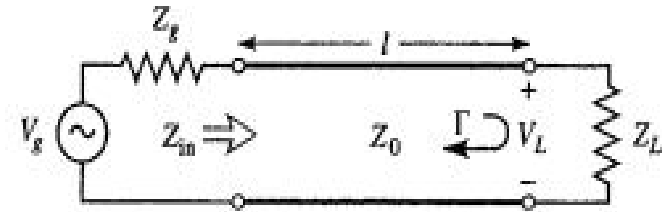
$$P_L = (V_g^2/4) \frac{1}{Z_0} (1 - |\Gamma|^2)$$

b. Find  $Z_{in}$  and compute

$$P_L = \frac{(V_g)^2}{(Z_g + Z_{in})^2} \text{Re}\{Z_{in}\}$$

c. Find  $V_L$  and compute

$$P_L = |V_L/Z_L|^2 \text{Re}\{Z_L\}$$



Given: load impedance  $Z_L = 60 - j40 \Omega$ ,

Transmission line characteristic impedance  $Z_0 = 75 \Omega$ ,

Now the reflection coefficient is given by,

$$\Gamma = \frac{Z_L - Z_0}{Z_L + Z_0}$$

Substituting the values of  $Z_L$  and  $Z_0$ ,  $\Gamma = \frac{60 - j40 - 75}{60 - j40 + 75} = -0.021 - j0.302$

$$\text{and } |\Gamma| = 0.3027$$

contd.

a. Substituting the values of  $V_g$  and  $|\Gamma|$  to compute  $P_L$ ,

$$\text{Hence } P_L = \left(\frac{15^2}{4}\right) \frac{1}{75} (1 - 0.3027^2) = \mathbf{0.681 \text{ W.}}$$

b. As the input impedance of a transmission line is given as,

$$Z_{in} = Z_0 \frac{Z_L + jZ_0 \tan \beta l}{Z_0 + jZ_L \tan \beta l} \dots\dots\dots (i), \text{ Where } \beta = 2\frac{\pi}{\lambda}$$

Substituting the values of  $Z_0$ ,  $Z_L$ , and  $l$  in equation (i),

$$Z_{in} = 75 \frac{60 + j190.8}{198.1 + j184.7} = 48.2 + j27.3 \Omega$$

Substituting the values of  $V_g$  and  $Z_g$  and  $Z_{in}$  to compute  $P_L$ ,

$$\text{Hence } P_L = \frac{(15)^2}{(75 + 48.2 + j27.3)^2} (48.2) = \mathbf{0.681 \text{ W.}}$$

c. As Voltage at a point a distance  $x$  from the load is given by,

$$V(x) = V^+(e^{-j\beta x} + \Gamma e^{+j\beta x}) \quad \text{where } V^+ = \frac{V_a}{2} = 7.5 \text{ V}$$

Hence the voltage at load i.e. at  $x=0$ ,

$$V_L = V(0) = v^+(1 + \Gamma) \dots\dots\dots (ii) \quad \text{contd.}$$

Substituting the values of  $V^+$ ,  $\Gamma$  in equation (ii) to compute  $V_L$ ,

$$\text{Hence } V_L = 7.5(1 - 0.021 - j0.302) = 7.3425 - j2.265$$

$$\text{And } |V_L| = 7.68$$

Substituting the value of  $V_L$ , to compute  $P_L$ ,

$$\text{Hence } P_L = |(7.3425 - j2.265)/(60 - j40)|^2 \operatorname{Re}\{60 - j40\}$$

$$= |7.68/72.1|^2 (60)$$

$$= \mathbf{0.681 \text{ W}}$$



Q5. For a purely reactive load impedance of the form  $Z_L = jX$ , show that the reflection coefficient magnitude  $|\Gamma|$  is always unity. Assume that the characteristic impedance  $Z_0$  is real.

Ans: Given,

$$Z_L = jX$$

The value of reflection co-efficient is:

$$\Gamma = \frac{Z_L - Z_0}{Z_L + Z_0} = \frac{jX - Z_0}{jX + Z_0}$$

$$\Gamma^* = \frac{-jX - Z_0}{-jX + Z_0}$$

$$|\Gamma|^2 = \Gamma \Gamma^* = \frac{jX - Z_0}{jX + Z_0} \times \frac{-jX - Z_0}{-jX + Z_0} = \frac{X^2 - jZ_0 X + jZ_0 X + Z_0^2}{X^2 - jZ_0 X + jZ_0 X + Z_0^2} = 1$$

Q6. A  $50\ \Omega$  transmission line is matched to a  $10\text{ V}$  source and feeds a load  $Z_L = 100\ \Omega$ . If the line is  $2.3\lambda$  long and has an attenuation constant  $\alpha = 0.5\text{ dB}/\lambda$ , find the powers that are delivered by the source, lost in the line, and delivered to the load  
(Additional  $\beta l = 108^\circ$ )

Ans:

$$Z_0 = Z_g = 50\ \Omega, V_g = 10\text{ V}, Z_L = 100\ \Omega, l = 2.3\ \lambda, \alpha = 0.5\text{ dB}/\lambda$$

$$\alpha = 0.5\text{ dB}/\lambda = 0.0576\text{ neper}/\lambda \quad (\text{Since } 1\text{ Neper} = 8.68\text{ dB})$$

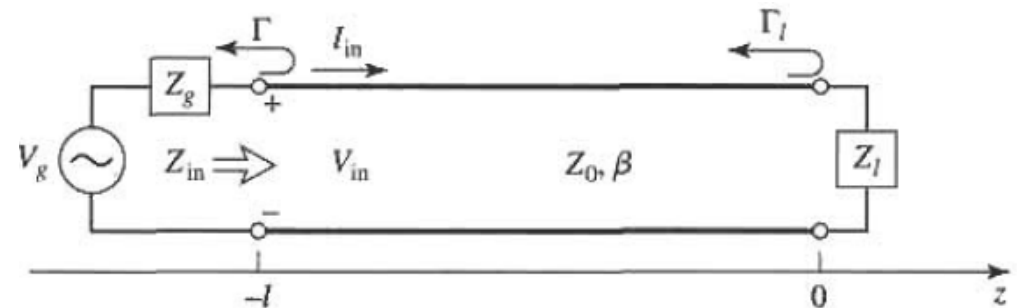
Since the generator is matched to the line, reflection coefficient seen looking into source  $\Gamma_g = 0$  in the formula

$$V_0^+ = V_g \frac{Z_0}{Z_0 + Z_g} \frac{e^{-\gamma l}}{1 - \Gamma_L \Gamma_g e^{-2\gamma l}} \quad (\text{eq 2.71})$$

where  $V_0^+$  is the incident voltage referenced at  $z = 0$

$$\text{Thus, } V_0^+ = \frac{V_g}{2} e^{-\gamma l}$$

$$\gamma l = (\alpha + j\beta) l = 0.1325 + j108^\circ$$



Ref: fig. 2.19 Terminated lossy line page 76  
D.M. Pozar 4<sup>th</sup> edition

Thus,

$$V_0^+ = \frac{10}{2} e^{-\alpha l} = 4.38V$$

$$\Gamma = \frac{Z_L - Z_0}{Z_L + Z_0} = \frac{100 - 50}{100 + 50} = 0.33 \text{ (}\Gamma \text{ is reflection coefficient at load)}$$

$$\Gamma(l) = \Gamma e^{-2\gamma l} = \text{reflection coefficient at distance } l \text{ from load}$$

$$\text{Power delivered to line } P_{in} = \frac{|V_0^+|^2}{2Z_0} [1 - |\Gamma(l)|^2] e^{2\alpha l} = \frac{4.38^2}{100} [e^{2(0.1325)} - 0.333^2 \cdot e^{-2(0.1325)}] = 0.2337W \text{ (eq 2.92)}$$

$$\text{Power delivered to load } P_L = \frac{|V_0^+|^2}{2Z_0} [1 - |\Gamma|^2] = \frac{4.38^2}{100} [1 - 0.333^2] = \mathbf{0.1706W} \text{ (eq 2.93)}$$

$$P_{loss} = P_{in} - P_L = 0.2337 - 0.1706 = \mathbf{0.0631W} \text{ (eq 2.94)}$$

Input impedance is

$$Z_{in} = Z_0 \frac{Z_L + Z_0 \tanh \gamma l}{Z_0 + Z_L \tanh \gamma l} = 50 \frac{100 + 50(0.845 + j2.19)}{50 + 100(0.845 + j2.19)} = 32.5 - j12.4 \Omega$$

Input current is

$$I_{in} = \frac{V_g}{R_g + Z_{in}} = \frac{10}{82.5 - j12.4} = 0.1199 \angle 8.5^\circ \text{ A}$$

Generator power is

$$P_s = \frac{V_g}{2} |I_{in}| = 5(0.1199) = \mathbf{0.6W}$$

Power lost in  $R_g$  =

$$P_{R_g} = \frac{1}{2} |I_{in}|^2 R_g = \frac{1}{2} |0.1199|^2 50 = 0.3594 \text{ W}$$

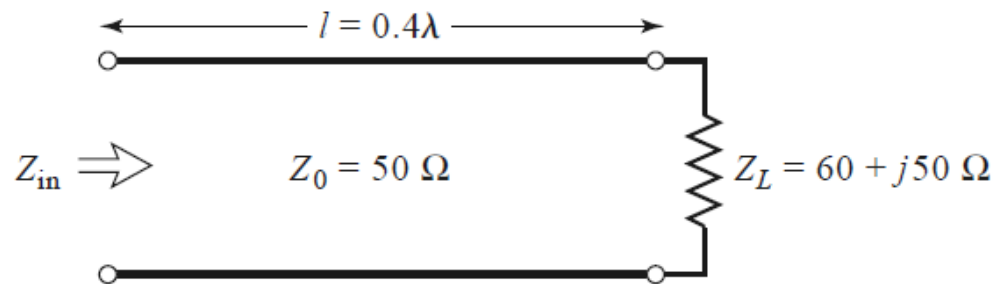
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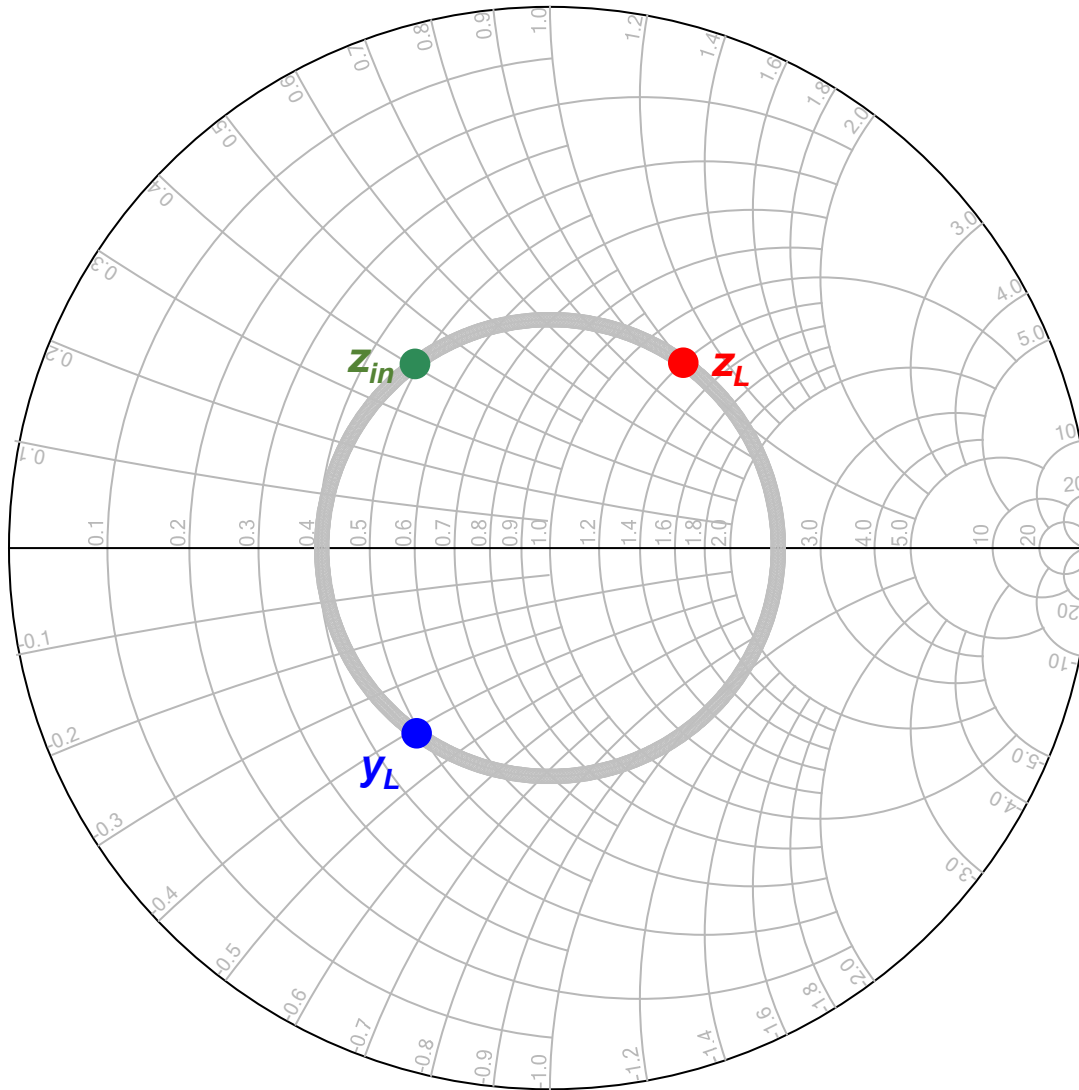
$$P_L + P_{loss} + P_{R_g} = 0.1706 + 0.0631 + 0.3594 = 0.5931 \text{ W} = P_s$$

$$P_{in} + P_{R_g} = 0.2337 + 0.3594 = 0.5931 \text{ W} = P_s$$

Q7. Use the Smith chart to find the following quantities for the transmission line circuit shown in the accompanying figure:

- (a) The SWR on the line.
- (b) The reflection coefficient at the load.
- (c) The load admittance.
- (d) The input impedance of the line.
- (e) The distance from the load to the first voltage minimum.
- (f) The distance from the load to the first voltage maximum.





First, mark normalized load impedance ( $z_L$ ) in the Smith Chart

$$z_L = Z_L / 50 = 1.2 + j1$$

(a) Draw a circle through  $z_L$ .  
This will give  $\text{SWR} = 2.46$ .

(b) Measure the angle and read the magnitude

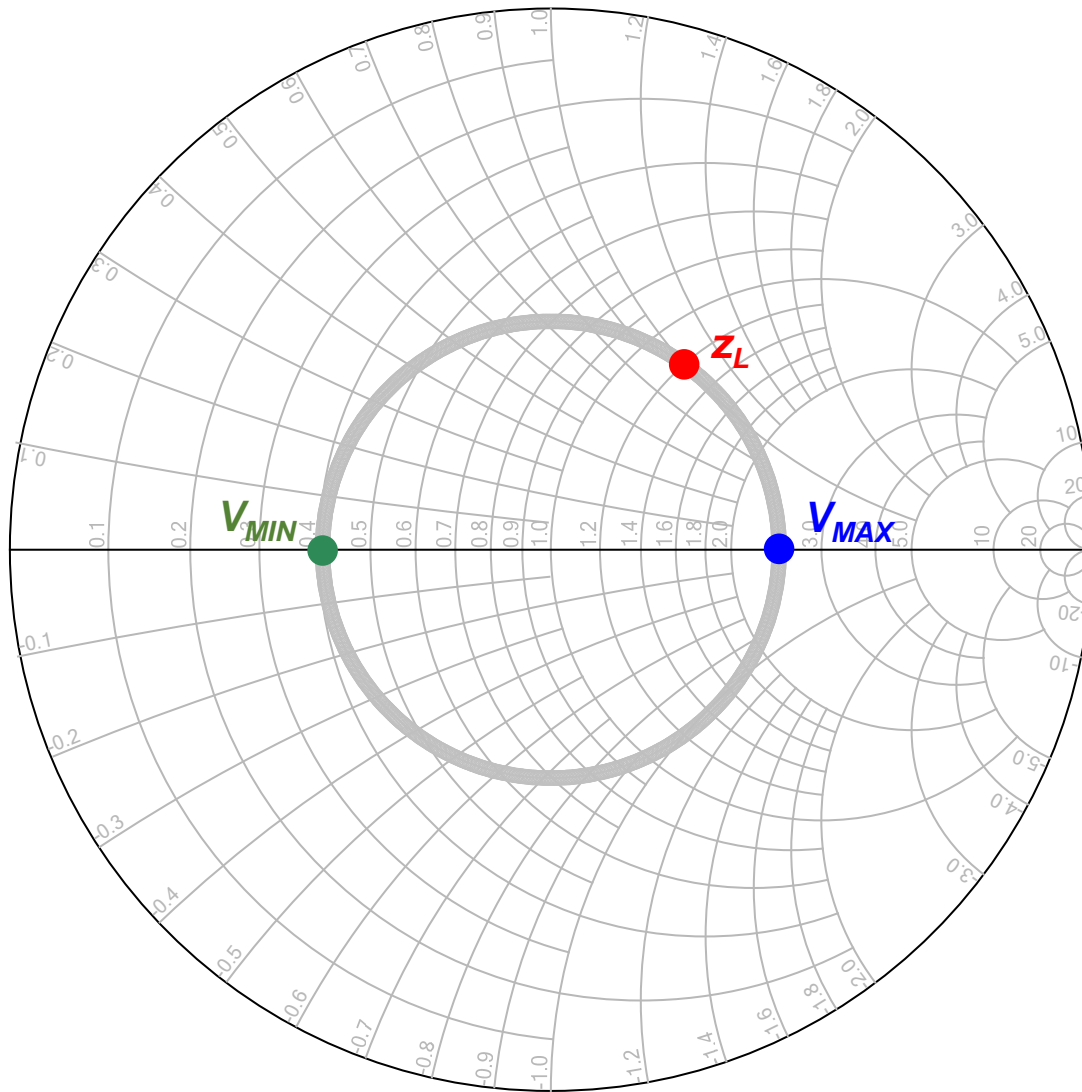
$$\Gamma = 0.422 \angle 54^\circ$$

(c) Move  $180^\circ$  along VSWR circle to get  $y_L$ .

$$Y_L = (0.492 - j0.412) / 50 = (9.84 - j8.2) \text{ mS}$$

(d) Traverse in the clock-wise direction along constant VSWR circle by  $0.4 \lambda$  to get  $z_{in}$

$$Z_{in} = (24.5 + j20.3) \Omega$$



(e)  $l_{MIN} = 0.325\lambda$

(f)  $l_{MAX} = 0.075\lambda$

At  $V_{MAX}$  location, the resistance will be the highest and reactive part is 0.

At  $V_{MIN}$  location, the resistance will be the lowest and reactive part is 0. Observe that, it is  $0.25\lambda$  more distant.

For both these cases, you have to traverse along VSWR circle in clock-wise direction.

Q8. Use the Smith chart to find the shortest lengths of a short-circuited  $75\ \Omega$  line to give the following input impedance:

(a)  $Z_{in} = 0$ .

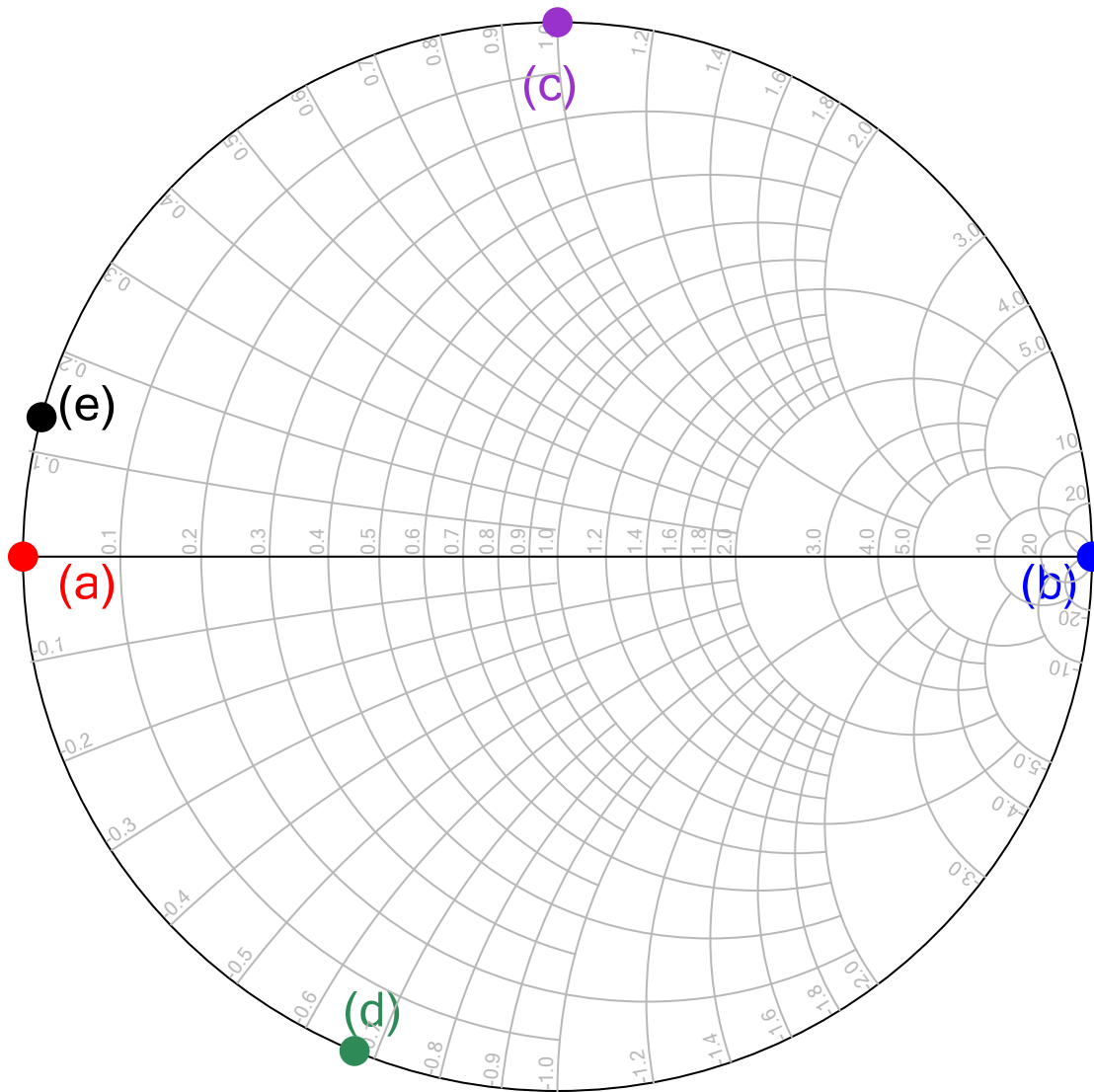
(b)  $Z_{in} = \infty$ .

(c)  $Z_{in} = j75$ .

(d)  $Z_{in} = -j50$ .

(e)  $Z_{in} = j10$





(a)  $Z_{in} = 0$ .

(a)  $L = 0$  or  $0.5 \lambda$

(b)  $Z_{in} = \infty$ .

(b)  $L = 0.25 \lambda$

(c)  $Z_{in} = j75$ .

(c)  $L = 0.125 \lambda$

(d)  $Z_{in} = -j50$ .

(d)  $L = 0.406 \lambda$

(e)  $Z_{in} = j10$

(e)  $L = 0.021 \lambda$

You have to traverse in the clock-wise direction along constant VSWR circle which is the outermost circle for all the cases.

For, (c), (d) and (e) just mark the normalized input impedance, which is,

$$z_{in} = Z_{in} / 75$$

and calculate the distance from the load (here, S.C point or (a) is the load) in the clock-wise direction.