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1 Input Parameters

Module			Column-to-C	olumn End Plate Connection
Main Module			M	oment Connection
Bending Moment (kNm) *				43.0
Shear Force	e (kN) *			43.0
Axial Ford	ce (kN)			43.0
	Column Section	- Mechanical	Properties	
	Beam Sect	ion *		HB 450*
	Materia	1 *		E 165 (Fe 290)
т ү	Ultimate Strengtl	h, F_u (MPa)		290
	Yield Strength,	F_y (MPa)		165
$(B-t)$ α	Mass, m (kg/m)	92.19	$I_z \text{ (cm}^4)$	40100.0
4 t	Area, $A \text{ (cm}^2)$	117.0	$I_y(\mathrm{cm}^4)$	2990.0
ZZ D	D (mm)	450.0	r_z (cm)	18.4
B B	B (mm)	250.0	r_y (cm)	5.04
R ₁	t (mm)	11.3	$Z_z \text{ (cm}^3\text{)}$	1780.0
В	T (mm)	13.7	$Z_y \text{ (cm}^3)$	239.0
Y	Flange Slope	94	Z_{pz} (cm ³)	2020.0
	$R_1 \text{ (mm)}$	15.0	$Z_{py} \ (\mathrm{cm}^3)$	398.0
	$R_2 \text{ (mm)}$	7.5		
	Bolt Details - Inp	out and Desig	n Preference	
Diameter	(mm) *		[8, 10, 12, 14, 16, 18, 20, 22, 24, 27, 30, 33, 36, 39,	
Diameter	(111111)		42, 45, 48, 52, 56, 60, 64]	
Property	Class *		[3.6,4.6,4.8,5.6,5.8,6.8,8.8,9.8,10.9,12.9]	
Туре	*		Bearing Bolt	
Bolt Te	nsion		N	Non pre-tensioned
Hole T	ype			Standard
Slip Facto	$r, (\mu_f)$			0.3
	Detailing -	Design Prefe	erence	
Edge Preparat	ion Method		Shear	red or hand flame cut
Are the Members Exposed	to Corrosive Influence	es?		False

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2 Design Checks

Design Status	Pass
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2.1 Member Capacity

Check	Required	Provided	Remarks
Section Classification		Plastic	
Section Classification		[Ref: Table 2, Cl.3.7.2 and 3.7.4, IS 800:2007]	
Axial Capacity Member (kN)	43	$T_{\text{dg}} = \frac{A_g f_y}{\gamma_{m0}}$ $= \frac{11700.0 \times 165}{1.1 \times 10^3}$ $= 1755.0$	Pass
Shear Capacity Member (kN)	43	[Ref. IS 800:2007, Cl.6.2] $V_{d_y} = \frac{A_v f_y}{\sqrt{3}\gamma_{m0}}$ $= \frac{422.6 \times 11.3 \times 165}{\sqrt{3} \times 1.1 \times 1000}$ $= 413.56$	Pass
Plastic Moment Capacity (kNm)		[Ref. IS 800:2007, Cl.10.4.3] $M_{dz} = \frac{\beta_b Z_p f y}{\gamma_{m0}}$ $= \frac{1 \times 2020000.0 \times 165}{1.1 \times 10^6}$ $= 303.0$ [Ref. IS 800:2007, Cl.8.2.1.2]	
Moment Deformation Criteria (kNm)		$M_{dc} = \frac{1.5Z_e fy}{\gamma_{m0} \times 10^6}$ $= \frac{1.5 \times 1780000.0 \times 165}{1.1 \times 10^6}$ $= 400.5$ [Ref. IS 800:2007, Cl.8.2.1.2]	

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Check	Required	Provided	Remarks
		$M_{d_{\mathbf{Z}}} = \min(M_{d_{\mathbf{Z}}}, \ M_{d_{c}})$	
		$= \min(303.0, 400.5)$	
Moment Capacity Member	43	= 303.0	Pass
(kNm)			
		[Ref. IS 800:2007, Cl.8.2]	

2.2 Load Consideration

Check	Required	Provided	Remarks
		I.R. axial $= P_{\rm x}/T_{\rm dg}$	
		=43.0/1755.0	
		= 0.02	
		I.R. moment = M_z/M_{dz}	
Interaction Ratio		=43.0/303.0	
		= 0.14	
		I.R. sum $=$ I.R. axial $+$ I.R. mon	ient
		= 0.02 + 0.14	
		= 0.17	

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Check	Required	Provided	Remarks
Minimum Required Load	$\begin{aligned} &\text{if I.R. axial} < 0.3 \text{ and I.R. moment} < 0.5 \\ &P_{\text{xmin}} = 0.3T_{\text{dg}} \\ &M_{\text{zmin}} = 0.5M_{dz} \end{aligned}$ $&\text{elif sum I.R.} <= 1.0 \text{ and I.R. moment} < 0.5 \\ &\text{if } (0.5 - \text{I.R. moment}) < (1 - \text{sum I.R.}) \\ &M_{\text{zmin}} = 0.5 \times M_{dz} \\ &\text{else} \\ &M_{\text{zmin}} = M_{\text{z}} + ((1 - \text{sum I.R.}) \times M_{dz}) \\ &P_{\text{xmin}} = P_{\text{x}} \end{aligned}$ $&\text{elif sum I.R.} <= 1.0 \text{ and I.R. axial} < 0.3 \\ &\text{if } (0.3 - \text{I.R. axial}) < (1 - \text{sum I.R.}) \\ &P_{\text{xmin}} = 0.3T_{\text{dg}} \\ &\text{else} \\ &P_{\text{xmin}} = P_{\text{x}} + ((1 - \text{sum I.R.}) \times T_{\text{dg}}) \\ &M_{\text{zmin}} = M_{\text{z}} \end{aligned}$ $&\text{else} \\ &P_{\text{xmin}} = P_{\text{x}} \\ &M_{\text{zmin}} = M_{\text{z}} \end{aligned}$	$M_{ m zmin} = 151.5$ $P_{ m xmin} = 526.5$ [Ref. IS 800:2007, Cl.10.7]	
Applied Axial Force (kN)	43.0	$P_u = \max(P_x, P_{xmin})$ = $\max(43.0, 526.5)$	

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Check	Required	Provided	Remarks
		$V_{y_{\min}} = \min(0.15V_{d_y}, 40.0)$	
		$= \min(0.15 \times 689.27, 40.0)$	
		=40.0	
Applied Shear Force (kN)	43.0	$V_u = \max(V_y, V_{y_{\min}})$	
		$= \max(43.0, 40.0)$	
		= 43.0	
		[Ref. IS 800:2007, Cl.10.7]	
		$M_u = \max(M_z, M_{z\min})$	
		$= \max(43.0, 151.5)$	
Applied Moment (kNm)	43.0	= 151.5	
		[Ref. IS 800:2007, Cl.8.2.1.2]	

2.3 Bolt Check

Check	Required	Provided	Remarks
Diameter (mm)	Bolt Quantity Optimization	d = 27.0	
Property Class	Bolt Grade Optimization	5.6	
Hole Diameter (mm)		$d_0 = 30.0$	
No. of Bolts (along one side of the web) (n)	$n_{bw} = 2 \times \left(\frac{D - (2 \times T_f) - (2 \times e)}{p} + 1\right)$ $= 2 \times \left(\frac{450.0 - (2 \times 13.7) - (2 \times 55)}{67.5} + 1\right)$ $= 10$	10	Pass
No. of Bolts (along one side of the flange overhang) (n)	$n_{bf} = 2 \times \left(\frac{b/2 - (T_w/2) - (2 \times e)}{p} + 1\right)$ $= 2 \times \left(\frac{250.0/2 - (0.5 \times 11.3) - (2 \times 55)}{67.5} + 1\right)$ $= 2$	2	Pass
Total No. of Bolts		10	

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Check	Required	Provided	Remarks
Shear Capacity (kN)		$V_{\text{dsb}} = \frac{f_{ub}n_n A_{nb}}{\sqrt{3}\gamma_{mb}}$ $= \frac{500.0 \times 1 \times 459}{1000 \times \sqrt{3} \times 1.25}$ $= 106.0$ [Ref. IS 800:2007, Cl.10.3.3]	
Bearing Capacity (kN)		$V_{\text{dpb}} = \frac{2.5k_b dt f_u}{\gamma_{mb}}$ $= \frac{2.5 \times 0.53 \times 27.0 \times 56.0 \times 290}{1000 \times 1.25}$ $= 464.79$	
Capacity (kN)	$V_{sb} = \frac{V}{n_{wb}}$ $= \frac{43.0}{10}$ $= 4.3$	[Ref. IS 800:2007, Cl.10.3.4] $V_{db} = \min (V_{dsb}, V_{dpb})$ $= \min (106.0, 464.79)$ $= 106.0$ [Ref. IS 800:2007, Cl.10.3.2]	Pass
Tension due to Moment and Axial Force (kN)	$T_1 = \frac{P}{n} + \frac{M \times y_{max}}{y_{sqr}}$ $= \frac{526.5 \times 10^3}{10} + \frac{151500.0 \times 10^6 \times 374.45}{605154.75}$ $= 146.39$		

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Check	Required	Provided	Remarks
	$Q = \frac{l_v}{2l_e} \left[T_e - \frac{\beta \eta f_o b_e t^4}{27 l_e l_v^2} \right]$ $l_v = e - t_w$ $= 55 - 0 = 55 \text{ mm}$		
	$f_o = 0.7 f_{ub}$ $= 0.7 \times 500.0$ $= 350.0 \text{ N/mm}^2$ $l_e = \min\left(e, 1.1t \sqrt{\frac{\beta f_o}{f_y}}\right)$ $= \min\left(55, 1.1 \times 56.0 \times \sqrt{\frac{2 \times 350.0}{165}}\right)$		
Prying force (kN)	$= \min \left(55, 1.1 \times 50.0 \times \sqrt{\frac{165}{165}} \right)$ $= \min(55, 89.72) = 55 \text{ mm}$ $\beta = 2 \text{ (non pre-tensioned bolt)}$ $\eta = 1.5$		OK
	$b_e = \frac{B}{n_c}$ $= \frac{250.0}{2} = 125.0 \text{ mm}$		
	$Q = \frac{55}{2 \times 55} \times$ $\left[146.39 - \left(\frac{2 \times 1.5 \times 350.0 \times 125.0 \times 56.0^4}{27 \times 55 \times 55^2}\right)\right]$ $Q = 2.72$	× 10 ⁻³]	
	[Ref. IS 800:2007, Cl.10.4.7]		

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Check	Required	Provided	Remarks
		$T_{\rm db} = 0.90 f_{ub} A_n / \gamma_{mb}$	
		$< f_{yb}A_{sb}(\gamma_{mb} / \gamma_{m0})$	
		$= \min \left(0.90 \times 500.0 \times 459 \ / \ 1.25, \right.$	
Tension demand (kN)	$T_b = T_1 + Q$ = 146 + 2.72	$300.0 \times 573 \times (1.25/1.1)$	Pass
	= 149.11	$= \min(165.24, 195.34)$	
		=156.27	
		[Ref. IS 800:2007, Cl.10.3.5]	
	$p_{\min} = 2.5d$		
	$=2.5\times27.0$		
Min. Pitch Distance (mm)	= 67.5	67.5	Pass
(IIIII)	[Ref. IS 800:2007, Cl.10.2.2]		
	$p/g_{\text{max}} = \min(32t, 300)$		
	$= \min(32 \times 56.0, 300)$		
	$= \min(1792.0, 300)$		
Max. Pitch Distance	= 300	67.5	Pass
(mm)	Where, $t = \min(56.0, 56.0)$		
	[Ref. IS 800:2007, Cl.10.2.3]		
	$e_{\min} = 1.7d_0$		
	$= 1.7 \times 30.0$		
Min. End Distance	= 51.0	55	Pass
(mm)			
	[Ref. IS 800:2007, Cl.10.2.4.2]		

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Check	Required	Provided	Remarks
Max. End Distance (mm)	$e_{\max} = 12t\varepsilon; \ \varepsilon = \sqrt{\frac{250}{f_y}}$		
	$e_1 = 12 \times 56.0 \times \sqrt{\frac{250}{165}} = 827.17$		
	$e_2 = 12 \times 56.0 \times \sqrt{\frac{250}{165}} = 827.17$	55	Pass
	$e_{\text{max}} = \min(e_1, e_2) = 827.17$		
	[Ref. IS 800:2007, Cl.10.2.4.3]		

2.4 End Plate Checks

Check	Required	Provided	Remarks
Min. Plate Length (mm)	450.0	450.0	Pass
Min. Plate Height (mm)	250.0	250.0	Pass
Min. Plate Thickness (mm)	$t_{p} = max \left(\sqrt{\frac{4M_{cr}}{b_{eff}(f_{y}/\gamma_{m0})}}, \right.$ $\sqrt[4]{\left(T_{1} - \frac{2Ql_{e}}{l_{v}} \right) \times \left(\frac{27l_{e}l_{v}^{2}}{\beta\eta f_{o}b_{e}} \right)} \right)}$ $= max \left(\sqrt{\frac{4 \times 7.12 \times 10^{6}}{67 \times (165/1.1)}}, \right.$ $\sqrt[4]{\left(146393.25 - \frac{2 \times 2.72 \times 55}{55} \right) \times \left(\frac{27 \times 5}{2 \times 1.5 \times 3} \right)}$	$ \frac{5 \times 55^{2}}{50.0 \times 125.0} $	
	= 56.0		
Moment Capacity (kNm)	$M_{ep} = \max (0.5 \text{ X Tension in first bolt X end dista}$ Tension in second bolt X end distance) = $\max(0.5T_h1e, T_h2e)$	$M_{dp} = \frac{\sigma_{\text{eff}} t_p J y}{4\gamma_{m0}}$	Pass
Thomas Capacity (ATTII)	$= \max(0.57616, 7626)$ $= \max(0.5 \times 146393.25 \times 55, 129494.68 \times 55)$ $= 7.12$	$= \frac{67.5 \times 56.0^2 \times 165}{4 \times 1.1}$ $= 7.94$	

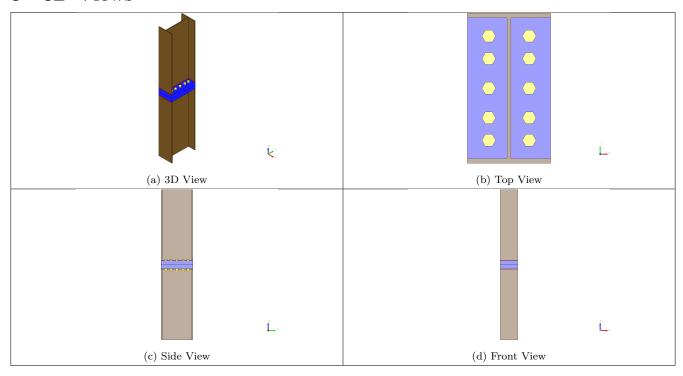
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2.5 Bolt Checks

Check	Required	Provided	Remarks
Diameter (mm)	Bolt Quantity Optimisation	The number of bolts for given bolt size(s)	
		are not sufficient to cater for the given sec-	
		tion and loads combination.	

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3 3D Views



4 Design Log