# Design and Implementation of a Multi-element radio interferometric array

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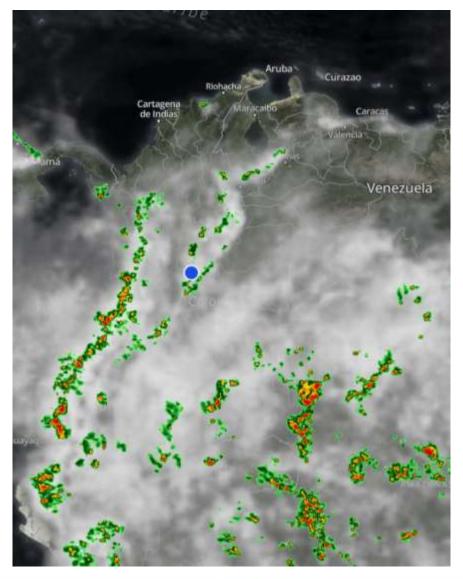
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2024



#### Introduction



Radio astronomy is a field that is gradually growing in Colombia thanks to several projects aiming to a more viable way of performing astronomical studies in a country whose climate conditions are predominantly cloudy.

Solar radio emissions account for different emission processes and the medium in which these are generated in the solar atmosphere.

#### Main Goal:

Design and implement a multi-element radio interferometer, each one with a collector dish, for observations at 1,42 GHz.





#### Introduction

The Phased Array Radio Interferometer at 21cm in the Observatorio Astronómico Nacional (PhAraON) is a novel prototype of radio interferometer, with Yagi-Uda antennas fabricated as printed circuit boards, with resonance frequency of 1,42GHz ( $\lambda$ =21 cm).

Stage 1 of PhAraON is a 2-element drift solar radio interferometer developed as a **Bachelor's** Thesis in Electronics Engineering at the Department of Electric and Electronics Engineering - Universidad Nacional de Colombia in 2016 [7], where antennas were deployed in a 2X2 array configuration, on an East-West baseline. Later a Sum-Difference coupler circuit working as an analog correlator, and USB dongles as signal receivers are used. This is considered as precursor stage of the ongoing project.

The current design uses these identical Yagi-Uda printed antennas at the focal point of a reflector dish, in order to enhance its directivity, hence its sensitivity.





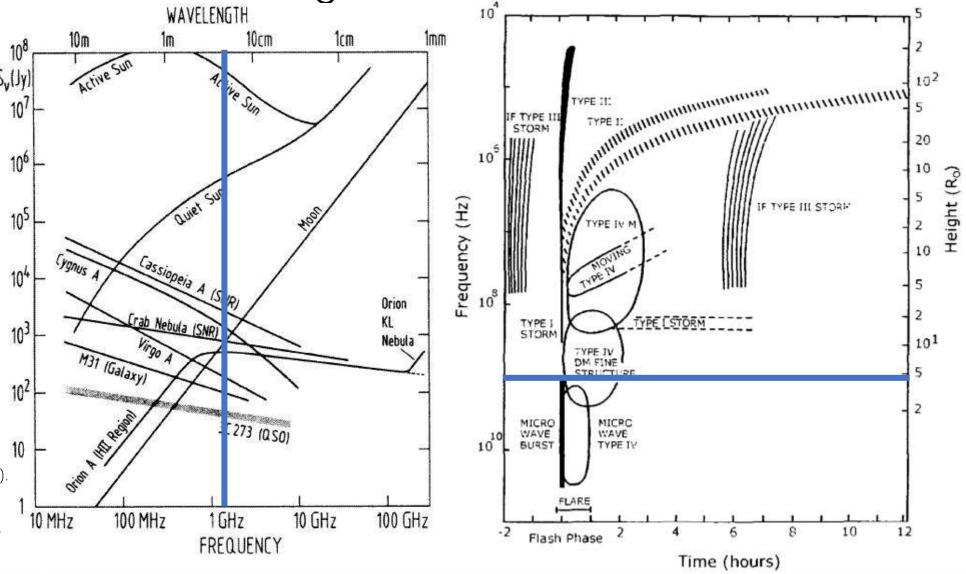


Figure 1: Flux of Several Astronomical Sources in Radio Frequency (Left). Classification of Solar Radio Bursts (Right).

The blue line highlights the 1,42GHz frequency of interest for our instrument.







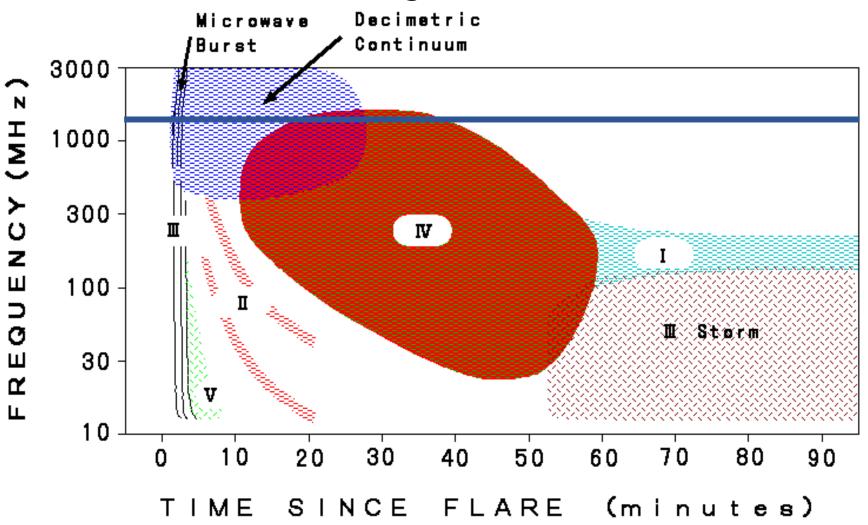


Figure 2: Schematic diagram showing the Classification of Solar Radio Bursts. Taken from NICT (http://sunbase.nict.go.jp/solar/denpa/hiras/types.html)



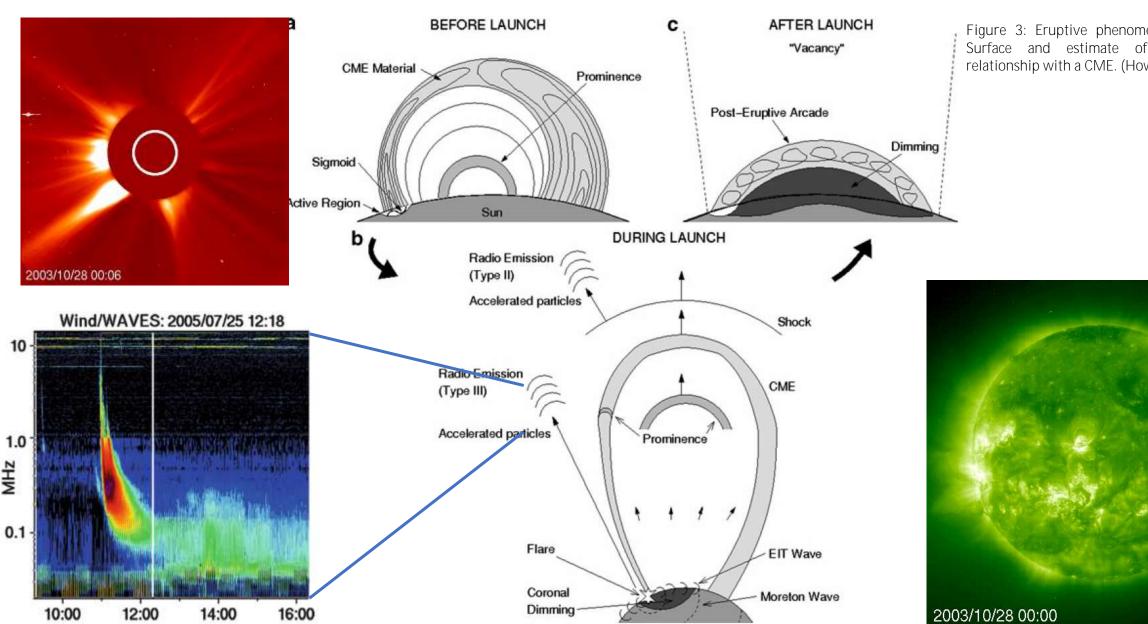


Figure 3: Eruptive phenomena on the solar Surface and estimate of their physical relationship with a CME. (Howard, 2011).

III	Fast frequency drift bursts.	Single Burst: 1 - 3 s	10 kHz -1 GHz	Active Regions,
	Occur singularly, in groups or	Groups: 1 - 5 min		Flares
	storms. Accompanied by	Storm: min - Hours		
	a second harmonic			
	Stationary Type IV.	hours- days	20 MHz - 2 GHz	Flares, Proton
IV	Broadband Continuum			emission
	with fine structure			
	Moving Type IV.	30 min - 2 hours	20 - 400 MHz	Eruptive
	Broadband, slow frequency drift			prominences,
	with smooth continuum			MHD shock waves
	Flare Continua.	3 - 45 min	25 - 200 MHz	Flares, Proton
	Broadband, smooth Continuum			emission

Figure 4: Classification of Solar Radio Bursts. Taken from Space Weather Services, Australian Bureau of Meteorology (http://www.sws.bom.gov.au/World\_Data\_Centre/1/9/3)

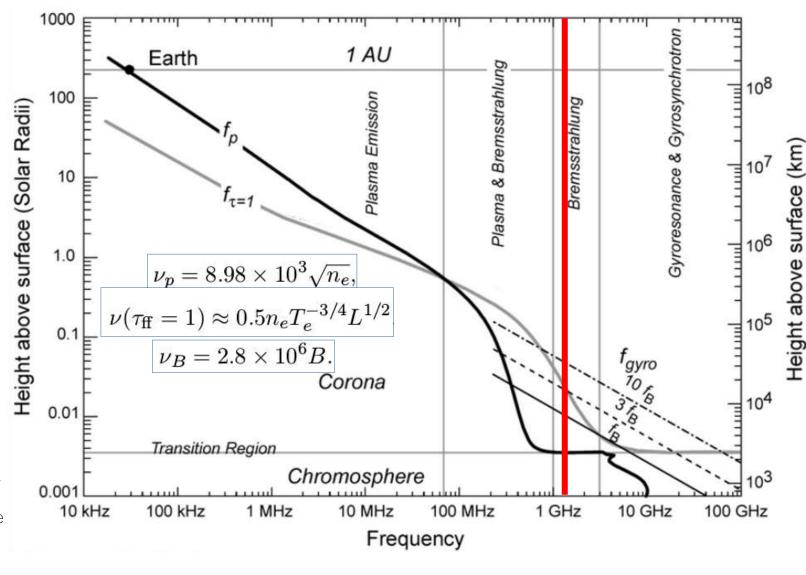






# 2024-03-29 00:05:46 UT

Figure 5. Left: EUV image from the Solar Dynamics Observatory (SDO) in the Fe IX line at 171 Å (March 29, 2024 – 00:05 UTC) Right: Characteristic Radio Frequencies for the solar atmosphere and the dominating type of emission mechanism (Gary, 2014)









### Previous Stage



Figure 6: 2-element drift Solar Radio Interferometer Installation. Observatorio Astronómico Nacional, Campus Building. (Hincapié Tarquino et. al. 2016). Left: Array installation. Top, Center: Antenna element in 2x2 Yagi-Uda antenna configuration. Top, Right: Rat-race coupler as analog correlator. Bottom, Right: Data acquisition & visualization system.







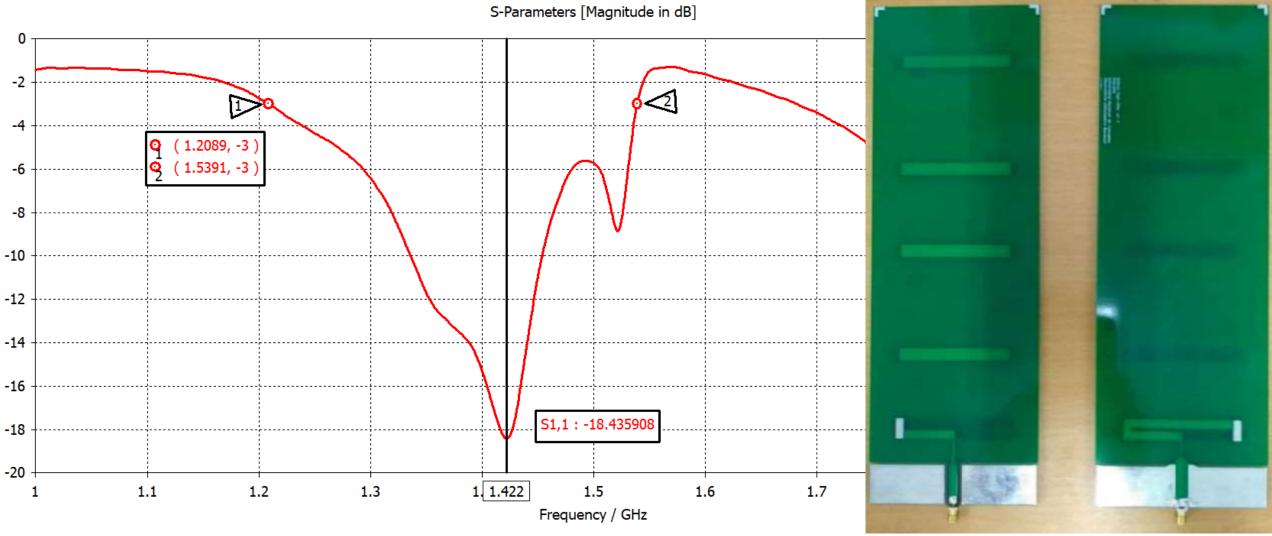


Figure 7. Left: Antenna Simulation: S11 Parameter - Antenna Reflection Coefficient. Right: Printed circuit Yagi-Uda antenna.



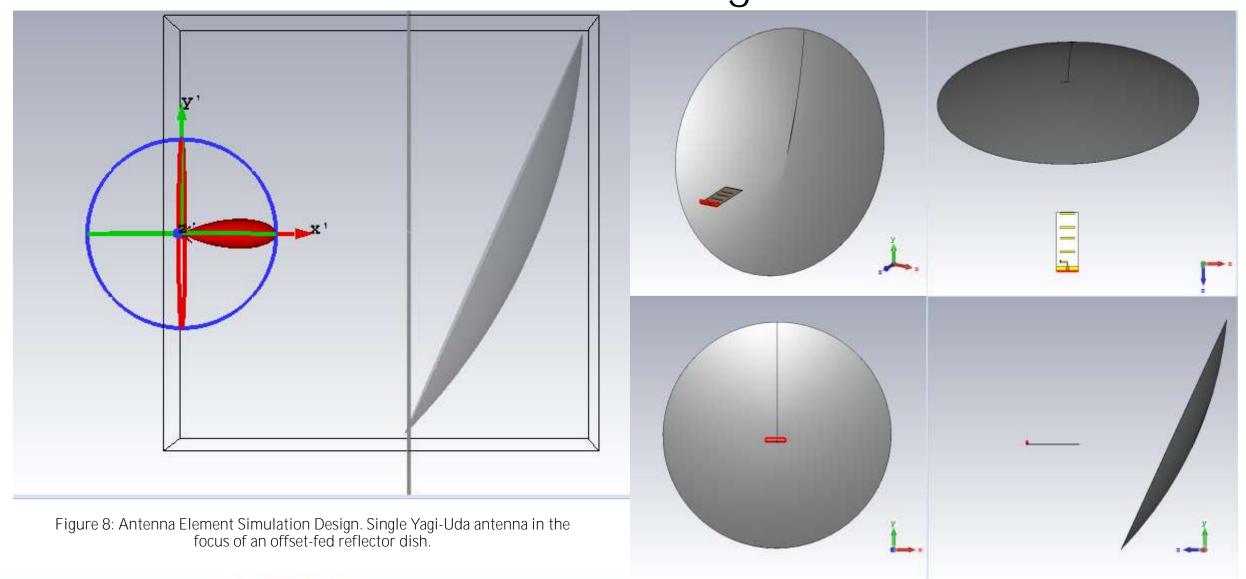
Simulations were performed in order to know the behavior of the antenna element, with the printed antenna on the focus of the parabolic reflector dish. This was done in two configurations for the feeding system: First as a single antenna (Figure 9), and then as a 2x2 array (Figure 10), as was used in the precursor drift interferometer.

Simulations results for the single antenna feed configuration yield higher gain and smaller side lobes in comparison with the 2x2 array. This means that the dish is subutilized with the 2x2 array. This was verified during the validation for all mechanical and RF systems, so the design chosen for the project is the single antenna configuration.

All simulations were performed in CST Microwave Studio Suite 1.











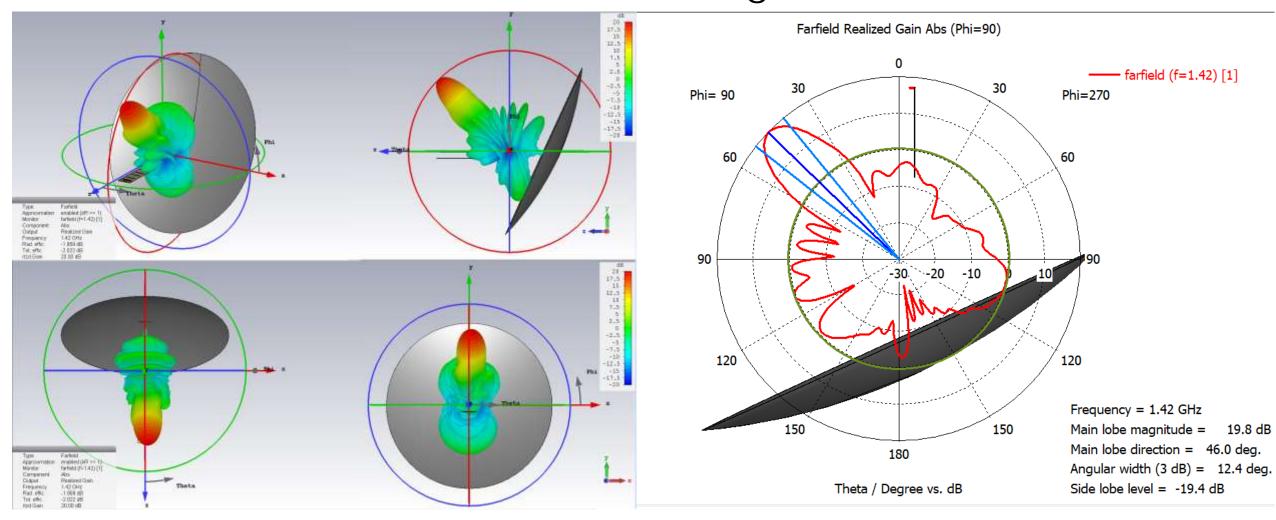


Figure 9: Antenna Simulation: 1 Antenna + Reflector. Realized Gain





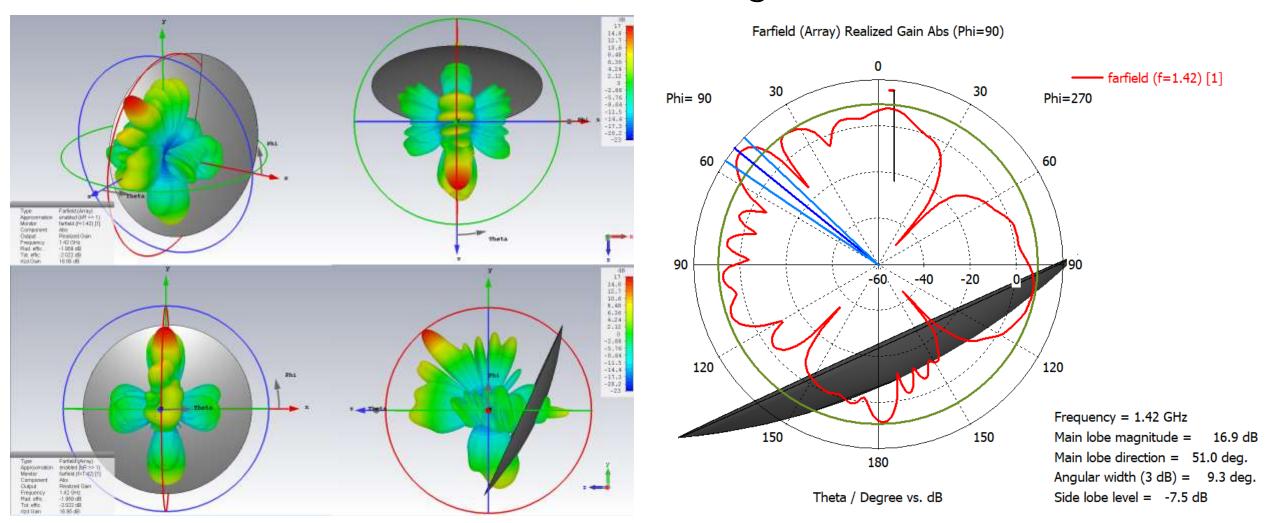


Figure 10: Antenna Simulation: 2x2 Antenna Array + Reflector. Realized Gain





	Isolated Antenna	2×2 Antenna	Single Antenna	2×2 Antenna Array
PARAMETER	without	Array without	with Offset-Fed	with Offset-Fed
	Reflector Dish [10]	Reflector Dish [10]	Reflector Dish	Reflector Dish
Input Reflection	-34.3583 dB	-34.3583 dB	-24.3591 dB	-24.3591 dB
Coefficient (S11	(at 1.422 GHz)	(at 1.422 GHz)	(at 1.422 GHz)	(at 1.422 GHz)
Parameter)				
Half-Power (-3 dB)	317.6 MHz	317.6 MHz	321 MHz	321 MHz
Bandwidth				
Directivity	10.99 dBi	15.56 dBi	21.96 dBi	20.07 dBi
Gain (IEEE)	9.397 dB	13.97 dB	20.18 dB	18.29 dB
Realized Gain	9.394 dB	13.96 dB	20.16 dB	18.28 dB
Half-Power	48.8 deg	31.1 deg	13.2 deg	9.9 deg
Beamwidth (HPBW)				
Front-to-Back	18.928 dB	18.924 dB	24.583 dB	22.002 dB
Ratio				

Figure 11: Simulation Result Summary for Single Yagi-Uda Antenna and 2X2 Antenna Array with Offset-Fed Reflector Dish



#### Steerable Pier: Preliminary and Final Design



Preliminary design for steerable pier consisted on a DC motor for azimuth motion and a DC actuator for elevation motion (Figure 12).

After preliminary tests were conducted for validation of RF and mechanical systems, we changed the design for a configuration of Stepper motors, each with reducer gearbox (Figure 13).

This, in order to get more torque and control for the antena motion. Additionally the actuator for elevation did not have uniform motion during the full







Azimuth & DC actuator for Elevation

# First Testing Phase



Figure 14: First Testing Phase with 2x2 Array Feed (Hincapié Tarquino et. al. in. prep.)







# First Testing Phase

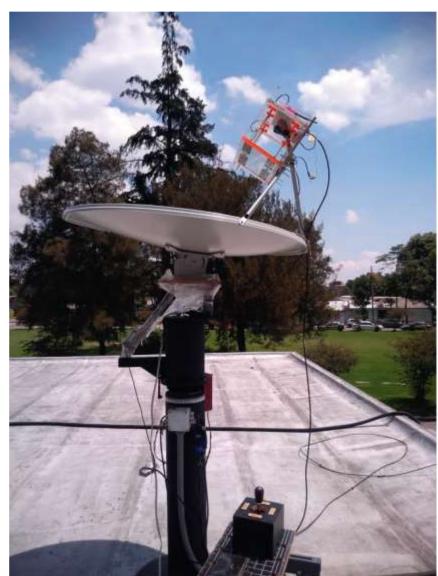
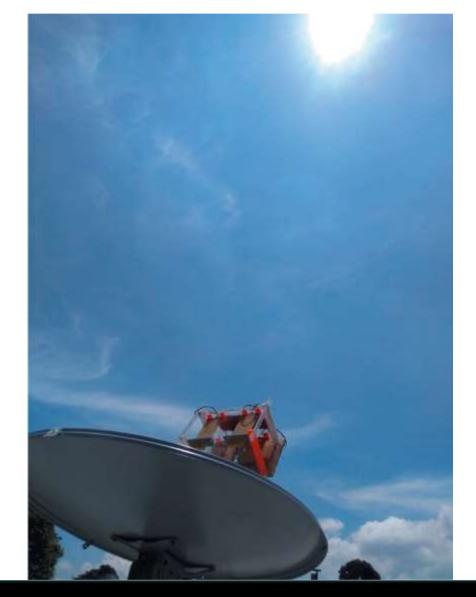


Figure 15: First Testing Phase with 2x2 Array Feed (Hincapié Tarquino et. al. in. prep.)







# Preliminary Results

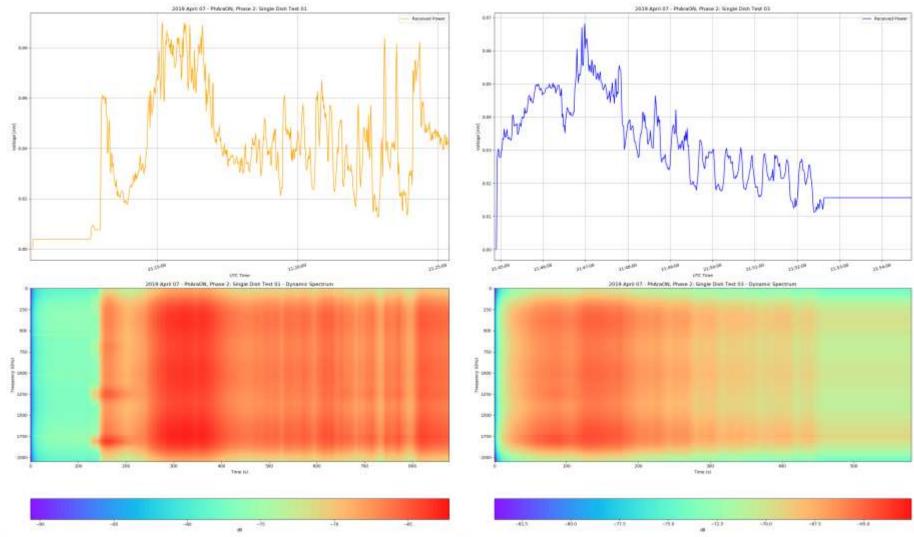


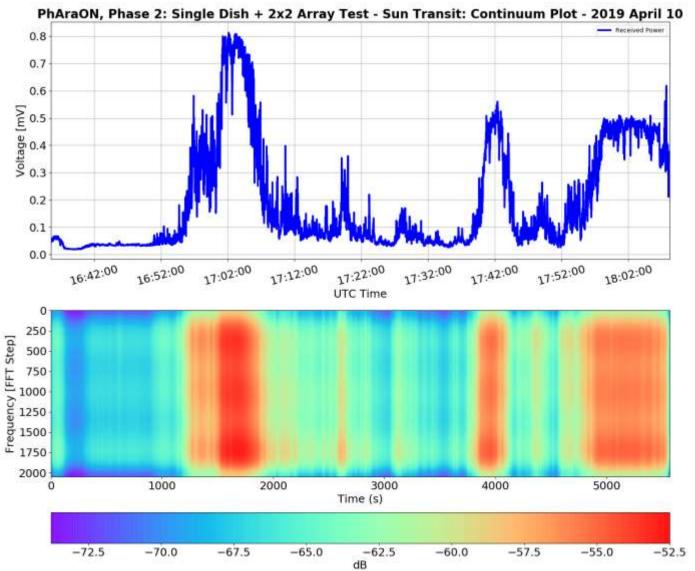


Figure 16: Preliminary Results: Solar Scan with 2x2 Array Feed





#### Preliminary Results









#### Preliminary Results



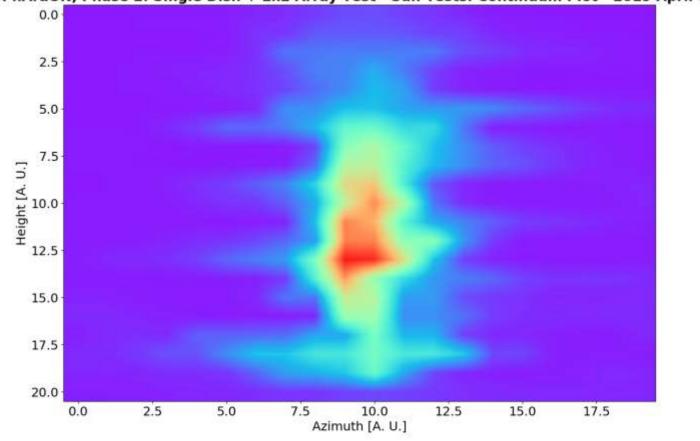
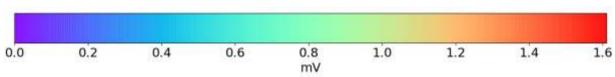


Figure 18: Preliminary Results: Solar Scan with 2x2 Array Feed. (Hincapié Tarquino et. al. in. prep.)







# Steerable Pier: Motor Assembly



Figure 19: Steerable Pier Assembly: Stepper Motor & Reducer Gearbox for each axis in Alt-Az motion. (Hincapié Tarquino et. al. in. prep.)





### Steerable Pier: Assembled elements



Figure 20: Installation of Antenna elements: Steerable Pier Assembly with reflector dish. (Hincapié Tarquino et. al. in. prep.)

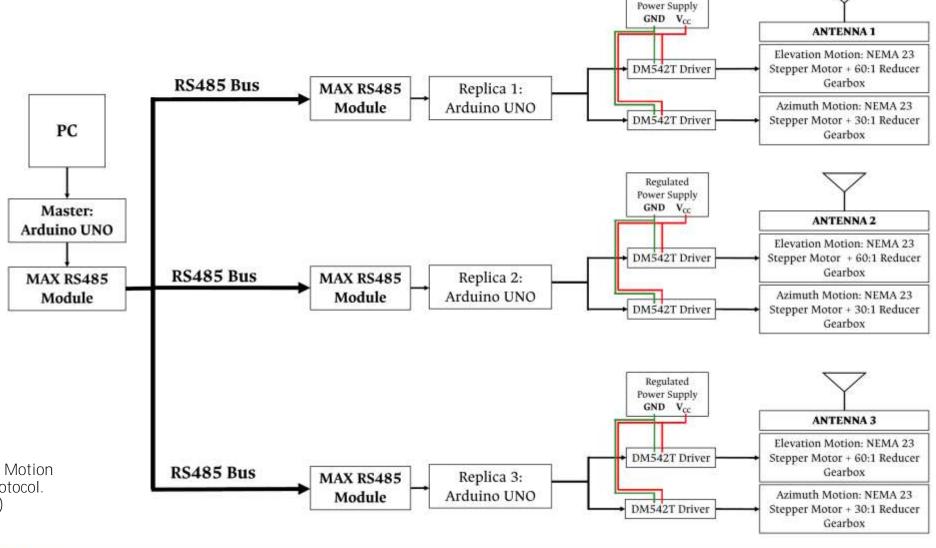




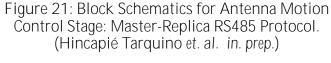


#### Steerable Pier: Motion Control

Antenna Motion Control Stage is implemented using RS485 serial protocol and Stellarium for automated control with an additional option for manual adjustment.



Regulated







#### RS485 serial protocol

Asyncronous serial communication. Uses Differential signal to transfer binary data from one device (Master)

to another (Replica)

- RS-485 supports a higher data transfer rate (30Mbps max).
- Maximum data transfer distance up to 1200 meters.
- Main advantage: multiple replicas with a single Master. (maximum of 32 devices connected).
- Immune to noise.
- RS-485 is faster compared to the I2C protocol.

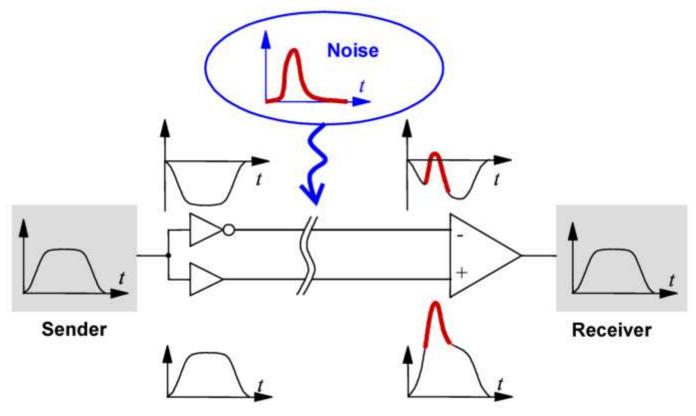


Figure 22: Schematics for communication using RS485 serial protocol.





# RS485 serial protocol

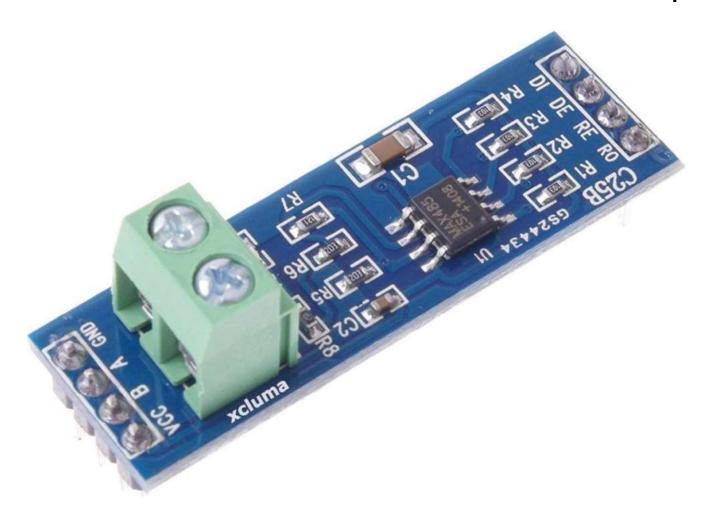


Figure 23: MAX RS485 serial module and pin descriptions.

Pin Name	Pin Description
VCC	5V
A	Non-inverting Receiver Input Non-Inverting Driver Output
В	Inverting Receiver Input Inverting Driver Output
GND	GND (0V)
R0	Receiver Out (RX pin)
RE	Receiver Output (LOW-Enable)
DE	Driver Output (HIGH-Enable)
DI	Driver Input (TX pin)





#### RS485 serial protocol

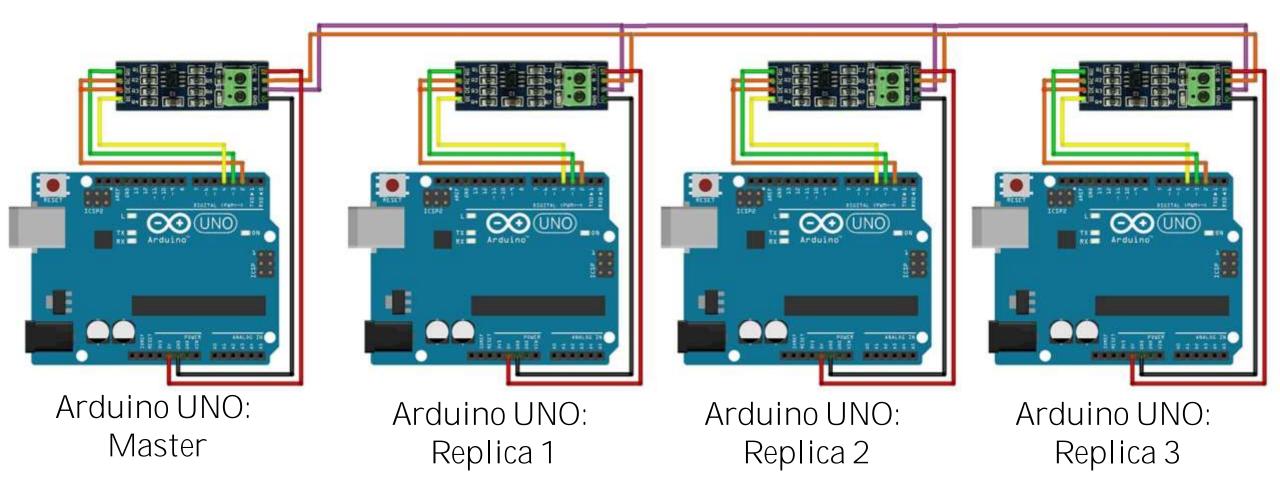


Figure 24: Connection diagram for Antenna Motion Control Stage: Master-Replica RS485 Protocol. (Hincapié Tarquino et. al. in. prep.)



#### Steerable Pier: Motion Control

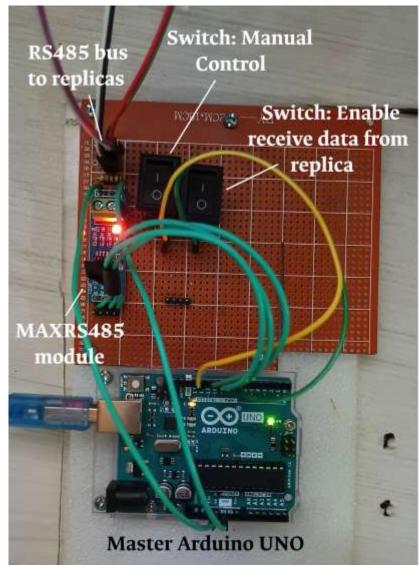




Figure 25: Control system for antenna motion control stage. Left: Master Arduino UNO with MAXRS485 module and bus to all replicas; Right: Isolated box with Replica Arduino UNO, MAXRS485 module and DMT542T drivers for each antenna element







#### Design: Array Implementation

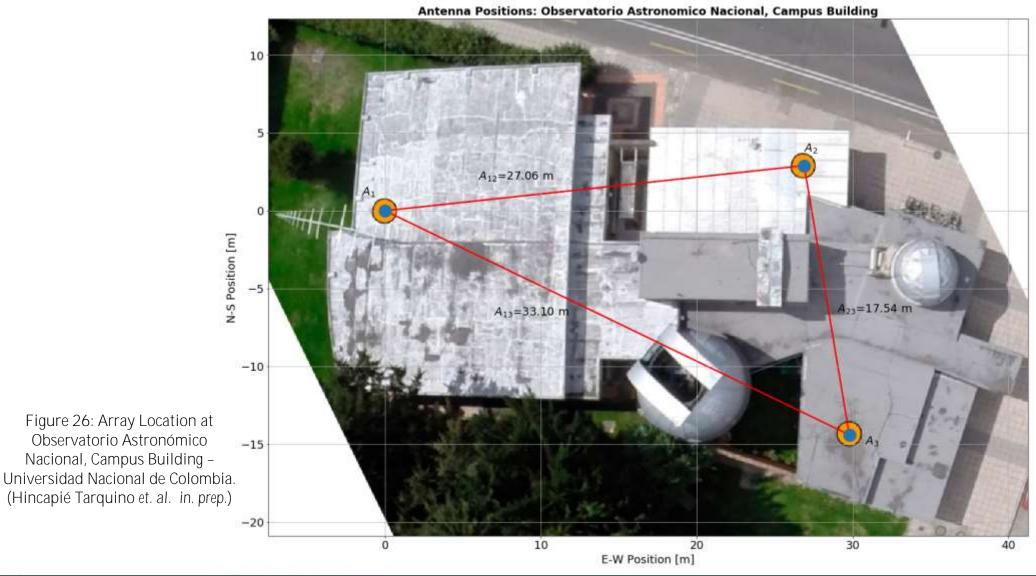




Figure 26: Array Location at Observatorio Astronómico Nacional, Campus Building -



### Design: Array Implementation

#### **Snapshot UV Coverage**

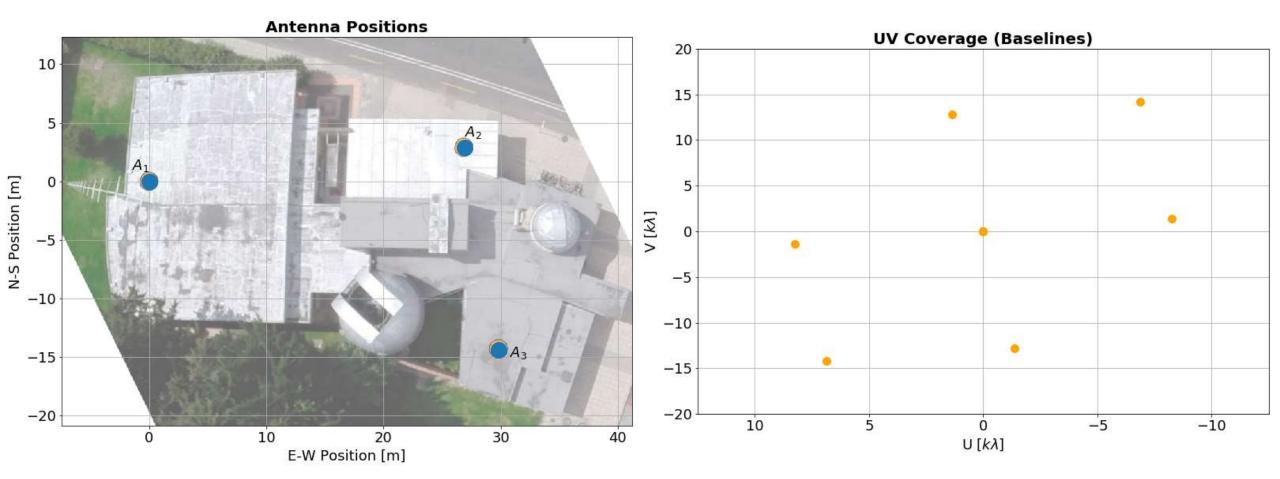


Figure 27: Snapshot UV Coverage for the interferometric array. (Hincapié Tarquino et. al. in. prep.)





#### Design: Array Implementation

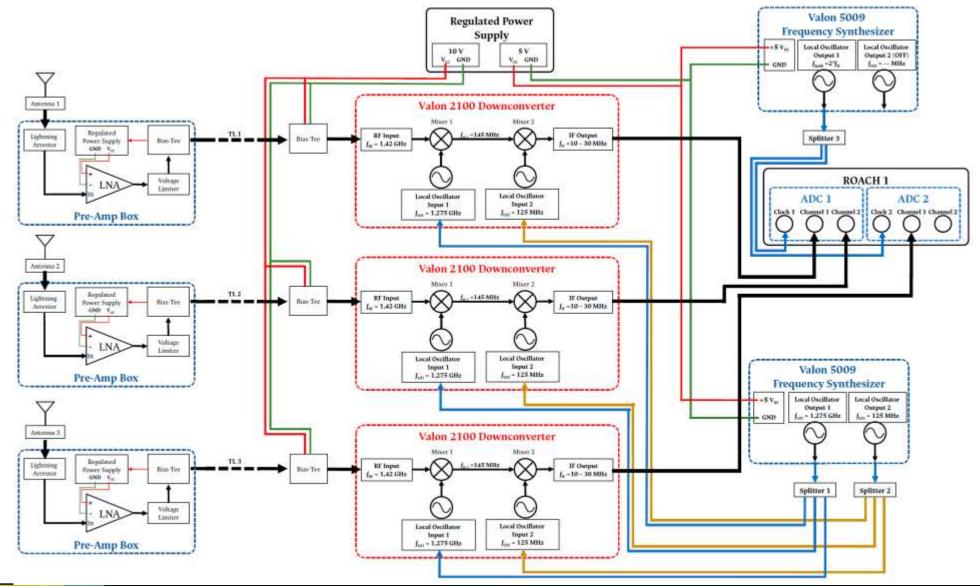


Figure 28: Block Schematics for full interferometric array. (Hincapié Tarquino et. al. in. prep.)

#### Front-End: Pre-Amp Stage

Pre-Amplification stage is based on the amplification stage used for several systems of the e-Callisto Solar Spectrometer Network. A similar stage is also used for FiCoRI, an interferometer dedicated to solar observations at the Observatorio Astronómico Nacional - Campus Building (Guevara Gómez, 2017).

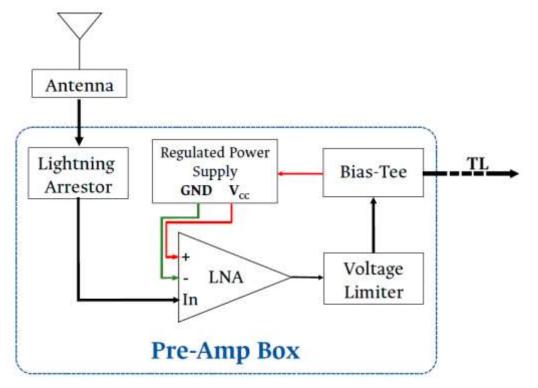




Figure 29: Block Schematics (Left) and implemented Pre-Amp stage (Right).





#### Downconversion

Downconversion shifts the signal to a lower frequency and reduces its sampling rate to facilitate subsequent processing stages.

DDCs are widely used in digital communication receivers to convert radio frequency (RF) or intermediate frequency (IF) signals to baseband.

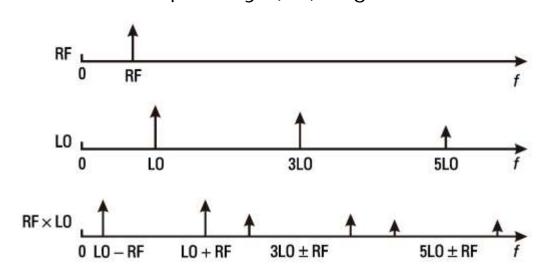


Figure 31: Downconversion frequency domain plot. Taken from Rogers & Plett, 2003.



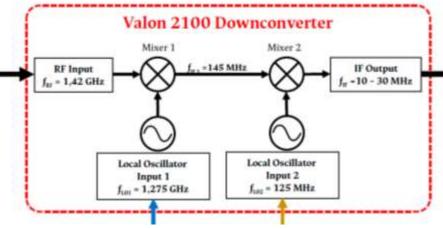
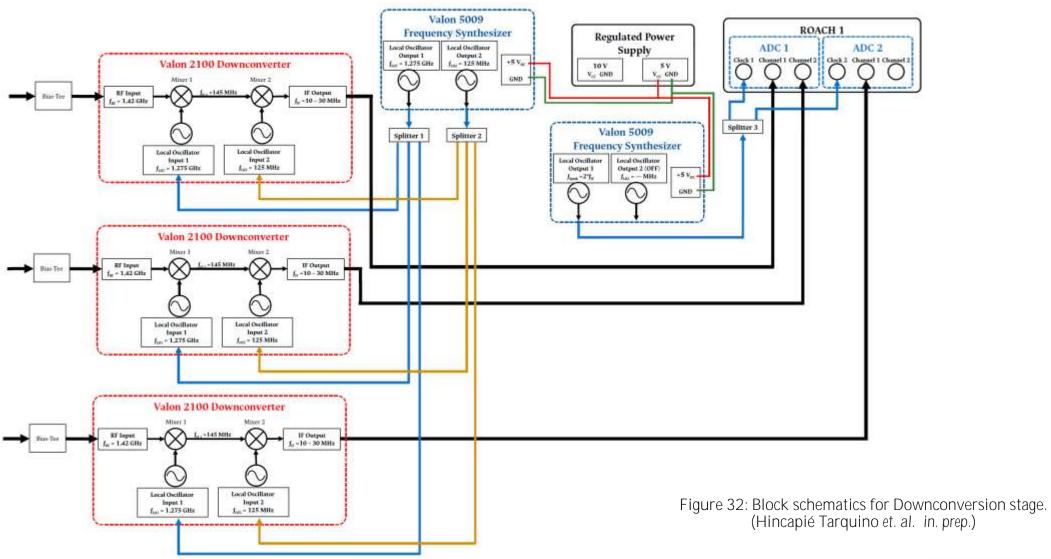


Figure 30: Valon 2100 21cm Downconverter. Top: Circuit: Bottom: Block schematics.





### Front-End: Downconversion Stage









#### Back-End: Correlator

- The ROACH (Reconfigurable Open Architecture Computing Hardware) is a standalone FPGA processing board.
- Developed by the Collaboration for Astronomy Signal Processing and Electronics Research (CASPER) group
- Centerpiece: Xilinx Virtex 5 FPGA





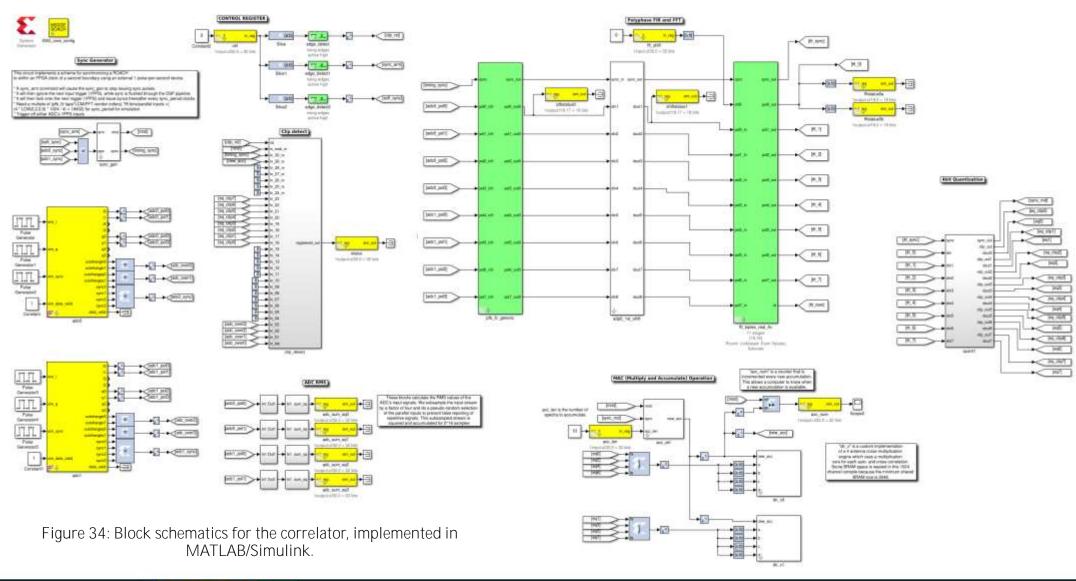
Figure 33: ROACH-1 standalone board







#### Back-End: Correlator





### Back-End: Correlator







Figure 35: Correlator Implemented with ROACH-1 board.







# Full Array Implementation



Figure 36: Full interferometric array implemented at Observatorio Astronómico Nacional, Campus Building – Universidad Nacional de Colombia.

#### Results: Solar Transit

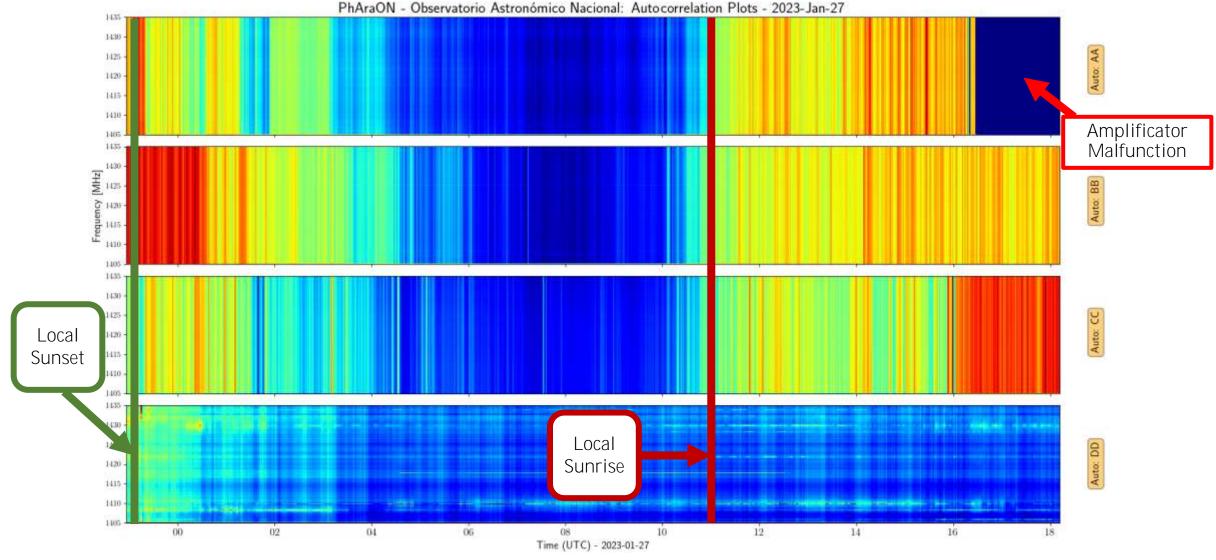


Figure 37: Results – Solar Transit: 2023 January 26, 18:00 – January 27, 13:00 (GMT -5). Auto-correlation plots (Hincapié Tarquino, et al. In prep.)



#### Results: Solar Transit

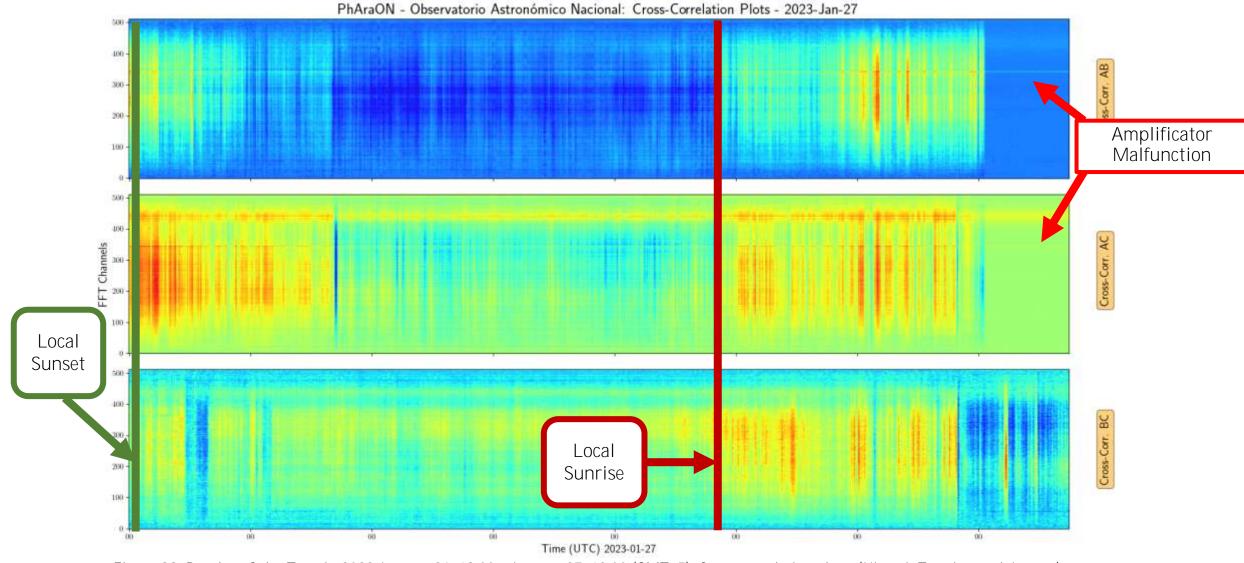
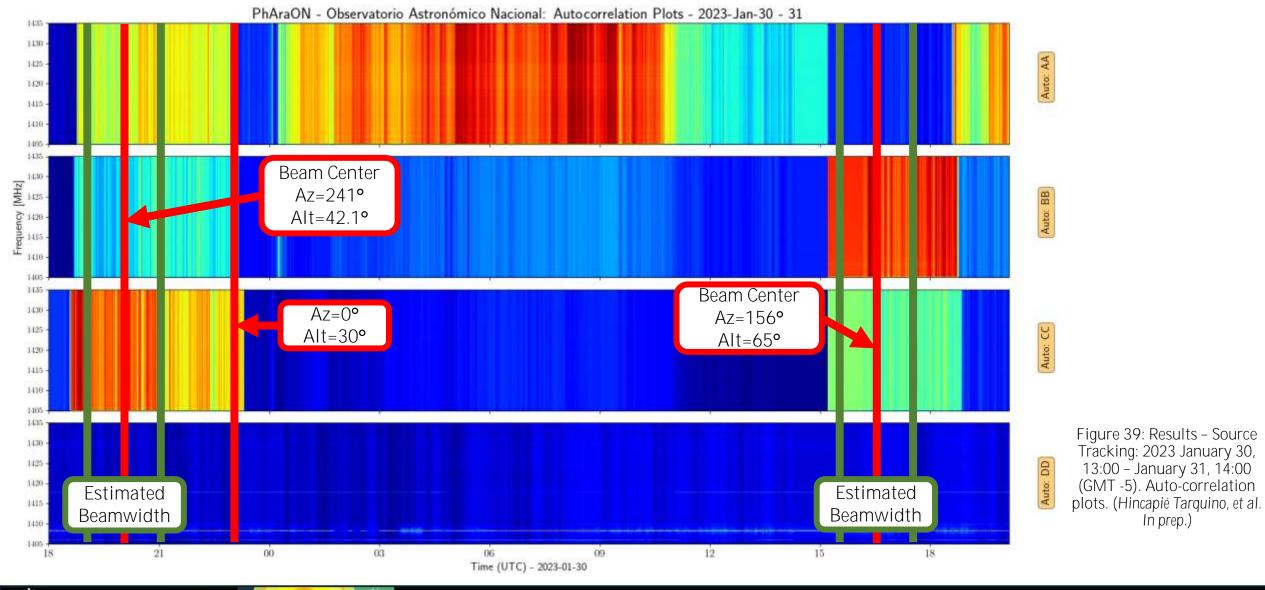


Figure 38: Results – Solar Transit: 2023 January 26, 18:00 – January 27, 13:00 (GMT -5). Cross-correlation plots. (Hincapié Tarquino, et al. In prep.)



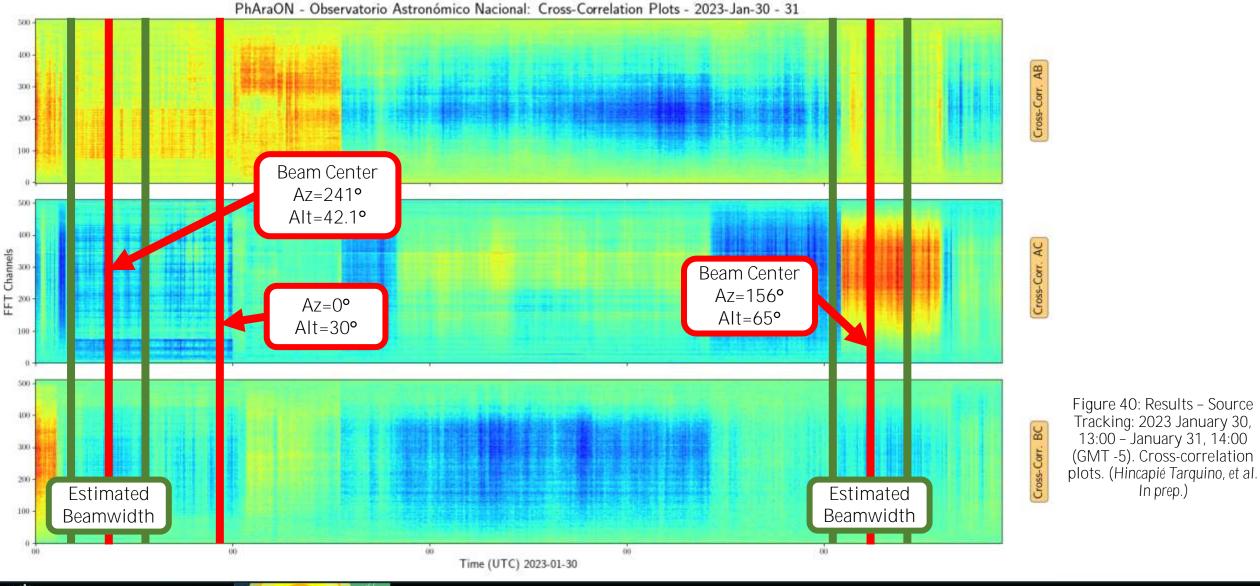
# Results: Source Tracking







# Results: Source Tracking





# Results: Source Tracking

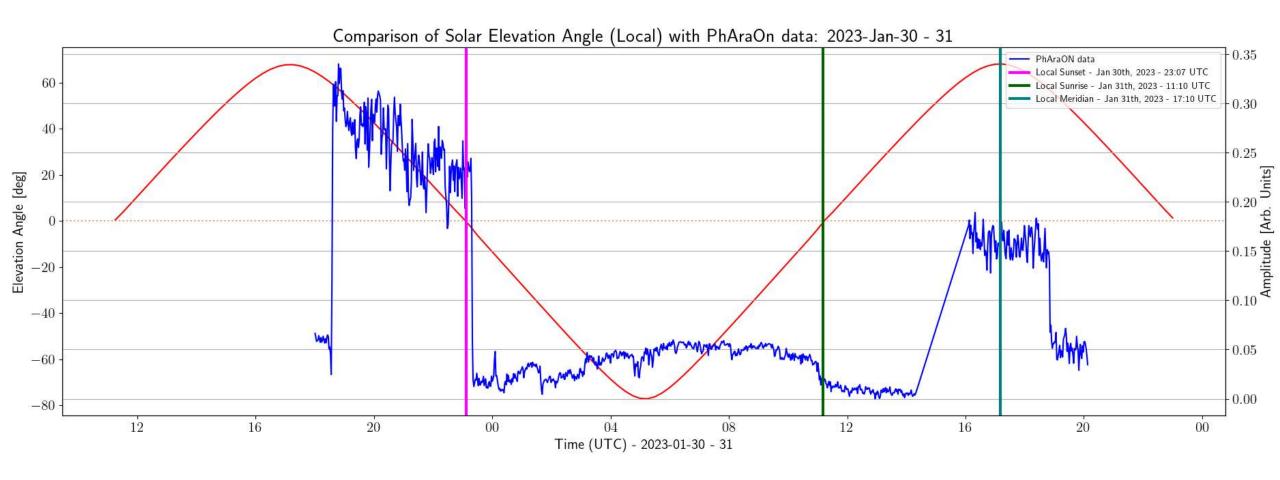
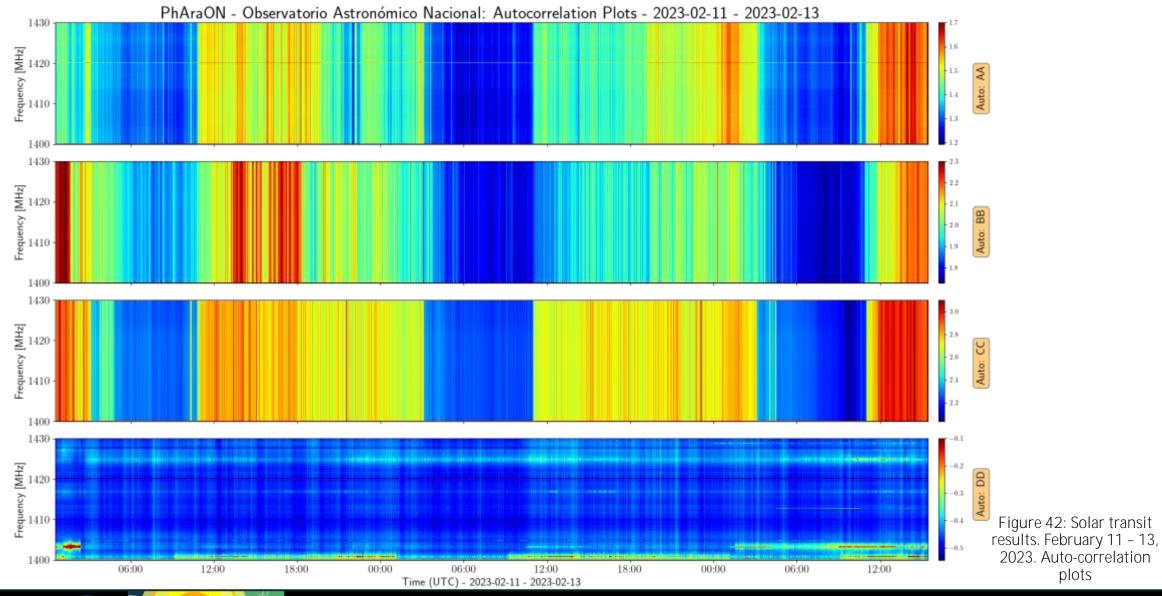
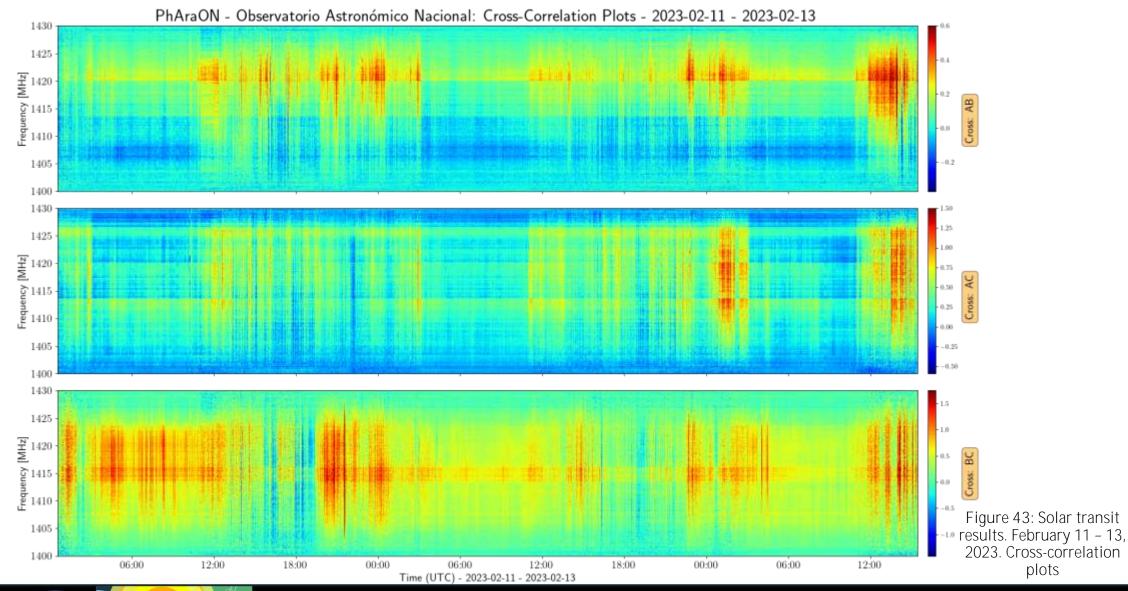


Figure 41: Comparison of obtained data with local solar elevation angle for Jan 30-31, 2023















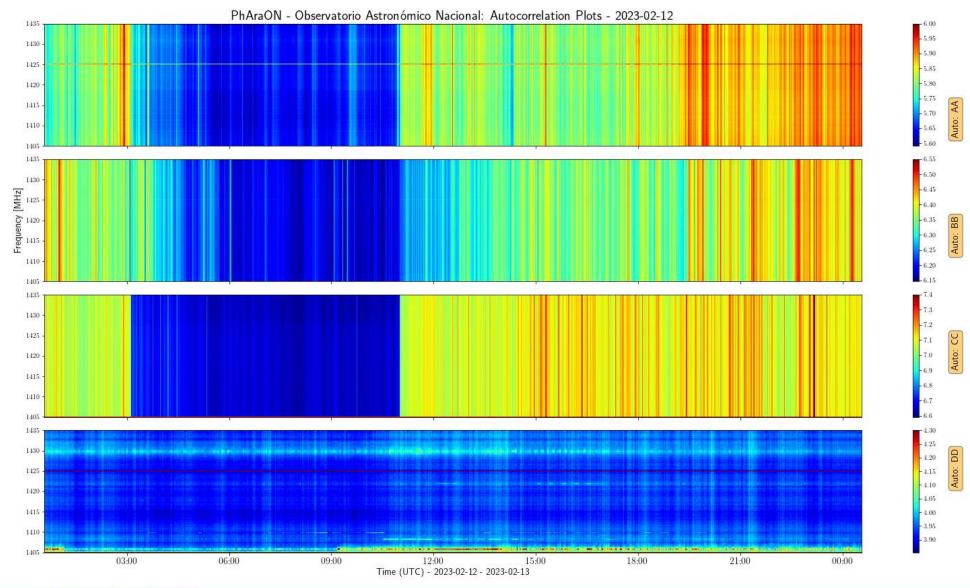


Figure 44: Solar transit results. February 12, 2023. Auto-correlation plots





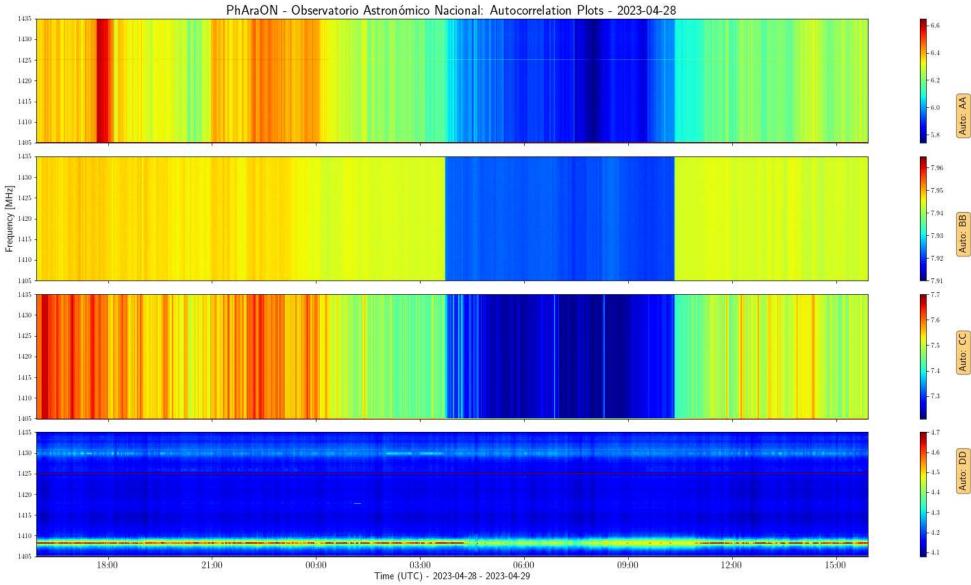


Figure 45: Solar transit results. April 28, 2023. Auto-correlation plots







#### Single dish:

- ★ Validation of the Antenna element operation. System works!
- ★ Redesign the pier motor assembly.

#### Full Array:

- ★ Successful detection of the Sun, both as a transiting source and with tracking. Verified when comparing the data to the local Solar elevation angle.
- ★ RFI visible at 1,408 GHz (Radiolocation applications)



#### Conclusions

- ➤ Successful design, development, implementation and testing of a multi-element radio interferometer, for astronomical observations at 1.42 GHz.
- ★ Correlator implemented with a ROACH-1 board makes the system versatile and easy to modify and update (Special considerations because of downconversion stage).
- ★ Instrument operation: Successful detection of an extended source.
- ★ Implementation of a dedicated filtering stage would improve the results.
- ★ Current stage of implementation and operation is very close to a fully implemented passive phased array, pending on an evaluation of an appropriate transmitter and phase switching stage to be integrated.





# Next Stage: Research

- ★ Implementation of a dedicated filtering stage.
- ★ Improvement of the instrument control stage: Source tracking
- ★ Observation of other cosmic radio sources emitting at 21cm (HI Line).
- ➤ Integration with other radio interferometers on-site: "Solar Radio-Interferometric Network of the Observatorio Astronómico Nacional (RRIS-OAN): Inter-calibration and Instrumental Integration" (Sánchez González et. al.)



FiCoRi: West Antenna

PhAraON:

Antenna 1

MICRAS

FiCoRi: East

Antenna





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# Thanks!



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