

Es 1

Dato S: $\begin{cases} \dot{x}_1 = -2x_1^3 + 2x_2 \\ \dot{x}_2 = x_2 - u \\ y = x_2 \end{cases}$ ① Espr. Analitica $y(t)$ con $x(0) = \begin{bmatrix} 1 \\ 0 \end{bmatrix}$ e $u(t) = \sin(t-1)$

Ce me freghiamo della non linearità di x_1 perché $y(t)$ dipende da x_2

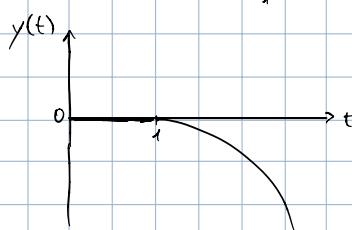
$$\begin{cases} \dot{x}_2(t) = x_2 - u \\ y(t) = x_2 \end{cases}$$

a) $0 \leq t < 1$
b) $t \geq 1$

a) $u(t) = 0 \quad x_2(0) = 0 \quad \dot{x}_2 = 0 \Rightarrow x_2(t) = 0 \quad y(t) = 0 \quad \forall t: 0 \leq t < 1$

b) $x_2(t) = e^{t(t-1)} x_2(1) + \int_1^t e^{t(t-\tau)} (-1) u(\tau) d\tau$
 $t_0 = 1 \quad ! = 0$

$$x_2(t) = \int_1^t -e^{t-t\tau} d\tau = e^t \int_1^t -e^{-\tau} d\tau = e^t \left[e^{-\tau} \right]_1^t = e^t (e^{-t} - e^{-1}) = 1 - e^{t-1} \quad \forall t \geq 1$$



2) Calcolare \bar{x} quando $u(t) = 1 = \bar{u}$

$$\begin{cases} 0 = -2\bar{x}_1^3 + 2\bar{x}_2 \quad -2\bar{x}_1^3 + 2 = 0 \rightarrow \bar{x}_1^3 = 1 \\ 0 = \bar{x}_2 - \bar{u} \rightarrow \bar{x}_2 - 1 = 0 \rightarrow \bar{x}_2 = 1 \\ \bar{y} = \bar{x}_2 \quad \bar{y} = \bar{x}_2 = 1 \end{cases}$$

$$\bar{x} = \begin{bmatrix} 1 \\ 1 \end{bmatrix} \quad \bar{u} = 1 \quad \bar{y} = 1$$

3) Stab \bar{x} \mathcal{S}' : $\begin{cases} \dot{\bar{x}}_1 = -6\bar{x}_1^2 \dot{x}_1 + 2\dot{x}_2 \\ \dot{\bar{x}}_2 = \dot{x}_2 - \dot{u} \\ \bar{y} = \dot{x}_2 \end{cases}$

$$A = \begin{bmatrix} -6\bar{x}_1^2 & +2 \\ 0 & 1 \end{bmatrix} \Big|_{\bar{x}} = \begin{bmatrix} -6 & +2 \\ 0 & 1 \end{bmatrix}$$

$\lambda_1 = -6 \quad \lambda_2 = 1$ INSTABILE

4) $K \in \mathbb{R} \quad \bar{x} = \begin{bmatrix} 1 \\ 1 \end{bmatrix}$

$v \in \mathbb{R}$
t.c. con \bar{x} S A.S.

$$\begin{cases} \dot{\bar{x}}_1 = -2\bar{x}_1^3 + 2\bar{x}_2 \\ \dot{\bar{x}}_2 = \bar{x}_2 - (v - K\bar{x}_2) = (1-K)\bar{x}_2 - v \\ \bar{y} = \bar{x}_2 \end{cases}$$

$$\begin{cases} 0 = -2\bar{x}_1^3 + 2\bar{x}_2 \\ 0 = (1-K)\bar{x}_2 - v \\ \bar{y} = \bar{x}_2 \end{cases}$$

$$\boxed{1-K = \bar{v}} \quad 1^{\text{a}} \text{ condizione}$$

$$\bar{y} = 1$$

$$\begin{cases} \dot{\bar{x}}_1 = -\bar{x}_1^2 \dot{x}_1 + 2\dot{x}_2 \\ \dot{\bar{x}}_2 = (1-K)\dot{x}_2 - \dot{v} \\ \bar{y} = \dot{x}_2 \end{cases}$$

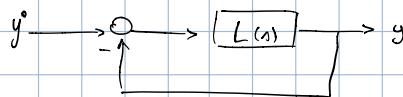
$$A = \begin{bmatrix} -\bar{x}_1^2 & 2 \\ 0 & 1-K \end{bmatrix} \Big|_{\bar{x}} = \begin{bmatrix} -6 & 2 \\ 0 & 1-K \end{bmatrix}$$

$$\lambda_1 = -6 \quad \lambda_2 = 1-K$$

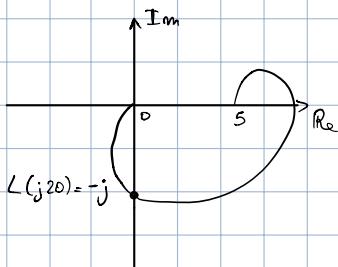
$\begin{cases} K > 1 \quad \text{eq. AS con } \bar{x} \\ \bar{v} = 1-K \end{cases}$

$1-K < 0 \iff \boxed{K > 1} \quad 2^{\text{a}} \text{ condiz.}$

ES. 2



$L(s)$ AS STABILE
con POLI REALI



1) È AS STAB $P=0$ × BODE

$$\text{AS STAB} \Leftrightarrow \mu_c = 5 > 0 \\ \varphi_m > 0$$

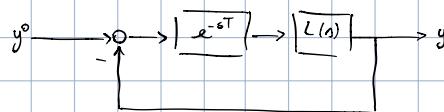
$$\omega_c = 20 \text{ rad/s} \\ \angle L(j20) = -90^\circ$$

$$\varphi_m = 180^\circ - |-90^\circ| = 90^\circ > 0 \quad \text{per Bode è AS}$$

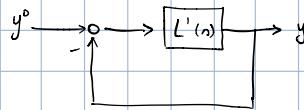
2) Risposta allo scalino (caso)

3) Si introduce un ritardo di $T=0,1$ ust nell'anello

come cambia la stab. del sistema retroazionato?



$$L'(s) = e^{-sT} L(s) \\ |L'(j\omega)| = |e^{-j\omega T}| \cdot |L(j\omega)| \\ = 1 \cdot |L(j\omega)|$$



Ci dice che il diagramma del modulo non cambia, e non cambia neanche $\omega_c \Rightarrow \omega_c = 20$

$$\angle(L'(j20)) = \underbrace{\angle(e^{j\omega_c T})}_{-90^\circ} + \underbrace{\angle(L(j20))}_{-90^\circ} = -\omega_c T \frac{180^\circ}{\pi} - 90^\circ = -205^\circ \\ \hookrightarrow \omega_c = 20 \text{ rad/s} \\ T = 0,1 \text{ ust} \quad \varphi_m \approx -25^\circ < 0 \\ \Rightarrow \text{INSTABILE}$$

Es. 3

$$\text{Data } G(s) = 10 \frac{1 - \frac{s}{3}}{(1 + \frac{s}{6,1})(1 + \frac{2s}{100} + \frac{s^2}{100^2})} \quad \text{III ORDINE} \\ (\Rightarrow \text{AS STAB})$$

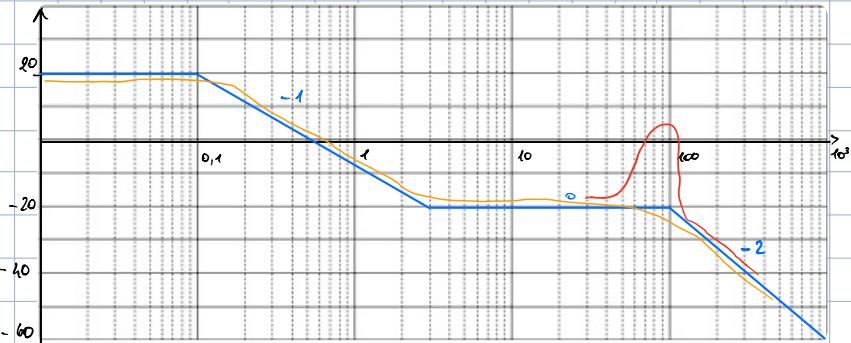
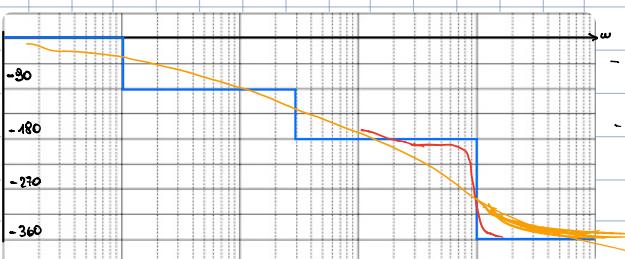
$\frac{1}{s+1}$
0,1 ~~WU~~

1) Tracciare Bode $\xrightarrow{u} [G(s)] \rightarrow y$

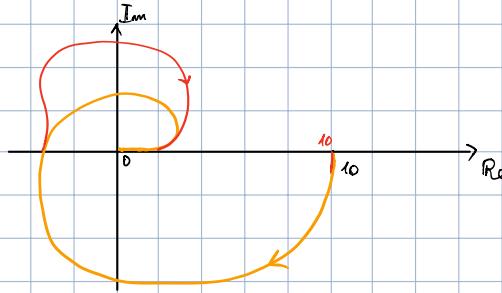
$$|\mu| = 10 = 20 \text{ dB} \\ \mu = 10 \quad \begin{cases} < 0 & +90^\circ \text{ FASE INIZ.} \\ > 0 & -90^\circ \text{ FASE INIZ.} \end{cases}$$

$\varphi = 0 \quad \begin{cases} -90^\circ & \text{pendenza iniz.} \\ -90^\circ & \varphi = 0^\circ \text{ fase iniz.} \end{cases}$

$$\begin{aligned} \omega_1 &= 0,1 \text{ rad/s} & \text{POLO SX} \\ \omega_2 &= 3 \text{ rad/s} & \text{ZERO DX} \\ \omega_3 &= 100 \text{ rad/s} & 2 \text{ POLI CC SX} \end{aligned}$$



② D. POLARI



③ $y_\infty(t)$

$$u(t) = \sin(0.01t) - \cos(10t)$$

$$u_1(t) = \sin(0.01t)$$

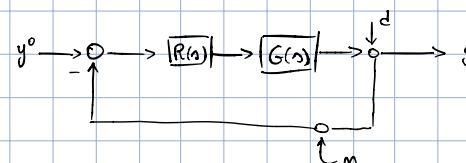
$$u_2(t) = -\cos(10t)$$

$$\begin{aligned} y_{1,\infty}(t) &= 1 \cdot |G(j0, 0.01)| \cdot \sin(0.01t + \angle G(j0, 0.01)) \approx 10 \sin(0.01t) \\ y_{2,\infty}(t) &= -1 \cdot |G(j10)| \cos(10t + \angle G(j10)) \approx -\frac{1}{3} \cos(10t - \pi) \end{aligned}$$

$$y_\infty(t) = 10 \sin(0.01t) - \frac{1}{3} \cos(10t - \pi)$$

ES. 4

$$G(s) = \frac{10}{(1+10s)^2} \quad \text{II ORD}$$



- $R(s) \quad t_c : \quad a) \quad e_\infty = 0 \quad y^0(t) = A \sin(\omega t)$
- $\omega_c \in [0, 1 ; 10] \text{ rad/s}$
- $\varphi_m \geq 80^\circ$
- $d(t) = \sin(0.01t) \text{ ATTENUATO DI ALMENO } 100 \text{ SU } y(t)$
- $m(t) = \sin(100t) \quad " \quad " \quad 1000 \quad "$

TRADUZIONE SPECIS: $\frac{Y(s)}{N(s)} = \frac{1}{1+L(s)} = S(s) \quad |S(j\omega)| \approx \begin{cases} 1 & |L(j\omega)| \ll 1 \quad \omega \gg \omega_c \\ \frac{1}{|L(j\omega)|} & |L(j\omega)| \gg 1 \quad \omega \ll \omega_c \end{cases}$

$$|S(j0.01)| = \frac{1}{|L(j0.01)|} \leq \frac{1}{100} \quad |L(j0.01)| \geq 100$$

$$\frac{Y(s)}{N(s)} = \frac{-L(s)}{1+L(s)} = -F(s) \quad |F(j\omega)| \approx \begin{cases} |L(j\omega)| & |L(j\omega)| \ll \omega \gg \omega_c \\ 1 & |L(j\omega)| \gg 1 \quad \omega \ll \omega_c \end{cases}$$

$$|F(j100)| \approx |L(j100)| \leq \frac{1}{1000} = -60 \text{ dB}$$

PROG STATICO

$$R(s) = \frac{\mu_R}{s}$$

$$a) \quad e_\infty = 0 \quad y^0(t) = A \sin(\omega t) \Rightarrow g = 1$$

$$R(s) = \frac{\mu_R}{s}$$

$$L(s) = 10 \frac{\mu_R}{s} \frac{1}{(1+\frac{s}{\omega_c})^2}$$

$$|L(j0, 0.01)| = \frac{10 \mu_R}{0.01} \cdot \frac{1}{|1+j \frac{0.01}{0.01}|^2} \approx 1000 \mu_R \quad \mu_R = 0, 1$$

$$|\mu_R| = 60 \text{ dB}$$

$$\approx 60 \text{ dB}$$

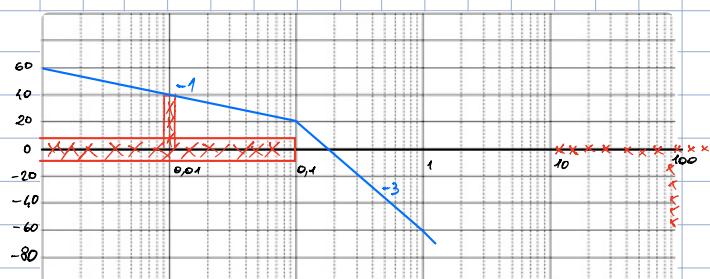
$$\mu_R = 1000 \mu_R = 100$$

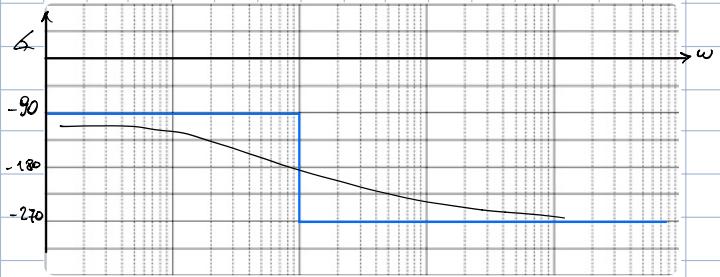
$$\mu_R > 0$$

$$g_L = 1$$

$$\omega_c = 0, 1 \text{ rad/s}$$

2 POLI SK





$w_c = 0,2 \text{ rad/s}$

$\angle L(j\omega_c) = -90^\circ - 2 \operatorname{tg}^{-1} \left(\frac{0,2}{0,1} \right) \approx -216^\circ$

$\varphi_m \approx -36^\circ < 0$

PROGETTO DIN. $R(s) = \frac{0,1}{s}$

$L(s) = \frac{1}{s} \frac{1}{(1 + s/10)^2}$

$w_c = 1 \text{ rad/s}$

$R(s) = \frac{0,1}{s} (1 + s/10)^2$

$\angle L(j\omega_c) = -90^\circ - 2 \operatorname{tg}^{-1} \left(\frac{1}{10} \right) \approx -86^\circ$

$\varphi_m \approx 84^\circ (> 80^\circ)$

$L(s) = \frac{1}{s} \frac{1}{1 + s/10}$

È realizzabile con un PID reale?

$R(s) = \frac{0,1}{s} \frac{(1 + s/10)^2}{(1 + s/10)}$

$PID_{Re}(s) = K_p \left(1 + \frac{1}{sT_i} + \frac{sT_d}{1 + sT_d/N} \right) = \frac{K_p}{T_i} \frac{1}{s} \frac{s^2(T_i T_d + T_i \frac{T_d}{N}) + s(T_i + T_d)}{1 + s \frac{T_d}{N}}$

$= 0,1 \frac{1}{s} \frac{1 + 20s + 100s^2}{1 + 0,1s}$

$\frac{T_d}{N} = 0,1$

$\frac{K_p}{T_i} = 0,1$

$T_i + \frac{T_d}{N} = 20$

$T_i = 20 - \frac{T_d}{N} = 19,9$

$K_p = 0,1 \quad T_i = 1,99$

$T_i T_d + T_i \frac{T_d}{N} = 100$

$T_d = \frac{1}{T_i} \left(100 - T_i \frac{T_d}{N} \right) = 6,825 \quad N = \frac{T_d}{0,1} = 68,25$

3) Attuatore è limitato tra $[-10, 10]$ disegnare lo schema di controllo in conf. anti-windup e com derivazione uscita

