

## B.1 U.S. Navy A-4D Attack Aircraft

The data given in Tables B.1a–B.1d are for the normal cruise configuration, clean airplane, where  $W = 17,578$  lb, mass  $m = 546$  slugs,  $S = 260$  ft<sup>2</sup>,  $b = 27.5$  ft,  $\bar{c} = 10.8$  ft, and the c.g. is at  $0.25\bar{c}$ . Figure B.1 is a sketch of the aircraft.

Note that the absence of derivatives implies negligible values. The stability derivatives are relative to the stability axes. All angles are in radian measure.

Table B.1a Geometric data

Condition	1	2	3	4	5	6
$h$ , ft	0(S/L)	15,000	15,000	15,000	35,000	35,000
$M$	0.4	0.4	0.6	0.9	0.6	0.9
$V$ , ft/s	447	423	634	952	584	876
$Q$ , lb/ft <sup>2</sup>	237	134	301	677	126	283
$I_x$ , slug-ft <sup>2</sup>	8,020	8,200	8,010	8,060	8,190	8,010
$I_y$ , slug-ft <sup>2</sup>	25,900	25,900	25,900	25,900	25,900	25,900
$I_z$ , slug-ft <sup>2</sup>	29,270	29,090	29,280	29,230	29,100	29,280
$I_{xz}$ , slug-ft <sup>2</sup>	−441	−1,989	41	1,042	−1,952	227
$\alpha_{\text{trim}}$ , deg	4.7	8.9	3.4	0.7	8.8	2.9

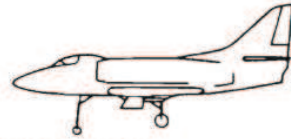
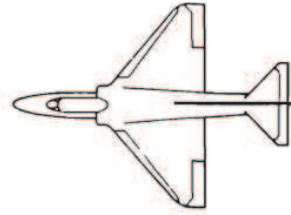


Fig. B.1 Sketch of A-4D aircraft.

Table B.1c Lateral-directional dimensional derivatives condition

Condition	1	2	3	4	5	6
$h$ , ft	0(S/L)	15,000	15,000	15,000	35,000	35,000
$M$	0.4	0.4	0.6	0.9	0.6	0.9
$Y_{\beta}$ , ft/s <sup>2</sup>	−110.94	−62.42	−144.6	−345.2	−60.38	−139.8
$L_{\beta}$ , s <sup>−2</sup>	−27.67	−14.01	−35.00	−87.19	−14.24	−40.32
$L_p$ , s <sup>−1</sup>	−1.732	−0.988	−1.516	−2.492	−0.671	−1.134
$L_r$ , s <sup>−1</sup>	0.933	0.607	0.874	1.346	0.464	0.672
$N_{\beta}$ , s <sup>−2</sup>	15.16	8.223	18.78	46.43	7.864	19.65
$N_p$ , s <sup>−1</sup>	0.040	0.000	0.040	0.125	−0.004	0.041
$N_r$ , s <sup>−1</sup>	−0.639	−0.401	−0.566	−0.958	−0.291	−0.428
$Y_{\delta_r}$ , ft/s <sup>2</sup>	19.65	10.83	25.09	52.24	10.46	21.78
$L_{\delta_r}$ , s <sup>−2</sup>	7.305	2.802	9.961	24.05	2.739	8.568
$N_{\delta_r}$ , s <sup>−2</sup>	−6.732	−3.651	−8.397	−17.41	−3.517	−7.241
$Y_{\delta_a}$ , ft/s <sup>2</sup>	−2.599	−0.795	−2.409	−5.291	−0.478	−2.420
$L_{\delta_a}$ , s <sup>−2</sup>	17.27	8.757	21.27	37.48	7.998	16.88
$N_{\delta_a}$ , s <sup>−2</sup>	0.334	−0.246	0.479	1.462	−0.139	0.414
$L'_{\beta}$ , s <sup>−2</sup>	−28.53	−16.27	−34.90	−81.56	−16.38	−39.77
$L'_p$ , s <sup>−1</sup>	−1.736	−1.004	−1.516	−2.488	−0.681	−1.134
$L'_r$ , s <sup>−1</sup>	0.968	0.717	0.872	1.227	0.542	0.660
$N'_{\beta}$ , s <sup>−2</sup>	15.59	9.336	18.73	43.53	8.963	19.35
$N'_p$ , s <sup>−1</sup>	0.066	0.069	0.038	0.036	0.042	0.032
$N'_r$ , s <sup>−1</sup>	−0.653	−0.450	−0.565	−0.914	−0.327	−0.423
$L'_{\delta_r}$ , s <sup>−2</sup>	7.682	3.750	9.918	21.90	3.635	8.365
$N'_{\delta_r}$ , s <sup>−2</sup>	−6.848	−3.907	−8.383	−16.63	−3.760	−7.176
$L'_{\delta_a}$ , s <sup>−2</sup>	17.26	8.965	21.27	37.84	8.162	16.90
$N'_{\delta_a}$ , s <sup>−2</sup>	0.073	−0.859	0.508	2.811	−0.686	0.545