

Technical Report

Solar Position Algorithm for Solar Radiation Applications

Ibrahim Reda and Afshin Andreas



NREL

National Renewable Energy Laboratory

1617 Cole Boulevard
Golden, Colorado 80401-3393

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Abstract

There have been many published articles describing solar position algorithms for solar radiation applications. The best uncertainty achieved in most of these articles is greater than $\pm 0.01^\circ$ in calculating the solar zenith and azimuth angles. For some, the algorithm is valid for a limited number of years varying from 15 years to a hundred years. This report is a step by step procedure for implementing an algorithm to calculate the solar zenith and azimuth angles in the period from the year -2000 to 6000, with uncertainties of $\pm 0.0003^\circ$. The algorithm is described by Jean Meeus [3]. This report is written in a step by step format to simplify the complicated steps described in the book, with a focus on the sun instead of the planets and stars in general. It also introduces some changes to accommodate for solar radiation applications. The changes include changing the direction of measuring azimuth angles to be measured from north and eastward instead of being measured from south and eastward, and the direction of measuring the observer's geographical longitude to be measured as positive eastward from Greenwich meridian instead of negative. This report also includes the calculation of incidence angle for a surface that is tilted to any horizontal and vertical angle, as described by Iqbal [4].

1. Introduction

With the continuous technological advancements in solar radiation applications, there will always be a demand for smaller uncertainty in calculating the solar position. Many methods to calculate the solar position have been published in the solar radiation literature, nevertheless, their uncertainties have been greater than $\pm 0.01^\circ$ in solar zenith and azimuth angle calculations, and some are only valid for a specific number of years[1]. For example, Michalsky's calculations are limited to the period from 1950 to 2050 with uncertainty of greater than $\pm 0.01^\circ$ [2], and the calculations of Blanco-Muriel et al.'s are limited to the period from 1999 to 2015 with uncertainty greater than $> \pm 0.01^\circ$ [1].

An example emphasizing the importance of reducing the uncertainty of calculating the solar position to lower than $\pm 0.01^\circ$, is the calibration of pyranometers that measure the global solar irradiance. During the calibration, the responsivity of the pyranometer is calculated at zenith angles from 0° to 90° by dividing its output voltage by the reference global solar irradiance (G), which is a function of the cosine of the zenith angle ($\cos \theta$). Figure 1 shows the magnitude of errors that the 0.01° uncertainty in θ can contribute to the calculation of $\cos \theta$, and consequently G that is used to calculate the responsivity. Figure 1 shows that the uncertainty in $\cos \theta$ exponentially increases as θ reaches 90° (e.g. at θ equal to 87° , the uncertainty in $\cos \theta$ is 0.7%, which can result in an uncertainty of 0.35% in calculating G ; because at such large zenith angles the normal incidence irradiance is approximately equal to half the value of G). From this arises the need to use a solar position algorithm with lower uncertainty for users that are interested in measuring the global solar irradiance with smaller uncertainties in the full zenith angle range from 0° to 90° .

In this report we describe a procedure for a Solar Position Algorithm (SPA) to calculate the solar zenith and azimuth angle with uncertainties equal to $\pm 0.0003^\circ$ in the period from the year -2000 to 6000. Figure 1 shows that the uncertainty of the reference global solar irradiance, resulting from $\pm 0.0003^\circ$ in calculating the solar zenith angle in the range from 0° to 90° is negligible. The procedure is adopted from *The Astronomical Algorithms* [3], which is based on the Variations Sèculaires des Orbites Planétaires Theory (VSOP87) that was developed by P. Bretagnon in 1982 then modified in 1987 by Bretagnon and Francou [3]. In this report, we summarize the complex algorithm elements scattered throughout the book to calculate the solar position, and introduce some modification to the algorithm to accommodate solar radiation applications. For example, in *The Astronomical Algorithms* [3], the azimuth angle is measured westward from south, but for solar radiation applications, it is measured eastward from north. Also, the observer's geographical longitude is considered positive west, or negative east from Greenwich, while for solar radiation applications, it is considered negative west, or positive east from Greenwich.

We start this report by:

- Describing the time scales because of the importance of using the correct time in the SPA
- Providing a step by step procedure to calculate the solar position and the solar incidence angle for an arbitrary surface orientation using the methods described in *An Introduction*

to Solar Radiation [4]

- Evaluating the SPA against the *Astronomical Almanac* (AA) data for the years 1994, 1995, 1996, and 2004.

Because of the complexity of the algorithm we included some examples, in the Appendix, to give the users confidence in their step by step calculations. We also included in the Appendix an explanation of how to calculate the equation of time, sun transit (solar noon), sunrise, sunset, and how to change the Julian Day to a Calendar Date. We also included a C source code with header file, for all the calculations in this report (except for the Julian Day to Calendar Date conversion). The users can incorporate this module into their own code by including the header file, declaring the SPA structure, filling in the required input parameters into the structure, and then call the SPA calculation function. This function will calculate all the output values and fill in the SPA structure for the user.

The users should note that this report is used to calculate the solar position for solar radiation applications only, and that it is purely mathematical and not meant to teach astronomy or to describe the Earth rotation. For more description about the astronomical nomenclature that is used through out the report, the user is encouraged to review the definitions in the *Astronomical Almanacs*, or other astronomical reference.

2. Time Scale

The following are the internationally recognized time scales:

- The Universal Time (UT), or Greenwich civil time, is based on the Earth's rotation and counted from 0-hour at midnight; the unit is mean solar day [3]. UT is the time used to calculate the solar position in the described algorithm. It is sometimes referred to as UT1.
- The International Atomic Time (TAI) is the duration of the System International Second (SI-second) and based on a large number of atomic clocks [5].
- The Coordinated Universal Time (UTC) is the bases of most radio time signals and the legal time systems. It is kept to within 0.9 seconds of UT1 (UT) by introducing one second steps to its value (leap second); to date the steps are always positive.
- The Terrestrial Dynamical or Terrestrial Time (TDT or TT) is the time scale of ephemerides for observations from the Earth surface.

The following equations describe the relationship between the above time scales (in seconds):

$$TT = TAI + 32.184 \quad , \quad (1)$$

$$UT = TT - \Delta T \quad , \quad (2)$$

where ΔT is the difference between the Earth rotation time and the Terrestrial Time (TT). It is derived from observation only and reported yearly in the *Astronomical Almanac* [5].

$$UT = UT1 = UTC + \Delta UT1 \quad , \quad (3)$$

where $\Delta UT1$ is a fraction of a second, positive or negative value, that is added to the UTC to adjust for the Earth irregular rotational rate. It is derived from observation, but predicted values are transmitted in code in some time signals, e.g. weekly by the U.S. Naval Observatory (USNO) [6].

3. Procedure

3.1. Calculate the Julian and Julian Ephemeris Day, Century, and Millennium:

The Julian date starts on January 1, in the year - 4712 at 12:00:00 UT. The Julian Day (JD) is calculated using UT and the Julian Ephemeris Day (JDE) is calculated using TT. In the following steps, note that there is a 10-day gap between the Julian and Gregorian calendar where the Julian calendar ends on October 4, 1582 ($JD = 2299160$), and after 10-days the Gregorian calendar starts on October 15, 1582.

3.1.1 Calculate the Julian Day (JD),

$$JD = INT(365.25 * (Y + 4716)) + INT(30.6001 * (M + 1)) + D + B - 1524.5 \quad , \quad (4)$$

where,

- INT is the Integer of the calculated terms (e.g. $8.7 = 8$, $8.2 = 8$, and $-8.7 = -8$..etc.).
- Y is the year (e.g. 2001, 2002, ..etc.).
- M is the month of the year (e.g. 1 for January, ..etc.). Note that if $M > 2$, then Y and M are not changed, but if $M = 1$ or 2 , then $Y = Y - 1$ and $M = M + 12$.
- D is the day of the month with decimal time (e.g. for the second day of the month at 12:30:30 UT, $D = 2.521180556$).
- B is equal to 0, for the Julian calendar {i.e. by using $B = 0$ in Equation 4, $JD < 2299160$ }, and equal to $(2 - A + INT(A/4))$ for the Gregorian calendar {i.e. by using $B = 0$ in Equation 4, $JD > 2299160$ }, where $A = INT(Y/100)$.

For users who wish to use their local time instead of UT, change the time zone to a fraction of a day (by dividing it by 24), then subtract the result from JD . Note that the fraction is subtracted from JD calculated before the test for $B < 2299160$ to maintain the Julian and Gregorian periods.

Table A4.1 shows examples to test any implemented program used to calculate the JD .

3.1.2. Calculate the Julian Ephemeris Day (*JDE*),

$$JDE = JD + \frac{\Delta T}{86400} \quad (5)$$

3.1.3. Calculate the Julian century (*JC*) and the Julian Ephemeris Century (*JCE*) for the 2000 standard epoch,

$$JC = \frac{JD - 2451545}{36525} \quad (6)$$

$$JCE = \frac{JDE - 2451545}{36525} \quad (7)$$

3.1.4. Calculate the Julian Ephemeris Millennium (*JME*) for the 2000 standard epoch,

$$JME = \frac{JCE}{10} \quad (8)$$

3.2. Calculate the Earth heliocentric longitude, latitude, and radius vector (*L*, *B*, and *R*):

“Heliocentric” means that the Earth position is calculated with respect to the center of the sun.

3.2.1. For each row of Table A4.2, calculate the term $L0_i$ (in radians),

$$L0_i = A_i * \cos(B_i + C_i * JME) \quad (9)$$

where,

- i is the i^{th} row for the term $L0$ in Table A4.2.

- A_i , B_i , and C_i are the values in the i^{th} row and A , B , and C columns in Table A4.2, for the term $L0$ (in radians).

3.2.2. Calculate the term $L0$ (in radians),

$$L0 = \sum_{i=0}^n L0_i \quad (10)$$

where n is the number of rows for the term $L0$ in Table A4.2.

3.2.3. Calculate the terms $L1$, $L2$, $L3$, $L4$, and $L5$ by using Equations 9 and 10 and changing the 0 to 1, 2, 3, 4, and 5, and by using their corresponding values in

columns A, B, and C in Table A4.2 (in radians).

3.2.4. Calculate the Earth heliocentric longitude, L (in radians),

$$L = \frac{L0 + L1 * JME + L2 * JME^2 + L3 * JME^3 + L4 * JME^4 + L5 * JME^5}{10^8} . \quad (11)$$

3.2.5. Calculate L in degrees,

$$L \text{ (in Degrees)} = \frac{L \text{ (in Radians)} * 180}{\pi} , \quad (12)$$

where π is approximately equal to 3.1415926535898.

3.2.6. Limit L to the range from 0° to 360° . That can be accomplished by dividing L by 360 and recording the decimal fraction of the division as F . If L is positive, then the limited $L = 360 * F$. If L is negative, then the limited $L = 360 - 360 * F$.

3.2.7. Calculate the Earth heliocentric latitude, B (in degrees), by using Table A4.2 and steps 3.2.1 through 3.2.5 and by replacing all the L s by B s in all equations. Note that there are no $B2$ through $B5$, consequently, replace them by zero in steps 3.2.3 and 3.2.4.

3.2.8. Calculate the Earth radius vector, R (in Astronomical Units, AU), by repeating step 3.2.7 and by replacing all L s by R s in all equations. Note that there is no $R5$, consequently, replace it by zero in steps 3.2.3 and 3.2.4.

3.3. Calculate the geocentric longitude and latitude (Θ and β):

“Geocentric” means that the sun position is calculated with respect to the Earth center.

3.3.1. Calculate the geocentric longitude, Θ (in degrees),

$$\Theta = L + 180 . \quad (13)$$

3.3.2. Limit Θ to the range from 0° to 360° as described in step 3.2.6.

3.3.3. Calculate the geocentric latitude, β (in degrees),

$$\beta = -B . \quad (14)$$

3.4. Calculate the nutation in longitude and obliquity ($\Delta\psi$ and $\Delta\epsilon$):

3.4.1. Calculate the mean elongation of the moon from the sun, X_0 (in degrees),

$$X_0 = 297.85036 + 445267.111480 * JCE - 0.0019142 * JCE^2 + \frac{JCE^3}{189474} \quad (15)$$

3.4.2. Calculate the mean anomaly of the sun (Earth), X_1 (in degrees),

$$X_1 = 357.52772 + 35999.050340 * JCE - 0.0001603 * JCE^2 - \frac{JCE^3}{300000} \quad (16)$$

3.4.3. Calculate the mean anomaly of the moon, X_2 (in degrees),

$$X_2 = 134.96298 + 477198.867398 * JCE + 0.0086972 * JCE^2 + \frac{JCE^3}{56250} \quad (17)$$

3.4.4. Calculate the moon's argument of latitude, X_3 (in degrees),

$$X_3 = 93.27191 + 483202.017538 * JCE - 0.0036825 * JCE^2 + \frac{JCE^3}{327270} \quad (18)$$

3.4.5. Calculate the longitude of the ascending node of the moon's mean orbit on the ecliptic, measured from the mean equinox of the date, X_4 (in degrees),

$$X_4 = 125.04452 - 1934.136261 * JCE + 0.0020708 * JCE^2 + \frac{JCE^3}{450000} \quad (19)$$

3.4.6. For each row in Table A4.3, calculate the terms $\Delta\psi_i$ and $\Delta\epsilon_i$ (in 0.0001 of arc seconds),

$$\Delta\psi_i = (a_i + b_i * JCE) * \sin\left(\sum_{j=0}^4 X_j * Y_{i,j}\right) \quad (20)$$

$$\Delta \varepsilon_i = (c_i + d_i * JCE) * \cos \left(\sum_{j=0}^4 X_j * Y_{i,j} \right) , \quad (21)$$

where,

- a_i , b_i , c_i , and d_i are the values listed in the i^{th} row and columns a, b, c, and d in Table A4.3.
- X_j is the j^{th} X calculated by using Equations 15 through 19.
- $Y_{i,j}$ is the value listed in i^{th} row and j^{th} Y column in Table A4.3.

3.4.7. Calculate the nutation in longitude, $\Delta \psi$ (in degrees),

$$\Delta \psi = \frac{\sum_{i=0}^n \Delta \psi_i}{36000000} , \quad (22)$$

where n is the number of rows in Table A4.3 (n equals 63 rows in the table).

3.4.8. Calculate the nutation in obliquity, $\Delta \varepsilon$ (in degrees),

$$\Delta \varepsilon = \frac{\sum_{i=0}^n \Delta \varepsilon_i}{36000000} . \quad (23)$$

3.5. Calculate the true obliquity of the ecliptic, ε (in degrees):

3.5.1. Calculate the mean obliquity of the ecliptic, ε_0 (in arc seconds),

$$\begin{aligned} \varepsilon_0 = & 84381.448 - 4680.93U - 1.55U^2 + 1999.25U^3 - \\ & 51.38U^4 - 249.67U^5 - 39.05U^6 + 7.12U^7 + \\ & 27.87U^8 + 5.79U^9 + 2.45U^{10} , \end{aligned} \quad (24)$$

where $U = JME/10$.

3.5.2. Calculate the true obliquity of the ecliptic, ε (in degrees),

$$\varepsilon = \frac{\varepsilon_0}{3600} + \Delta \varepsilon . \quad (25)$$

3.6. Calculate the aberration correction, $\Delta\tau$ (in degrees):

$$\Delta\tau = -\frac{20.4898}{3600 * R} . \quad (26)$$

3.7. Calculate the apparent sun longitude, λ (in degrees):

$$\lambda = \Theta + \Delta\psi + \Delta\tau . \quad (27)$$

3.8. Calculate the apparent sidereal time at Greenwich at any given time, ν (in degrees):

3.8.1. Calculate the mean sidereal time at Greenwich, ν_0 (in degrees),

$$\nu_0 = 280.46061837 + 360.98564736629 * (JD - 2451545) + 0.000387933 * JC^2 - \frac{JC^3}{38710000} . \quad (28)$$

3.8.2. Limit ν_0 to the range from 0° to 360° as described in step 3.2.6.

3.8.3. Calculate the apparent sidereal time at Greenwich, ν (in degrees),

$$\nu = \nu_0 + \Delta\psi * \cos(\varepsilon) . \quad (29)$$

3.9. Calculate the geocentric sun right ascension, α (in degrees):

3.9.1. Calculate the sun right ascension, α (in radians),

$$\alpha = \text{Arc tan 2} \left(\frac{\sin \lambda * \cos \varepsilon - \tan \beta * \sin \varepsilon}{\cos \lambda} \right) , \quad (30)$$

where Arctan2 is an arctangent function that is applied to the numerator and the denominator (instead of the actual division) to maintain the correct quadrant of the α where α is in the range from $-\pi$ to π .

3.9.2. Calculate α in degrees using Equation 12, then limit it to the range from 0° to 360° using the technique described in step 3.2.6.

3.10. Calculate the geocentric sun declination, δ (in degrees):

$$\delta = \text{Arc sin}(\sin \beta * \cos \varepsilon + \cos \beta * \sin \varepsilon * \sin \lambda) , \quad (31)$$

where δ is positive or negative if the sun is north or south of the celestial equator, respectively. Then change δ to degrees using Equation 12.

3.11. Calculate the observer local hour angle, H (in degrees):

$$H = \nu + \sigma - \alpha \quad , \quad (32)$$

Where σ is the observer geographical longitude, positive or negative for east or west of Greenwich, respectively.

Limit H to the range from 0° to 360° using step 3.2.6 and note that it is measured westward from south in this algorithm.

3.12. Calculate the topocentric sun right ascension α' (in degrees):

“Topocentric” means that the sun position is calculated with respect to the observer local position at the Earth surface.

3.12.1. Calculate the equatorial horizontal parallax of the sun, ξ (in degrees),

$$\xi = \frac{8.794}{3600 * R} \quad , \quad (33)$$

where R is calculated in step 3.2.8.

3.12.2. Calculate the term u (in radians),

$$u = \text{Arc tan} (0.99664719 * \tan \varphi) \quad , \quad (34)$$

where φ is the observer geographical latitude, positive or negative if north or south of the equator, respectively. Note that the 0.99664719 number equals $(1 - f)$, where f is the Earth's flattening.

3.12.3. Calculate the term x ,

$$x = \cos u + \frac{E}{6378140} * \cos \varphi \quad , \quad (35)$$

where E is the observer elevation (in meters). Note that x equals $\rho * \cos \varphi'$ where ρ is the observer's distance to the center of Earth, and φ' is the observer's geocentric latitude.

3.12.4. Calculate the term y ,

$$y = 0.99664719 * \sin u + \frac{E}{6378140} * \sin \varphi \quad , \quad (36)$$

note that y equals $\rho * \sin \varphi'$,

3.12.5. Calculate the parallax in the sun right ascension, $\Delta\alpha$ (in degrees),

$$\Delta\alpha = \text{Arc tan} 2 \left(\frac{-x * \sin \xi * \sin H}{\cos \delta - x * \sin \xi * \cos H} \right) \quad . \quad (37)$$

Then change $\Delta\alpha$ to degrees using Equation 12.

3.12.6. Calculate the topocentric sun right ascension α' (in degrees),

$$\alpha' = \alpha + \Delta\alpha \quad . \quad (38)$$

3.12.7. Calculate the topocentric sun declination, δ' (in degrees),

$$\delta' = \text{Arc tan} 2 \left(\frac{(\sin \delta - y * \sin \xi) * \cos \Delta\alpha}{\cos \delta - x * \sin \xi * \cos H} \right) \quad . \quad (39)$$

3.13. Calculate the topocentric local hour angle, H' (in degrees),

$$H' = H - \Delta\alpha \quad . \quad (40)$$

3.14. Calculate the topocentric zenith angle, θ (in degrees):

3.14.1. Calculate the topocentric elevation angle without atmospheric refraction correction, e_0 (in degrees),

$$e_0 = \text{Arc sin} (\sin \varphi * \sin \delta' + \cos \varphi * \cos \delta' * \cos H') \quad . \quad (41)$$

Then change e_0 to degrees using Equation 12.

3.14.2. Calculate the atmospheric refraction correction, Δe (in degrees),

$$\Delta e = \frac{P}{1010} * \frac{283}{273 + T} * \frac{1.02}{60 * \tan \left(e_0 + \frac{10.3}{e_0 + 5.11} \right)} \quad , \quad (42)$$

Note that $\Delta e = 0$ when the sun is below the horizon.

where,

- P is the annual average local pressure (in millibars).
- T is the annual average local temperature (in °C).
- e_0 is in degrees. Calculate the tangent argument in degrees, then convert to radians if required by calculator or computer.

3.14.3. Calculate the topocentric elevation angle, e (in degrees),

$$e = e_0 + \Delta e \quad . \quad (43)$$

3.14.4. Calculate the topocentric zenith angle, θ (in degrees),

$$\theta = 90 - e \quad . \quad (44)$$

3.15. Calculate the topocentric azimuth angle, Φ (in degrees):

3.15.1. Calculate the topocentric astronomers azimuth angle, Γ (in degrees),

$$\Gamma = \text{Arc tan 2} \left(\frac{\sin H'}{\cos H' \sin \varphi - \tan \delta' \cos \varphi} \right) \quad , \quad (45)$$

Change Γ to degrees using Equation 12, then limit it to the range from 0° to 360° using step 3.2.6. Note that Γ is measured westward from south.

3.15.2. Calculate the topocentric azimuth angle, Φ for navigators and solar radiation users (in degrees),

$$\Phi = \Gamma + 180 \quad , \quad (46)$$

Limit Φ to the range from 0° to 360° using step 3.2.6. Note that Φ is measured eastward from north.

3.16. Calculate the incidence angle for a surface oriented in any direction, I (in degrees):

$$I = \text{Arc cos}(\cos \theta * \cos \omega + \sin \omega * \sin \theta * \cos (\Gamma - \gamma)) \quad , \quad (47)$$

where,

- ω is the slope of the surface measured from the horizontal plane.
- γ is the surface azimuth rotation angle, measured from south to the projection of the surface normal on the horizontal plane, positive or negative if oriented west or east from south, respectively.

4. SPA Evaluation and Conclusion

Because the solar zenith, azimuth, and incidence angles are not reported in the *Astronomical Almanac* (AA), the following sun parameters are used for the evaluation: The main parameters (ecliptic longitude and latitude for the mean Equinox of date, apparent right ascension, apparent declination), and the correcting parameters (nutations in longitude, nutations in obliquity, obliquity of ecliptic, and true geometric distance). Exact trigonometric functions are used with the AA reported sun parameters to calculate the solar zenith and azimuth angles, therefore it is adequate to evaluate the SPA uncertainty using these parameters. To evaluate the uncertainty of the SPA, we chose the second day of each month, for each of the years 1994, 1995, 1996, and 2004, at 0-hour Terrestrial Time (TT). Figures 2 shows that the maximum difference between the AA and SPA main parameters is -0.00015° . Figure 3 shows that the maximum difference between the AA and SPA for calculating the zenith or azimuth angle is 0.00003° and 0.00008° , respectively. This implies that the SPA is well within the stated uncertainty of $\pm 0.0003^\circ$.

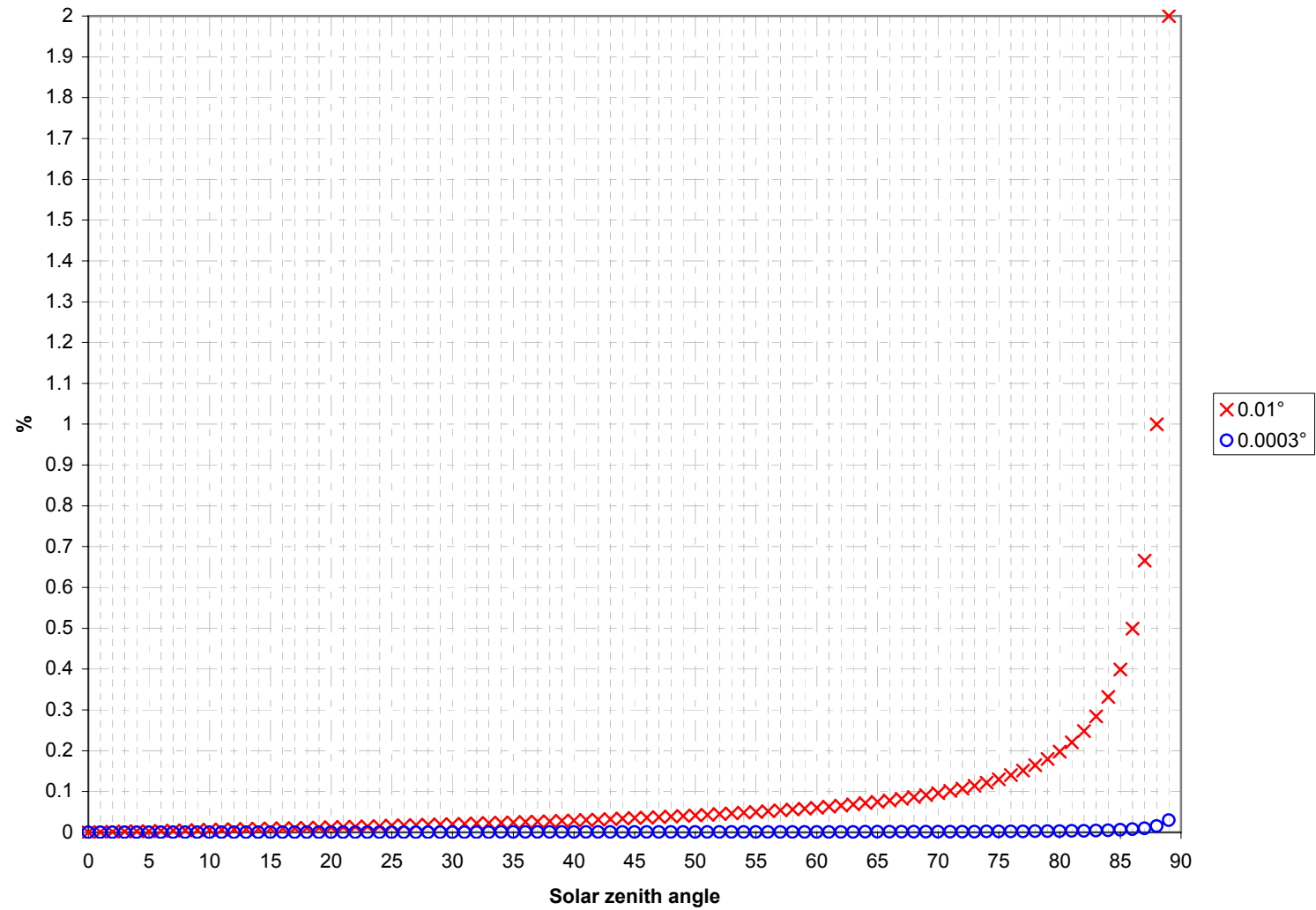


Figure 1. Uncertainty of cosine the solar zenith angle resulting from 0.01° and 0.0003° uncertainty in the angle calculation

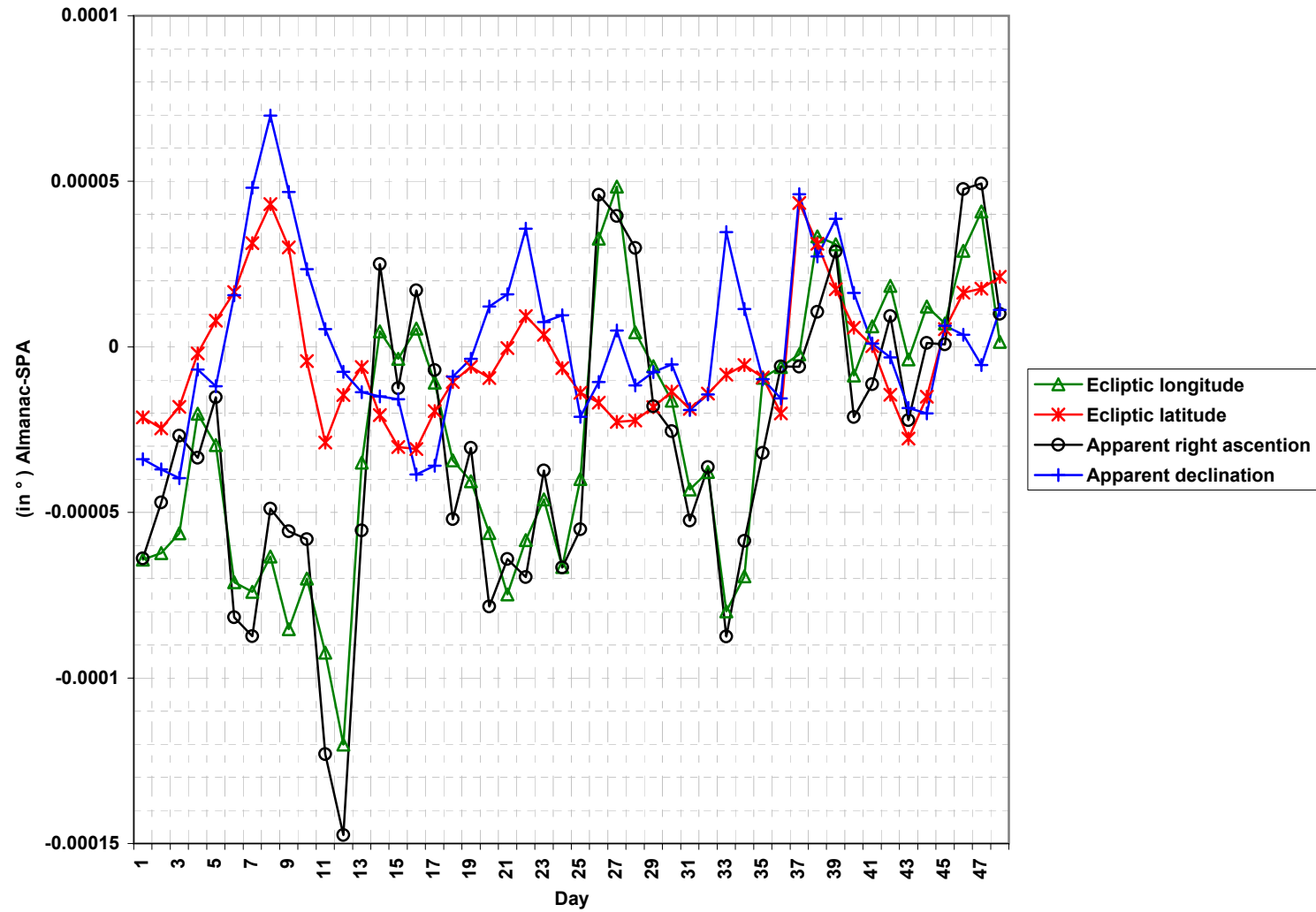


Figure 2. Difference between the Almanac and SPA for the ecliptic longitude, ecliptic latitude, apparent right ascension, and apparent declination on the second day of each month at 0-TT for the years 1994, 1995, 1996, and 2004

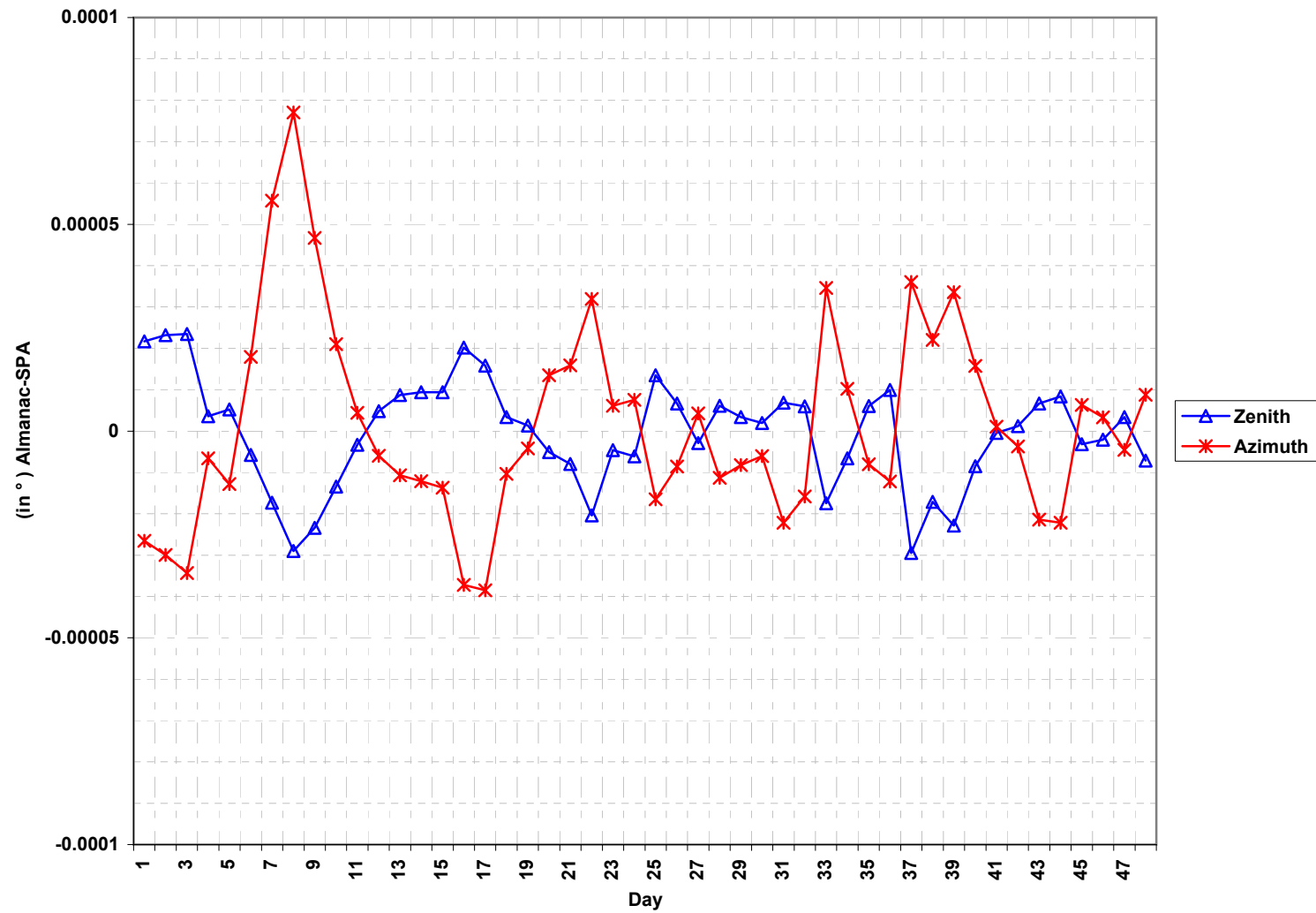


Figure 3. Difference between the Almanac and SPA for the solar zenith and azimuth angles on the second day of each month at 0-TT for the years 1994, 1995, 1996, 2004

References

1. Blanco-Muriel, M., et al. "Computing the Solar Vector". *Solar Energy*. Vol. 70, No. 5, 2001; pp. 431-441, 2001, Great Britain.
2. Michalsky, J. J. "The Astronomical Almanac's Algorithm for Approximate Solar Position (1950-2050)". *Solar Energy*. Vol. 40, No. 3, 1988; pp. 227-235, USA.
3. Meeus, J. "Astronomical Algorithms". Second edition 1998, Willmann-Bell, Inc., Richmond, Virginia, USA.
4. Iqbal, M. "An Introduction to Solar Radiation". New York: 1983; pp. 23-25.
5. The Astronomical Almanac. Norwich:2004.
6. The U.S. Naval Observatory. Washington, DC, <http://www.usno.navy.mil/>.

Appendix

Note that some of the symbols used in the appendix are independent from the symbols used in the main report.

A.1. Equation of Time

The Equation of Time, E , is the difference between solar apparent and mean time. Use the following equation to calculate E (in degrees),

$$E = M - 0.0057183 - \alpha + \Delta\psi * \cos \varepsilon , \quad (A1)$$

where,

- M is the sun's mean longitude (in degrees),

$$M = 280.4664567 + 360007.6982779 * JME + 0.03032028 * JME^2 + \frac{JME^3}{49931} - \frac{JME^4}{15300} - \frac{JME^5}{2000000} , \quad (A2)$$

where JME is the Julian Ephemeris Millennium calculated from Equation 8, and M is limited to the range from 0° to 360° using step 3.2.6.

- α is the geocentric right ascension, from Equation 30 (in degrees).

- $\Delta\psi$ is the nutation in longitude, from Equation 22 (in degrees).

- ε is the obliquity of the ecliptic, from Equation 25 (in degrees).

Multiply E by 4 to change its unit from degrees to minutes of time. Limit E if its absolute value is greater than 20 minutes, by adding or subtracting 1440.

A.2. Sunrise, Sun Transit, and Sunset

The value of 0.5667° is typically adopted for the atmospheric refraction at sunrise and sunset times. Thus for the sun radius of 0.26667° , the value -0.8333° of sun elevation (h'_0) is chosen to calculate the times of sunrise and sunset. On the other hand, the sun transit is the time when the center of the sun reaches the local meridian.

A.2.1. Calculate the apparent sidereal time at Greenwich at 0 UT, v (in degrees), using Equation 29.

A.2.2. Calculate the geocentric right ascension and declination at 0 TT, using Equations 30 and 31, for the day before the day of interest (D_{-1}), the day of interest (D_0),

then the day after (D_{+1}). Denote the values as $\alpha_{-1} \quad \delta_{-1}$
 $\alpha_0 \quad \delta_0$, in degrees.

A.2.3. Calculate the approximate sun transit time, m_0 , in fraction of day,

$$m_0 = \frac{\alpha_0 - \sigma - \nu}{360} , \quad (A3)$$

where σ is the observer geographical longitude, in degrees, positive east of Greenwich..

A.2.4. Calculate the local hour angle corresponding to the sun elevation equals -
 0.8333° , H_0 ,

$$H_0 = \text{Arc cos} \left(\frac{\sin h'_0 - \sin \varphi * \sin \delta_0}{\cos \varphi * \cos \delta_0} \right) , \quad (A4)$$

where,

- h'_0 equals -0.8333° .
- φ is the observer geographical latitude, in degrees, positive north of the equator.

Note that if the argument of the Arccosine is not in the range from -1 to 1, it means that the sun is always above or below the horizon for that day.

Change H_0 to degrees using Equation 12, then limit it to the range from 0° to 180° using step 3.2.6 and replacing 360 by 180.

A.2.5. Calculate the approximate sunrise time, m_1 , in fraction of day,

$$m_1 = m_0 - \frac{H_0}{360} . \quad (A5)$$

A.2.6. Calculate the approximate sunset time, m_2 , in fraction of day,

$$m_2 = m_0 + \frac{H_0}{360} . \quad (A6)$$

A.2.7. Limit the values of m_0 , m_1 , and m_2 to a value between 0 and 1 fraction of day using step 3.2.6 and replacing 360 by 1.

A.2.8. Calculate the sidereal time at Greenwich, in degrees, for the sun transit, sunrise, and sunset, ν_i ,

$$\nu_i = \nu + 360.985647 * m_i \quad , \quad (A7)$$

where i equals 0, 1, and 2 for sun transit, sunrise, and sunset, respectively.

A.2.9. Calculate the terms n_i ,

$$n_i = m_i + \frac{\Delta T}{86400} \quad , \quad (A8)$$

where $\Delta T = TT - UT$.

A.2.10. Calculate the values α'_i and δ'_i , in degrees, where i equals 0, 1, and 2,

where,

$$\alpha'_i = \alpha_0 + \frac{n_i(a + b + c * n_i)}{2} \quad , \quad (A9)$$

and,

$$\delta'_i = \delta_0 + \frac{n_i(a' + b' + c' * n_i)}{2} \quad , \quad (A10)$$

where,

- a and a' equal $(\alpha_0 - \alpha_{-1})$ and $(\delta_0 - \delta_{-1})$, respectively.

- b and b' equal $(\alpha_{+1} - \alpha_0)$ and $(\delta_{+1} - \delta_0)$, respectively.

- c and c' equal $(b - a)$ and $(b' - a')$, respectively.

If the absolute value of a , a' , b , or b' is greater than 2, then limit its value between 0 and 1 as shown in step A.2.7.

A.2.11. Calculate the local hour angle for the sun transit, sunrise, and sunset, H'_i (in degrees),

$$H'_i = \nu_i + \sigma - \alpha'_i \quad . \quad (A11)$$

H'_i in this case is measured as positive westward from the meridian, and negative eastward from the meridian. Thus limit H'_i between -180° and 180° . To preserve the quadrant sign of H'_i limit it to $\pm 360^\circ$ first, then if H'_i is less than or equal -180° , then add 360° to force its value to be between 0° and 180° . And if H'_i is greater than or equal 180° , then add -360° to force its value to be between 0° and -180° .

A.2.12. Calculate the sun altitude for the sun transit, sunrise, and sunset, h_i (in degrees),

$$h_i = \text{Arc sin} (\sin \varphi * \sin \delta'_i + \cos \varphi * \cos \delta'_i * \cos H'_i) \quad . \quad (\text{A12})$$

A.2.13. Calculate the sun transit, T (in fraction of day),

$$T = m_0 - \frac{H'_0}{360} \quad . \quad (\text{A13})$$

A.2.14. Calculate the sunrise, R (in fraction of day),

$$R = m_1 + \frac{h_1 - h'_0}{360 * \cos \delta'_1 * \cos \varphi * \sin H'_1} \quad . \quad (\text{A14})$$

A.2.15. Calculate the sunset, S (in fraction of day), by using Equation A14 and replacing R by S , and replacing the suffix number 1 by 2.

The fraction of day value is changed to UT by multiplying the value by 24.

To evaluate the uncertainty of the SPA, we chose the second day of each month, for each of the years 1994, 1995, 1996, and 2004, at 0-hour Terrestrial Time (TT). Figure A2.1 shows that the maximum difference between the AA and SPA sun transit time is -0.23 seconds.

Because the sunrise and sunset are recorded in the AA to a one minute resolution, we compared the SPA calculations at only three data points at Greenwich meridian at 0-UT. The comparison result in Table A2.1 shows that the maximum difference between AA and SPA is 15.4 seconds (0.26 minute), which is well within the AA resolution of one minute.

Note that UT can be changed to local time by adding the time zone as a fraction of a day (time zone is divided by 24), and limiting the result to the range from 0 to 1.

Table A2.1. The AA and SPA Results for Sunrise and Sunset at Greenwich Meridian at 0-UT

Date	Observer Latitude	Sunrise		Sunset	
		AA	SPA	AA	SPA
January 2, 1994	35°	7:08	7:08:12.8	17:00	16:59:55.9
July 5, 1996	-35°	7:08	7:08:15.4	17:00	17:01:04.5
December 4, 2004	-35°	4:39	4:38:57.1	19:02	19:02:2.5

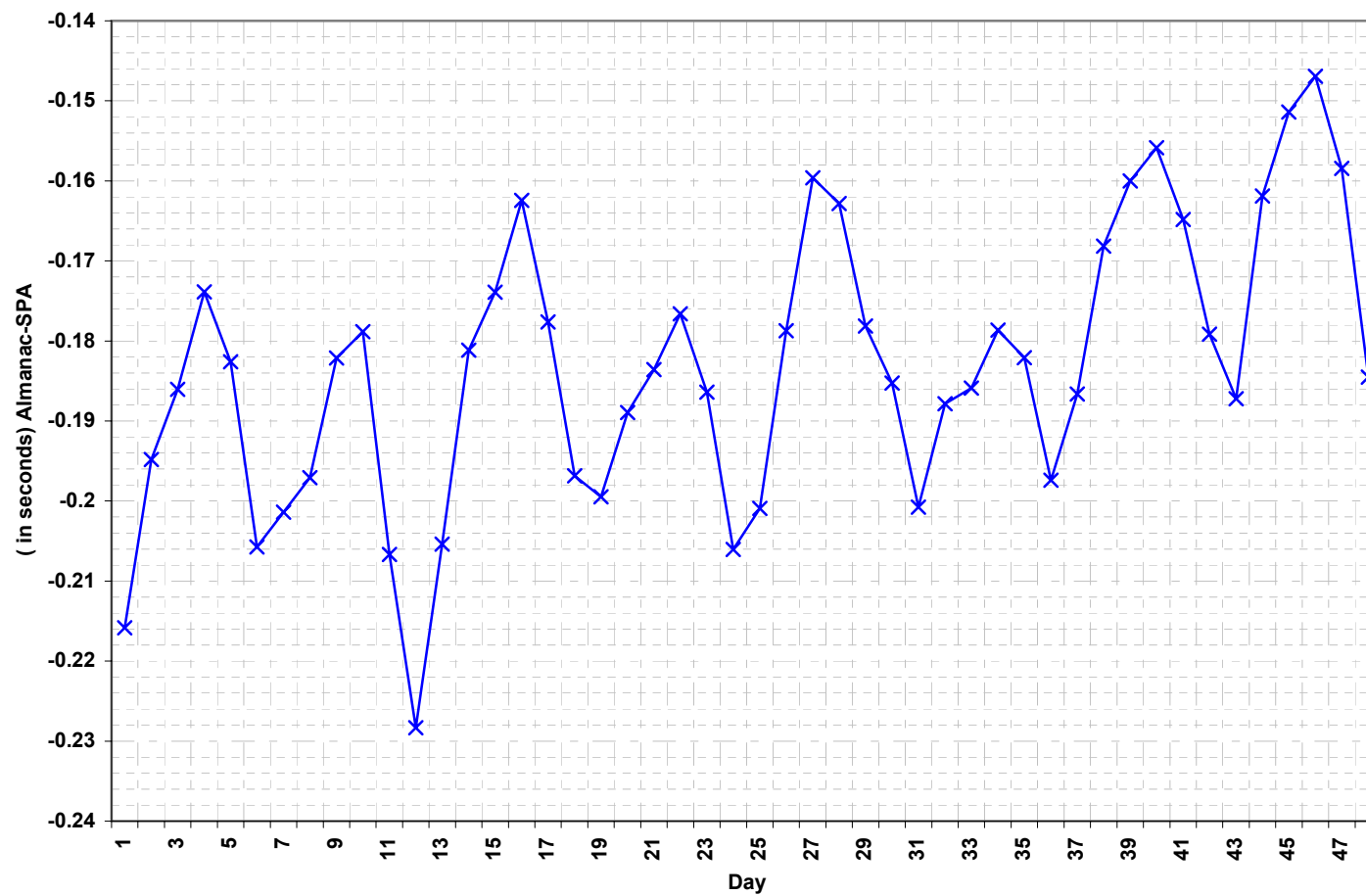


Figure A2.1. Difference between the Almanac and SPA for the Ephemeris Transit on the second day of each month at 0-TT for the years 1994, 1995, 1996, 2004

A.3. Calculation of Calendar Date from Julian Day

A.3.1. Add 0.5 to the Julian Day (JD), then record the integer of the result as Z , and the fraction decimal as F .

A.3.2. If Z is less than 2299161, then record A equals Z . Else, calculate the term B ,

$$B = INT \left(\frac{Z - 1867216.25}{36524.25} \right) , \quad (A15)$$

Then calculate the term A ,

$$A = Z + 1 + B - INT \left(\frac{B}{4} \right) . \quad (A16)$$

A.3.3. Calculate the term C ,

$$C = A + 1524 . \quad (A17)$$

A.3.4. Calculate the term D ,

$$D = INT \left(\frac{C - 122.1}{365.25} \right) . \quad (A18)$$

A.3.5. Calculate the term G ,

$$G = INT (365.25 * D) . \quad (A19)$$

A.3.6. Calculate the term I ,

$$I = INT \left(\frac{C - G}{30.6001} \right) . \quad (A20)$$

A.3.7. Calculate the day number of the month with decimals, d ,

$$d = C - G - INT (30.6001 * I) + F . \quad (A21)$$

A.3.8. Calculate the month number, m ,

$$\begin{aligned} m &= I - 1 , \quad IF \ I < 14 , \\ m &= I - 13 , \quad IF \ I \geq 14 . \end{aligned} \quad (A22)$$

A.3.9. Calculate the year, y ,

$$\begin{aligned} y &= D - 4716, \quad \text{IF } m > 2, \\ y &= D - 4715, \quad \text{IF } m \leq 2. \end{aligned} \quad (\text{A23})$$

Note that if local time is used to calculate the JD , then the local time zone is added to the JD in step A.3.1 to calculate the local Calendar Date.

A.4. Tables

Table A4.1. Examples for Testing any Program to Calculate the Julian Day

Date	UT	JD	Date	UT	JD
January 1, 2000	12:00:00	2451545.0	December 31, 1600	00:00:00	2305812.5
January 1, 1999	00:00:00	2451179.5	April 10, 837	07:12:00	2026871.8
January 27, 1987	00:00:00	2446822.5	December 31, -123	00:00:00	1676496.5
June 19, 1987	12:00:00	2446966.0	January 1, -122	00:00:00	1676497.5
January 27, 1988	00:00:00	2447187.5	July 12, -1000	12:00:00	1356001.0
June 19, 1988	12:00:00	2447332.0	February 29, -1000	00:00:00	1355866.5
January 1, 1900	00:00:00	2415020.5	August 17, -1001	21:36:00	1355671.4
January 1, 1600	00:00:00	2305447.5	January 1, -4712	12:00:00	0.0

Table A4.2. Earth Periodic Terms

Term	Row Number	A	B	C
$L0$	0	175347046	0	0
	1	3341656	4.6692568	6283.07585
	2	34894	4.6261	12566.1517
	3	3497	2.7441	5753.3849
	4	3418	2.8289	3.5231
	5	3136	3.6277	77713.7715
	6	2676	4.4181	7860.4194
	7	2343	6.1352	3930.2097
	8	1324	0.7425	11506.7698
	9	1273	2.0371	529.691
	10	1199	1.1096	1577.3435

	11	990	5.233	5884.927
	12	902	2.045	26.298
	13	857	3.508	398.149
	14	780	1.179	5223.694
	15	753	2.533	5507.553
	16	505	4.583	18849.228
	17	492	4.205	775.523
	18	357	2.92	0.067
	19	317	5.849	11790.629
	20	284	1.899	796.298
	21	271	0.315	10977.079
	22	243	0.345	5486.778
	23	206	4.806	2544.314
	24	205	1.869	5573.143
	25	202	2.458	6069.777
	26	156	0.833	213.299
	27	132	3.411	2942.463
	28	126	1.083	20.775
	29	115	0.645	0.98
	30	103	0.636	4694.003
	31	102	0.976	15720.839
	32	102	4.267	7.114
	33	99	6.21	2146.17
	34	98	0.68	155.42
	35	86	5.98	161000.69
	36	85	1.3	6275.96
	37	85	3.67	71430.7
	38	80	1.81	17260.15
	39	79	3.04	12036.46
	40	75	1.76	5088.63
	41	74	3.5	3154.69
	42	74	4.68	801.82
	43	70	0.83	9437.76
	44	62	3.98	8827.39

	45	61	1.82	7084.9
	46	57	2.78	6286.6
	47	56	4.39	14143.5
	48	56	3.47	6279.55
	49	52	0.19	12139.55
	50	52	1.33	1748.02
	51	51	0.28	5856.48
	52	49	0.49	1194.45
	53	41	5.37	8429.24
	54	41	2.4	19651.05
	55	39	6.17	10447.39
	56	37	6.04	10213.29
	57	37	2.57	1059.38
	58	36	1.71	2352.87
	59	36	1.78	6812.77
	60	33	0.59	17789.85
	61	30	0.44	83996.85
	62	30	2.74	1349.87
	63	25	3.16	4690.48
<i>LI</i>	0	628331966747	0	0
	1	206059	2.678235	6283.07585
	2	4303	2.6351	12566.1517
	3	425	1.59	3.523
	4	119	5.796	26.298
	5	109	2.966	1577.344
	6	93	2.59	18849.23
	7	72	1.14	529.69
	8	68	1.87	398.15
	9	67	4.41	5507.55
	10	59	2.89	5223.69
	11	56	2.17	155.42
	12	45	0.4	796.3
	13	36	0.47	775.52
	14	29	2.65	7.11

	15	21	5.34	0.98
	16	19	1.85	5486.78
	17	19	4.97	213.3
	18	17	2.99	6275.96
	19	16	0.03	2544.31
	20	16	1.43	2146.17
	21	15	1.21	10977.08
	22	12	2.83	1748.02
	23	12	3.26	5088.63
	24	12	5.27	1194.45
	25	12	2.08	4694
	26	11	0.77	553.57
	27	10	1.3	6286.6
	28	10	4.24	1349.87
	29	9	2.7	242.73
	30	9	5.64	951.72
	31	8	5.3	2352.87
	32	6	2.65	9437.76
	33	6	4.67	4690.48
L2	0	52919	0	0
	1	8720	1.0721	6283.0758
	2	309	0.867	12566.152
	3	27	0.05	3.52
	4	16	5.19	26.3
	5	16	3.68	155.42
	6	10	0.76	18849.23
	7	9	2.06	77713.77
	8	7	0.83	775.52
	9	5	4.66	1577.34
	10	4	1.03	7.11
	11	4	3.44	5573.14
	12	3	5.14	796.3
	13	3	6.05	5507.55
	14	3	1.19	242.73

	15	3	6.12	529.69
	16	3	0.31	398.15
	17	3	2.28	553.57
	18	2	4.38	5223.69
	19	2	3.75	0.98
L3	0	289	5.844	6283.076
	1	35	0	0
	2	17	5.49	12566.15
	3	3	5.2	155.42
	4	1	4.72	3.52
	5	1	5.3	18849.23
	6	1	5.97	242.73
L4	0	114	3.142	0
	1	8	4.13	6283.08
	2	1	3.84	12566.15
L5	0	1	3.14	0
B0	0	280	3.199	84334.662
	1	102	5.422	5507.553
	2	80	3.88	5223.69
	3	44	3.7	2352.87
	4	32	4	1577.34
B1	0	9	3.9	5507.55
	1	6	1.73	5223.69
R0	0	100013989	0	0
	1	1670700	3.0984635	6283.07585
	2	13956	3.05525	12566.1517
	3	3084	5.1985	77713.7715
	4	1628	1.1739	5753.3849
	5	1576	2.8469	7860.4194
	6	925	5.453	11506.77
	7	542	4.564	3930.21
	8	472	3.661	5884.927
	9	346	0.964	5507.553
	10	329	5.9	5223.694

	11	307	0.299	5573.143
	12	243	4.273	11790.629
	13	212	5.847	1577.344
	14	186	5.022	10977.079
	15	175	3.012	18849.228
	16	110	5.055	5486.778
	17	98	0.89	6069.78
	18	86	5.69	15720.84
	19	86	1.27	161000.69
	20	65	0.27	17260.15
	21	63	0.92	529.69
	22	57	2.01	83996.85
	23	56	5.24	71430.7
	24	49	3.25	2544.31
	25	47	2.58	775.52
	26	45	5.54	9437.76
	27	43	6.01	6275.96
	28	39	5.36	4694
	29	38	2.39	8827.39
	30	37	0.83	19651.05
	31	37	4.9	12139.55
	32	36	1.67	12036.46
	33	35	1.84	2942.46
	34	33	0.24	7084.9
	35	32	0.18	5088.63
	36	32	1.78	398.15
	37	28	1.21	6286.6
	38	28	1.9	6279.55
	39	26	4.59	10447.39
<i>R1</i>	0	103019	1.10749	6283.07585
	1	1721	1.0644	12566.1517
	2	702	3.142	0
	3	32	1.02	18849.23
	4	31	2.84	5507.55

	5	25	1.32	5223.69
	6	18	1.42	1577.34
	7	10	5.91	10977.08
	8	9	1.42	6275.96
	9	9	0.27	5486.78
R2	0	4359	5.7846	6283.0758
	1	124	5.579	12566.152
	2	12	3.14	0
	3	9	3.63	77713.77
	4	6	1.87	5573.14
	5	3	5.47	18849.23
R3	0	145	4.273	6283.076
	1	7	3.92	12566.15
R4	0	4	2.56	6283.08

Table A4.3. Periodic Terms for the Nutation in Longitude and Obliquity

Coefficients for Sin terms					Coefficients for $\Delta\psi$		Coefficients for Δe	
Y0	Y1	Y2	Y3	Y4	a	b	c	d
0	0	0	0	1	-171996	-174.2	92025	8.9
-2	0	0	2	2	-13187	-1.6	5736	-3.1
0	0	0	2	2	-2274	-0.2	977	-0.5
0	0	0	0	2	2062	0.2	-895	0.5
0	1	0	0	0	1426	-3.4	54	-0.1
0	0	1	0	0	712	0.1	-7	
-2	1	0	2	2	-517	1.2	224	-0.6
0	0	0	2	1	-386	-0.4	200	
0	0	1	2	2	-301		129	-0.1
-2	-1	0	2	2	217	-0.5	-95	0.3
-2	0	1	0	0	-158			
-2	0	0	2	1	129	0.1	-70	
0	0	-1	2	2	123		-53	
2	0	0	0	0	63			
0	0	1	0	1	63	0.1	-33	
2	0	-1	2	2	-59		26	

0	0	-1	0	1	-58	-0.1	32	
0	0	1	2	1	-51		27	
-2	0	2	0	0	48			
0	0	-2	2	1	46		-24	
2	0	0	2	2	-38		16	
0	0	2	2	2	-31		13	
0	0	2	0	0	29			
-2	0	1	2	2	29		-12	
0	0	0	2	0	26			
-2	0	0	2	0	-22			
0	0	-1	2	1	21		-10	
0	2	0	0	0	17	-0.1		
2	0	-1	0	1	16		-8	
-2	2	0	2	2	-16	0.1	7	
0	1	0	0	1	-15		9	
-2	0	1	0	1	-13		7	
0	-1	0	0	1	-12		6	
0	0	2	-2	0	11			
2	0	-1	2	1	-10		5	
2	0	1	2	2	-8		3	
0	1	0	2	2	7		-3	
-2	1	1	0	0	-7			
0	-1	0	2	2	-7		3	
2	0	0	2	1	-7		3	
2	0	1	0	0	6			
-2	0	2	2	2	6		-3	
-2	0	1	2	1	6		-3	
2	0	-2	0	1	-6		3	
2	0	0	0	1	-6		3	
0	-1	1	0	0	5			
-2	-1	0	2	1	-5		3	
-2	0	0	0	1	-5		3	
0	0	2	2	1	-5		3	
-2	0	2	0	1	4			

-2	1	0	2	1	4			
0	0	1	-2	0	4			
-1	0	1	0	0	-4			
-2	1	0	0	0	-4			
1	0	0	0	0	-4			
0	0	1	2	0	3			
0	0	-2	2	2	-3			
-1	-1	1	0	0	-3			
0	1	1	0	0	-3			
0	-1	1	2	2	-3			
2	-1	-1	2	2	-3			
0	0	3	2	2	-3			
2	-1	0	2	2	-3			

A.5. Example

The results for the following site parameters are listed in Table A5.1:

- Date = October 17, 2003.
- Time = 12:30:30 Local Standard Time (LST).
- Time zone(TZ) = -7 hours.
- Longitude = -105.1786°.
- Latitude = 39.742476°.
- Pressure = 820 mbar.
- Elevation = 1830.14 m.
- Temperature = 11°C.
- Surface slope = 30°.
- Surface azimuth rotation = -10°.
- ΔT = 67 Seconds.

LST must be changed to UT by subtracting TZ from LST, and changing the date if necessary.

Table A5.1. Results for Example

<i>JD</i>	2452930.312847		
<i>L0</i>	172067561.526586	<i>L1</i>	628332010650.051147
<i>L2</i>	61368.682493	<i>L3</i>	-26.902819
<i>L4</i>	-121.279536	<i>L5</i>	-0.999999
<i>L</i>	24.0182616917°		
<i>B0</i>	-176.502688	<i>B1</i>	3.067582
<i>B</i>	-0.0001011219°		
<i>R0</i>	99653849.037796	<i>R1</i>	100378.567146

$R2$	-1140.953507	$R3$	-141.115419
$R4$	1.232361		
R	0.9965422974 AU		
Θ	204.0182616917°	β	0.0001011219°
$\Delta\psi$	-0.00399840°	$\Delta\epsilon$	0.00166657°
ϵ	23.440465°	λ	204.0085519281°
α	202.22741°	δ	-9.31434°
H	11.105900°	H'	11.10629°
α'	202.22704°	δ'	-9.316179°
θ	50.11162°	ϕ	194.34024°
I	25.18700°	M	205.8971722516°
E	14.641503 minutes	$Transit$	18:46:04.97 UT
$Sunrise$	13:12:43.46 UT	$Sunset$	00:20:19.19 UT

A.6. C source code for SPA

NREL has developed a C source code for the Solar Position Algorithm. It is available for download at:

<http://www.nrel.gov/midc/spa/>

NREL also has other related solar models and tools that might be of interest:

http://www.nrel.gov/redc/models_tools.html

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