

# Interaction Control (Human-Quadcopter)

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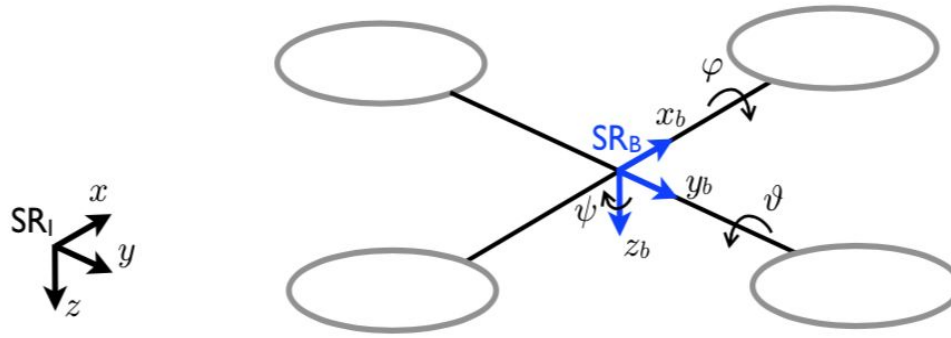
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# Introduction

- The proposed task is to apply the framework of Force Control to a Quadrotor, allowing an interaction between the vehicle and its environment, mainly, interaction with humans. This hybrid Position/Force control technique has been already deeply researched for manipulators and ground robots, but not for aerial robots.



# Quadcopter Model

- In order to design our controller, we performed a linear approximation of the system dynamics around a desired equilibrium point considering:

- Near-hover condition:  $\omega = (p, q, r) = (\dot{\phi}, \dot{\theta}, \dot{\psi})$
- State:  $\xi = (x, y, z, \dot{x}, \dot{y}, \dot{z}, \phi, \theta, \psi, \dot{\phi}, \dot{\theta}, \dot{\psi}, \tau_\phi, \tau_\theta, \tau_\psi)$

$X = (x, y, z)$  is the position of  $SR_B$  w.r.t  $SR_I$ ;

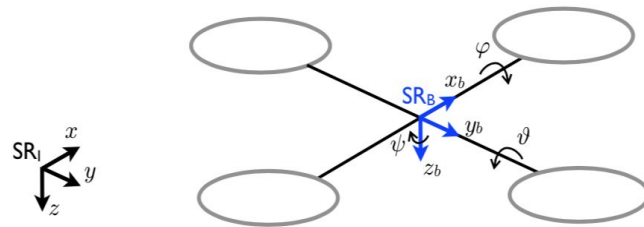
$\dot{X} = (\dot{x}, \dot{y}, \dot{z})$  is the velocity of  $SR_B$  w.r.t  $SR_I$ ;

$\Theta = (\phi, \theta, \psi)$  are the RPY angles expressing orientation of  $SR_B$  w.r.t  $SR_I$ ;

$\dot{\Theta} = \omega = (\dot{\phi}, \dot{\theta}, \dot{\psi})$  are the rotational rates;

$\tau = (\tau_\phi, \tau_\theta, \tau_\psi)$  are the torques around  $x_b, y_b$  and  $z_b$ , respectively;

$SR_I$  is the inertial (world) frame and  $SR_B$  is the body frame fixed to the quadrotor.



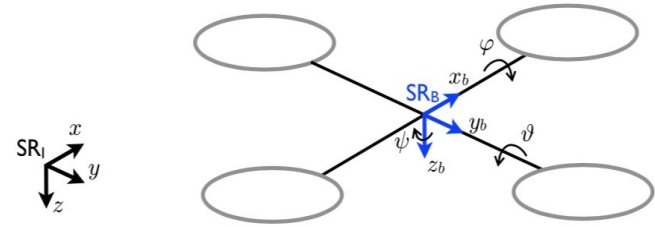
# Quadcopter Model

- In case of Hovering and in the absence of wind it is possible to approximate the rotation matrix around this equilibrium, yielding the dynamic equations:

$$m\ddot{\vec{X}} = -mgS(\Theta)\vec{e}_3 - T\vec{e}_3 \quad (1)$$

$$\dot{\Theta} = \omega \quad (2)$$

$$I\dot{\omega} = \tau \quad (3)$$



Where  $S$  is the skew-symmetric matrix defined by:

$$S(\Theta) = \begin{bmatrix} 0 & -\psi & \theta \\ \psi & 0 & -\phi \\ -\theta & \phi & 0 \end{bmatrix}$$

# Quadcopter Model

- It is possible to divide system (1)-(3) into 4 SISO systems. The Quadrotor will have 4 control inputs - the collective Thrust command and the 3 rotational body rates:

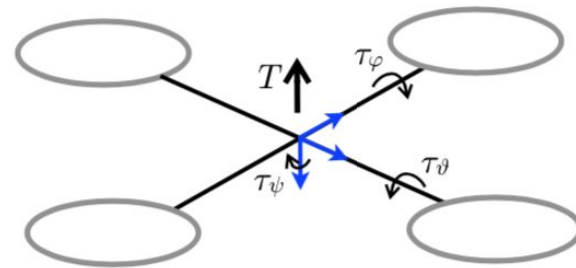
$$u = (T, \dot{\phi}_{cmd}, \dot{\theta}_{cmd}, \dot{\psi}_{cmd})$$

- The generated Torque by the vehicle reacts as a first-order system to the commanded inputs. The commanded torque is designed also to react as a first-order system to the commanded input rotational rates.

$$\tau_{cmd} = \frac{I}{T_2}(\omega_{cmd} - \omega)$$

$$\dot{\tau} = \frac{1}{T_1}(\tau_{cmd} - \tau)$$

$$\dot{\tau} = \frac{I}{T_1 T_2} \omega_{cmd} - \frac{I}{T_1 T_2} \omega - \frac{1}{T_1} \tau$$



# Position & Attitude Controller

## Altitude and Yaw Subsystems

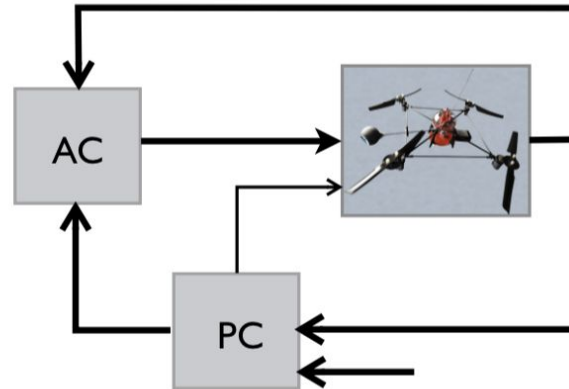
$$m\ddot{z} = -T$$

$$I_z\ddot{\psi} = \tau_\psi$$

## Control Strategy

$$T = -m[k_{zp}(z_r - z) + k_{zd}(\dot{z}_r - \dot{z}) + \ddot{z}_r]$$

$$\dot{\psi}_{cmd} = k_\psi(\psi_r - \psi) + \dot{\phi}_r$$



# Position & Attitude Controller

## X + Pitch Subsystem

## Control Strategy

$$\begin{cases} \ddot{x} = -g\theta \\ \ddot{\theta} = \frac{\tau_{\theta}}{I_y} \end{cases} \quad (x_1, x_2, x_3, x_4) = (x, \dot{x}, \theta, \dot{\theta}) \longrightarrow$$

$$\begin{cases} \dot{x}_1 = x_2 \\ \dot{x}_2 = -gx_3 \\ \dot{x}_3 = x_4 \\ \dot{x}_4 = \frac{\tau_{\theta}}{I_y} \end{cases}$$

$$\theta_r = x_{3r} = -\frac{1}{g}[k_{xp}(x_r - x) + k_{xd}(\dot{x}_r - \dot{x}) + \ddot{x}_r]$$

$$\dot{\theta}_{cmd} = k_{\theta}(\theta_r - \theta) + \dot{\theta}_r$$

## Y + Roll Subsystem

## Control Strategy

$$\begin{cases} \ddot{y} = g\varphi \\ \ddot{\varphi} = \frac{\tau_{\varphi}}{I_x} \end{cases}$$

$$\varphi_r = \frac{1}{g}[k_{yp}(y_r - y) + k_{yd}(\dot{y}_r - \dot{y}) + \ddot{y}_r]$$

$$\dot{\varphi}_{cmd} = k_{\varphi}(\varphi_r - \varphi) + \dot{\varphi}_r$$



# Admittance Controller

- Designed to behave like a Mass-Spring-Damper system that changes the desired reference to comply with the force

$$M(\ddot{X}_d - \ddot{X}_r) + D(\dot{X}_d - \dot{X}_r) + K(X_d - X_r) = -F$$

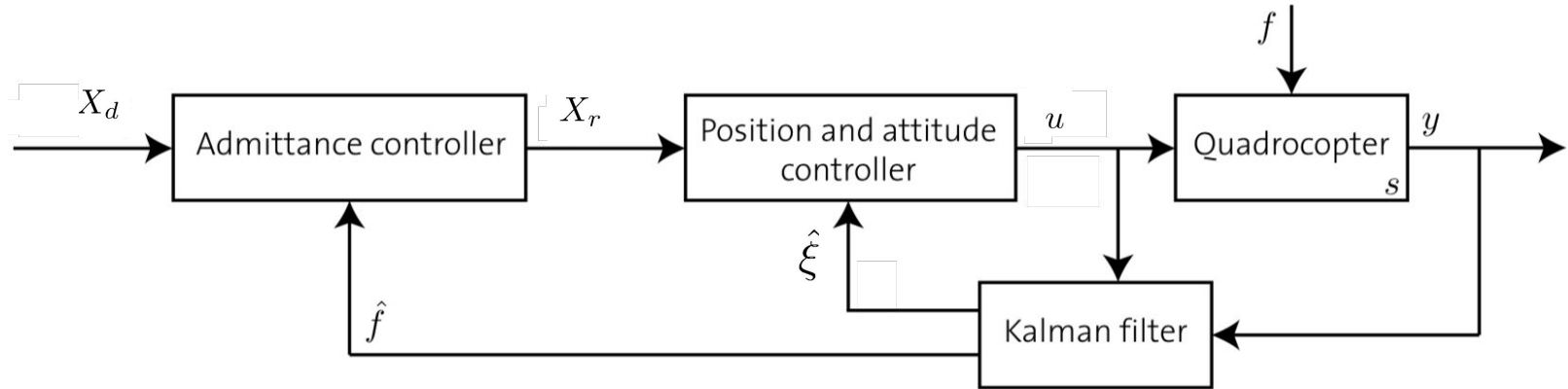
- $X_d$  = Desired Trajectory (Input to Admittance Controller);
- $X_r$  = Modified Reference Trajectory;
- $M$  = Apparent Inertia;
- $D$  = Desired Damping;
- $K$  = Desired Stiffness;
- $F = (F_x, F_y, F_z)$  is the applied force to the Quadrotor.





# Control Strategy

## Full Control Scheme



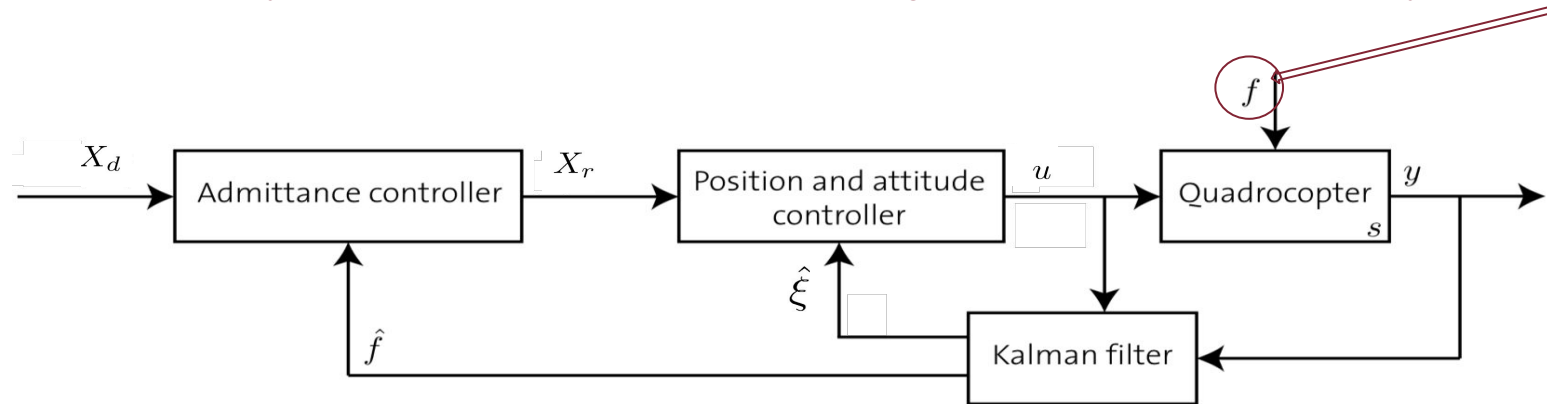
# Force Estimation

## Kalman Filter with extended state

- A Kalman Filter is used to determine the state of the system together with the external forces acting on it. We thus choose the augmented state:

$$\xi_k = (\xi, F)$$

- We define  $f = 1/m \cdot (F_x, F_y, F_z)$  as the mass-normalized force, allowing to assume that the force is purely driven by noise



# State Space Model

## Linearized Model

Quadcopter

$$\begin{cases} \dot{\xi} = A\xi + Bu + f + w \\ y = C\xi + Du + v \end{cases}$$

Position & Attitude

$$u = K_{\xi}\hat{\xi} + K_r X_r$$

Kalman Filter

$$\begin{cases} \dot{\xi}_k = A_k \xi_k + B_k u + w_k \\ y_k = C_k \xi_k + v \end{cases}$$

$$A_k = \begin{bmatrix} A & A_{k1[15 \times 3]} \\ 0_{[3 \times 3]} & 0_{[3 \times 3]} \end{bmatrix}$$

$$B_k = \begin{bmatrix} B \\ 0_{[3 \times 3]} \end{bmatrix}$$

$$C_k = [C \quad 0_{[3 \times 3]}]$$

Admittance Controller

$$\begin{cases} \dot{\xi}_{ad} = A_{ad} \xi_{ad} + B_{ad} u_{ad} \\ y = C_{ad} \xi_{ad} \end{cases}$$

$$A_{ad} = \begin{bmatrix} 0_{[3 \times 3]} & I_{[3 \times 3]} \\ -M^{-1}K & -M^{-1}D \end{bmatrix}$$

$$B_{ad} = \begin{bmatrix} 0_{[3 \times 3]} & 0_{[3 \times 3]} \\ M^{-1}K & -M^{-1} \end{bmatrix}$$

$$C_{ad} = [I_{[3 \times 3]} \quad 0_{[3 \times 3]}]$$



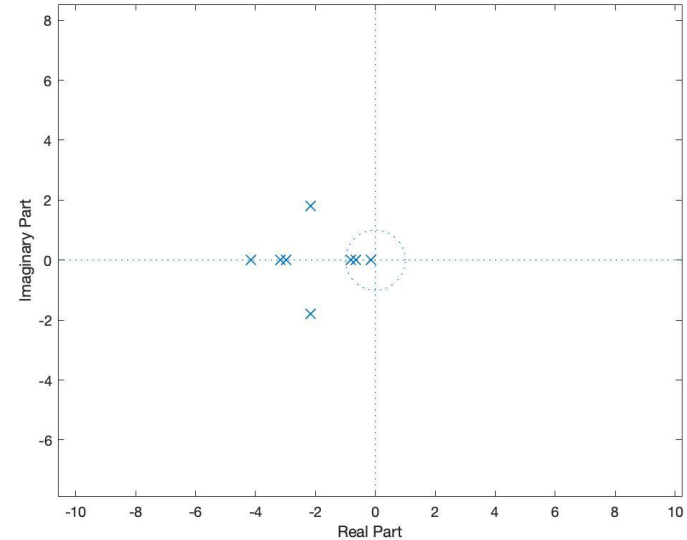
# Stability

## Admittance Controller

Since we are imposing the behaviour of a spring-mass-damper system:

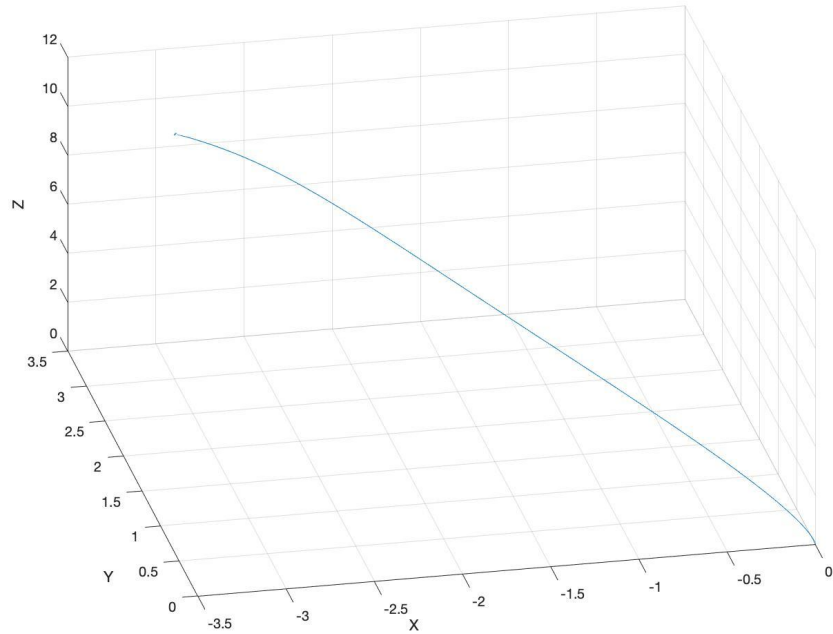
- The system will be stable for a stiffness different than zero (with 3 pairs of complex-conjugate poles)
- The system will be marginally stable if the stiffness is set to be zero (with a triple pole at the origin and another real triple pole).

## Kalman Filter

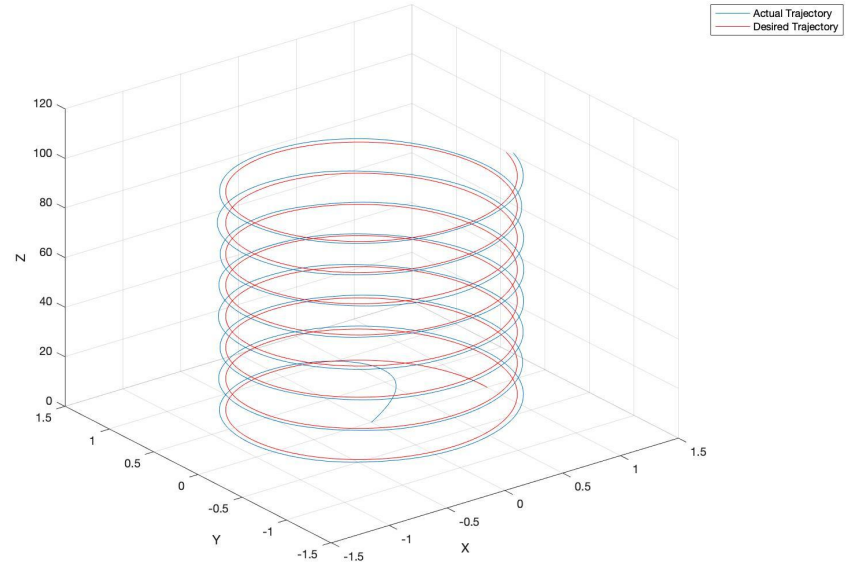


# Analysis & Results

## Regulation

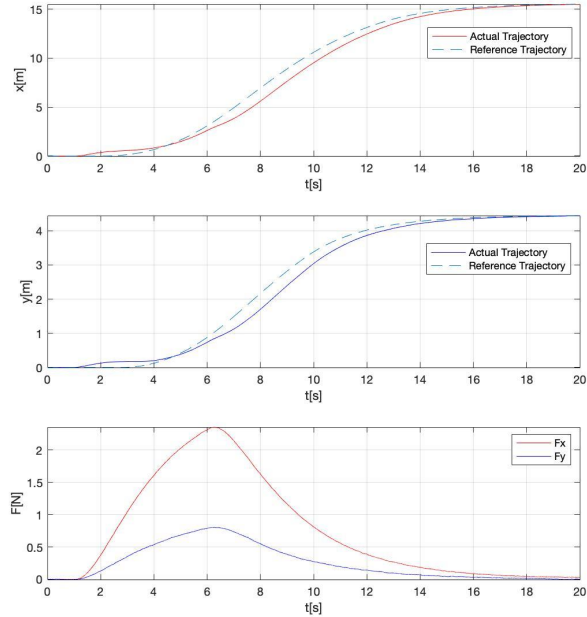


## Trajectory Tracking

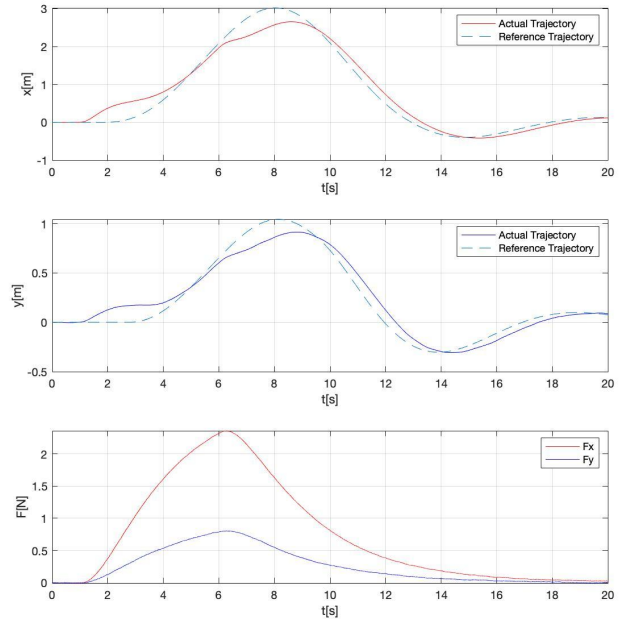


# Experiments

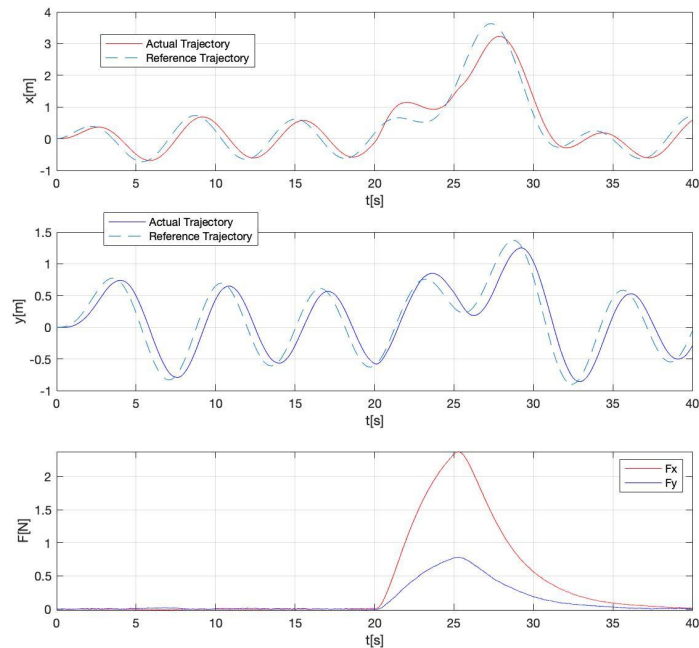
## 1. Constant Force with No stiffness



## 2. Constant Force with Stiffness

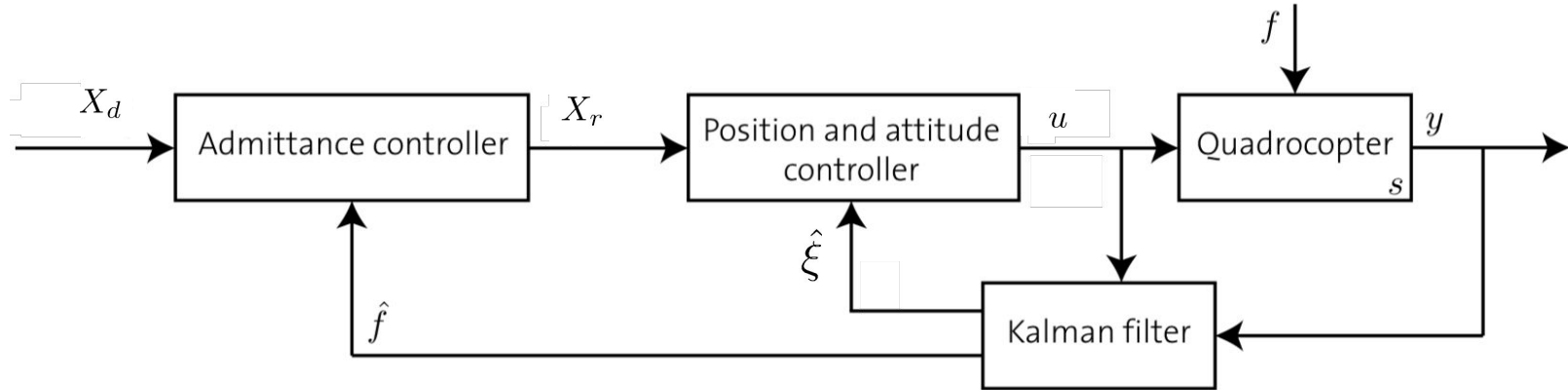


## 3. Constant Force with stiffness while performing circular motion



# Conclusion

- Good first approach to the problem with sufficiently accurate results
- Main limitation lies on the delay between the application of the force and its estimation





# THANK YOU



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