F.13/ Instead of the de in DCM we can use the de. for Euler angles (A.5)

$$\frac{\dot{\Theta}}{\dot{\omega}_{b}^{ibb}} = \frac{1}{4} \left( \underline{w}_{b}^{ib}, \underline{n}_{c}^{b} \right)$$

$$\frac{\dot{\omega}_{b}^{ibb}}{\dot{\omega}_{b}^{ib}} = \frac{1}{4} \left( \underline{w}_{b}^{ib}, \underline{n}_{c}^{b} \right)$$

$$\frac{\dot{\Theta}(t_{o})}{\dot{\omega}_{b}^{ib}} = \frac{1}{4} \left( \underline{w}_{b}^{ib}, \underline{n}_{c}^{ib} \right)$$

$$\underline{\theta} = \begin{bmatrix} \theta_1 \\ \theta_2 \\ \theta_3 \end{bmatrix} \qquad (3-1-1) \quad \text{Euler Ang.}$$

$$D_{\rho}^{\rho}(\underline{\theta})$$
 is given in A-105

$$D_{p}^{\theta}(\underline{\theta}) = \begin{cases} 1 & \sin\theta_{1} & \cos\theta_{1} & \cos\theta_{1} & \cos\theta_{2} \\ 0 & \cos\theta_{1} & -\sin\theta_{2} \\ 0 & \sin\theta_{1}/\cos\theta_{2} & \cos\theta_{1}/\cos\theta_{2} \end{cases}$$

Here 
$$X = \begin{bmatrix} \underline{\theta} \\ \underline{w}_b^{ib} \end{bmatrix}$$

Note: D.e. for Wib can be solved without solving d.e. for Q, Inot the other way

B.3 Torque\_free motion of a rigid\_body

Assume  $J_{xx} > J_{yy} > J_{zz}$ We want to randale  $w_b^{ib}$  and  $w_b^{ii}$  (we find trajetories, not the time function)

Ellipsoid of itelia
Inelia mahix  $J_c = \int_c^b \int_c^T$ 

=) pos. definite matrix and by using the expression:

If we chose f in the main axis.

$$\int_{-2}^{2} \frac{1}{2} \frac{x}{x} \int_{-1}^{1} \int_{-1}^{1} \int_{-1}^{1} \frac{x}{x} dx = \frac{1}{2} \int_{-1}^{3} \int_{-1}^{1} \frac{x}{x} dx$$

This eg on std. form:

$$\frac{X_1}{2J_1} + \frac{X_2}{2J_2} + \frac{X_3}{2J_2} = 1$$

Halfaxis: a; = \frac{2}{J\_{ii}} \text{ for i=1,2,3}

a, < a\_2 < a\_3

axis:

1=x
2=y
3=2

The form
of the ellipsoid
coinsides with
the form of the
body

Ellipsoide of inertia represents the torm of the body (w.r.t. rotation)

Kinetic notation energy ellipsoide

Multiphy the Enter equations (B-152)

(assume n. = 0, i.e. torque free motion)

with wx, wy and wz for line 1, 2 and

3 respectively, and add them up.

$$O = \sum_{i=1}^{3} \int_{ii} \dot{W}_{i} W_{i}$$

$$V_{i} = \sum_{i=1}^{3} \int_{ii} \dot{W}_{i} W_{i}$$

Integrate w.r.t time.

$$\int_{t_{i}}^{t} \int_{i=1}^{3} \int_{i}^{\infty} \frac{dw_{i}}{dt} w_{i} dt' = \int_{t_{i}}^{t} O dt = 0$$

 $\int_{1}^{4} \frac{1}{2} \sum_{i=1}^{3} J_{ii} W_{i}^{2}(t) = 0$ 

$$\frac{1}{2} \sum_{i=1}^{3} J_{ii} W_{i}(t) = \frac{1}{2} \sum_{i=1}^{3} J_{ii} W_{i}(t_{o}) = K_{o}$$

1.e.  $\frac{\frac{2}{W_{1}(t)}}{2K_{1}/J_{11}} + \frac{\frac{2}{W_{2}(t)}}{2K_{1}/J_{21}} + \frac{\frac{2}{W_{3}(t)}}{2K_{1}/J_{33}} = 1$ 

Half axis:  $\sqrt{\frac{2K_0}{J_{ii}}}$ 

We see that the binetic notation energy ellipsoid has the same form as the ellipsoid of inertia (can choose J=Ko)

Wib(t) has to stay on the kinetic rol. energy. ellipsoide

Angular momentum ellipsvide (spinnellipsvide)

When the outer force is zero  $(\vec{n}_c = \vec{o}) = \vec{h}_c = \vec{o}$ and  $||\vec{h}_c|| = \vec{h}_o$  (ronstant length) and the same direction in  $\vec{J}$ .

Angular velocity seen from  $F^b$   $\frac{h_c}{h_c} = \int_c^b W_b^{ib} = \begin{bmatrix} J_{xx} W_x \\ J_{55} W_5 \\ J_{22} W_2 \end{bmatrix}$ the main axis
the length of  $h_c$  is constant:  $\left(\frac{h_c}{h_c}\right)^T \frac{h_b}{h_c} = h_o$   $\frac{3}{1-1} J_{ii}^2 W_i^2 = h_o$ 

This ran be with on std. form of an ellipsoid.

$$\frac{W_{1}(t)}{h_{o}^{2}/J_{11}^{2}} + \frac{W_{2}(t)}{h_{o}^{2}/J_{22}^{2}} + \frac{W_{3}(t)}{h_{o}^{2}/J_{33}^{2}} = 1$$

Half axis: ho/Jii

We see that the kin. rol. energy ellipside and the angular momentum ellipside do not have the same half axis

=) different form of the ellipsoids and they need to intercent.

Wb (+) is on the intersection (pole had) of the two ellipsoids

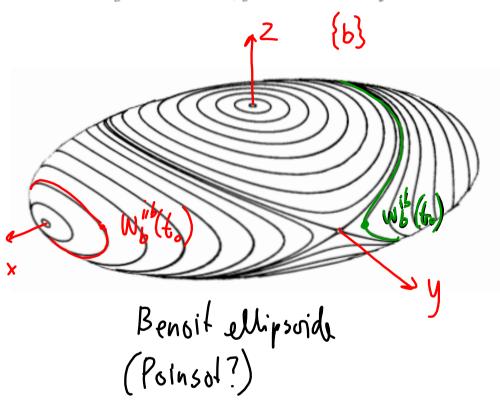
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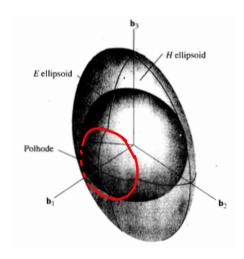
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# B.3.1 Beskrivelse av bevegelsen sett fra b-systemet

## Teorem B.13 Bevegelsen av et stivt legeme sett fra det roterende b-systemet

Anta b-systemet faller sammen med hovedaksene for det stive legemet. For et stivt legeme som ikke er utsatt for utre moment beveger vinkelhastighetsvektoren ( $\underline{\omega}_b^{ib}$ ) seg da, sett fra b-systemet, på skjeringa (polhode) mellom spinnellipsoida og den kinetiske rotasjonsenergiellipsoida. Bevegelsen til det stive legemet er i hvert øyeblikk en ren rotasjon om vinkelhastighetsvektoren.



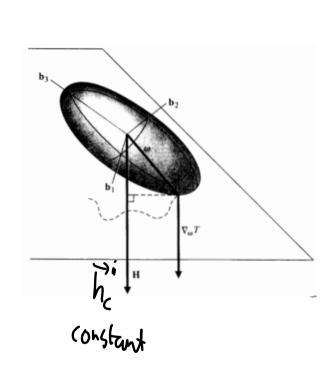


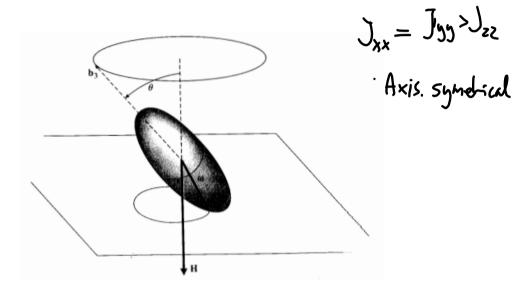
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# B.3.2 Beskrivelse av bevegelsen sett fra i-systemet

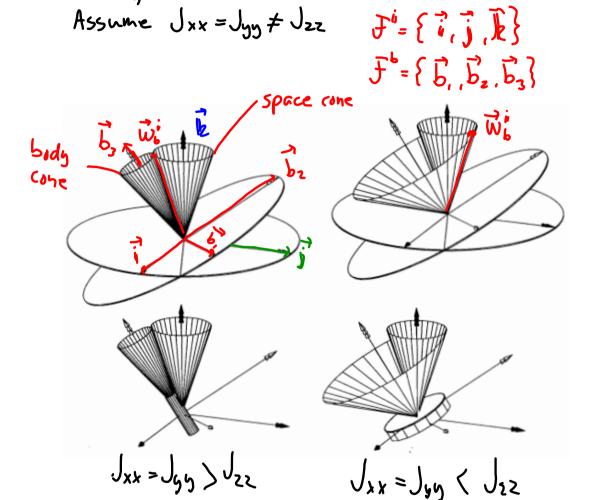
## Teorem B.14 Bevegelsen av et stivt legeme sett fra treghhetssystemet i

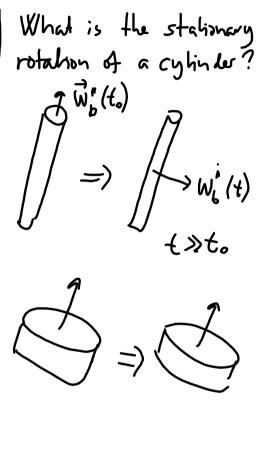
Bevegelsen av et stivt legeme som ikke er utsatt for et ytre moment er beskrevet, sett fra treghetsrommet, av at den kinetiske energiellipsoida ruller på det invariable plan (plan  $\bot$  spinnvektoren  $\vec{h}^i$ ) uten å gli. Rullinga følger polhodet på den kinetiske energiellipsoida (kontaktpunktet mellom det invariable plan og ellipsoida er dermed enden på  $\vec{\omega}_b^i$ -vektoren).





B. Y. Torque tree notion of a axis symmetrical body.





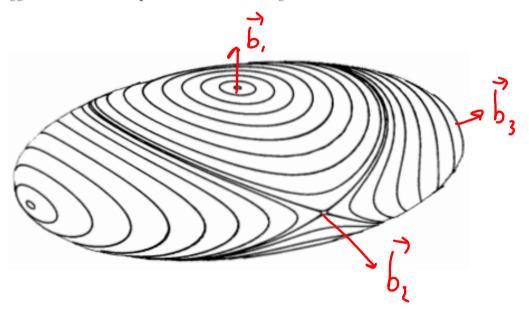
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#### B.3.3 Stabilitet om hovedaksene

Vi vil her undersøke stabiliteten til bevegelsen for små perturbasjoner om hovedaksene for et stivt legeme. Ovenfor så vi på bevegelsene i stort.

### Teorem B.15 Stabiliteten om hovedaksene for et stivt legeme

Anta b-systemet faller sammen med hovedaksene for det stive legemet og  $J_{xx}^b > J_{yy}^b > J_{zz}^b$ . Da gir linearisering om  $\vec{b}_1$ -aksen  $(J_{xx}^b)$  eller  $\vec{b}_3$ -aksen  $(J_{zz}^b)$  et lineært system med kompleks konjugerte egenverdier. Linearisering om  $\vec{b}_2$ -aksen  $(J_{yy}^b)$  gir et lineært system med to egenverdier, den ene ligger i venstre halvplan den andre i høgre.



# B.3.3 Stability of main axis

1) Rotation around b, -axis (x-axis)

Assume 
$$|W_x| \gg |W_y| \approx |W_z|$$
, set  $W_y w_z \approx 0$    
 Enler equations under these assuptions:

04,20

$$\dot{W}_{x} = (J_{yy} - J_{zz}) W_{y} W_{z} / J_{xx} = 0 =) W_{x}(t) = W_{xo}$$
 $\dot{W}_{y} = (J_{zz} - J_{xx}) W_{x} W_{z} / J_{yy} = \frac{J_{zz} - J_{xx}}{J_{yy}} W_{z} W_{xo} = -\alpha, W_{z} =) \dot{W}_{y} = -\alpha, W_{z}$ 
 $\dot{W}_{z} = (J_{xx} - J_{yy}) W_{x} W_{y} / J_{zz} = \frac{J_{xx} - J_{yy}}{J_{zz}} W_{y} W_{xo} = \alpha, W_{y} =) \dot{W}_{z} = \alpha_{z} W_{y}$ 

$$\begin{bmatrix} \dot{w}_{5} \\ \dot{w}_{z} \end{bmatrix} = \begin{bmatrix} O & -\alpha_{1} \\ \alpha_{2} & O \end{bmatrix} \begin{bmatrix} w_{5} \\ w_{z} \end{bmatrix}$$

$$\begin{bmatrix}
\dot{w}_{5} \\ \dot{w}_{z}
\end{bmatrix} = \begin{bmatrix}
0 & -\alpha_{1} \\ \alpha_{2} & 0
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\lambda & -\alpha_{2} \\ -\alpha_{2}$$

$$\lambda_{i,l} = \pm \sqrt{-\alpha_i \alpha_l} = \pm \sqrt{\alpha_i \alpha_l}$$