# Homework 1

- **1.** A control law for a simple rotation table is to be designed. The table has a rotational moment of inertia (J) of 10 kg-m2 and rotational damping (b) of 1 N-m-s/rad. Torque is commanded to the motor and the table's position is measured using a rotary encoder.
  - (a) Derive the simple differential equation for the system.
  - (b) Convert the system into a state-space format.
  - (c) What are the eigenvalues of the system.

## Solution:

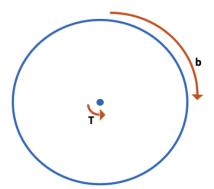


Figure 1: System Diagram.

Summing the moments on the table.

$$\sum M = J\ddot{\theta} = T - b\dot{\theta}$$

$$= 10\ddot{\theta} = T - 1\dot{\theta}$$

$$T = 10\ddot{\theta} + \dot{\theta}$$
(1)

Linearizing the system and putting it in matrix form.

$$\begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} \theta \\ \dot{\theta} \end{bmatrix} \\
\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} \dot{\theta} \\ \ddot{\theta} \end{bmatrix} = \begin{bmatrix} x_2 \\ 0.1(u - x_2) \end{bmatrix} = \begin{bmatrix} \dot{\theta} \\ 0.1(T - \dot{\theta}) \end{bmatrix} \\
y = \theta$$
(2)

Formulating the state space equations.

$$\dot{x} = Ax + Bu 
\begin{bmatrix} \dot{\theta} \\ \ddot{\theta} \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ 0 & -0.1 \end{bmatrix} \begin{bmatrix} \theta \\ \dot{\theta} \end{bmatrix} + \begin{bmatrix} 0 \\ 0.1 \end{bmatrix} T$$
(3)

$$y = Cx$$

$$\begin{bmatrix} y \end{bmatrix} = \begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} \theta \\ \dot{\theta} \end{bmatrix}$$
(4)

Solving for the eigenvalues of the open-loop system.

$$0 = det(sI - A)$$

$$0 = det \begin{bmatrix} s & -1 \\ 0 & s + 0.1 \end{bmatrix}$$

$$0 = s(s + 0.1)$$

$$s = 0, -0.1$$

$$(5)$$

# 2. Design an observer for the above system.

- (a) Show that the system is observable.
- (b) Design L such that the error dynamics have  $f_n=50$  Hz and  $\zeta=0.7$ .
- (c) Provide a plot of the step response of the estimator.

# Solution:

To determine the observability of the system, the rank of the observability matrix is checked. For this system this must equal 2 (the dimension of A).

$$\mathcal{O} = \begin{bmatrix} C \\ CA \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} \tag{6}$$

$$rank(\mathcal{O}) = 2 \tag{7}$$

The system is observable and the poles of the observer can be placed using the dynamics defined.

$$0 = s^{2} + 2\omega_{n}\zeta s + \omega_{n}^{2}$$

$$0 = s^{2} + 2(2\pi f_{n})\zeta s + (2\pi f_{n})^{2}$$

$$0 = s^{2} + 2(100\pi)0.7s + (100\pi)^{2}$$

$$s = -219.91 \pm 224.35i = s_{obsv}$$
(8)

$$L = place(A', C', s_{obsv})' = \begin{bmatrix} 439.72 \\ 98652.08 \end{bmatrix}$$
 (9)

The new closed-loop A matrix.

$$A_{obsv} = A - LC = \begin{bmatrix} -439.72 & 1\\ -98652.08 & -0.1 \end{bmatrix}$$
 (10)

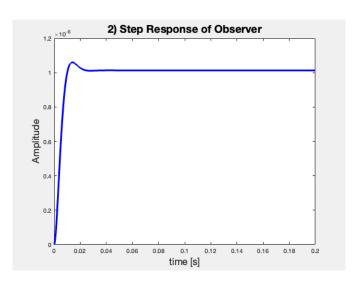


Figure 2: Observer Step Response.

- 3. Design a state-feedback controller for the table.
  - (a) Show that the system is controllable.
  - (b) Design K such that  $f_n = 10$  Hz and  $\zeta = 0.7$ .
  - (c) Provide a plot of the step response of the combined estimator and controller.

# Solution:

To determine the controllability of the system, the rank of the controllability matrix is checked. For this system this must equal 2 (the dimension of A).

$$C = \begin{bmatrix} B & AB \end{bmatrix} = \begin{bmatrix} 0 & 0.1 \\ 0.1 & -0.01 \end{bmatrix} \tag{11}$$

$$rank(\mathcal{C}) = 2 \tag{12}$$

The system is controllable and the poles of the controller can be placed using the dynamics defined.

$$0 = s^{2} + 2\omega_{n}\zeta s + \omega_{n}^{2}$$

$$0 = s^{2} + 2(2\pi f_{n})\zeta s + (2\pi f_{n})^{2}$$

$$0 = s^{2} + 2(20\pi)0.7s + (20\pi)^{2}$$

$$s = -43.98 \pm 44.87i = s_{cont}$$
(13)

$$K = place(A, B, s_{cont}) = \begin{bmatrix} 39478.40 & 878.65 \end{bmatrix}$$
 (14)

The new combined closed-loop system.

$$A = \begin{bmatrix} A - BK & BK \\ 0 & A - LC \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 & 0 \\ -3947.84 & -87.96 & 3947.84 & 87.86 \\ 0 & 0 & -439.72 & 1 \\ 0 & 0 & -98652.07 & -0.1 \end{bmatrix}$$

$$B = \begin{bmatrix} B \\ 0 \end{bmatrix} = \begin{bmatrix} 0 \\ 0.1 \\ 0 \\ 0 \end{bmatrix}$$

$$C = \begin{bmatrix} C & 0 \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 & 0 \end{bmatrix}$$

$$D = 0$$

$$(15)$$

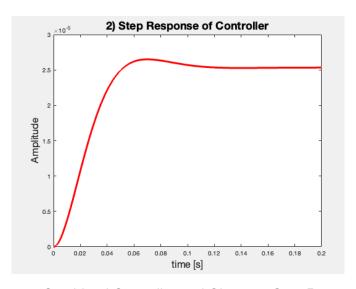


Figure 3: Combined Controller and Observer Step Response.

- **4.** Solve for the equivalent compensator for the system.
  - (a) What kind of classical compensator does it resemble?
  - (b) Calculate the closed loop transfer function.
  - (c) Plot the Bode Plot of the closed-loop system.
  - (d) Find the gain and phase margin.

## Solution:

Transforming the controller and observer defined above into an equivalent compensator results in the following system.

$$A_{comp} = A - BK - LC = \begin{bmatrix} -439.72 & 1\\ -102599.92 & -87.96 \end{bmatrix}$$

$$B_{comp} = L = \begin{bmatrix} 439.72\\ 98652.08 \end{bmatrix}$$

$$C_{comp} = -K = \begin{bmatrix} -39478.40 & -878.65 \end{bmatrix}$$
(16)

With an equivalent transfer function of:

$$\frac{U(s)}{Y(s)} = C_{comp}(sI - A_{comp})^{-1}B_{comp} = -K(sI - A + BK + LC)^{-1}L$$

$$= \frac{-1.04(10^8)s - 3.896(10^9)}{s^2 + 527.7s + 1.413(10^5)}$$
(17)

This resembles a "lead-lag" compensator because of the extra pole in the denominator (first order numerator, second order denominator).

The closed-loop transfer function is calculated similarly to the compensator transfer function but uses the B and C matrices from the system dynamics.

$$\frac{U(s)}{Y(s)} = -C(sI - A + BK + LC)^{-1}B$$

$$= \frac{-0.1}{s^2 + 527.7s + 1.413(10^5)}$$
(18)

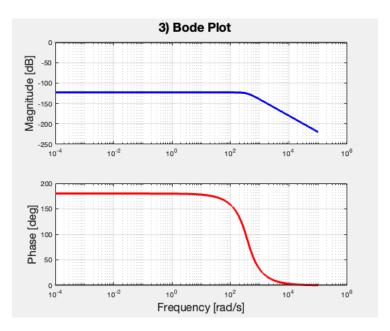


Figure 4: Closed-Loop Compensator Bode Plot.

Using the MATLAB function margin, the gain and phase margin are easily calculated and can be confirmed by analyzing the Bode Plot above.

$$G_m = 123.0 \, \mathrm{dB}$$
 
$$\phi_m = \infty \, \mathrm{dB}$$
 (19)

- 5. Design the controller in the discrete domain assuming a 1 KHz sample rate.
  - (a) Discretize the state space model. Where are the eigenvalues?
  - (b) Design L to provide the same response as problem 2.
  - (c) Design K to provide the same response as problem 3.
  - (d) Where are the closed-loop estimator and controller poles located?

(e) Solve for the equivalent compensator transfer function.

## Solution:

To discretize the continuous model, the MATLAB function c2d was used in combination with ss to transform the continuous model into state-space.

$$sys = c2d(ss(A, B, C, D), 1/1000)$$

$$A_z = \begin{bmatrix} 1 & 0.001 \\ 0 & 0.999 \end{bmatrix}$$

$$B_z = \begin{bmatrix} 5(10^-8) \\ 1(10^-4) \end{bmatrix}$$

$$C_z = \begin{bmatrix} 1 & 0 \end{bmatrix}$$

$$D_z = 0$$
(20)

To find the discrete poles,  $s_{obsv}$  and  $s_{cont}$  must be converted to discrete poles.

$$z = e^{sT}$$

$$z_{obsv} = e^{s_{obsv}*T} = e^{(-219.91 \pm 224.35i)*1/1000} = 0.7825 \pm 0.1786i$$

$$z_{cont} = e^{s_{cont}*T} = e^{(-43.98 \pm 44.87i)*1/1000} = 0.9560 \pm 0.0429i$$
(21)

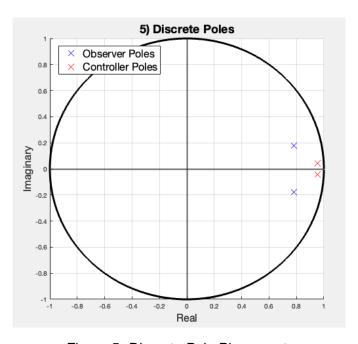


Figure 5: Discrete Pole Placement.

These new poles can then be used in the MATLAB place function to create the discrete observer and controller.

$$L = place(A'_z, C'_z, z_{obsv})' = \begin{bmatrix} 439.72 \\ 98652.08 \end{bmatrix}$$

$$K = place(A_z, B_z, z_{cont}) = \begin{bmatrix} 39478.40 & 878.65 \end{bmatrix}$$
(22)

Using the same method of finding the compensator transfer function from above:

$$\frac{Y(z)}{U(z)} = -K_z(zI - A_z + B_zK + L_zC_z)^{-1}L_z$$

$$= \frac{-8.451(10^4)z + 8.152(10^4)}{z^2 - 1.477z + 0.594}$$
(23)

6. Compare the continuous and discrete response using simulation and using equivalent compensator. Plot the simulated and equivalent compensator responses. Compare the expected and actual response.

#### Solution:

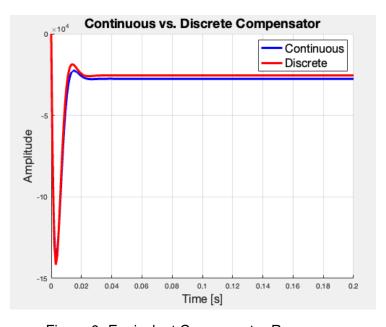


Figure 6: Equivalent Compensator Response.