
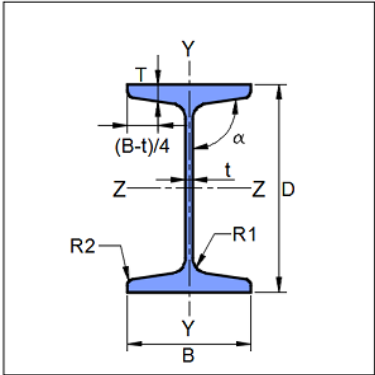


		Created with 	
Company Name		Project Title	Beam to Beam Cover Plate
Group/Team Name		Subtitle	
Designer		Job Number	
Date	21 /01 /2025	Client	

1 Input Parameters

Module		Beam-to-Beam Cover Plate Bolted Connection		
Main Module		Moment Connection		
Bending Moment (kNm) *		34.0		
Shear Force (kN) *		34.0		
Axial Force (kN)		34.0		
Beam Section - Mechanical Properties				
	Beam Section		JB 175	
	Material *		E 165 (Fe 290)	
	Ultimate Strength, F_u (MPa)		290	
	Yield Strength, F_y (MPa)		165	
	Mass, m (kg/m)	8.07	I_z (cm ⁴)	480.0
	Area, A (cm ²)	1020.0	I_y (cm ⁴)	9.65
	D (mm)	175.0	r_z (cm)	6.83
	B (mm)	50.0	r_y (cm)	0.97
	t (mm)	3.2	Z_z (cm ³)	54.9
	T (mm)	4.8	Z_y (cm ³)	3.86
	Flange Slope	91.5	Z_{pz} (cm ³)	64.2
	R_1 (mm)	5.0	Z_{py} (cm ³)	6.32
	R_2 (mm)	1.5		
Bolt Details - Input and Design Preference				
Diameter (mm) *		[8, 10, 12, 14, 16, 18, 20, 22, 24, 27, 30, 33, 36, 39, 42, 45, 48, 52, 56, 60, 64]		
Property Class *		[np.float64(3.6), np.float64(4.6), np.float64(4.8), np.float64(5.6), np.float64(5.8), np.float64(6.8), np.float64(8.8), np.float64(9.8), np.float64(10.9), np.float64(12.9)]		
Type *		Bearing Bolt		
Hole Type		Standard		
Slip Factor, (μ_f)		0.3		
Edge Preparation Method		Sheared or hand flame cut		
Gap Between Beams (mm)		3.0		
Are the Members Exposed to Corrosive Influences?		False		



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Plate Details - Input and Design Preference	
Preference *	Outside
Ultimate Strength, F_u (MPa)	290
Yield Strength, F_y (MPa)	165
Material *	E 165 (Fe 290)
Thickness (mm) *	[8, 10, 12, 14, 16, 18, 20, 22, 25, 28, 32, 36, 40, 45, 50, 56, 63, 75, 80, 90, 100, 110, 120]


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2 Design Checks

Design Status	Fail
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2.1 Member Capacity


Check	Required	Provided	Remarks
Section Classification		Plastic [Ref: Table 2, Cl.3.7.2 and 3.7.4, IS 800:2007]	
Axial Capacity Member (kN)	$P_x = 34.0$	$T_{dg} = \frac{A_g f_y}{\gamma_{m0}}$ $= \frac{1020.0 \times 165}{1.1 \times 10^3}$ $= 153.0$ [Ref. IS 800:2007, Cl.6.2]	
Shear Capacity Member (kN)		$V_{dy} = \frac{A_v f_y}{\sqrt{3} \gamma_{m0}}$ $= \frac{165.4 \times 3.2 \times 165}{\sqrt{3} \times 1.1 \times 1000}$ $= 45.84$ [Ref. IS 800:2007, Cl.10.4.3]	
Allowable Shear Capacity (kN)	$V_y = 34.0$	$V_d = 0.6 V_{dy}$ $= 0.6 \times 45.84$ $= 27.5$ [Limited to low shear]	Fail
Plastic Moment Capacity (kNm)		$M_{dz} = \frac{\beta_b Z_p f_y}{\gamma_{m0}}$ $= \frac{1 \times 64200.0 \times 165}{1.1 \times 10^6}$ $= 9.63$ [Ref. IS 800:2007, Cl.8.2.1.2]	

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Check	Required	Provided	Remarks
Moment Deformation Criteria (kNm)		$M_{dc} = \frac{1.5Z_e f_y}{\gamma_{m0} \times 10^6}$ $= \frac{1.5 \times 54900.0 \times 165}{1.1 \times 10^6}$ $= 12.35$ [Ref. IS 800:2007, Cl.8.2.1.2]	
Moment Capacity Member (kNm)	$M_z = 34.0$	$M_{dz} = \min(M_{dz}, M_{dc})$ $= \min(9.63, 12.35)$ $= 9.63$ [Ref. IS 800:2007, Cl.8.2]	

2.2 Load Consideration


Check	Required	Provided	Remarks
Interaction Ratio		I.R. axial $= P_x / T_{dg}$ $= 34.0 / 153.0$ $= 0.2222$ I.R. moment $= M_z / M_{dz}$ $= 34.0 / 9.63$ $= 3.5306$ I.R. sum $= \text{I.R. axial} + \text{I.R. moment}$ $= 0.2222 + 3.5306$ $= 3.7528$	

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Check	Required	Provided	Remarks
Minimum Required Load	<p>if I.R. axial < 0.3 and I.R. moment < 0.5</p> $P_{x\min} = 0.3T_{dg}$ $M_{z\min} = 0.5M_{dz}$ <p>elif sum I.R. ≤ 1.0 and I.R. moment < 0.5</p> <p>if $(0.5 - \text{I.R. moment}) < (1 - \text{sum I.R.})$</p> $M_{z\min} = 0.5 \times M_{dz}$ <p>else</p> $M_{z\min} = M_z + ((1 - \text{sum I.R.}) \times M_{dz})$ $P_{x\min} = P_x$ <p>elif sum I.R. ≤ 1.0 and I.R. axial < 0.3</p> <p>if $(0.3 - \text{I.R. axial}) < (1 - \text{sum I.R.})$</p> $P_{x\min} = 0.3T_{dg}$ <p>else</p> $P_{x\min} = P_x + ((1 - \text{sum I.R.}) \times T_{dg})$ $M_{z\min} = M_z$ <p>else</p> $P_{x\min} = P_x$ $M_{z\min} = M_z$ <p>Note: AL is the user input for load</p>	$M_{z\min} = 34.0$ $P_{x\min} = 34.0$ <p>[Ref. IS 800:2007, Cl.10.7]</p>	
Applied Axial Force (kN)	$P_x = 34.0$	$P_u = \max(P_x, P_{x\min})$ $= \max(34.0, 34.0)$ $= 34.0$	

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Check	Required	Provided	Remarks
Applied Shear Force (kN)	$V_y = 34.0$	$V_{y\min} = \min(0.15V_{dy}, 40.0)$ $= \min(0.15 \times 45.84, 40.0)$ $= 6.88$ $V_u = \max(V_y, V_{y\min})$ $= \max(34.0, 6.88)$ $= 34.0$ [Ref. IS 800:2007, Cl.10.7]	
Applied Moment (kNm)	$M_z = 34.0$	$M_u = \max(M_z, M_{z\min})$ $= \max(34.0, 34.0)$ $= 34.0$ [Ref. IS 800:2007, Cl.8.2.1.2]	
Force Carried by Web		$A_w = \text{Axial force in web}$ $= \frac{(D - 2T)tA_u}{A}$ $= \frac{(175.0 - 2 \times 4.8) \times 3.2 \times 34.0}{1020.0}$ $= 17.64 \text{ kN}$ $M_w = \text{Moment in web}$ $= \frac{Z_w M_u}{Z}$ $= \frac{21885.73 \times 34.0}{64200.0}$ $= 11.59 \text{ kNm}$	

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Check	Required	Provided	Remarks
Force Carried by Flange		$A_f = \text{Axial force in flange}$ $= \frac{AuBT}{A}$ $= \frac{34.0 \times 50.0 \times 4.8}{1020.0}$ $= 8.0 \text{ kN}$ $M_f = \text{Moment in flange}$ $= Mu - M_w$ $= 34.0 - 11.59$ $= 22.41 \text{ kNm}$ $F_f = \text{flange force}$ $= \frac{M_f \times 10^3}{D - T} + A_f$ $= \frac{22.41 \times 10^3}{175.0 - 4.8} + 8.0$ $= 139.67 \text{ kN}$	

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3 3D Views

	<div>C:3-env-packages.png</div> <div>(a) 3D View</div>		<div>C:3-env-packages.png</div> <div>(b) Top View</div>	
	<div>C:3-env-packages.png</div> <div>(c) Side View</div>		<div>C:3-env-packages.png</div> <div>(d) Front View</div>	

4 Design Log

2025-01-21 13:47:45 - Osdag - WARNING - : The value of factored shear load exceeds by 0.6 times the shear capacity of the member, 27.5 kN.

2025-01-21 13:47:45 - Osdag - ERROR - : Design of members in high shear is not recommended by Osdag. Design is unsafe.

2025-01-21 13:47:45 - Osdag - INFO - :=====End Of design=====