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# Homework 3 Assignment Submission

## Exercise 1.

Consider the following Euler representation of rotation:

$$R(\alpha, \beta, \gamma) = R_z(\gamma)R_y(\beta)R_z(\alpha).$$

(a) Determine matrix  $R(\alpha, \beta, \gamma)$ .

(b) Show that  $R(\alpha, \beta, \gamma) = R(\alpha - \pi, -\beta, \gamma - \pi)$ .

(c) Given a rotation matrix  $R'$ , determine  $\alpha$ ,  $\beta$ , and  $\gamma$  in terms of elements of  $R'$ . (Hint: denote the element of  $R'$  in the  $i$ th row and  $j$ th column by  $R'_{ij}$ , and write your solutions in terms of these elements.)

## Matrix $R(\alpha, \beta, \gamma)$ :

To find the rotation matrix  $R(\alpha, \beta, \gamma)$ , we have to find the rotation matrices for each individual rotation and then multiply them together.

$$\text{The first rotation } R_z(\alpha) = \begin{pmatrix} \cos \alpha & -\sin \alpha & 0 \\ \sin \alpha & \cos \alpha & 0 \\ 0 & 0 & 1 \end{pmatrix}$$

$$R_y(\beta) = \begin{pmatrix} \cos \beta & 0 & \sin \beta \\ 0 & 1 & 0 \\ -\sin \beta & 0 & \cos \beta \end{pmatrix}$$

$$R_z(\gamma) = \begin{pmatrix} \cos \gamma & -\sin \gamma & 0 \\ \sin \gamma & \cos \gamma & 0 \\ 0 & 0 & 1 \end{pmatrix}$$

$$R_z(\gamma)R_y(\beta)R_z(\alpha) = \begin{pmatrix} \cos \alpha \cos \beta \cos \gamma - \sin \alpha \sin \gamma & -\cos \alpha \cos \beta \sin \gamma - \sin \alpha \cos \gamma & \cos \alpha \sin \beta \\ \sin \alpha \cos \beta \cos \gamma + \cos \alpha \sin \gamma & -\sin \alpha \cos \beta \sin \gamma + \cos \alpha \cos \gamma & \sin \alpha \sin \beta \\ -\sin \beta \cos \gamma & \sin \beta \sin \gamma & \cos \beta \end{pmatrix}$$

$$= R(\alpha, \beta, \gamma)$$

## **$R(\alpha, \beta, \gamma) = R(\alpha - \pi, -\beta, \gamma - \pi)$ :**

We can show that  $R(\alpha, \beta, \gamma) = R(\alpha - \pi, -\beta, \gamma - \pi)$  by substituting those new values ( $\alpha - \pi, -\beta, \gamma - \pi$ ) into the matrices we already derived and show that they have the same value.

$$R_z(\alpha - \pi) = \begin{pmatrix} \cos(\alpha - \pi) & -\sin(\alpha - \pi) & 0 \\ \sin(\alpha - \pi) & \cos(\alpha - \pi) & 0 \\ 0 & 0 & 1 \end{pmatrix} = \begin{pmatrix} -\cos \alpha & \sin \alpha & 0 \\ -\sin \alpha & -\cos \alpha & 0 \\ 0 & 0 & 1 \end{pmatrix}$$

$$R_y(-\beta) = \begin{pmatrix} \cos(-\beta) & 0 & \sin(-\beta) \\ 0 & 1 & 0 \\ -\sin(-\beta) & 0 & \cos(-\beta) \end{pmatrix} = \begin{pmatrix} \cos \beta & 0 & -\sin \beta \\ 0 & 1 & 0 \\ \sin \beta & 0 & \cos \beta \end{pmatrix}$$

$$R_z(\gamma - \pi) = \begin{pmatrix} \cos(\gamma - \pi) & -\sin(\gamma - \pi) & 0 \\ \sin(\gamma - \pi) & \cos(\gamma - \pi) & 0 \\ 0 & 0 & 1 \end{pmatrix} = \begin{pmatrix} -\cos \gamma & \sin \gamma & 0 \\ -\sin \gamma & -\cos \gamma & 0 \\ 0 & 0 & 1 \end{pmatrix}$$

$$R(\alpha - \pi, -\beta, \gamma - \pi) = \begin{pmatrix} \cos \alpha \cos \beta \cos \gamma - \sin \alpha \sin \gamma & -\cos \alpha \cos \beta \sin \gamma - \sin \alpha \cos \gamma & \cos \alpha \sin \beta \\ \sin \alpha \cos \beta \cos \gamma + \cos \alpha \sin \gamma & -\sin \alpha \cos \beta \sin \gamma + \cos \alpha \cos \gamma & \sin \alpha \sin \beta \\ -\sin \beta \cos \gamma & \sin \beta \sin \gamma & \cos \beta \end{pmatrix}$$

$$= R(\alpha, \beta, \gamma)$$

## **Given Rotation Matrix $R'$ Determine $\alpha, \beta, \gamma$ in Terms of $R'$ :**

Let the elements of  $R'$  be denoted as:

$$R' = \begin{pmatrix} R'_{11} & R'_{12} & R'_{13} \\ R'_{21} & R'_{22} & R'_{23} \\ R'_{31} & R'_{32} & R'_{33} \end{pmatrix}$$

From the structure of  $R(\alpha, \beta, \gamma)$ , we can extract:

- $\beta$  can be determined from the third row, third column element:

$$\cos \beta = R'_{33} \Rightarrow \beta = \arccos(R'_{33})$$

- $\alpha$  can be determined from the first and second rows of the third column:

$$\sin \alpha = R'_{23} / \sin \beta, \quad \cos \alpha = R'_{13} / \sin \beta$$

Thus:

$$\alpha = \arctan2(R'_{23} / \sin \beta, R'_{13} / \sin \beta)$$

- $\gamma$  can be determined from the first and second rows of the first column:

$$\sin \gamma = R'_{21} / \sin \beta, \quad \cos \gamma = R'_{11} / \sin \beta$$

Thus:

$$\gamma = \arctan2(R'_{21} / \sin \beta, R'_{11} / \sin \beta)$$

## Exercise 2.

Consider the 3-link manipulator in Figure 1. The links  $A_1$ ,  $A_2$ , and  $A_3$  are identical.

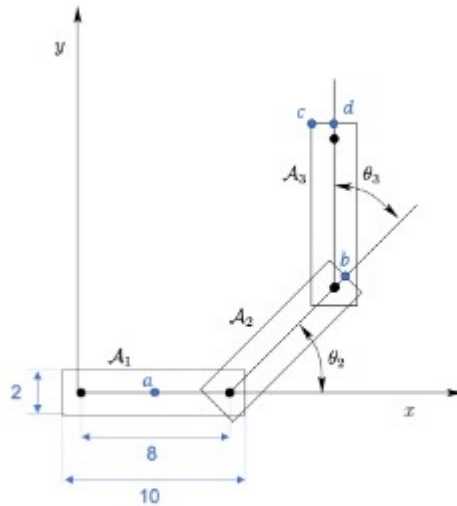


Figure 1: 3-link manipulator.

- For the configuration  $(\theta_1, \theta_2, \theta_3) = (\pi/4, \pi/2, -\pi/6)$ , determine the locations of points a, b, and c.
- Find the configuration(s) of the robot when point d is at (0, 4).

### Locations For Points a, b, c at $(\theta_1, \theta_2, \theta_3) = (\pi/4, \pi/2, -\pi/6)$ :

The manipulator's configuration involves calculating the positions of points a, b, and c based on the joint angles and link lengths.

**Point a:** is located halfway up the first link and rotated up by  $\pi/4$  so is located at the point  $(4\cos(\pi/4), 4\sin(\pi/4))$ .

**Point b:** Point b is 9 units away from point a along the second link, and the second link is rotated by another  $2\pi$  relative to point a. The total rotation at point b is the sum of the rotations from the base and the second joint: Total rotation at b =  $\pi/4 + \pi/2 = 3\pi/4$ .

The change in coordinates from a to b is given by:

$$\Delta x = 9\cos(3\pi/4)$$

$$\Delta y = 9\sin(3\pi/4)$$

$$\text{Since } \cos(3\pi/4) = \frac{-\sqrt{2}}{2} \text{ and } \sin(3\pi/4) = \frac{\sqrt{2}}{2}$$

$$\Delta x = 9 \times \frac{-\sqrt{2}}{2} \approx 9 \times -0.707 \approx -6.363$$

$$\Delta y = 9 \times \frac{\sqrt{2}}{2} \approx 9 \times 0.707 \approx 6.363$$

Adding these changes to the coordinates of point a (which are (2.828, 2.828)):

$$b_x = 2.828 - 6.363 \approx -3.535 \quad b_y = 2.828 + 6.363 \approx 9.191$$

Therefore, the coordinates of point b are approximately:

$$b = (-3.535, 9.191)$$

This places point b 9 units away from point a, rotated by a total of  $3\pi/4$ .

### Point c:

Position the end of the third link relative to point b:

We already calculated the position of point b as  $(-3.535, 9.191)$ .

The third link is 9 units long, and it connects 1 unit back from point b in the direction of the previous rotation, which is at  $3\pi/4$ .

So, we first move 1 unit back from point b along this direction.

The change in position for this movement is:

$$\Delta x = 1 \cos(3\pi/4) = 1 \times \frac{-\sqrt{2}}{2} \approx -0.707 \quad \Delta y = 1 \sin(3\pi/4) = 1 \times \frac{\sqrt{2}}{2} \approx 0.707$$

So, the coordinates of the point where the third link starts, call it b', are:

$$b'_x = b_x + (-0.707) = -3.535 - 0.707 = -4.242 \quad b'_y = b_y + 0.707 = 9.191 + 0.707 = 9.898$$

So,  $b' \approx (-4.242, 9.898)$ .

Find the end of the third link (before accounting for the side shift):

From b', the third link extends 9 units in the direction of the **current rotation**. Since the second link rotated by  $\pi/2$ , the new rotation for the third link =  $3\pi/4 - \pi/6 = 5\pi/12$

The change in position for the end of the third link (let's call it c') is:

$$\Delta x = 9 \cos(5\pi/12) \quad \Delta y = 9 \sin(5\pi/12)$$

Numerically:

$$\cos(5\pi/12) \approx 0.2588 \quad \sin(5\pi/12) \approx 0.9659$$

Therefore, the change in coordinates is:

$$\Delta x = 9 \times 0.2588 \approx 2.33 \quad \Delta y = 9 \times 0.9659 \approx 8.693$$

Adding these to the coordinates of b':

$$c_x' = b_x' + 2.33 = -4.242 + 2.33 = -1.912 \quad c_y' = b_y' + 8.693 = 9.898 + 8.693 = 18.591$$

So, the coordinates of  $c' \approx (-1.912, 18.591)$ .

### Shift point c by 1 unit counterclockwise:

Now, we need to apply the final shift: point c is 1 unit **counterclockwise** from the end of the third link. A counterclockwise shift by 90 degrees from  $-\pi/6$  (the rotation at  $c'$ ) brings the direction to  $\pi/3$ .

The change in position due to this shift is:

$$\Delta x = 1 \cos(\pi/3) = 1 \times \frac{1}{2} = 0.5 \quad \Delta y = 1 \sin(\pi/3) = 1 \times \frac{\sqrt{3}}{2} \approx 0.866$$

So, the final coordinates of point c are:

$$c_x = c_x' + 0.5 = -1.912 + 0.5 = -1.412 \quad c_y = c_y' + 0.866 = 18.591 + 0.866 = 19.457$$

Therefore, the corrected coordinates of point c are approximately:

$$c = (-1.412, 19.457)$$

## Configurations When d is at (0,4):

**Set up the kinematic equations:** The end position of the manipulator's point d is determined by the joint angles and the lengths of the links.

The forward kinematics in terms of  $\theta_1$ ,  $\theta_2$ , and  $\theta_3$  for the position of point d can be written as:

$$x_d = 8\cos(\theta_1) + 8\cos(\theta_1 + \theta_2) + 9\cos(\theta_1 + \theta_2 + \theta_3) \quad y_d = 8\sin(\theta_1) + 8\sin(\theta_1 + \theta_2) + 9\sin(\theta_1 + \theta_2 + \theta_3)$$

Since point d is at (0,4), we have:

$$0 = 8\cos(\theta_1) + 8\cos(\theta_1 + \theta_2) + 9\cos(\theta_1 + \theta_2 + \theta_3) \quad 4 = 8\sin(\theta_1) + 8\sin(\theta_1 + \theta_2) + 9\sin(\theta_1 + \theta_2 + \theta_3)$$

**Solve for  $\theta_1$ :** The fact that  $x_d = 0$  suggests that the manipulator must align symmetrically about the y-axis. A natural assumption here is that  $\theta_1 = 2\pi$ , which would align the first link vertically along the y-axis.

Substituting  $\theta_1 = 2\pi$  simplifies the equations:

$$0 = 8\cos(2\pi) + 8\cos(2\pi + \theta_2) + 9\cos(2\pi + \theta_2 + \theta_3) \quad 4 = 8\sin(2\pi) + 8\sin(2\pi + \theta_2) + 9\sin(2\pi + \theta_2 + \theta_3)$$

These simplify further to:

$$0 = -8\sin(\theta_2) - 9\sin(\theta_2 + \theta_3) \quad 4 = 8 + 8\cos(\theta_2) + 9\cos(\theta_2 + \theta_3)$$

**Solve for  $\theta_2$  and  $\theta_3$ :** From the first equation:

$$\sin(\theta_2) + 9/8\sin(\theta_2 + \theta_3) = 0$$

This implies:

$$\sin(\theta_2 + \theta_3) = -8/9\sin(\theta_2)$$

Now, use the second equation:

$$4 = 8 + 8\cos(\theta_2) + 9\cos(\theta_2 + \theta_3)$$

Rearrange this to:

$$-4 = 8\cos(\theta_2) + 9\cos(\theta_2 + \theta_3)$$

Solving these two equations simultaneously you get:

$$\theta_2 \approx 1.586 \text{ radians}$$

$$\theta_3 \approx -2.681 \text{ radians}$$

### Exercise 3.

Express the configuration spaces of the following systems in terms of a Cartesian product of simpler spaces (such as  $\mathbb{R}^n$ ,  $S^n$ , etc.) and determine their dimensions. Justify your answer.

- (a) Two trains on two train tracks.
- (b) A spacecraft that can translate and rotate in 2D.
- (c) Two mobile robots rotating and translating in the plane.
- (d) Two translating and rotating planar mobile robots connected rigidly by a bar.
- (e) A cylindrical rod that can translate and rotate in 3D. (Hint: if the rod is rotated about its central axis, it is assumed that the rod's position and orientation are not changed in any detectable way.)
- (f) A spacecraft that can translate and rotate in 3D and is equipped with a 3-link robot arm (revolute joints only).
- (g) The manipulator in Figure 2.

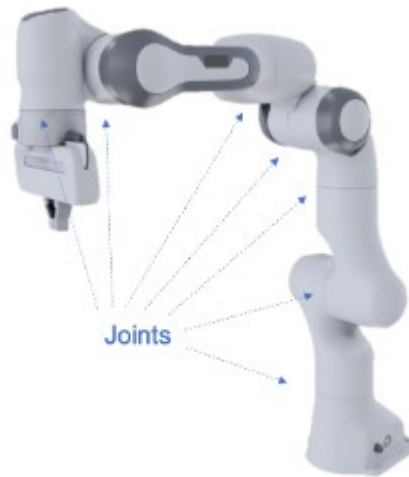


Figure 2: Robotic manipulator with revolute joints

#### (a) Two trains on two train tracks

Each train can be described by its position along a track and its orientation (direction). Assuming the tracks are straight and infinite:

- Each train's position can be represented by  $R$  (a real line).
- Orientation can be represented by  $S1$  (a circle, since it can face any direction).

Thus, the configuration space for one train is  $R \times S1$ . For two trains:

$$C = (R \times S1) \times (R \times S1) = R^2 \times (S1)^2.$$

**Dimension:**  $2+2=4$ .

### **(b) A spacecraft that can translate and rotate in 2D**

The spacecraft can translate in 2D space and can rotate about a point:

- Translational degrees of freedom:  $R2$ .
- Rotational degree of freedom:  $S1$ .

The configuration space is:

$$C = R^2 \times S1.$$

**Dimension:**  $2+1=3$ .

### **(c) Two mobile robots rotating and translating in the plane**

Each robot can translate in 2D and rotate:

- For one robot:  $R^2 \times S1$ .
- For two robots:

$$C = (R^2 \times S1) \times (R^2 \times S1) = R^4 \times (S1)^2.$$

**Dimension:**  $4+2=6$ .

### **(d) Two translating and rotating planar mobile robots connected rigidly by a bar**

The two robots have the same translational and rotational coordinates. However, since they are connected by a rigid bar, they can't move independently:

- One robot's position and orientation:  $R^2 \times S1$ .

The configuration space can be described by the position of one robot and the angle between the bar and the reference direction:

- Position:  $R2$ .
- Angle:  $S1$ .

Thus:

$$C = R^2 \times S1.$$

**Dimension:**  $2+1=3$ .

### **(e) A cylindrical rod that can translate and rotate in 3D**

The rod can translate in 3D and can rotate about its central axis:

- Translational degrees of freedom:  $R^3$ .
- Rotational degree of freedom (around the central axis, which can be represented as a circle):  $S^1$ .

The configuration space is:

$$C = R^3 \times S^1.$$

**Dimension:**  $3+1=4$ .

### **(f) A spacecraft that can translate and rotate in 3D and is equipped with a 3-link robot arm (revolute joints only)**

The spacecraft can translate and rotate in 3D:

- Translational degrees of freedom:  $R^3$ .
- Rotational degrees of freedom:  $S^3$  (for full orientation in 3D).

The 3-link robot arm has 3 revolute joints:

- Each joint adds one rotational degree of freedom:  $S^1$  for each joint.

Thus, the configuration space for the arm is  $(S^1)^3$ .

Combining these:

$$C = R^3 \times S^3 \times (S^1)^3.$$

**Dimension:**  $3+3+3=9$ .

### **Configuration Space for a 7-Joint Revolute Manipulator Arm**

Each revolute joint contributes one rotational degree of freedom, represented as  $S^1$ . Therefore, for 7 revolute joints, the configuration space can be expressed as:

$$C = (S^1)^7.$$

#### **Dimension**

The dimension of this configuration space is simply the number of joints, which is:

**Dimension:** 7.

## **Exercise 4.**

Consider workspace  $W \subseteq \mathbb{R}^n$  with convex obstacles. Show that the C-space obstacles are also convex for a convex robot with translational motion in  $W$ .



**Select Two Configurations:** Let  $q_1$  and  $q_2$  be two configurations in the C-space such that both configurations lead to the robot intersecting the obstacle  $O$ . Each configuration  $q_i$  consists of a position in the workspace and a configuration of the robot.

**Translate the Robot:** The C-space obstacle corresponding to  $O$  can be defined as:

$$O_C = \{q \in C \mid R(q) \cap O \neq \emptyset\}$$

where  $R(q)$  is the position and orientation of the robot based on the configuration  $q$ .

**Consider a Line Segment:** For  $\lambda \in [0,1]$ , define a point on the line segment connecting  $q_1$  and  $q_2$  as:

$$q_\lambda = (1-\lambda)q_1 + \lambda q_2.$$

**Check Intersections:** To show  $O_C$  is convex, we need to show that  $R(q_\lambda) \cap O \neq \emptyset$ :

Since  $O$  is convex, for any points  $x_1$  and  $x_2$  in  $O$ , the line segment connecting them lies entirely within  $O$ .

If both configurations  $q_1$  and  $q_2$  lead to intersections with  $O$ , then the positions  $R(q_1)$  and  $R(q_2)$  must both intersect the obstacle.

Therefore, for any point along the line segment connecting the configurations, the robot can be placed in a way that it still intersects the obstacle.

**Conclusion:** Since any linear combination of configurations  $q_\lambda$  results in the robot intersecting the convex obstacle  $O$ , it follows that the C-space obstacle  $O_C$  is also convex.