



NAKUJA 4 SOLIDS TEAM

WEEK 2 PROGRESS REPORT



THIS WEEK'S OBJECTIVES:

1. Analysis and research of the previous static test
2. Preparation of the tensile test workpieces
3. Conducted the tensile test on the specimens.
4. Developing calculations for the new casing.
5. Searching for suppliers of the new casing.
6. Cutting of the bulkhead material.
7. Re-making of the liner.



1. Results from the analysis

- Calculated working pressure was found to be equal to the simulated motor pressure.
- The liner acted as an insulating layer and ablative layer where pyrolysis occurred.

2.Preparation of the tensile test work pieces

Using hacksaws,square files and round file a work piece was made from the aluminium casing according to the ASTM B557M Standard.

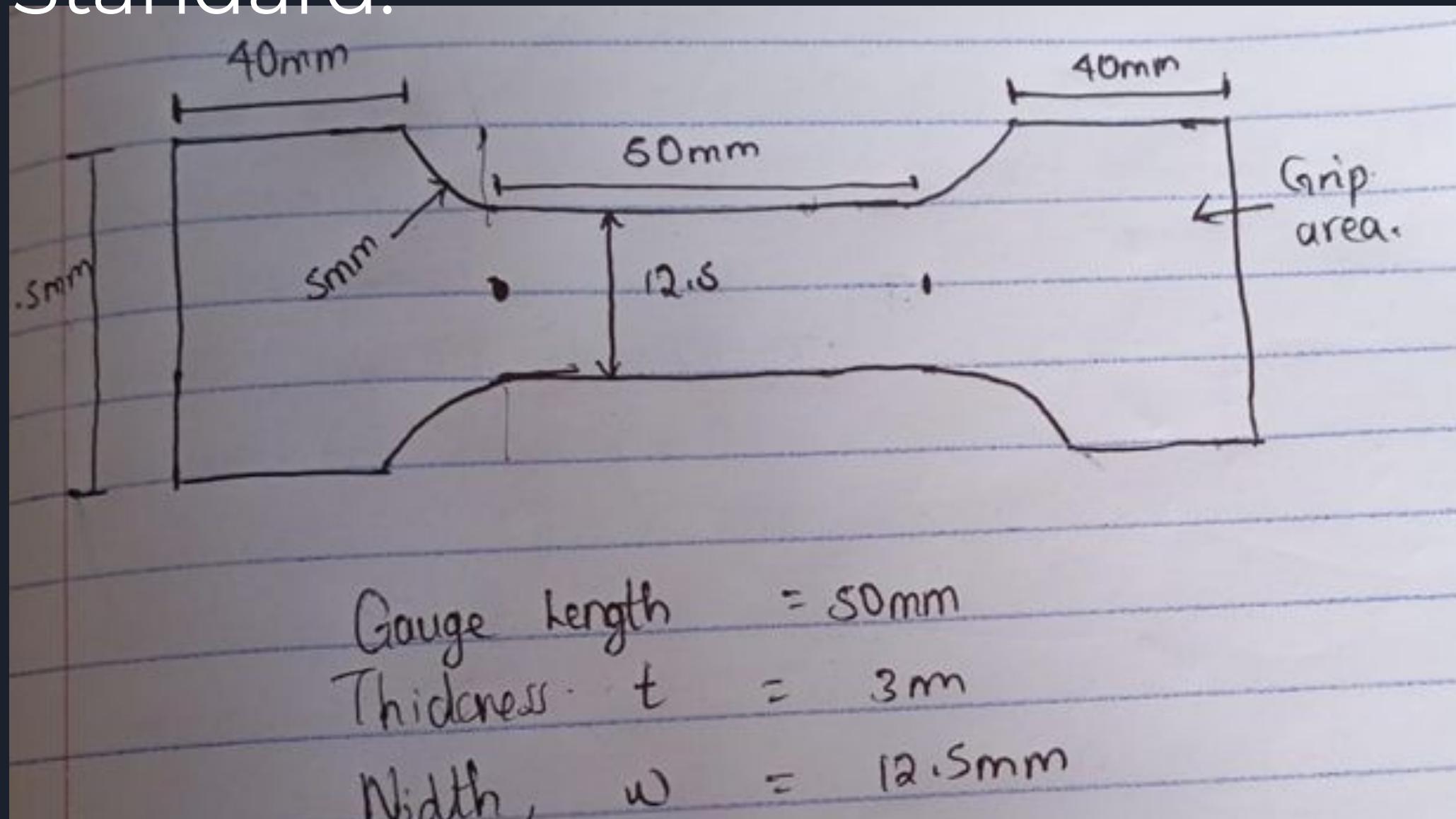


Fig 1: Dimensions of work piece with standards

Photo of the activity.



Fig 2. Workpiece preparation



Fig 3. Workpieces after activity

3.Tensile testing

The specimen were tested using a Shimadzu universal tensile testing machine.

The method was customised within the Trapeziumx software and the batch number specified. The specimen was loaded onto the jaws of the machine and loading began.

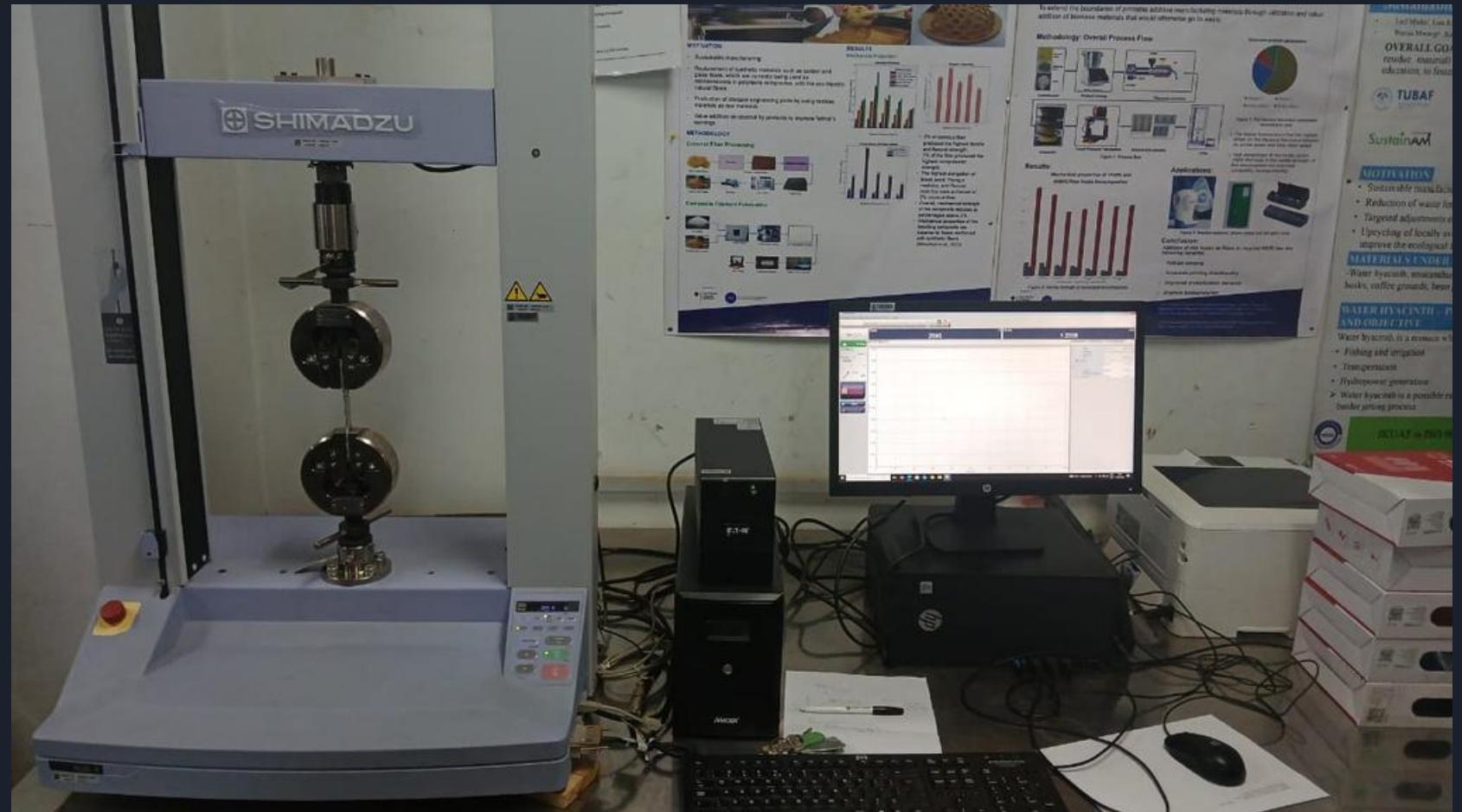


Fig 4. Tensile test setup



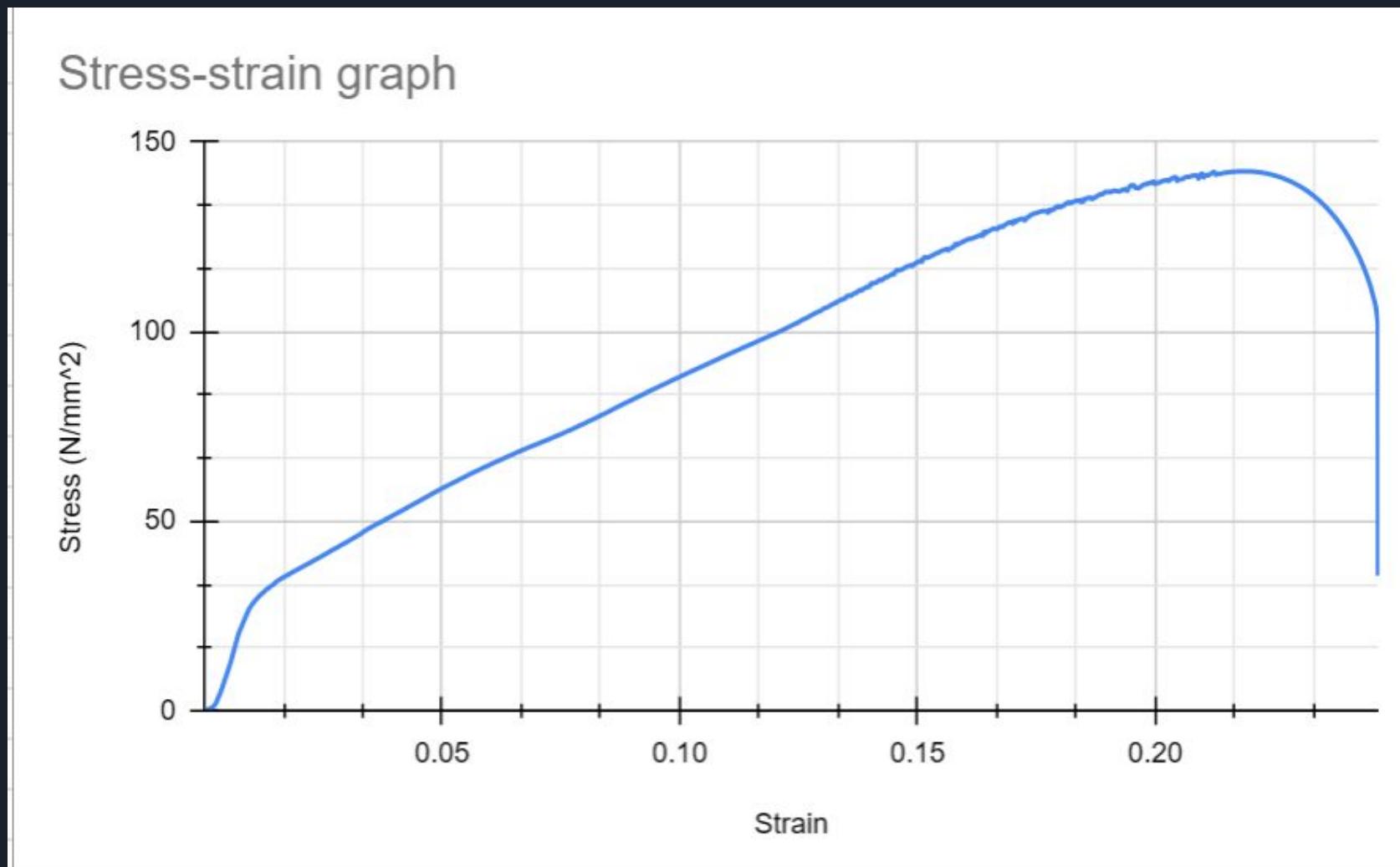
Fig 5. Workpiece in machine

Results of the tensile test

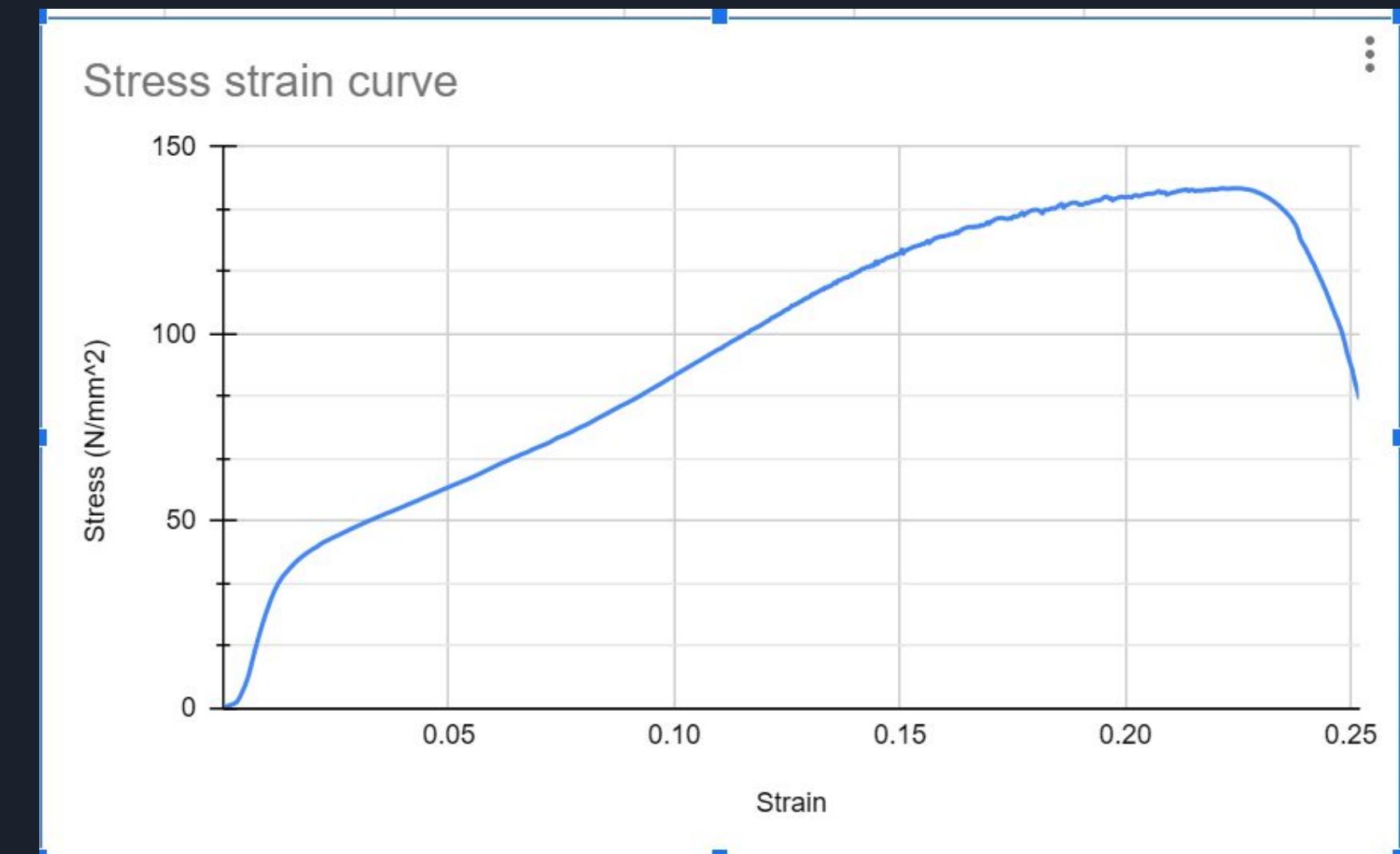
| Name | YP(%FS)_Force | YP(%FS)_Stress | YP(%FS)_Stroke | YP(%FS)_Stroke_Strain |
|--------------------|---------------|-------------------|----------------|-----------------------|
| Parameters | 0.1 % | 0.1 % | 0.1 % | 0.1 % |
| Unit | N | N/mm ² | mm | % |
| 1 _ 1 | 4949.61 | 123.125 | 8.97683 | 17.9537 |
| 1 _ 2 | 5496.29 | 119.433 | 7.23260 | 14.4652 |
| Average | 5222.95 | 121.279 | 8.10472 | 16.2095 |
| Standard Deviation | 386.561 | 2.61064 | 1.23336 | 2.46674 |
| Range | 546.680 | 3.69200 | 1.74423 | 3.48850 |

| Name | Max_Force | Max_Stress | Max_Stroke | Max_Stroke_Strain |
|--------------------|-----------------------|-----------------------|-----------------------|-----------------------|
| Parameters | Calc. at Entire Areas |
| Unit | N | N/mm ² | mm | % |
| 1 _ 1 | 5291.45 | 131.628 | 10.9368 | 21.8736 |
| 1 _ 2 | 6396.05 | 138.984 | 11.0643 | 22.1285 |
| Average | 5843.75 | 135.306 | 11.0006 | 22.0011 |
| Standard Deviation | 781.070 | 5.20147 | 0.09016 | 0.18024 |
| Range | 1104.60 | 7.35599 | 0.12750 | 0.25490 |

Excel analysis of the results



Sample 1 stress-strain curve



Sample 2 stress-strain curve

Mechanical properties from the supplier

| CIRCULAR TUBE | | | | | |
|----------------------|----------|--------|-------|------|------|
| <u>CIRCULAR TUBE</u> | | | | | |
| No. | NEW CODE | OD | ID | T | Kg/M |
| 23 | 105-0509 | 100.00 | 94.00 | 3.00 | 2.60 |

| MECHANICAL PROPERTIES | | Al 6063 | |
|--|--------------------------|---------|-----|
| Properties | Unit | T5 | T6 |
| Ultimate Tensile Strength | N/mm ² | 150 | 250 |
| 0.2 % Proof Stress | N/mm ² | 110 | 160 |
| Hardness (Brinell) | BHN | 55 | 65 |
| Ult. Shear Strength | N/mm ² | 155 | |
| Elongation on 50 mm | % | 8 | |
| Density | g/cm ³ | 2.7 | |
| Melting Range | g/cm ³ | 600-500 | |
| Coefficient on Linear Expansion | X10 ⁻² Deg °C | 23 | |
| Modulus Of Elasticity | N/mm ² | 67000 | |
| Fatigue Strength (50*10 ⁶) Cycle | N/mm ² | 75 | |



Conclusion of the test

From the tensile test, it is evident that the Yield stress from the supplier was concurrent with yield stress of the test. The same is true for the Ultimate tensile stress

Material properties of different Al alloys

| Physical Properties | Metric | English |
|------------------------------|-----------------|---------------------------|
| Density | <u>2.7 g/cc</u> | 0.0975 lb/in ³ |
| Mechanical Properties | | |
| Hardness, Brinell | 60 | 60 |
| Hardness, Knoop | 83 | 83 |
| Hardness, Vickers | 70 | 70 |
| Ultimate Tensile Strength | <u>186 MPa</u> | 27000 psi |
| Tensile Yield Strength | <u>145 MPa</u> | 21000 psi |
| Elongation at Break | <u>12 %</u> | 12 % |
| Modulus of Elasticity | <u>68.9 GPa</u> | 10000 ksi |
| Poisson's Ratio | 0.33 | 0.33 |
| Fatigue Strength | <u>68.9 MPa</u> | 10000 psi |

Al 6063

T5

| Physical Properties | Metric | English |
|------------------------------|-----------------|---------------------------|
| Density | <u>2.7 g/cc</u> | 0.0975 lb/in ³ |
| Mechanical Properties | | |
| Hardness, Brinell | 95 | 95 |
| Hardness, Knoop | 120 | 120 |
| Hardness, Rockwell A | 40 | 40 |
| Hardness, Rockwell B | 60 | 60 |
| Hardness, Vickers | 107 | 107 |
| Ultimate Tensile Strength | <u>310 MPa</u> | 45000 psi |
| Tensile Yield Strength | <u>276 MPa</u> | 40000 psi |
| Elongation at Break | <u>12 %</u> | 12 % |
| Elongation at Break | <u>17 %</u> | 17 % |
| Modulus of Elasticity | <u>68.9 GPa</u> | 10000 ksi |

Al 6061

T6

4.Calculation of the casing

Casing Dimensions and Design Factors

$D_o = 100$ in. (mm) Diameter, outside
 $t = 3$ in. (mm) wall thickness
 $S_D = 1.5$ Design Safety factor

Material Properties

$F_{ty} = 110$ ksi (MPa) Yield Strength
 $F_{tu} = 150$ ksi (MPa) Ultimate Strength
 $E = 68900$ Msi (MPa) Modulus of Elasticity
 $\nu = 0.33$ Poisson Ratio

$\beta = 0.733$ Fty/Ftu
 $B = 1.474$ Burst factor

Design and Burst Pressures

$P_D = 4400$ psi (kPa) Design pressure
 $P_U = 9727$ psi (kPa) Burst pressure
 $S_U = 2.21$ Burst Safety Factor

Elastic Deformation under Pressure *

$\Delta D = 0.00009$ in. (m.) Change in casing diameter, at P_D
 $\Delta c = 0.00028$ in. (m.) Change in casing circumference, at P_D

Casing Dimensions and Design Factors

$D_o = 100$ in. (mm) Diameter, outside
 $t = 3$ in. (mm) wall thickness
 $S_D = 1.5$ Design Safety factor

Material Properties

$F_{ty} = 276$ ksi (MPa) Yield Strength
 $F_{tu} = 310$ ksi (MPa) Ultimate Strength
 $E = 68900$ Msi (MPa) Modulus of Elasticity
 $\nu = 0.33$ Poisson Ratio

$\beta = 0.890$ Fty/Ftu
 $B = 1.266$ Burst factor

Design and Burst Pressures

$P_D = 11040$ psi (kPa) Design pressure
 $P_U = 20959$ psi (kPa) Burst pressure
 $S_U = 1.90$ Burst Safety Factor

Elastic Deformation under Pressure *

$\Delta D = 0.00022$ in. (m.) Change in casing diameter, at P_D
 $\Delta c = 0.00070$ in. (m.) Change in casing circumference, at P_D

Fig 12. Casing calculations for AL 6063 T5

Fig 12. Casing calculations for AL 6061 T6

5. Suppliers from the internet

Select variations and quantity

1000 - 4999 kilograms 5000 - 49999 kilograms >= 50000 kilograms

US\$2.50 **US\$2.20** **US\$1.80**

Outer Diameter(1): 5-650mm

x 1000
5-650mm

Thickness(1)

0.8mm ~ 30mm

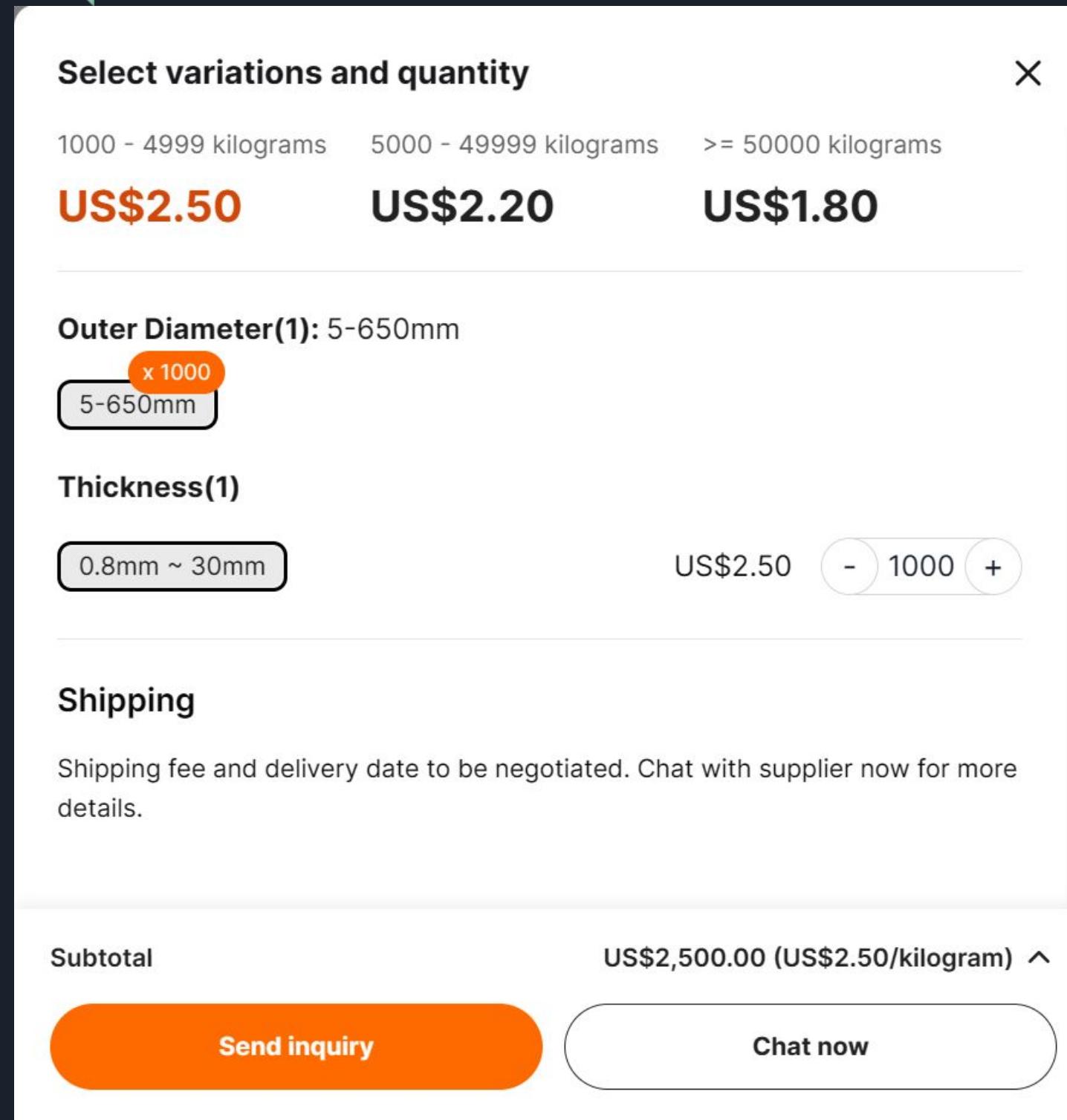
US\$2.50 - 1000 +

Shipping

Shipping fee and delivery date to be negotiated. Chat with supplier now for more details.

Subtotal US\$2,500.00 (US\$2.50/kilogram) ^

Send inquiry **Chat now**



Order sample

Maximum order quantity for samples: 10 kilograms

US\$2 /kilogram

Outer Diameter(1): 5-650mm

x 10
5-650mm

Thickness(1)

0.8mm ~ 30mm

US\$2 - 10 +

Shipping

UPS Expedited (Standard) [Alibaba.com Logistics](#) [Change >](#)

Shipping fee: US\$626.52 for 10 Kilograms
Estimated delivery by Jul 22-Aug 13

Subtotal US\$646.52 (US\$64.65/kilogram) ^

Order sample

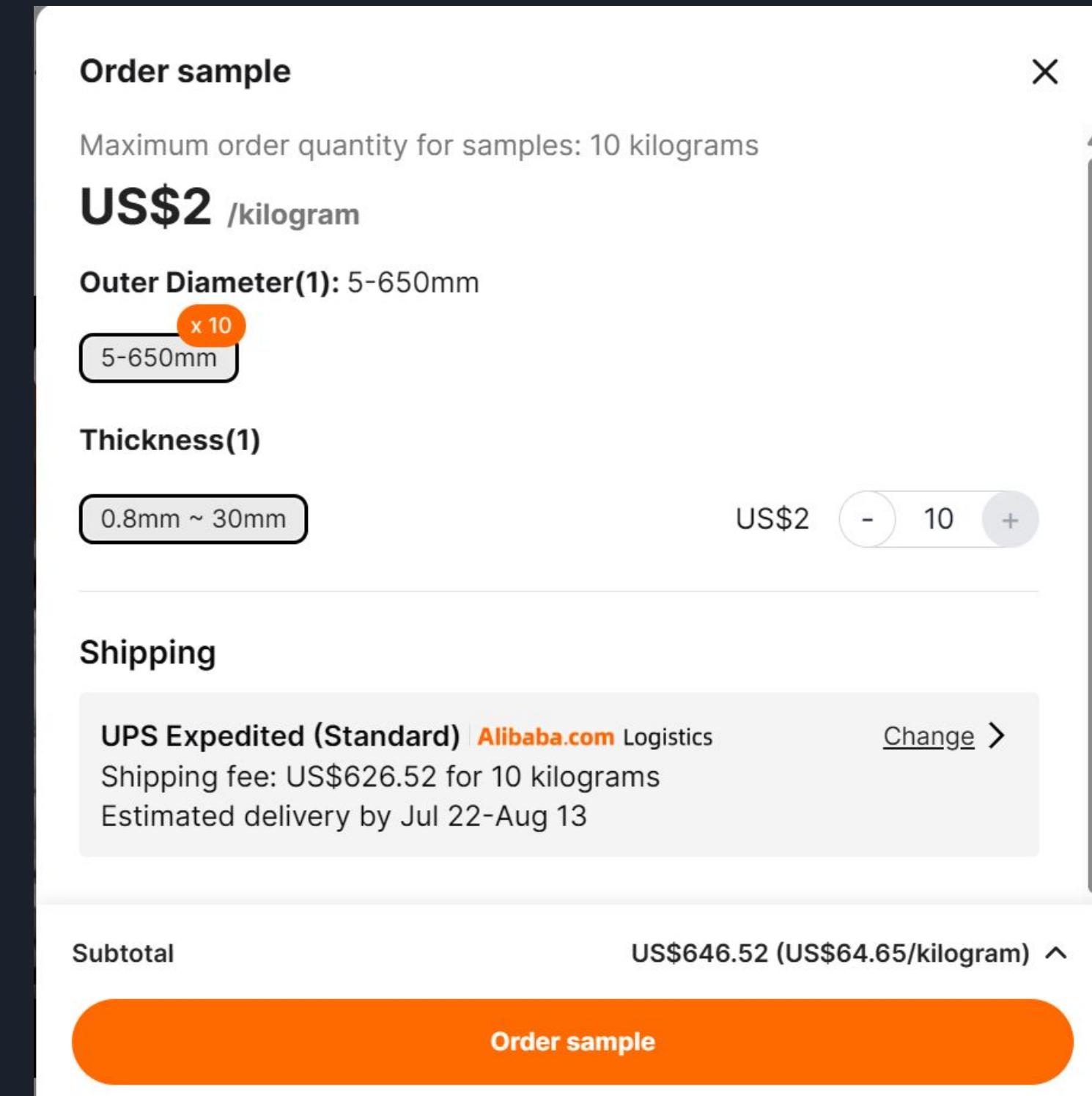


Fig 14&15. Alibaba supplier

6. Cutting of the bulkhead to specific size.

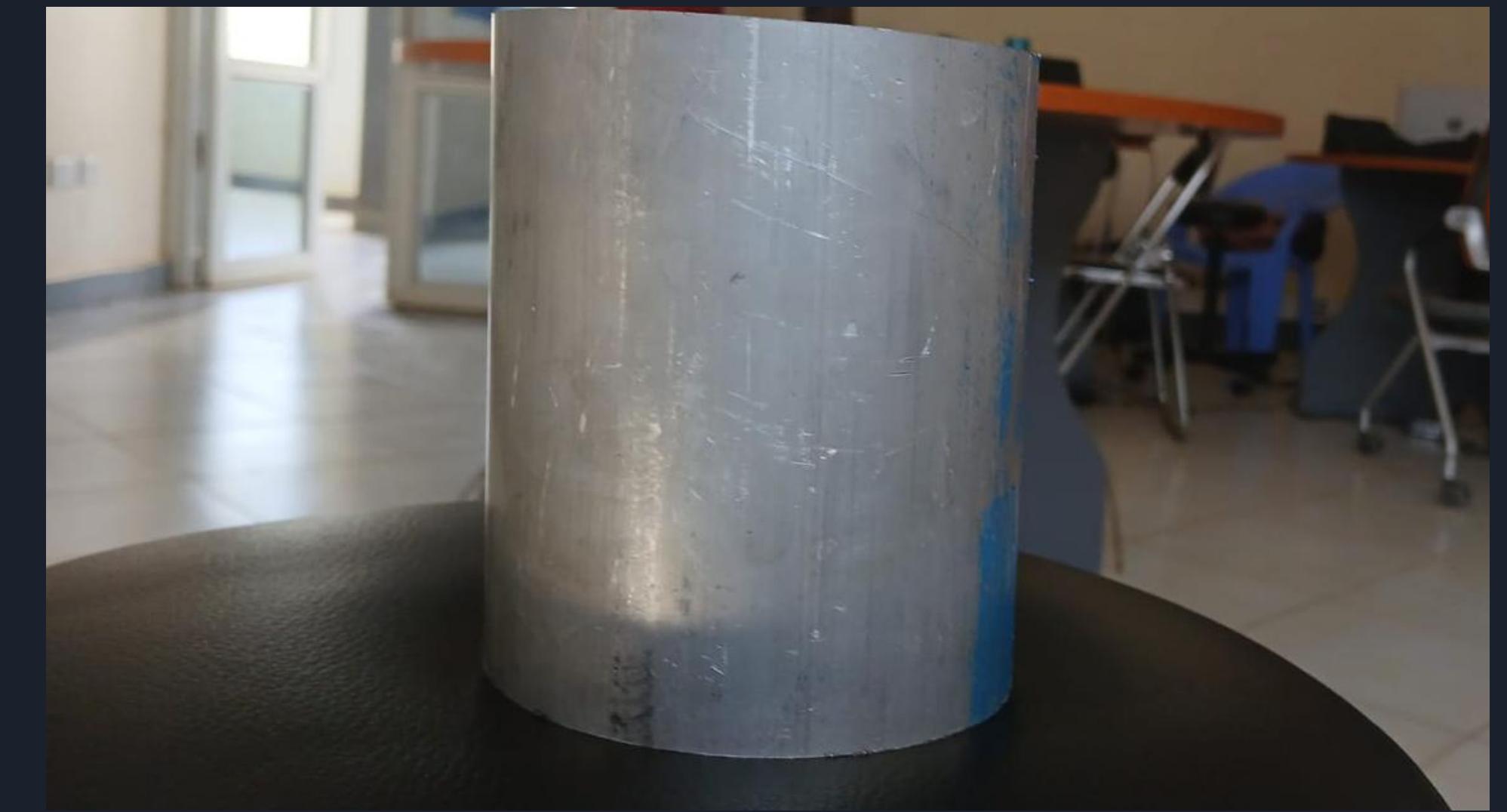


Fig 16. Bulkhead material cut to dimension

Re-making of the Liner according to the new casing dimensions



Fig 16. Liner made to 94mm dimension



NEXT WEEK'S OBJECTIVES

1. Simulating of the new casing performance in Ansys
2. Machining of the bulkheads to be used in the hydrostatic test (**consult on how to conduct our own pressure test during hot fires - piping system connection**)
3. Conducting the hydrostatic test
4. Obtaining Sorbitol and Potassium Nitrate
5. Cooking of the grains



THANK YOU

N4 SOLIDS TEAM