

ETG Turbulence Isotropization

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Drift Wave Instabilities

- Drift waves are characterized as density, temperature or pressure fluctuations in plasmas.
- Modes relevant to tokamak physics include ion-temperature-gradient modes (ITG), electron-temperature-gradient modes (ETG), and trapped electron modes (TEM).
- Low-frequency drift wave turbulence is largely responsible for the anomalous transport of plasma particles across magnetic field lines (Horton 1999).



Ion-Temperature-Gradient Mode Growth

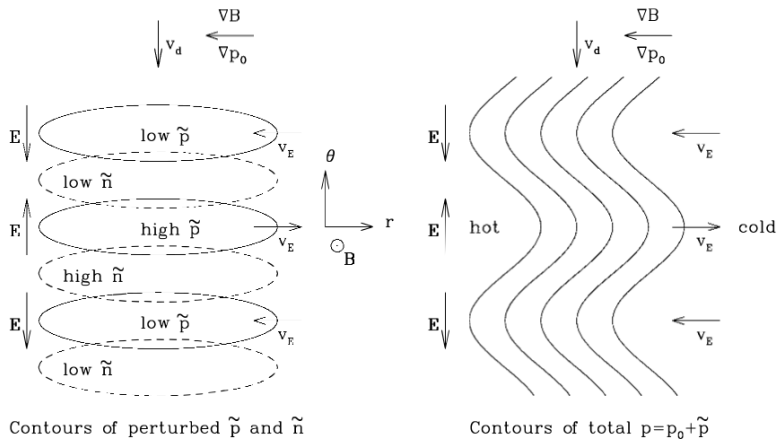
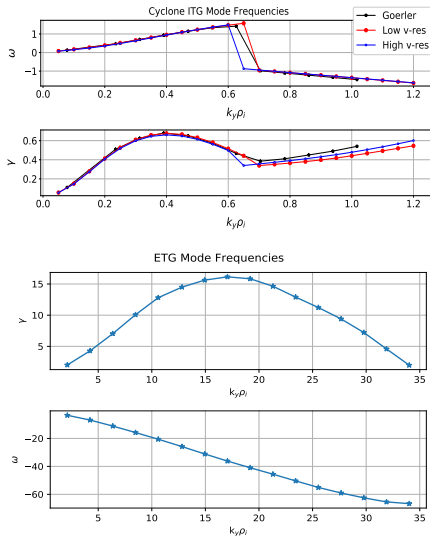


Figure: Picture of ITG instability (Beer 1994).

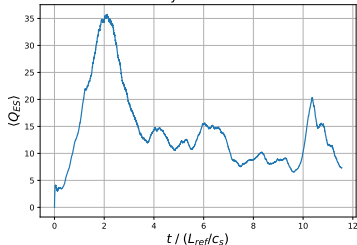
ETG Simulation in GENE



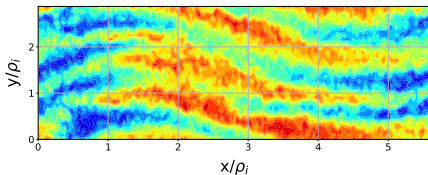
- Successful reproduction of Görler benchmark with kinetic ions and electrons (Görler 2016).
- Conversion of ITG to ETG flux-tube case prior to running non-linear simulations.

ETG "Streamers" in GENE

Electron GyroBohm Heat Flux



ϕ



- ETG turbulence in toroidal gyrokinetic simulations is associated with radially elongated "streamers".
- Multiscale turbulence simulations have shown that streamers dominate electron heat flux and lead to experimental tokamak heat flux values (Howard 2016).

Hasegawa-Mima Fluid ETG Model

- Partial differential equation derived from fluid continuity and momentum equations.
- Approximations made that are useful to describing turbulence in tokamak plasmas.
 - Cyclotron motion periods much smaller than time scales that quantities of interest change on (B, Φ, n) .
 - Long length scales along \hat{b} -direction - $k_{\parallel}/k_{\perp} \equiv \epsilon \ll 1$.
 - Quasi-neutrality of particle densities is enforced.
 - Adiabatic ions.
 - Isothermal equation of state, with $\delta P_e = \delta n_e T_e$ ($\delta T_e = 0$).
- Shown to cause isotropic behavior for long wavelength modes as well as an inverse energy-cascade (Hasegawa 1978).

Hasegawa-Mima Equations

We start with the fluid continuity and momentum equations with $\tau = T_e/T_i$, where we have already taken the approximations discussed on the previous slide:

$$\frac{\partial n_e}{\partial t} + \nabla \cdot (n_e \vec{v}_e) = 0, \quad (1)$$

$$m_e \frac{d\vec{v}_e}{dt} = (1 + \tau) e \nabla \delta \Phi - \frac{e}{c} \vec{v}_e \times \vec{B} - \frac{\nabla P_e}{n_e}. \quad (2)$$

Then \vec{v}_e is solved for using (2) and plugged into (1), dropping terms higher order than ϵ to get a final PDE describing the evolution of $\delta \Phi$. The derivation is carried out in the Appendix A.

Hasegawa-Mima Equations

Taking a standard electron dynamic normalization,

$$\begin{aligned}\Phi &= \frac{e\delta\Phi}{T_i}, \quad -\frac{1}{r_n} = \frac{\partial_x n_e}{n_e}, \quad -\frac{1}{r_t} = \frac{\partial_x T_e}{T_e}, \quad \eta_e = \frac{r_n}{r_t}, \\ \rho_e &= \sqrt{\frac{\tau m_e}{m_i}} \rho_i, \quad \vec{x} = \frac{\vec{X}}{\rho_e}, \quad t = \frac{\rho_e}{r_n} \omega_{ce} t,\end{aligned}\tag{3}$$

and plugging into (10) gives the form of the H-M ETG model,

$$\begin{aligned}-\left(1 - \frac{1+\tau}{2\tau} \nabla_\perp^2\right) \partial_t \Phi &+ \frac{1+\tau}{2\tau} \frac{r_n^2}{\rho_e^2} \partial_t^{-1} \nabla_\parallel^2 \Phi + \frac{(1+\tau)(1+\eta_e)}{4\tau} \partial_y \nabla_\perp^2 \Phi \\ &+ \frac{1+\eta_e}{2\tau} \partial_y \Phi + \frac{(1+\tau)^2}{\tau^2} \frac{r_n}{4\rho_e} (\hat{b} \times \nabla_\perp \Phi \cdot \nabla_\perp) \nabla_\perp^2 \Phi = 0.\end{aligned}\tag{4}$$

Hasegawa-Mima Equations

We drop the higher order parallel gradient term and simplify the bracketed expression for a 2-D slab geometry to find the final form,

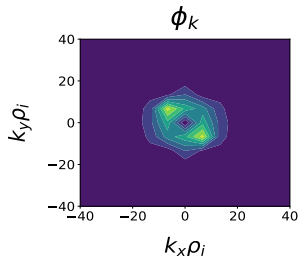
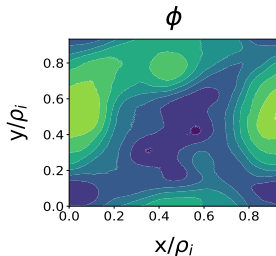
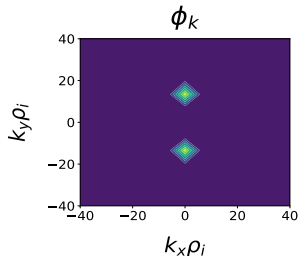
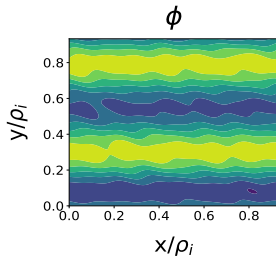
$$\begin{aligned} \partial_t \left[\Phi - \frac{1+\tau}{2\tau} \zeta \right] = & \frac{(1+\tau)(1+\eta_e)}{4\tau} \zeta_y + \frac{1+\eta_e}{2\tau} \Phi_y \\ & + \frac{(1+\tau)^2}{\tau} \frac{r_n}{4\rho_e} [\Phi_x \zeta_y - \zeta_x \Phi_y], \end{aligned} \quad (5)$$

where $\zeta = \nabla^2 \Phi$ and x, y subscripts denote partial derivatives. The non-linear terms lead to rotation in k-space and eventually isotropization.

Pseudo-Spectral Solver

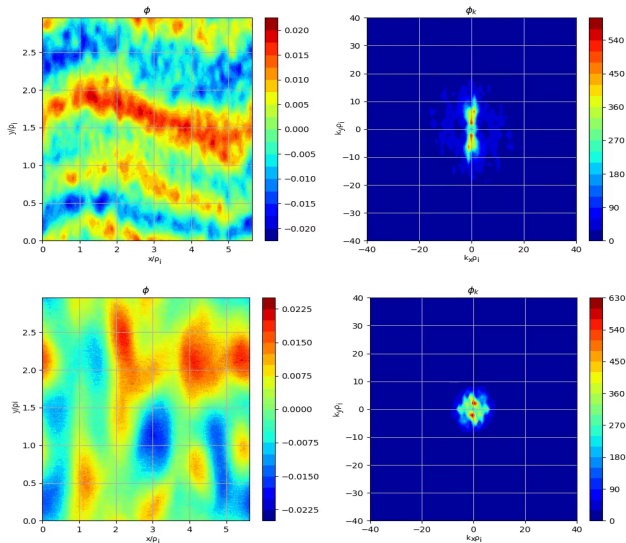
- Equation (6) is solved numerically using the pseudo-spectral method.
 - Fourier transform the equation and get $\zeta = -(k_x^2 + k_y^2)\Phi$.
 - Inverse Fourier transform $\zeta_{x,y}$ and $\Phi_{x,y}$ back into real space.
 - Calculate the non-linear products between ζ and Φ in real space and then Fourier transform the products so they can be added to the other terms in Fourier space.
 - Time advance Φ discretely.
- Time advancement is done using the 4th order Runge-Kutta method.
- The pseudo-spectral method requires de-aliasing of modes due to non-linear terms. This is explored in Appendix B.

ETG H-M Results



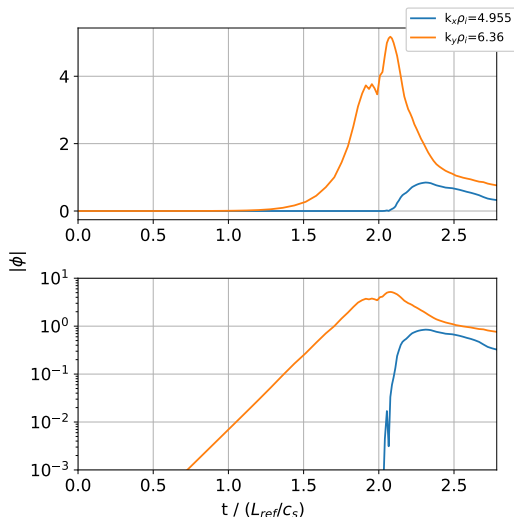
- Results of H-M code. Initial condition (above) isotropizes at late time (below).
- Parameters:
 - $\tau = 1$
 - $\eta_e = 3$
 - $r_n/\rho_i = 500$

GENE ETG Streamer Test



- Test of GENE saturated ETG results into H-M code. Initial condition (above) isotropizes at late time (below).
- Inverse energy cascade observed as well.

Zonal Flow Excitation



- Zonal flow can be spontaneously excited by intermediate-scale ETG turbulence in tokamak geometries - $k_{\perp}\rho_e \ll 1 \ll k_{\perp}\rho_i$.
- Plan to carry out large-scale ETG simulations with GENE to compare to theory of zonal flow excitation by ETG modes.

Four-Wave Weak Turbulence Model

$$\begin{aligned}(\partial_t + \gamma_z(1 + d_z k_z^2 \rho_e^2))\chi_z A_z &= \sqrt{\pi/2} W k_z^3 \rho_e^3 (A_+ A_0^* a_n^* - A_-^* A_0 a_n), \\ [\partial_t + i\Delta - \gamma_s] A_+ &= -W k_z \rho_e A_z A_0 / \sqrt{2\pi}, \\ [\partial_t + i\Delta - \gamma_s] A_- &= W k_z \rho_e A_z^* A_0 / \sqrt{2\pi}, \\ [\partial_t - \gamma_n] A_0 &= -W k_z \rho_e (A_z A_- - A_z^* A_+) / \sqrt{2\pi}, \\ (\partial_t - 2\gamma_n) |A_0|^2 &= (2\gamma_s - \partial_t) (|A_+|^2 + |A_-|^2)\end{aligned}$$

- $A_z \equiv$ Zonal Flow Amp.
- $A_{\pm} \equiv$ Sideband Amp.'s
- $A_0 \equiv$ ETG Pump Wave
- $a_n \equiv$ Parallel coupling fn.
- $W \equiv$ Bandwidth
- $\gamma_{z,n,s} \equiv$ Growth rates
- $\chi_z \equiv$ Susceptibility
- $k_z \equiv$ radial k

Appendix A: H-M Fluid Model

We break up (2) into parallel and perpendicular components by taking a dot product with \hat{b} to find,

$$\frac{d\vec{v}_{e,\parallel}}{dt} = (1 + \tau) \frac{e}{m_e} \partial_t^{-1} \nabla_{\parallel} \delta\Phi \Rightarrow v_{\parallel} \simeq (1 + \tau) \frac{k_{\parallel} e \delta\Phi}{m_e \omega}, \quad (6)$$

$$\frac{d\vec{v}_{e,\perp}}{dt} = (1 + \tau) \frac{e}{m_e} \nabla_{\perp} \delta\Phi - \omega_{c,e} \vec{v}_{e,\perp} - \frac{\hat{b} \times \nabla P_e}{m_e n_e}. \quad (7)$$

Appendix A: H-M Fluid Model

Then we can split up \vec{v}_e by ordering

$$\begin{aligned}\vec{v}_{e,0} &= \vec{v}_{\parallel} + \vec{v}_{\perp,0} = \vec{v}_{\parallel} + (1 + \tau) \vec{v}_E + \vec{v}_D, \\ \vec{v}_{e,1} &= \vec{v}_{\perp,1} = -\frac{1}{\omega_{c,e}} (\partial_t + \vec{v}_{e,0} \cdot \nabla) (\hat{b} \times \vec{v}_{e,0}) \\ &\simeq \frac{e(1 + \tau)}{m_e \omega_{c,e}^2} \partial_t \nabla_{\perp} \delta \Phi - \left[\frac{\vec{b} \times \nabla P_e}{n_e} \cdot \nabla_{\perp} \right] \frac{e(1 + \tau)}{m_e^2 \omega_{c,e}^3} \nabla_{\perp} \delta \Phi \\ &\quad + \frac{e^2(1 + \tau)^2}{m_e^2 \omega_{c,e}^3} [\hat{b} \times \nabla_{\perp} \delta \Phi \cdot \nabla_{\perp}] \nabla_{\perp} \delta \Phi.\end{aligned}\tag{8}$$

Appendix A: H-M Fluid Model

Now, with incompressibility and to lowest order, $\nabla \cdot \vec{v}_{e,0,\perp} = 0$ and so (1) becomes,

$$\partial_t \delta n_e + n_e \nabla \cdot (\vec{v}_{\parallel} + \vec{v}_{e,1}) + \nabla \delta n_e \cdot \vec{v}_D + (1 + \tau) \delta n_e \cdot \vec{v}_E = 0, \quad (9)$$

and plugging in $\delta n_e = \delta n_i$, we find that to order ϵ ,

$$\begin{aligned} & -n_e \partial_t \frac{e\delta\Phi}{T_i} + n_e(1 + \tau) \frac{e}{m_e} \partial_t^{-1} \nabla_{\parallel}^2 \delta\Phi + \frac{en_e(1 + \tau)}{m_e \omega_{c,e}^2} \partial_t \nabla_{\perp}^2 \delta\Phi \\ & - \frac{e(1 + \tau)}{m_e^2 \omega_{c,e}^3} [\hat{b} \times \nabla P_e \cdot \nabla_{\perp}] \nabla_{\perp}^2 \delta\Phi + \frac{e^2 n_e (1 + \tau)^2}{m_e^2 \omega_{c,e}^3} [\hat{b} \times \nabla_{\perp} \delta\Phi \cdot \nabla_{\perp}] \nabla_{\perp}^2 \delta\Phi \\ & + \nabla_{\perp} \frac{e\delta\Phi}{T_i} \cdot \frac{\hat{b} \times \nabla P_e}{m_e \omega_{c,e}} + \frac{e(1 + \tau)}{m_e \omega_{c,e}} \nabla n_e \cdot \hat{b} \times \nabla \Phi = 0. \end{aligned} \quad (10)$$

Appendix B: Pseudo-Spectral De-Aliasing

Our Fourier transforms go as $e^{-ik_j z_n}$ with wave-vectors $k_j = 2\pi j/N\Delta$, and grid points $x_n = n\Delta$, where $j = -N/2, \dots, N/2$, and $n = 0, \dots, N-1$. So the final form for our modes is $e^{-2\pi i n j/N}$. If we consider non-linear terms then we can take $j' = j + lN$ with $l = \dots, -1, 0, 1, \dots$, which will take j out of the range well-resolved by the Fourier transform. The extra term $e^{-2\pi i l n} = 1$ results in the same values at our grid points. This means non-linear terms can lead to biasing of lower, well-resolved modes via higher modes. To de-alias we choose the truncation (or 2/3) rule which says to zero out modes between $[-N/2, -K]$ and $[K, N/2]$. That way if we have two modes $|j + k| > N/2$ the final mode is resolved as $j + k - N$ which must be $< -K$ to be zeroed out. Since the largest allowed option is K for each mode, we get $2K - N < -K \Rightarrow K < N/3$. This means keeping 2/3 of the original modes when considering non-linear terms.