

# PLANETS 望遠鏡の開発 能動主鏡支持機構などを 用いた最終研磨量削減の試み

Development of PLANETS telescope:  
An attempt to reduce polishing volume  
in final polishing process by using an active mirror support

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関連投稿 : P-CG18-P03

High dynamic range observation using a 1.8-m off-axis telescope PLANETS: feasibility study and telescope assembly

# Summary

2

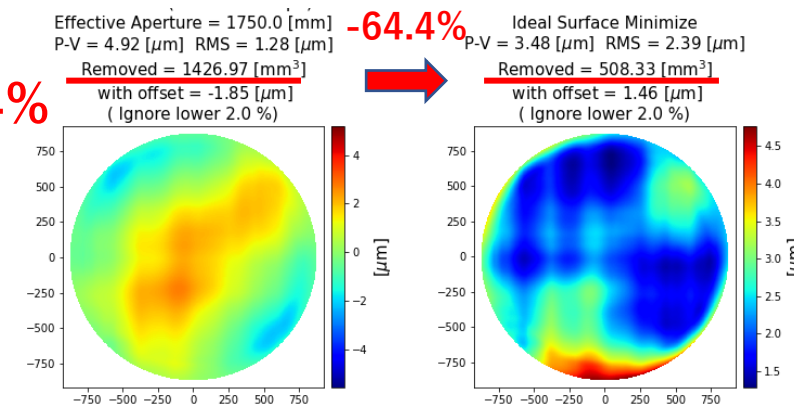
Background : PLANETS is 1.85m telescope with **off-axis parabola (OAP)** for the observation of the planetary faint atmosphere and plasma

The final polishing process of the primary mirror (M1) will be held in June 2021

Purpose : In the final polishing process, small polishing volume is desirable.

Method : A : Tuning OAP parameters to find best-fit parameters  
B : Correcting the surface figure error with the active support mechanism

Result : With only A method, **polishing volume is reduced 64.4%**  
With combination of A and B method, reduced 67.5%  
FEM model doesn't simulate actual surface accurately



Discussion : **It is effective to reduce polishing volume by tuning the OAP parameters**

For current M1 surface error, we will only use method A

## Key technology

- 1.85m telescope with **off-axis parabola (OAP)**
- The primary mirror (M1) is mounted on the active support system
- Various observation equipment : coronagraph, polarimetry, and high-resolution spectroscopy
- Will be installed at the **Haleakala observatory**, Hawaii in collaboration with Japan, USA, Germany, and Brazil

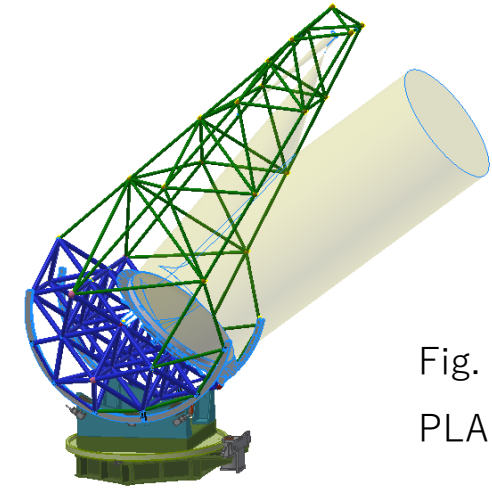


Fig. 1 :  
PLANETS overview

## Strength

- Low-scattered optics
- High-dynamic range (HDR) observation
- Long-term continuous observations



## Scientific targets

Faint atmosphere and plasma emission near bright body

- Icy moons' atmosphere (Europa, Enceladus)
- Magnetospheric plasma (Io plasma torus, etc.)
- Escaping plasma and neutrals (Mars, Venus)

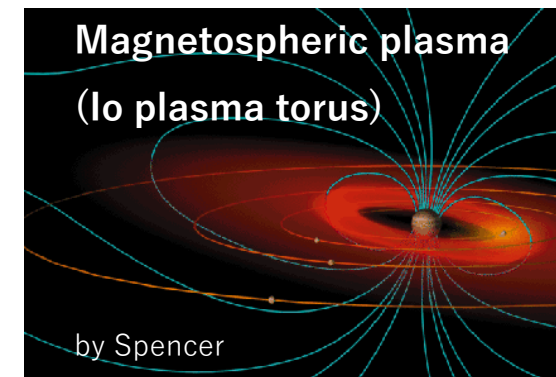


Fig. 2 : Scientific targets

# Previous study of active support structure

## TMT (Thirty Meter Telescope)

- 30m telescope with segmented mirrors
  - To compensate for residual polishing errors, installation errors, gravity effects and parasitic forces in the whiffletree support, each segment is equipped with 21 warping harness mechanisms
  - The WH mechanism consists of a Linear Actuator, Ball Link and a Leaf Spring with strain gauge sensor
  - With active support, measured Zernike modes were within 4% of commanded modes

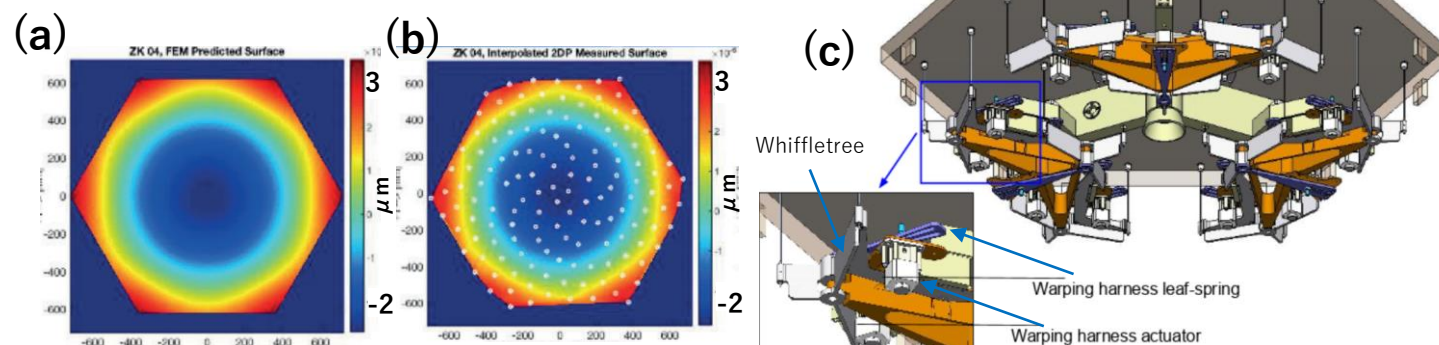


Fig. 3 : TMT warping harness and whiffletree (Visser et al. 2017)

- (a) Predicted surface in FEM (Zernike 4<sup>th</sup>) (PV=6.276 $\mu$ m, RMS=1.597 $\mu$ m)
- (b) Interpolated 2D profilometry measured surface (PV=1.663 $\mu$ m, RMS=5.549 $\mu$ m)
- (c) Leaf springs are used to apply a moment to the whiffletree

## DKIST (Daniel K. Inouye Solar Telescope)

- 4.2m off-axis solar telescope
  - Consists of 118 axial actuators and 24 lateral actuators, and each axial support force is about 220~280N
  - Uses active support in polishing and metrology process, but the adjustment for each actuators is about -2.5~+2.5N (only 1% of the support force)

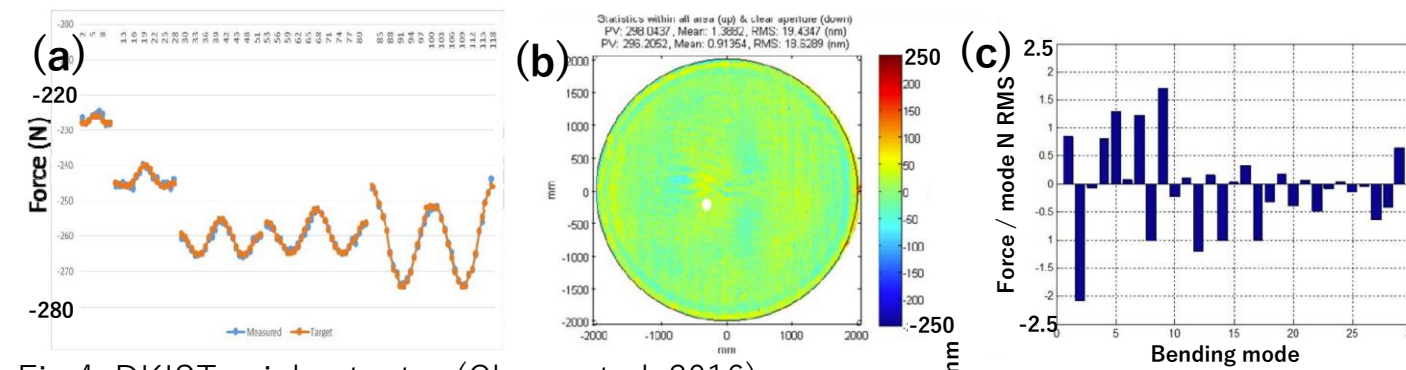


Fig 4. DKIST axial actuator (Chang et al. 2016)

- (a) Targeted supported force distribution and measured force in each axial actuator
- (b) Surface measurement from CGH null interferometry (PV=296.2nm, RMS=18.63nm)
- (c) Modal correction force

# Purpose

## Surface measurement and polishing of OAP

- In order to compensate for several surface errors in observation, PLANETS adopts whiffletree and active support (warping harness), and they can also be applied to the final measurement and polishing process
- Large volume of mirror material to be removed by polishing (polishing volume) leads to an increase in the time and cost required.

➤ **Purpose : To reduce polishing volume**

We will reduce the polishing volume by using both of the following two methods.

- Tuning off-axis paraboloid parameters**
- Correcting the surface figure error with the active support mechanism**

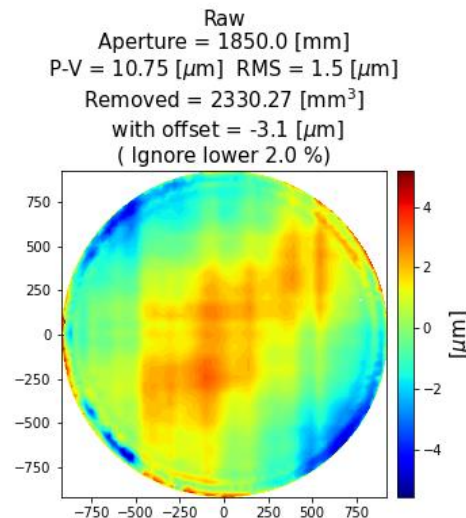


Fig. 5 : Current M1 surface error

The final polishing aims to achieve the surface error  $< 20 \text{ nm}$  RMS for 30-cm spatial scale.

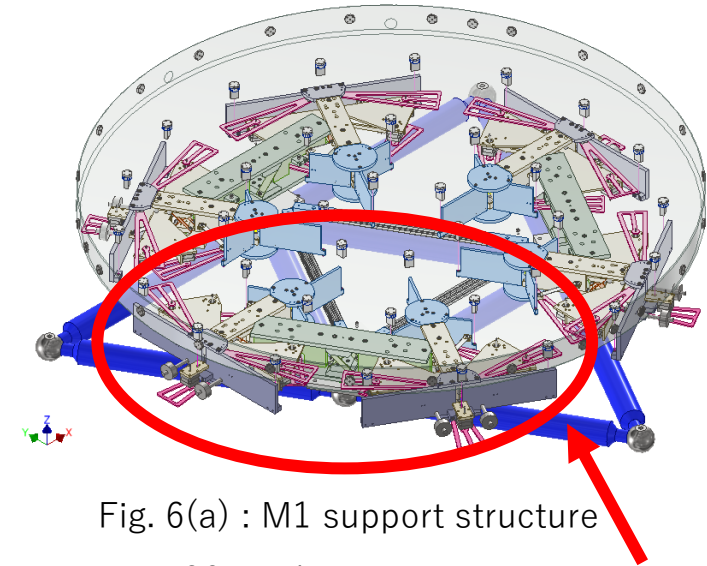


Fig. 6(a) : M1 support structure uses 36 axial actuators

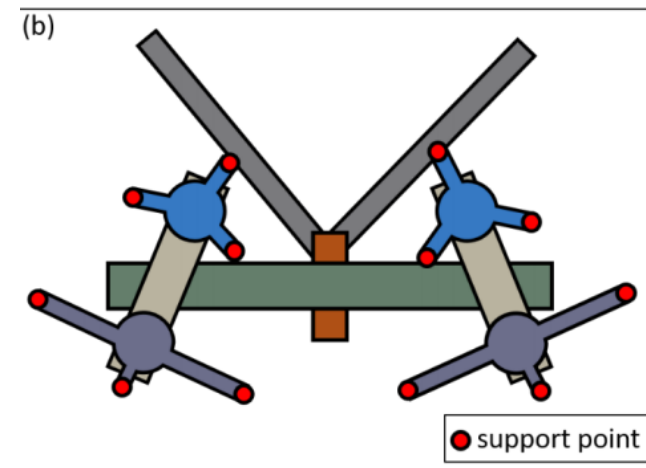


Fig. 6(b) : Enlarged view

Support structure is  $120^\circ$  symmetric



# A : Tuning off-axis paraboloid (OAP) parameters

## Original OAP

- $p = 8667$  mm :  
Radius of curvature
- $q = 1800$  mm :  
Off-axis distance
- $\Phi = 0$  mrad :  
Rotation angle  
on the support structure



Tuning params

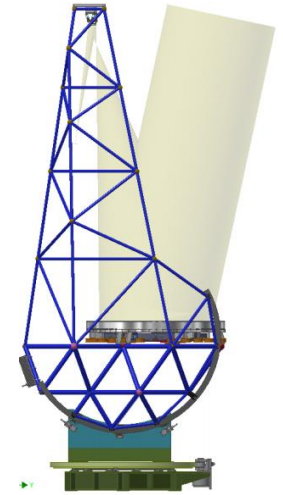
$$p = 8667 \pm 100 \text{ mm}$$

$$q = 1800 \pm 100 \text{ mm}$$

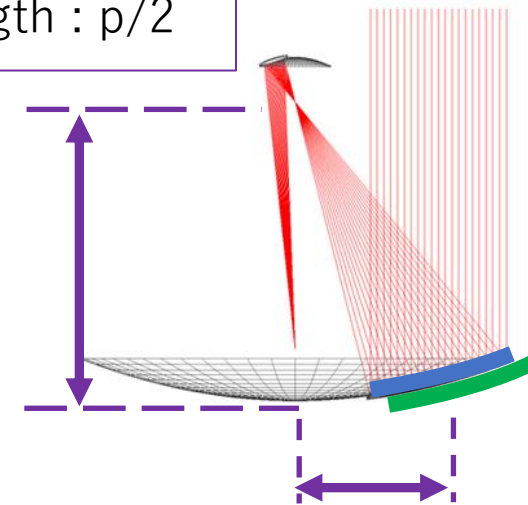
$$\Phi = 0 \pm 10 \text{ mrad}$$

## Tuned OAP

- Change of parameters ( $p, q, \phi$ )  
deform surface figure
- Polishing volume is minimized with  
best-fit parameters



Focal length :  $p/2$



Off-axis distance :  $q$

Fig. 9 : each parameters

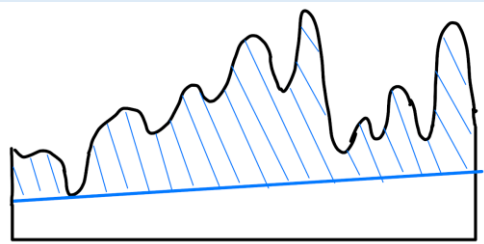


Fig.7 : original OAP  
(Large polishing volume)



e.g.) make tilt smaller  
using longer  $q$

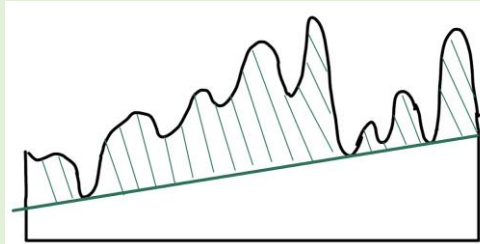


Fig.8 : Tuned OAP  
(Small polishing volume)

# B : Correcting the surface figure error with the active support

## ◆ Active support in general telescope

- **Adjust mirror surface error** due to posture change and manufacturing error of support structure in observation

## ◆ Active support in PLANETS

- Also used in the final polishing process

- Active support consists of 36-point whiffletree and 33 warping harness (leaf springs and linear motors to control the support force at each support point)
- **We also use the active support to reduce polishing volume by decreasing the surface figure error on large spatial scale**
- Active support is mainly used in observation, so small motor drive amount is desirable in polishing process.

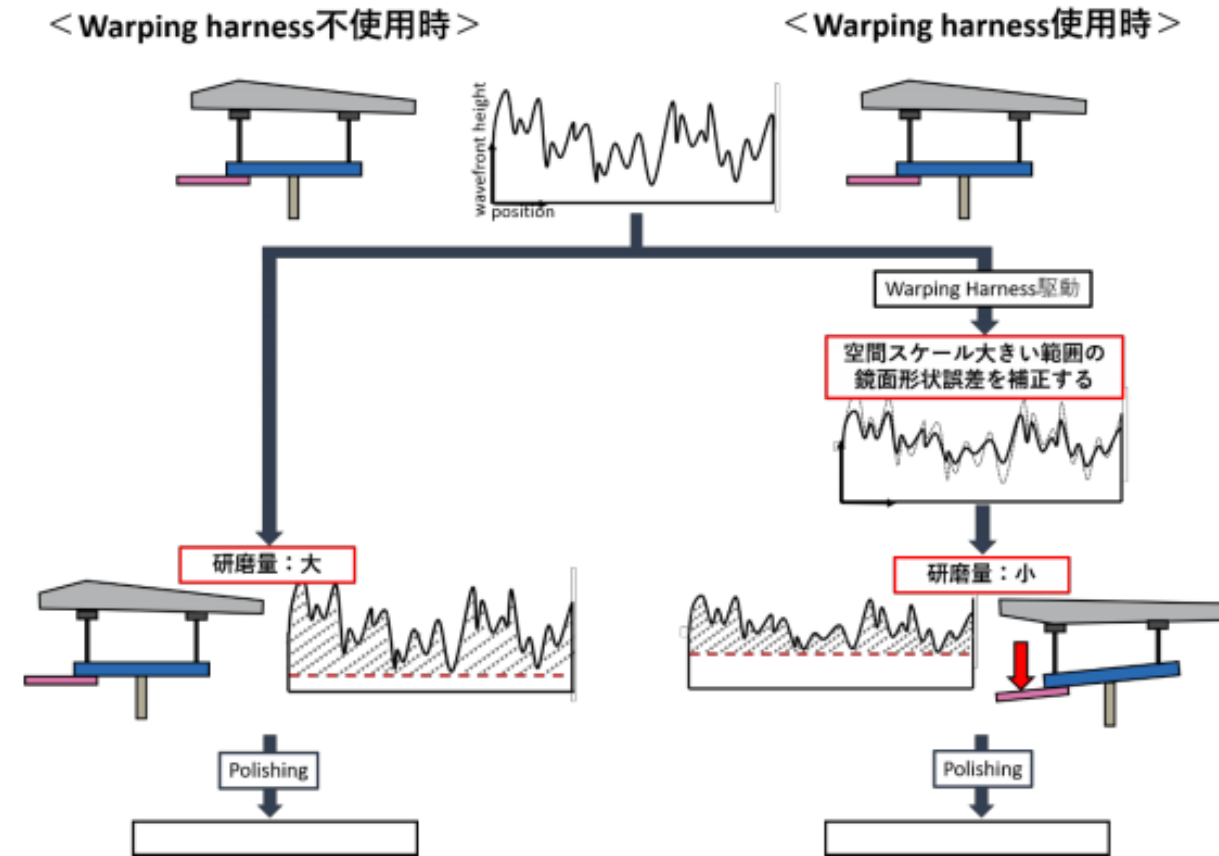


Fig. 10 : Reduce polishing volume with active support (Suzuki 2019)

# Combination result of A and B

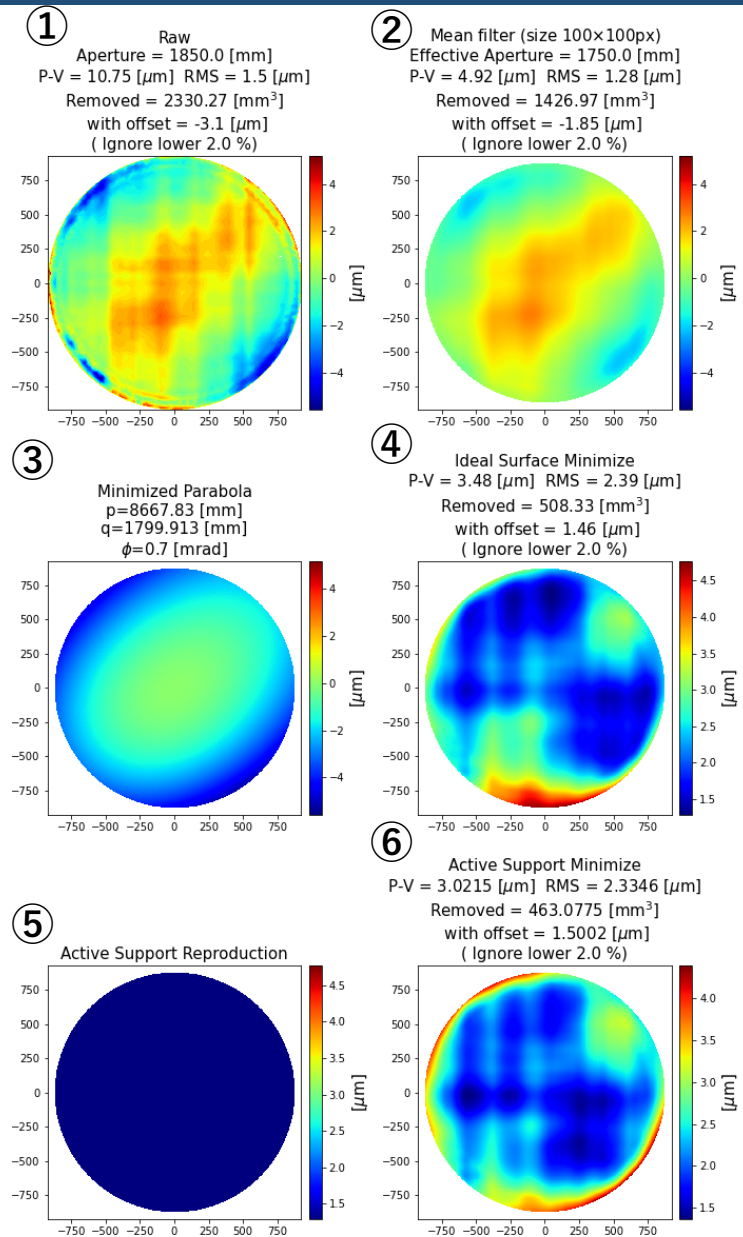
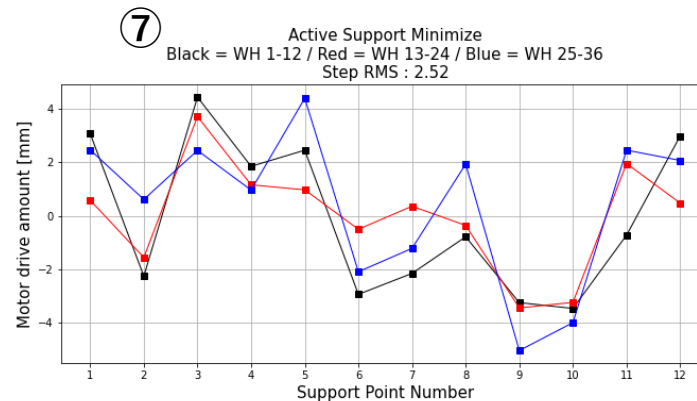


Fig. 11 : Procedure of minimization

- ① Current M1 surface error
- ② Smoothing for ① (to exclude outliers)
- ③ Best-fit OAP for ②
- ④ Residual from ② to ③
- ⑤ Reproduction by active support to ④ simulated in finite element method (FEM)
- ⑥ Residual from ④ to ⑤ (Removed in final polishing)
- ⑦ Motor drive amount for ⑤ (plotted every 120 degrees)



## ● Current M1 status :

- P-V :  $4.92 \mu\text{m}$
- RMS :  $1.28 \mu\text{m}$
- polishing volume :  $1426.97 \text{ mm}^3$

## ➤ Only by tuning OAP parameters :

- P-V :  $3.48 \mu\text{m}$
- RMS :  $2.39 \mu\text{m}$
- polishing volume :  $508.33 \text{ mm}^3$
- **Reduced : 64.4%**

## ➤ If B is also used (combination of A and B):

- P-V :  $3.02 \mu\text{m}$
- RMS :  $2.33 \mu\text{m}$
- polishing volume :  $463.08 \text{ mm}^3$
- **Reduced : 67.5%**
- The maximum motor drive amount of  $\pm 5\text{mm}$  is almost used up (e.g. WH03, 29, 33)



# Control repeatability and stability of active support

- Give a drive amount for each actuator and measure local tilt in M1 with autocollimator
  - Measure local tilt in the center of M1 and 40mm from the edge
  - Calculate the difference of local tilt (edge - center) and compare with the result of FEM model
  - Check the control repeatability and stability of active support structure
  - Update FEM model



- Repeatability and stability
  - Currently being analyzed.  
(Please check the additional resources)
- FEM model
  - doesn't simulate actual surface accurately
    - Not a perfect reproduction of the whiffletree structure
    - In the final measurement process, we use three-probe method with robot-arm. Spatial distribution smaller than the spatial resolution of the method can't measure
    - Necessary to consider the stability when combined with the Optical support structure in the future

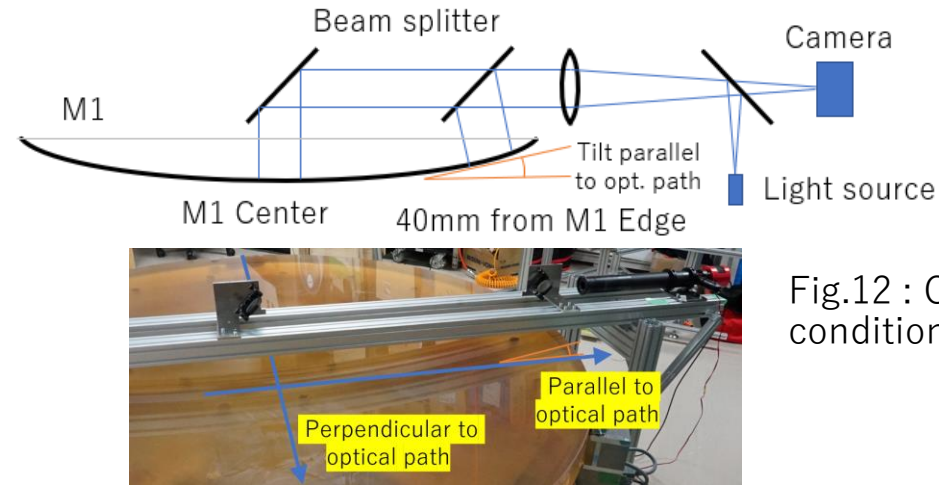


Fig.12 : Optical path and actual condition of the experiment

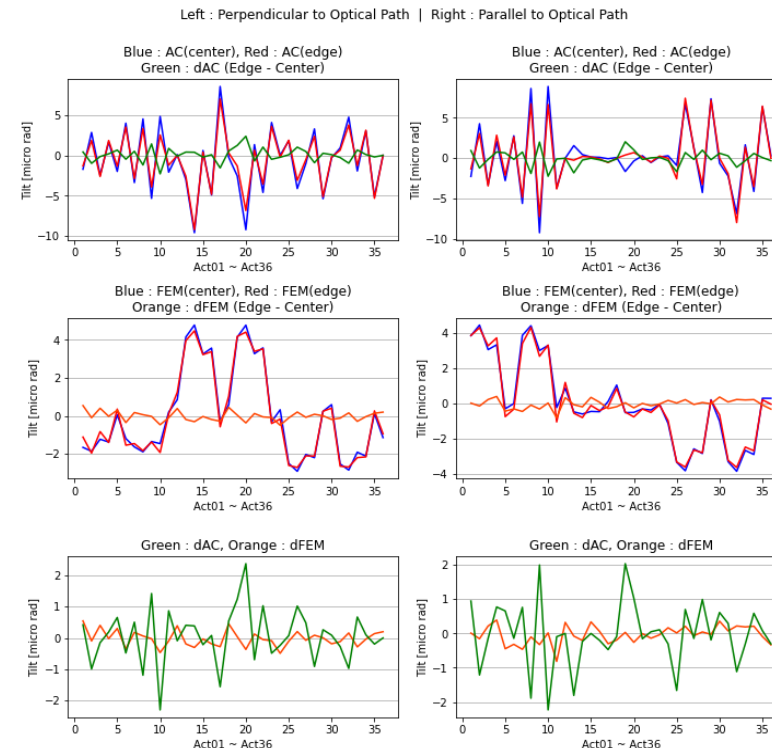


Fig. 13

- By calculating the difference between the tilt of the center and the edge, the influence of entire tilt can be removed.

# Discussion

- OAP surface shape is deformed by each parameters ( $p$ ,  $q$ ,  $\phi$ ) and each minute deformation is a linear superposition
  - Current surface shape can be roughly reproduced by superimposing deformations by  $p$  and  $\phi$
- Depending on the mirror surface error, it is effective to reduce polishing volume by tuning the OAP parameters
- In current surface shape, method B (reduce polishing volume with active support) is unnecessary
  - Only 3% improvement compared to A alone  
(Only A : 64.4%  $\rightarrow$  A+B : 67.5%)
  - The maximum motor drive amount of  $\pm 5\text{mm}$  is almost used up, and leaving no room for correction during observation

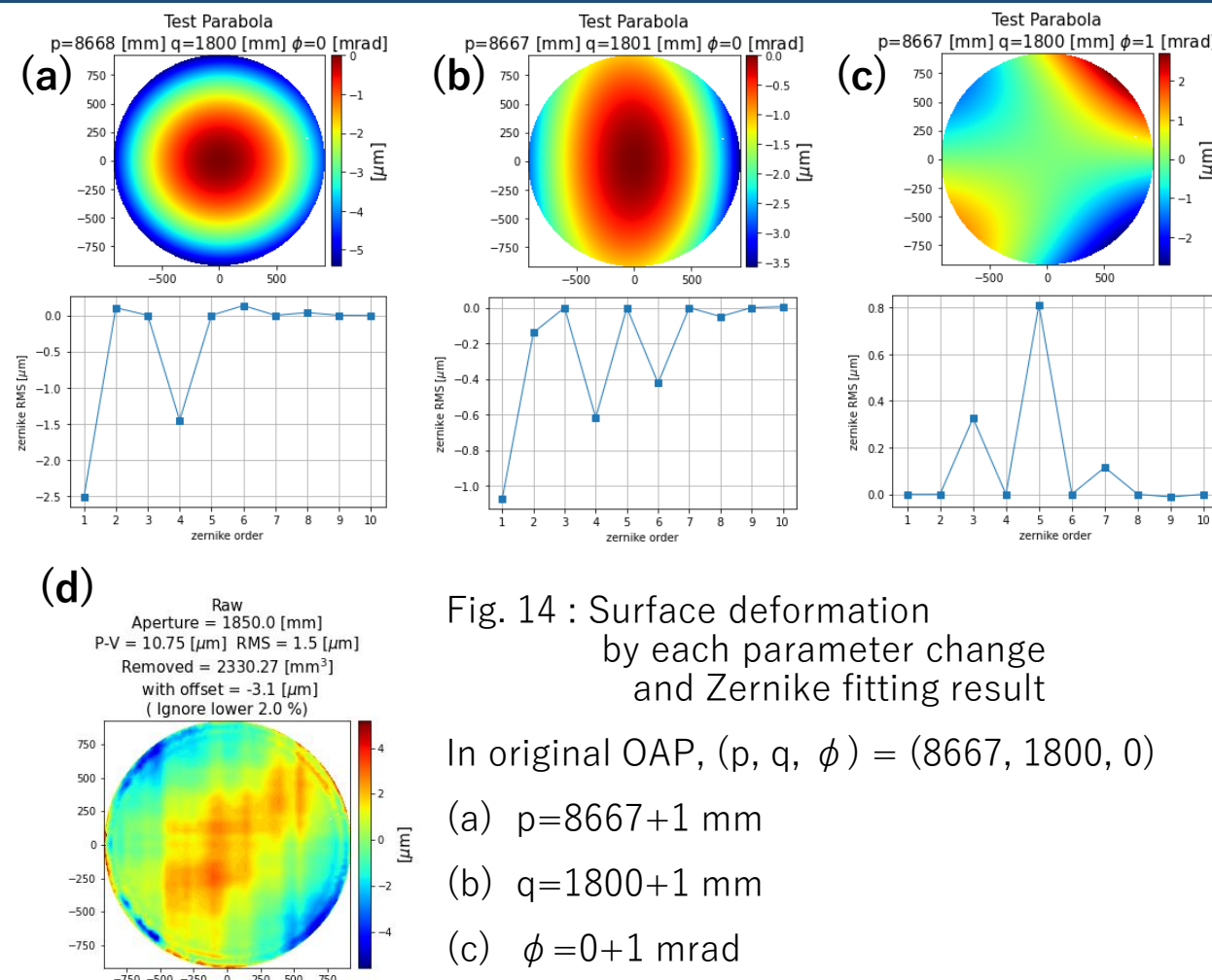


Fig. 14 : Surface deformation by each parameter change and Zernike fitting result

In original OAP, ( $p$ ,  $q$ ,  $\phi$ ) = (8667, 1800, 0)

(a)  $p=8667+1$  mm

(b)  $q=1800+1$  mm

(c)  $\phi=0+1$  mrad

(d) Current M1 status

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