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Modelling the effects of temperature on Microbial Fuel Cells

A Research Proposal



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1 Abstract

- May not be necessary
- A summary of the initial report

2 Introduction

- General opener

2.1 Wastewater in the UK

Reporting by Conway (2022) indicates that untreated sewage has been repeatedly released or dumped into rivers across the United Kingdom. In total, it is believed that sewage was dumped more than 3000 times between 2017 and 2021. This is despite regulation controls by Ofwat, whose stated vision is “to make the greatest contribution possible to improving life through water” Ofwat (2014). According to the Environment Audit Committee 36% of this pollution stems from sewage and wastewater sources, EAC (2022). As a result, only 14% of rivers in England can claim to have good ecological status.

2.2 A Potential Solution

A potential solution to this ecological problem is the introduction of new technology to current wastewater treatment techniques. Microbial Fuel Cells (MFCs) have been around since the mid 19th Century, but the technology was not considered to be a viable source of power generation, Scott and Hao Yu (2016). They are considered desirable for wastewater treatment due to their ability to treat waste water whilst simultaneously generating electricity.

Recently, these cells have undergone a revival in research and sources such as Herrero-Hernandez, Smith, and Akid (2013) claim that the technology is now at a stage where it should be considered workable.

Figure 1 below shows a typical diagram of an MFC.

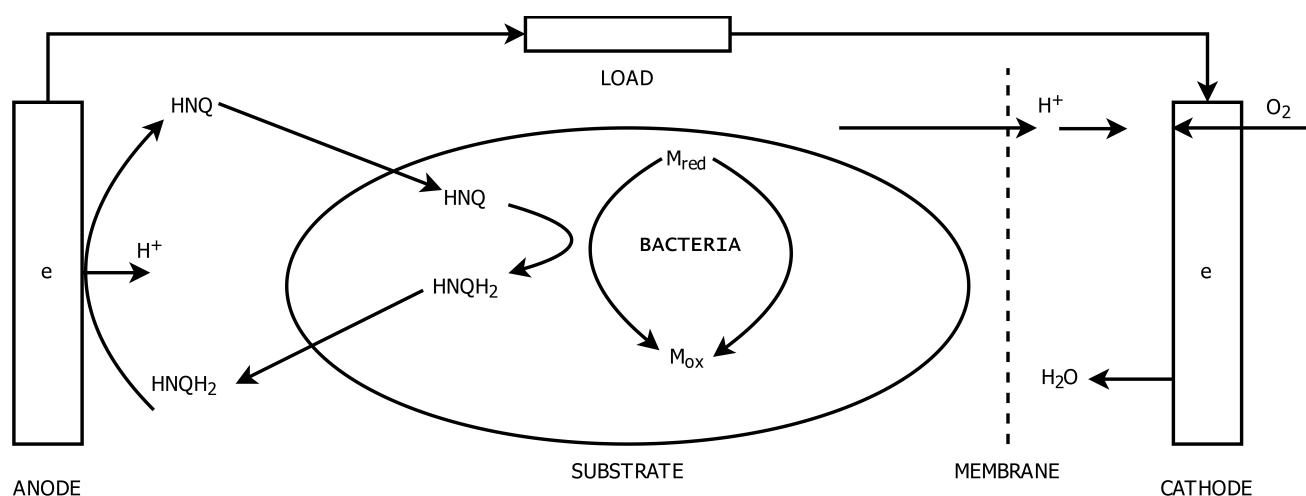


Figure 1: Diagram of a Microbial Fuel Cell (Zhang and Halme, 1995)

MFCs operate by oxidising organic components to release electrons and protons, Cao et al. (2019), which are then used for power generation. The principal components of a Microbial Fuel Cell are an anode and a cathode, Logan (2008). These can be arranged in a variety of ways with multiple of either comprising the cell. In addition, a membrane can be included to separate anodic and cathodic liquids however these are not preferred as they increase the internal resistance of the cell, reducing electron transfer.

2.3 Key Parameters

The key operational and fundamental parameters that affect MFCs are shown below in Table 1. Several of these have been expanded within the Technical Background section of this proposal.

Table 1: List of parameters

Parameter	Notes
Feed COD	Variable
COD Removal Efficiency	Variable
Culture Purity	Variable
Biofilm	Variable
Architecture	Fixed
Material	Fixed
Oxidising agent	Fixed
Feed Flow rate	Variable
Temperature	Variable

3 Motivation

- Avid hiker and canoer
- I want to help this problem
- I enjoy clean water
- I like modelling

4 Technical Context & Overview

This section has been designed to provide technical context to a reader who may be looking for some background on Microbial Fuel Cells and concerns the key parameters mentioned earlier.

4.1 Power Generation

A typical circuit arrangement involves including a source of external resistance alongside the MFC, Logan (2008). It is essential to use an external source of resistance as the internal

resistance inside the cell is not enough for feasible power generation and increasing it would rapidly decrease the performance of the cell. Alternating this external resistance within a circuit provides a variable voltage output.

This output can be used to plot a polarisation curve of the external resistance against the cell voltage which can be used to calculate the current. From this the current density can be plotted against the cell voltage to produce a power curve. This power curve can generally be divided into three separate zones, referred to as the kinetic region, ohmic region and the mass-transfer region. This is because as the current density increases different factors hold more sway over the cell. The most important region is the ohmic region as this shows the internal resistance of the cell, a key parameter to be minimised.

4.2 Feed COD

The Chemical Oxygen Demand (COD) of wastewater is defined as the quantity of water necessary to oxidise the organic matter present in said water Scimed (2021). If water with a high COD is discharged then downstream organisms will face increased competition for oxygen which will affect the aquatic life present.

4.3 COD Removal Efficiency

For effective wastewater treatment a high COD removal efficiency is desirable to reduce downstream competition for oxygen. It is calculated as $\frac{COD_{Inlet} - COD_{Outlet}}{COD_{Inlet}} \times 100$.

4.3.1 Coulombic Efficiency

A related parameter is the Coulombic efficiency which is the fraction of electrons recovered as current versus that in the starting organic matter, Logan (2008). A desirable MFC will have a high COD removal efficiency and Coulombic efficiency to maximise both the power generated and the volume of wastewater that can be treated.

4.4 Mixed vs pure culture

Due to the biological nature of MFCs, the purity of bacterial species used on the anode is a parameter for optimisation as considered by Jadhav and Ghangrekar (2020). Pure cultures tend to produce an increased power output and Coulombic efficiency compared to mixed cultures. In addition, as stated by Cao et al. (2019) cells using pure cultures are useful to explain the complicated electron transfer mechanisms within MFCs.

However, this comes at the cost of an increased cost to procure the bacteria, due to the inherent difficulty of fully separating bacterial strains, as well as the risk of contamination from wastewater. On the other hand, mixed cultures are better for overall functionality due to their reduced substrate specificity and resistance to shock load conditions. Therefore, the more feasible MFC designs for scale-up will contain mixed cultures.

4.5 Biofilm

The biofilm of an MFC is the layers of bacteria that form on the anode. As the thickness of the biofilm increases the quantity of bacteria increases, this allows for an increased rate of electron release as the organic matter present is broken down. However, if the biofilm is too thick then there will be mass transport issues that will reduce the power output of the cell. As a result, according to Logan (2008), biofilms are generally a few millimetres thick.

Within literature there are two main types of electron transfer through the cell, direct and indirect. Direct electron transfer involves direct contact between the bacterial cell surface and the electrode, whilst indirect transfer uses electron mediators, Cao et al. (2019). For examples, Paquete et al. (2014) investigated the effects of different electron “shuttles” on electron transfer but notes that the area remains poorly explored.

4.6 Architecture

- The previous work should go into the introduction section
- It makes the most sense when compared with the diagram from Zhang and Halme
- What should go here is the stuff that appears in the literature review
- Half and full cell models and how they relate to single and double chamber MFCs

4.7 Materials

For large scale reactors, practical and inexpensive materials are desirable. These must be suitable for the anode, cathode and, if one is used, a membrane. The cathode generally requires a catalyst and this is usually Pt although a non-precious metal alternative would be preferred. When decided on a construction, material, Logan (2008) suggests that it should have a surface area to volume ratio of $100 \text{ m}^2 \text{ m}^3$ of reactor.

Common material options are carbon based and include: carbon foam, carbon felt, carbon cloth and carbon paper. These were all compared by Mateo et al. (2018) were able to achieve a specific surface area of $7500 \text{ m}^2/\text{m}^3$. As a result, the material used could vary depending on price fluctuations at the time of cell production.

4.8 Cathode oxidising agent

In an MFC the oxidised organic matter releases protons which are then reduced in the presence of a catalyst, Scott and Hao Yu (2016). This is typically oxygen as it is readily available. This results in MFCs producing water as a by-product.

4.9 Flow rate

The flow rate of wastewater dictates the available COD for the cell. By increasing it, the cell will be in contact with more organic matter in a set period of time which as Ieropoulos, Winfield, and

Greenman (2010) states, is beneficial to treating wastewater. However, if the flow rate is too high then the cell may not be able to achieve the required levels of COD removal. This could necessitate the inclusion of further downstream treatment steps. Additionally, Villaseñor et al. (2013) established that at high flow rates there is a risk of unoxidised matter entering the cathodic chamber, causing it to enter into anaerobic condition, stopping the MFC from working.

4.10 Maintenance

- How does one maintain a cell?
- Important consideration for both lab and industrial scale

4.11 Temperature

As the processes inside an MFC are fundamentally biological in nature the cell is affected by temperature. A higher temperature correlates with a larger power output as lower temperatures slow down the growth and reproduction of bacteria.

- Cold temperatures considered by Dai et al. (2022)

5 Wastewater Treatment

A potential configuration for a domestic Wastewater Treatment Plant (WWTP) was considered by Logan (2008) and is shown below in Figure 2.

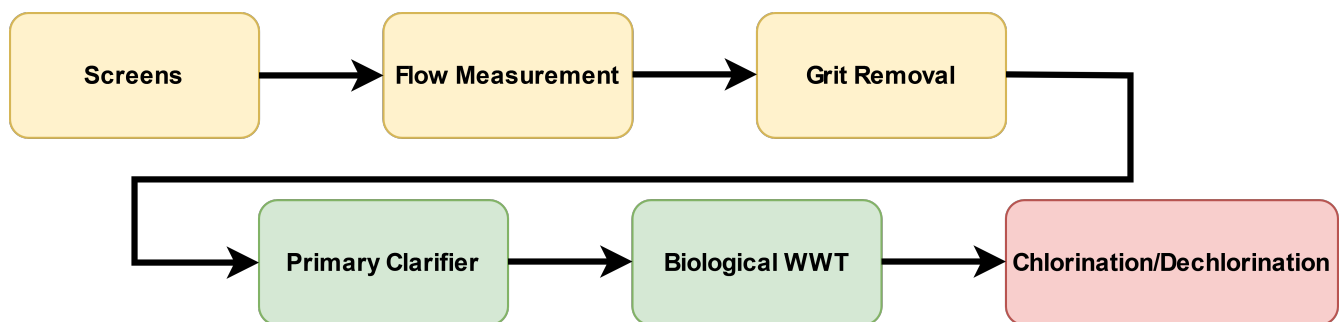


Figure 2: Process flow train for a domestic wastewater treatment plant (Logan, 2008)

First the wastewater is screened to remove large pieces of debris that may have entered upstream. The wastewater's flow is then measured and recorded. This allows for comparison with past data to determine any anomalous flow that may enter the system as a result of flooding or similar events. The wastewater then undergoes grit removal to prevent gritty particles such as coffee grinds or bones from damaging pumps. Typically, this will involve a hydraulic residence time (HRT) of between 1-20 minutes. Following this, the wastewater will be tested for either its biochemical oxygen demand (BOD) or its chemical oxygen demand (COD). The BOD takes 5

days and shows what material can be biologically removed, whilst the rapid COD test provides an assessment of all organic matter present.

Some biological material present as particulates is then removed in the primary clarifier, usually by collecting solids that accumulate at the bottom of the tank in a process with an HRT between 1-3 hours. Once this has been done the biological material will have been reduced to around 200 mg L^{-1} and the water will be ready for the wastewater treatment. It is proposed that this step will be done by a system based on MFCs to take advantage of the electricity generation and other related benefits over current systems. Finally, the wastewater goes a chlorination stage to kill of any remaining bacteria and then a dechlorination stage to prevent harm coming to aquatic life located where the water is released.

6 Literature Review

- GO BACK AND MENTION PARAMETERS CONSIDERED EARLIER

Within recent years interest in MFCs has increased. This is made clear by review papers considering the current state of modelling work such as those by Ortiz-Martínez et al. (2015) and Xia et al. (2018). These papers are very useful as they provide a broad overview into the technical work in key areas such as potential cell architecture, key parameters to consider and common model assumptions.

For instance, comprehensive models that seek to model all major processes such as the mass diffusion and substrate consumption can be either half cell models that consider the activity around the anode or full cell models that consider both the anode and cathode. Whilst the reaction around the anode is generally considered the limiting stage within the cell, the model for this proposed project will be a full model to provide as much insight into the internal processes of the cell when supplied with a low temperature feed. As a result, the model will be able to produce outputs relating to the biofilm thickness, fuel flow rate and concentration in addition to the electricity generation for comparison to experimental data.

6.1 Experimental Work

The experimental work concerning MFCs has been studied for longer than the modelling aspect and as a result there are plenty of papers available that provide experimental data for comparison with the results from a model. For this project, the main papers considered for this proposal focused on long term operation of MFCs. Santoro et al. (2012) operated a cell for 26 weeks, operated at 30°C whilst Moon, Chang, and Kim (2006) were able to operate multiple cells for 2 years over a range of temperatures. These results illustrate the operational viability of MFCs as successful long term operation reduces the need for maintenance or replacement of cells. This in turn allows MFC systems to be operated for longer resulting in reliable wastewater treatment.

However, the temperatures considered by both of these papers are not reflective of typical temperatures of UK wastewater *Access Database evidence*. Therefore, there is scope for research

into the performance of MFCs at lower temperatures to determine potential power outputs and thus potential feasibility.

To provide experimental data for direct comparison with the proposed model the work done by Cheng, Xing, and Logan (2011) has been considered. The research involved testing the power output of MFCs between 4-30°C having initialised them at 15°C or 30°C prior. This research suggests that cells initialised at higher temperatures produce reasonable quantities of power and could be used within a WWTP in the UK. This is an important fact to establish prior to any modelling work as it demonstrates that operation of these cells at lower temperatures is possible and therefore time spent modelling them is not being wasted.

Further work has been done testing the ability of MFCs to directly treat wastewater discharge at its source. Harewood et al. (2017) and Wen et al. (2009) have both investigated the potential of these cells to treat brewery wastewater whilst Rahman, Borhan, and Rahman (2018) considered the treatment of sugar beet processing wastewater. These experiments were able to produce power in addition to dealing with the industrial waste created, highlighting the feasibility of treating wastewater at the source.

Wen et al. (2009) used a single air-cathode MFC using carbon fibre as the anode material whilst Harewood et al. (2017) used a dual chamber setup which most notably contained a chitosan/polymalic acid-citric acid membrane. This was designed to introduce multiple charged groups to increase mass transport through the cell. These two studies saw very different maximum densities with Wen et al. (2009) achieving a density of 264 mW/m² whilst Harewood et al. (2017) achieved a density of 3022.39 mW/m². It is worth noting that the former used a COD of 626.58 mg/L whilst the latter had a COD of 3228 mg/L an increase of 525%. Whilst this goes some way to explaining the large difference in power densities a further explanation is that the technology surrounding MFCs has improved since the initial experiment conducted by Wen et al. (2009).

6.2 Modelling Work

- methodologies
- approaches
- equations
- assumptions
- Aim for a 1/2 a page more
- Pick out interesting points at the end of modelling work
- Link to objectives section

The large amount of experimental work provides plenty of data to validate new and existing MFC models. One such example is a model developed by Oliveira et al. (2013) that could correctly predict how the substrate concentration and temperature affected the cells biofilm thickness and performance. As part of this the temperature considered by model was adjusted between the values of 20°C, 30°C and 40°C. The key takeaway from this is that there are models accurate and reliable models available that allow for adjustment of the temperature. Therefore, this model could potentially be adapted to investigate MFC performance at lower temperatures as part of

the proposed project

Other potential models that could be used as the basis for the project include those considered by Pinto et al. (2010) and Zeng et al. (2010). Both of these were able to successfully predict MFC behaviour and performance when compared to experimental data despite being based on different principles. Pinto et al. (2010) developed a half-cell model based on the anode whilst Zeng et al. (2010) developed a model based on the cathode. This was unusual as the anodic step is generally considered to be reaction limiting. The existence and accuracy of these models demonstrates that there is good degree of flexibility available when initially building and then refining a model. As a result, the final model considered by the project may differ significantly from the one considered initially.

It is notable that Pinto et al. (2010) and another model by Littfinski et al. (2022) used similar assumptions concerning the biofilm formation and retention. In both cases the expected changes to the biofilm were not computed by the model directly but were instead taken from a different and specific biofilm model designed to model biofilm growth on an anode. This is a fairly common practice among MFC models, Ortiz-Martínez et al. (2015), and is done due to the difficulty of integrating a more complete simulation of the biofilm's growth within an MFC model. Other notable assumptions include a fixed cathode potential as mentioned by Xia et al. (2018) which is used for single chamber, half cell models concerning the anode. Additionally, some models such as those by Zhang and Halme (1995) assumed that the mass transport through the cell was rapid to be discounted. This assumption was made as this model was one of the very first models created to model MFC performance and is very rarely used today, Ortiz-Martínez et al. (2015). A further assumption, made by Littfinski et al. (2022) and Wang et al. (2011) is to neglect the substrate consumption gradient within the cell and instead assume a fixed value.

7 Objectives

From the above literature review, it is clear that there is a deficit in the papers modelling the effects of temperature on Microbial Fuel Cells. The broad aim of the dissertation will therefore be to model the effects of temperature on these cells. This breaks down into the following objectives:

1. Produce a model that is able to calculate the effects of temperature of key design parameters of a typical MFC such as its COD removal efficiency and power generation.
2. Use said model to determine achievable levels of wastewater treatment and power generation at lower temperatures.
3. Assess and comment on the viability of using such a cell within the UK's wastewater management scheme.

8 Work Schedule

A proposed work schedule for the upcoming project is shown below in Figure 3.

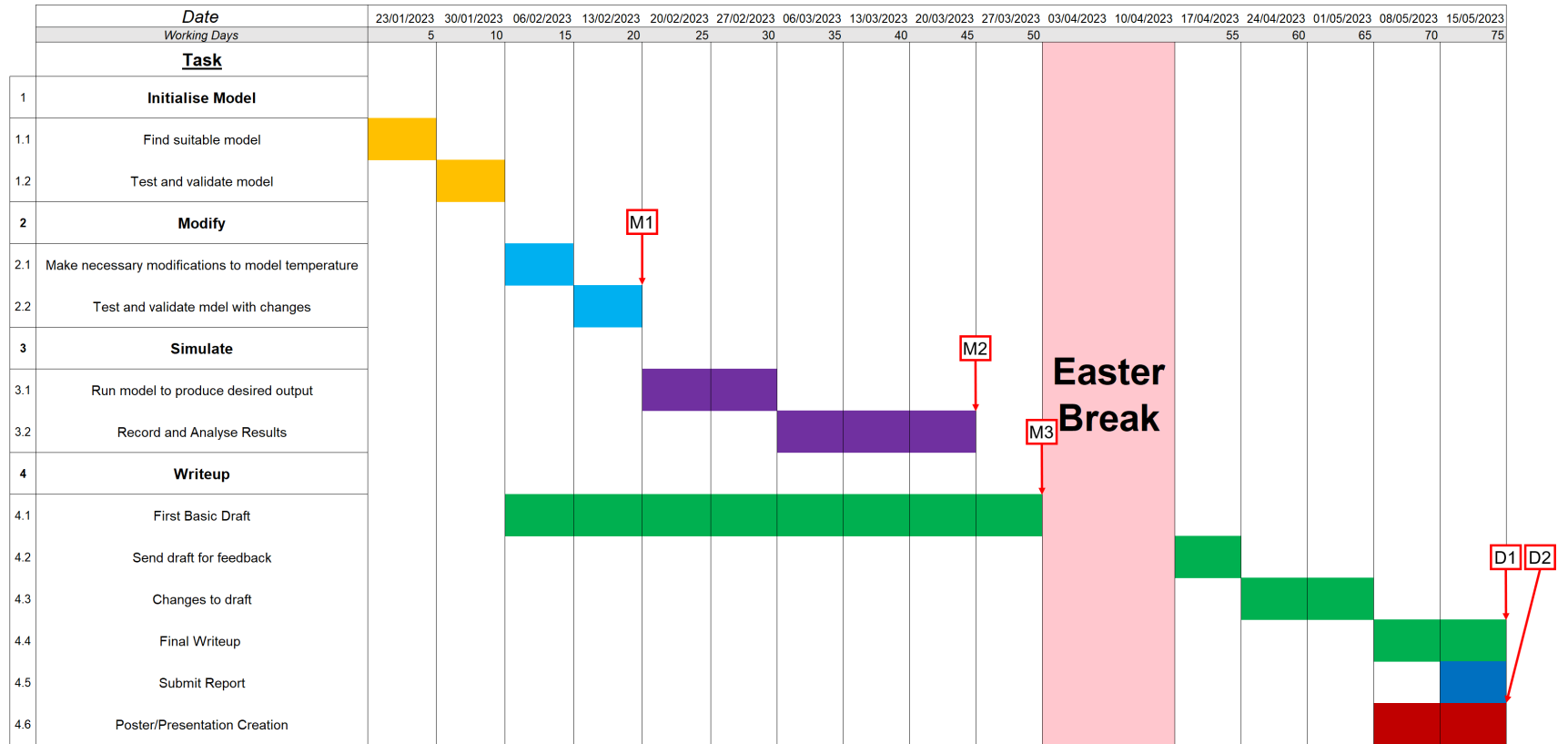


Figure 3: Proposed Project Schedule

The project plan above features several key milestones and deliverables, notated with 'M' and 'D' respectively. These have been added for future reference to ensure that the project is on track and show the expected completion time of the assessed tasks.

Milestone 1 will be reached when a modified model has been tested and validated for use in the project. This is key to ensuring that the project is able to deliver on its intended objectives. Milestone 2 will be reached when this model has been used to produce then desire outputs which have then been analysed. This is essential to ensure that the dissertation report is able to provide key insights into the technical challenges facing MFCs as well as a commentary on their effectiveness at different temperatures. Milestone 3 will be completed when the draft report contains a detailed write-up of the previous milestones. This is a crucial step to complete as otherwise there may not be sufficient time to produce a quality report that accurately reflects the work done.

These milestones should help in the completion of the deliverables. Deliverable 1 is a report finished to a high standard that will have undergone several changes and iterations based upon feedback from the Supervisor. As the report is worth 40 credits, missing the deadline would be undesirable. Deliverable 2 is the production of either a presentation or poster that will be used to summarise and present the key findings of the project.

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