

Photonic Analog-to-Digital Converters A Tutorial

George C. Valley
Electronics and Photonics Laboratory
The Aerospace Corporation
george.valley@aero.org
310-336-0336

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Coworkers

The Aerospace Corp: Jason Chou, Josh Conway, George Sefler, Bob Walden

University of California: Los Angeles: Shalabh Gupta, Bahram Jalali

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Outline

- What is a photonic ADC?
- Electronic ADC basics—sampling and quantization
- State of the art:
 - ADCs
 - Interleaved digitizers
 - Digital oscilloscopes
- Classes of photonic ADCs: Photonic-
 - Assisted
 - Sampled
 - Quantized
 - Delta-sigma modulator
- Microwave photonic links in photonic ADCs
- Examples of photonic ADCs
- Recent results time-stretch ADCs
 - 10 Terasample/second transient digitizer
 - 7-ENOB 10 GHz 2-channel ADC
 - 150 Gigasample/second continuous time digitizer
- Summary



What is a photonic analog-to-digital converter?

- Optical signal
 - Input analog optical signal
 - Output digital optical signal
 - Relatively little work here
 - Most analog optical signals are incoherent light
- RF signal
 - Input analog electronic signal
 - Do something to electronic signal using photonics
 - Output digital electronic signal
 - Most photonic ADC work is here



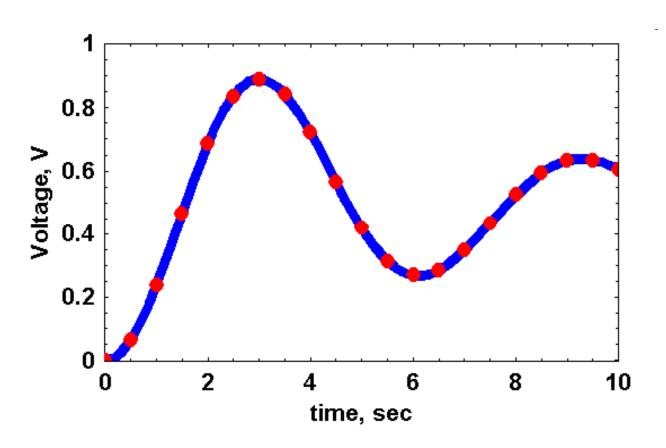
Sampling rate and number of bits

- Familiar quantities
 - Sampling rate—e.g. CD 44.1 kHz or kilo sample/sec (kS/s)
 - Number of read-out bits (stated bits)—CD 16 bits
- More useful characterizations of ADC performance
 - Input bandwidth—e.g. CD 20 Hz to 20 kHz
 - Nyquist sampling theorem says sampling rate must be > 2 x bandwidth
 - ADC noise bandwidth = input bandwidth
 - Effective number of bits (ENOB)
 - Depends on Signal-to-Noise-and-Distortion Ratio (SNDR)
 - Factor of 4 (6 dB) in SNDR gives 1 additional bit.
 - Need SNDR > 96 dB to fully utilize CDs 16 bits
 - Need SNDR > 144 DB to fully utilize the DVD audio disk's 24 bits



Sample and Hold

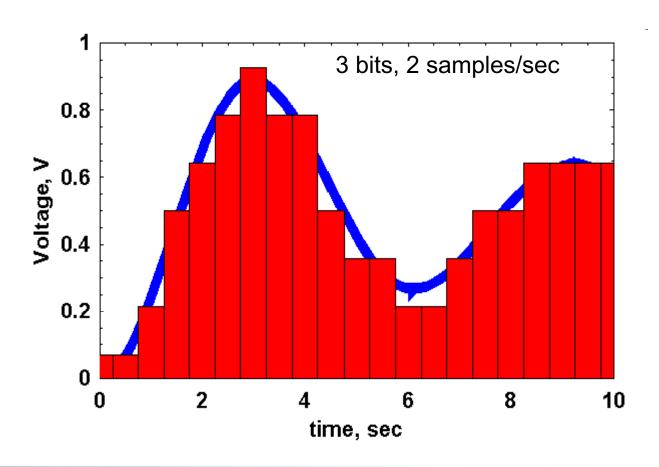
ADC Step 1: Sample and hold an RF signal in time





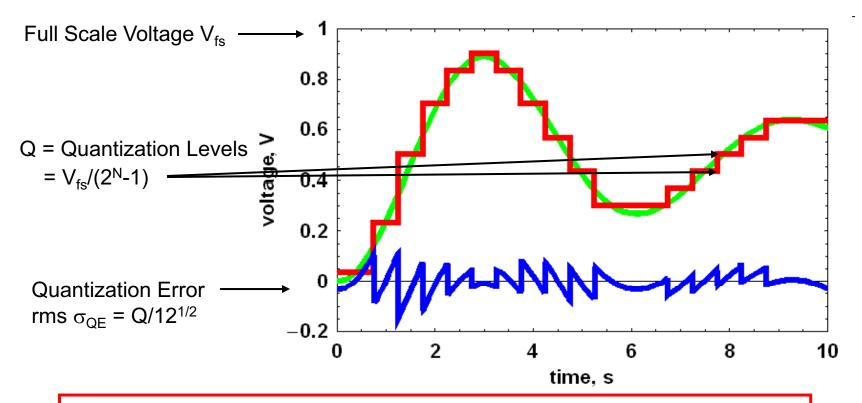
Quantize Voltage

ADC Step 2: During sample time quantize the voltages in 2^{N} -1 levels. N = number of bits (stated bits or read-out bits)





Quantization Error



Quantization error is intrinsic to an ADC Non-idealities usually cause errors with rms greater than Q/12^{1/2}



How do you calculate ENOB?

- Relate the number of bits N in an ideal ADC to the signal-to-noise ratio
- Quantization noise is the only noise in an ideal ADC

$$-$$
 SNR_{QE} = 20 $log_{10}(V_{rms}/\sigma_{QE})$

$$-V_{rms} = V_{fs}/(2^{3/2})$$
 for a sine wave

$$-V_{fs} = (2^N - 1)^{1/2}Q$$

$$-\sigma_{QE} = Q/12^{1/2}$$
 for a sine wave

Solve for N in terms of SNR_{QE}

$$- N = [SNR_Q - 20 \log_{10}(12^{1/2}/2^{3/2})]/(20 \ln 2/\ln 10)$$

$$-N = (SNR_Q - 1.76)/6.02$$

- The effective number of bits (ENOB) is defined by analogy as
 - ENOB = (SNDR-1.76)/6.02 with SNDR in dB

The factor of 6.02 reflects the notion that to improve ENOB by 1 bit, either the full-scale voltage must be increased by 2 x or the rms noise (and distortion) must be reduced by 2 x.



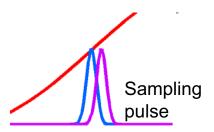
Other sources of error

Noise and other non-idealities reduce ADC resolution

- Amplitude Errors
 - Noise
 - Thermal
 - Shot
 - Spontaneous emission
 - RIN
 - Nonlinearities
 - Harmonics at frequency: $2 \omega_S 3\omega_S ...$
 - Intermodulation products (spurs) at freq.:

$$\omega_1$$
- ω_2 , ω_1 - $2\omega_2$, ω_2 - $2\omega_1$

- Optical nonlinearities
- Timing Errors
 - Clock jitter
 - Circuit response time (RC time constant, carrier lifetimes, Comparator ambiguity)





Comments on timing error

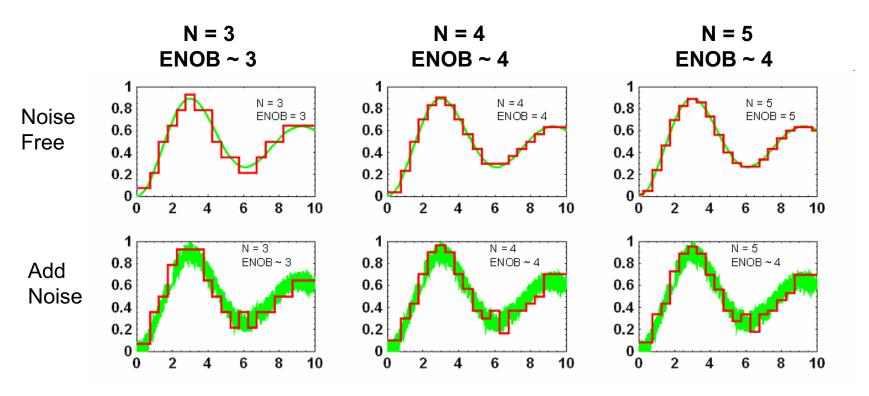
- Estimate required timing jitter
 - Voltage error roughly $V_{fs}/(12^{1/2} 2^{ENOB})$
 - Equivalent error in the time domain suggests Timing jitter should be $T_{\rm sample}$ /($12^{1/2}~2^{\rm ENOB}$)
 - Detailed calculations give ENOB = $log_2[1/(3^{1/2} \pi f_s \sigma_i)]$
 - Example: ENOB = 24, 96 kS/s requires ~100 fs jitter
- Time to perform quantization is 1/(sampling rate)
 - Electronic comparator must decide between two adjacent voltage levels in time $1/f_s$
 - For voltages midway between levels quantization, this is relatively easy
 - For voltages near a quantization level, the decision process slows down

Timing jitter and comparator ambiguity are the most important limitations on the performance of high speed ADCs



Difference between ENOB and read-out bits N

Example: amplitude noise limits effective number of bits (ENOB)



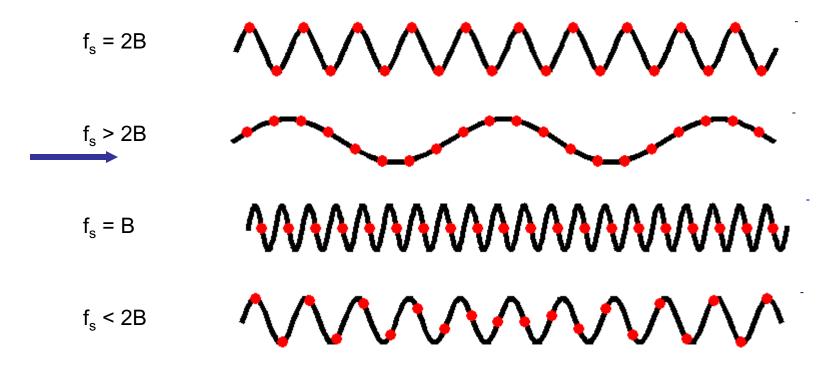
Achieving one additional effective bit requires 6dB increase in SNDR

Taking a 4-ENOB prototype system to 10 ENOB requires increasing SNDR by 36 dB ~ 4,000 !



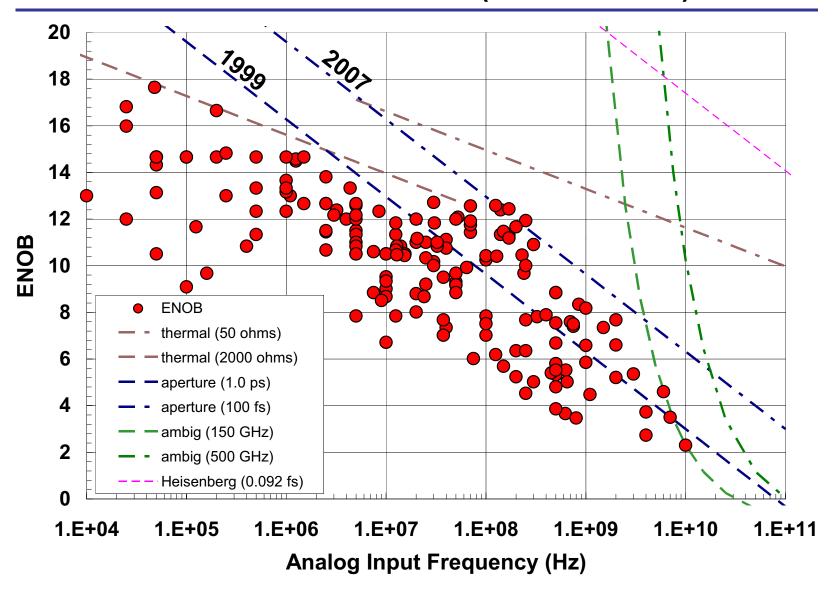
Nyquist-Shannon Sampling Theorem

Given a continuous time signal whose maximum bandwidth is B, perfect reconstruction can be obtained if the sampling rate f_s is greater than 2 B.





ADC State-of-the-Art (Walden 2008)





Modules and Digital Oscilloscopes

- Maxtek Data Converter Module: 6.25 GHz, 6.6 ENOB
- Agilent Digital Oscilloscope: 13 GHz, ~5 ENOB
- Tektronix Digital Oscilloscope: 20 GHz, ~ 5 ENOB
- LeCroy Digital Oscilloscope: 18 GHz, ~ 5 ENOB
- ADC Definitions
 - Real-time digitizers
 - Single chip ADC
 - Interleaved digitizer (2 or more ADC chips)
 - Digital Oscilloscope (Interleaved digitizer plus storage, display, processing etc.)
 - Sampling Oscilloscope—not real time
 - Digitizes repetitive waveforms



Where are photonic ADCs needed?

Rule of Thumb:

Viable photonics systems must either provide substantial improvement over electronics or provide completely new functionality unavailable in electronics.

- Why?
 - High rate of progress of electronics
 - Non-recurring engineering costs of photonic systems
 - Complexity of photonic systems
- From Walden's chart a 2 ENOB margin over electronics implies

Input Bandwidth	ENOB
1 GHz	>10-11
6 GHz	>8-9
20 GHz	>7
>20 GHz	>3



Estimate power consumption for a photonic ADC?

- Figure of merit for ADCs
 - Energy per conversion step (pJ/cs)

- Best electronic results: ~0.2 pJ/cs @ ~50MHz
- At 1-10 GHz electronic ADCs consume 10-100 pJ/cs!
- Estimate power consumption for

10 ENOB, 10 GS/s (10/10) electronic ADC

 $- @ 0.2 \, pJ/cs$: $P = 2 \, W$

- @ 10 pJ/cs: P = 100 W

- @ 100 pJ/cs: P = 1000 W

Photonic 10/10 ADC would be attractive at P < 10W

Can a photonic ADC achieve < 1 pJ/cs in the GHz band?



Classes of Photonic ADCs

Photonic Assisted

RF signal not modulated on optical beam. Photonics helps electronic ADC. Photonic Sampled

RF modulated on Pulsed optical beam. Use low Jitter of mode-Locked pulses To reduce Sampling jitter Photonic Quantized

RF modulated on cw optical beam. Photonic process aids or replaces electronic quantizer. Photonic Sampled & Quantized

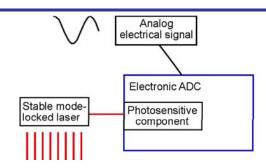
RF modulated on Pulsed optical beam. Photonic process aids or replaces electronic quantizer.

All photonic ADCs in these classes contain analog optical links

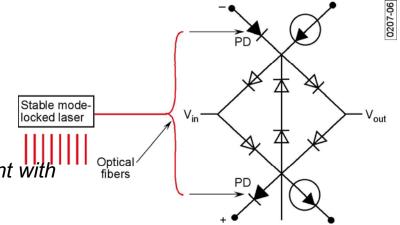


Photonics Assisted ADCs

- Generic version
 - Origins in Auston switch (1975)
 - Mode-locked laser at Nyquist rate



- Optically clocked Track and Hold (Jacobs et al. 2004)
 - Ultra-stable mode-locked laser source switches electronic track and hold circuit-
 - Bridge turns off when photodiodes are illuminated
 - Benefits
 - Reduced aperture time
 - High clock isolation
 - Low clock jitter
 - Optical clock distribution
 - Results—1 GS/s track and hold consistent with
 - 11.8 SFDR bits, 9.6 SNR bits



Photonics-assisted approach—no RF modulator Careful path matching required to maintain timing



Analog Optical Links

Consider a *lossless* analog optical link with shot, thermal and RIN noise

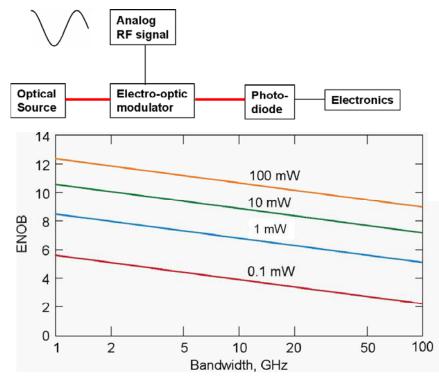
$$CNR = \frac{(mRP)^2/2}{(\sigma_s^2 + \sigma_{th}^2 + \sigma_{RIN}^2)}$$

With no nonlinear distortion

$$ENOB = [CNR(dB)-1.76]/6.02$$

Best case parameters

$$m = 0.5, R = 1 \text{ A/W}, R_{load} = 50 \Omega, RIN = 0$$



10 ENOB at 10 GHz requires > 30 mW at the Photodiode



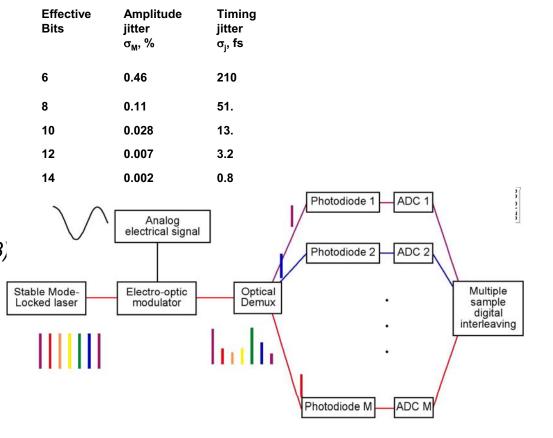
Photonic Sampled ADC

- Three variants
 - Optical sampling to a single high rate ADC

Optical sampling with wavelength or time demultiplexing to a bank of lower rate

ADCs

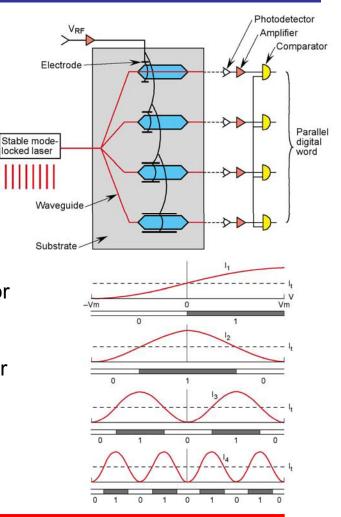
- Requirements on laser source @ 5 GHz
- Results
 - 12 ENOB at 208 MS/s
 - 10 ENOB at 505 MS/s
 (Williamson et al. 2003)
 - 4 ENOB at 100 GHz (Clark et al. 1999)





Photonic sampled and quantized: Intensity quantization

- Taylor scheme (1979) and variants produced interesting photonic ADCs thru the 1980s.
- Issue: each extra bit requires another factor of 2 in the longest modulator. Eventually drive voltage or insertion loss become prohibitive.
- Recent work
 quantizing optical intensity with semi-conductor
 saturable absorbers,n₂ nonlinearity, cross phase modulation, self-phase modulation,
 solitons, supercontinuum generation, nonlinear
 optical loop mirrors, microring resonators ...

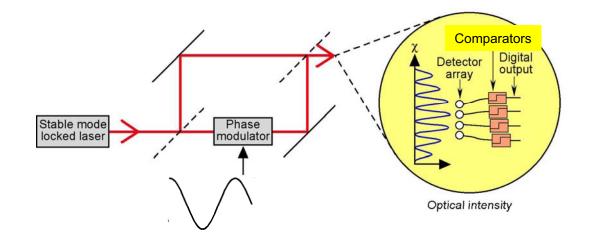


Low loss modulators ($V_{pi} \sim 0.1 \text{ V}$) would revive interest in Taylor's scheme



Photonic sampled and quantized: Angle quantization

- The very first photonic ADC (Wright et al. 1974) used angle modulation
- Most angle modulators are too slow to compete with today's electronics
- Stigwall and Galt (2005, 2006) developed a system in which an electro-optic phase modulator shifts an optical interference pattern incident on an array of detectors.
- Issues
 - Speed
 - ENOB
 - Path Loss



Advantage: phase modulation is linear



Photonic sampled and quantized:Photonic $\Delta\Sigma$ modulator

First order $\Delta\Sigma$ modulator

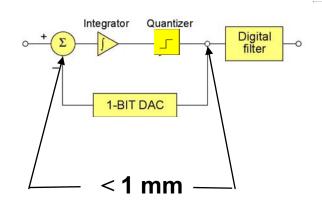
Required components for a $\Delta\Sigma$ modulator

Adder

Integrator

Quantizer

Feedback DAC



Electronic $\Delta\Sigma$ modulators now operate at ~20 GHz

Photonic $\Delta\Sigma$ modulator at 200 GHz. Clock period = 5 ps => 1 mm (n = 1.5)

In a $\Delta\Sigma$ modulator need feedback delay < clock period

In a $\Delta\Sigma$ modulator need quantizer response time << clock period

Really want at least 2^{nd} order $\Delta\Sigma$ modulator to take advantage of oversampling

The challenges of building multiple, integrated, all-optical adders, integrators and quantizers in 1 mm seem daunting

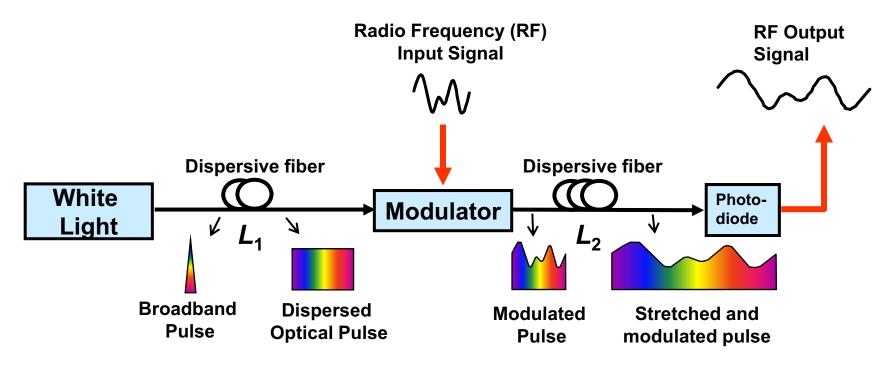


Recent results on time-stretch ADCs

- 10 Tera-sample per second digitization of 90 GHz waveform
 - Stretch ratio 250
 - ENOB ~ 3 @ 50 GHz
 - Transient digitizer
 - Chou et al. 2007
- 2-channel 10 GHz system
 - Stretch ratio 10
 - ENOB ~ 7 @ 10 GHz
 - Scalable to continuous time
 - PHOBIAC, Sefler et al. 2008
- 150 GS/s 4 channel system
 - Stretch ratio 3
 - Continuous time
 - Input bandwidth to 48 GHz
 - ENOB ~ 3 @ 10 GHz
 - Chou et al. 2008



Conceptual Diagram—Time-stretch ADC

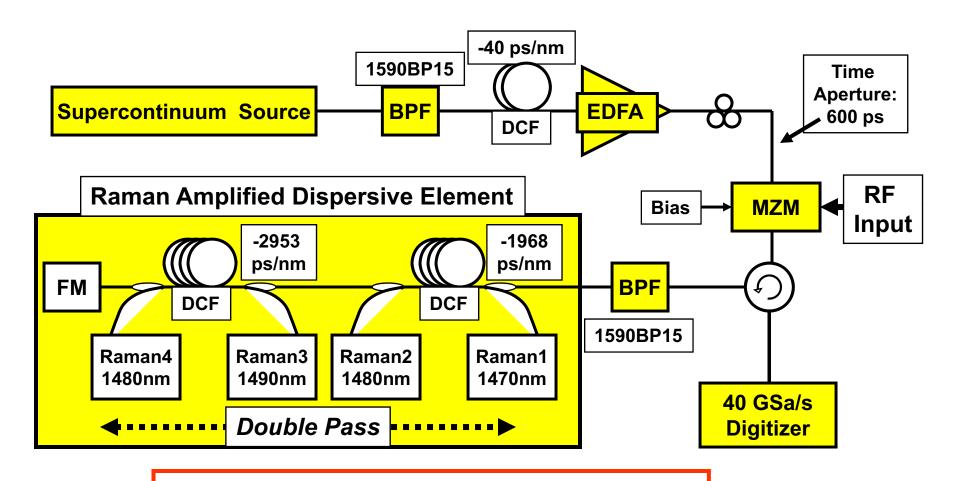


- RF signals are modulated on to the envelope of a dispersed optical pulse
- Dispersion is used a second time to temporally stretch the RF signal and optical pulse
- Stretch Ratio M is related to the fiber dispersions D_1 , $D_2 \sim$ fiber length

$$M = (L_1 + L_2) / L_1$$



10 TSample/s Real-Time Digitizer Schematic (Chou et al. 2007)



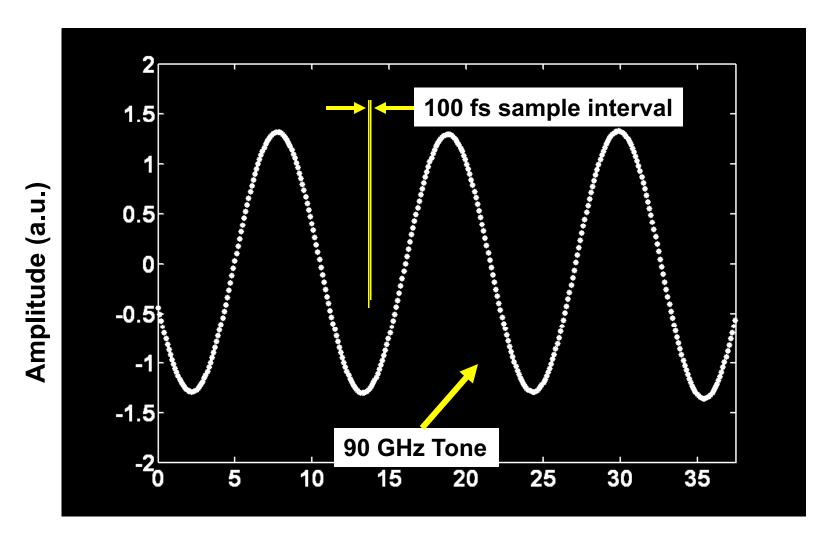
Time Stretch Factor = 250

Eff. Sampling Rate = 40 GSa/s x 250 = 10 TSa/s

Eff. Sampling Interval = 25 ps ÷ 250 = 100 fs



Direct digitization with 100 fs sample time



Input Time (ps)

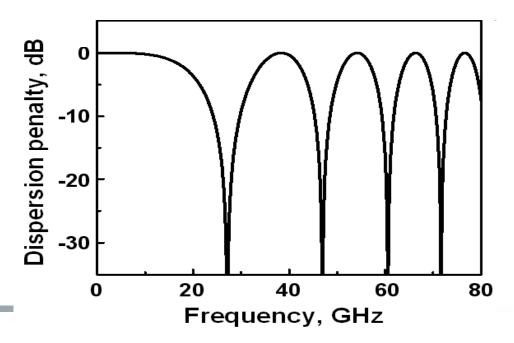


Dispersion Penalty

Optical signal after modulator consists of upper sideband, $f_{\rm Opt}$ + $f_{\rm RF}$, lower sideband, $f_{\rm Opt}$ - $f_{\rm RF}$ carrier, $f_{\rm Opt}$

At photodiode upper sideband and lower sideband beat with carrier to produce current at $f_{
m RF}$

Upper and lower sidebands travel at differing group velocities in dispersive media between modulator and photodetector leading to destructive interference



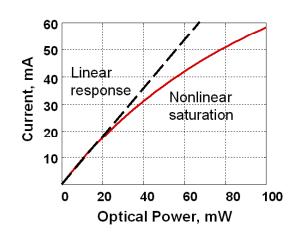


Major sources of nonlinearity

- Intensity Modulator
 - Electro-optic modulators are very linear phase modulators $\phi_{\text{opt}} \sim \textit{V}_{\text{RF}}$
 - Conversion of phase modulation to intensity modulation nonlinear

$$I_{opt} \sim cos(\pi V_{RF}/V_{\pi})$$

Photodiode saturation

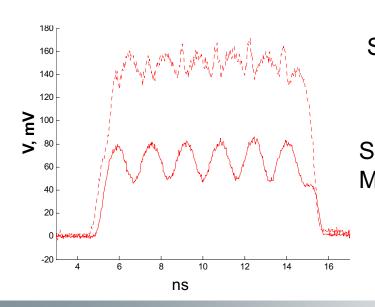


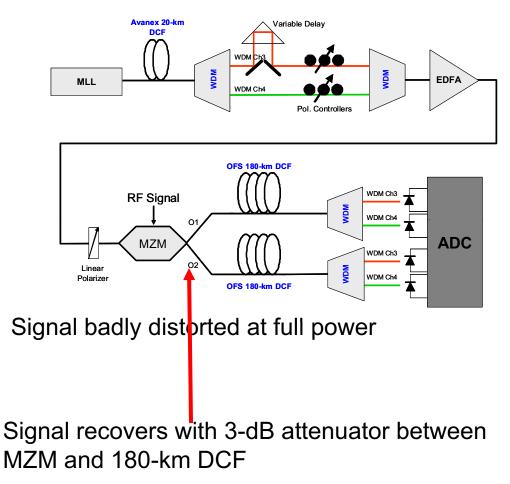
- Optical nonlinearities
 - Kerr nonlinearity
 - Four-wave mixing
 - Stimulated Brillouin scattering
 - Stimulated Raman scattering



Optical Nonlinearities in 2-channel 10 GHz system

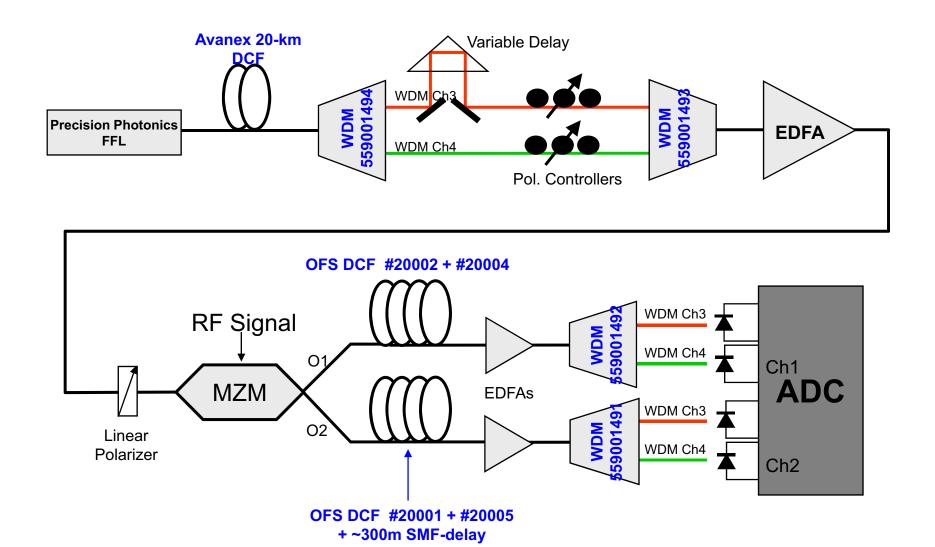
- EDFA Power 23 dBm,
- MZM insertion loss ~4 dB,
- 3 dB split,
- ~16 dBm into 180-km DCF
- 5:1 duty cycle
- 200 mW launched power







Revised 2-channel 10 GHz schematic—EDFAs after DCF





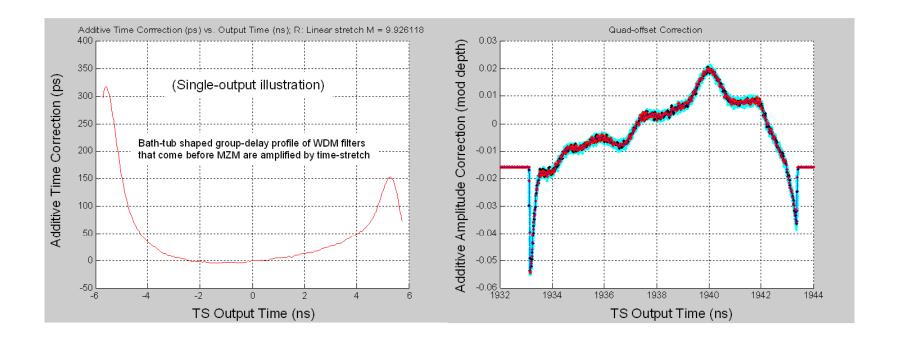
Distortion Corrections in 2-channel 10-GHz system

Time-mapping correction

Issue: wavelength dependence of group delay in the optical elements

MZM bias correction

Issue: wavelength dependece of modulator properties



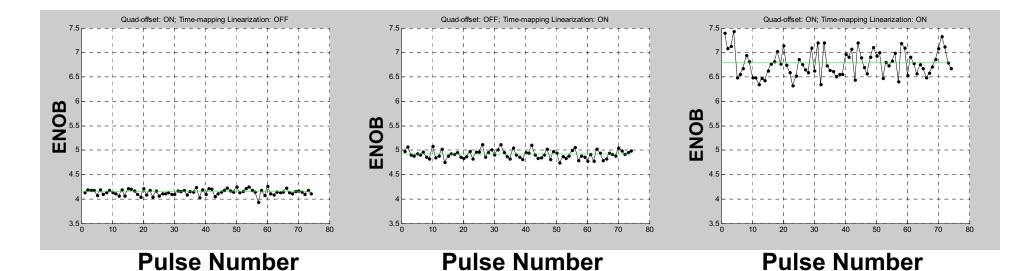


Single-Channel Performance @ 6.5 GHz

w/o MZM bias correction

w/o time mapping correction

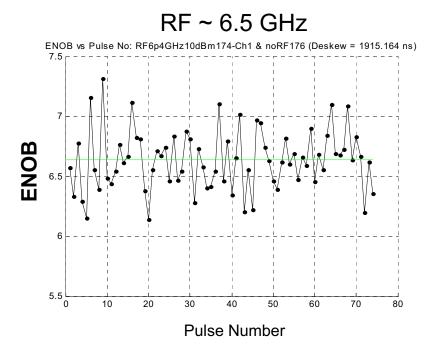
with time mapping correction and MZM bias correction

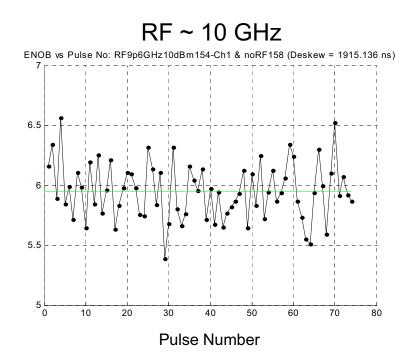




Sine-fit ENOBs

- Filter: DC to 10 GHz "Brickwall" Noise+Distortion
- 8-ns Time Window with time-mapping correction
- Stretch Ratio = 10
- ENOB drops at 10 GHz because of dispersion penalty

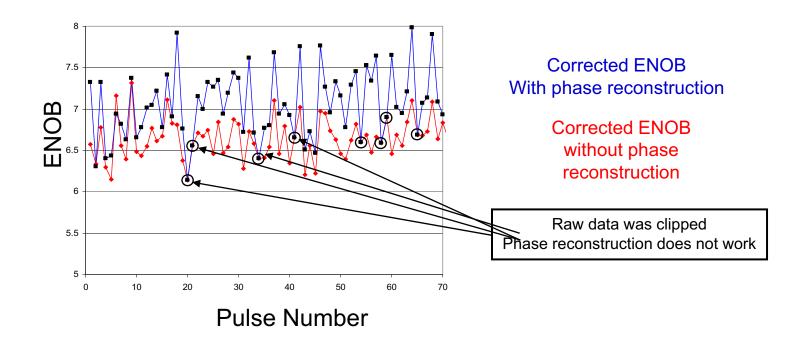






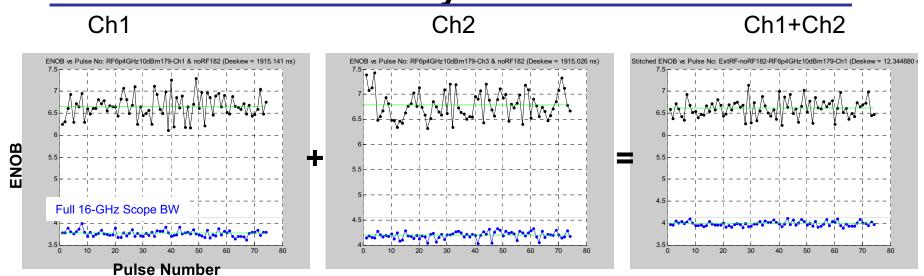
Phase Reconstruction Post-Processing used To further increase ENOB

- Technique originally developed for CFBGs (Conway et al. Opt. Lett. 2008)
- Use measured intensity and phase simulated by propagating through optical components with measured transfer functions
- Mean ENOB increased from 6.64 to 7.05 for 6.5 GHz data



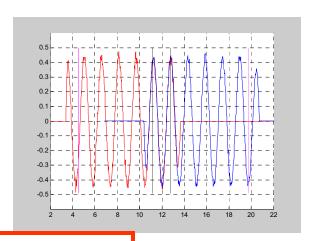


Stitching 6.5-GHz signals from 2 channels in 2-channel 10-GHz System



Stitching algorithm

- Perform all single-channel calibrations/processing
- Equalize the modulation index in 2 channels
- Correlate channels within 1.6-ns overlap region
- Align 2 channels in time based on max correlation
- Average 2 channels in overlap region
- Calculate sine-fit ENOB for full 2-channel run



Stitched waveforms show several pulses ~7 ENOB



Issues in the 7 ENOB 10 GHz experiments

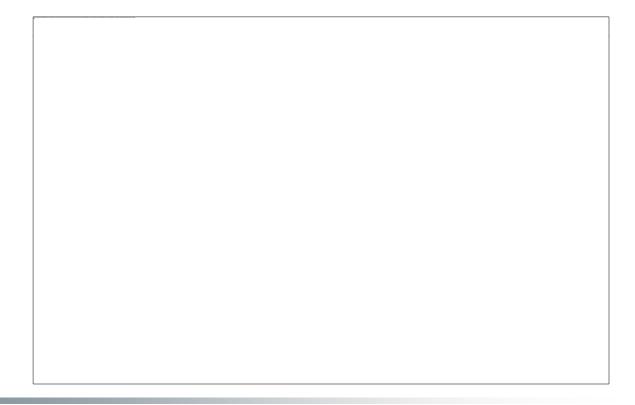
- Backend digitizer single channel limited to ENOB_{max} ~ 7. @ 1GHz
- Time domain vs Frequency domain ENOBs
 - Ringing at pulse edges for brick wall TD filter
 - Different noise bandwidths
 - Different treatment of distortions
- All commercial components
 - Relatively inexpensive fs source—phase aberrations really unknown
 - WDMs have dispersion that looks minimal but effects are enhanced by stretching process
- Effect of optical nonlinearities greater than anticipated
- Large pulse-to-pulse variations in ENOB
 - Laser noise and non-idealities: phase, amplitude, wavelength vs time, random chirp
 - Oscilloscope noise
 - RF/laser timing variations



Continuous-Time Operation

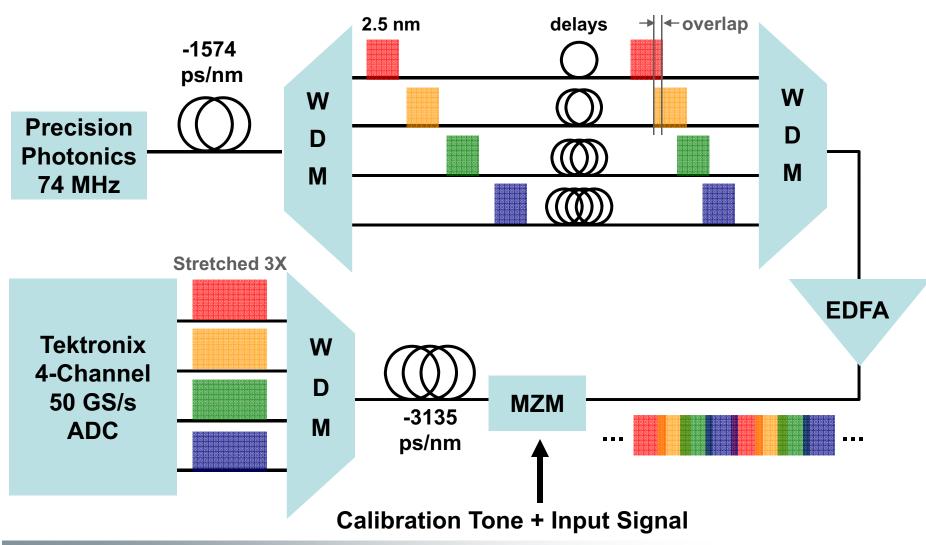
Operating the time-stretch ADC in continuous time requires:

- 1) stretching the pulses input to the modulator to the interpulse time
- 2) demultiplexing the signal to M or more photodiodes and ADCs

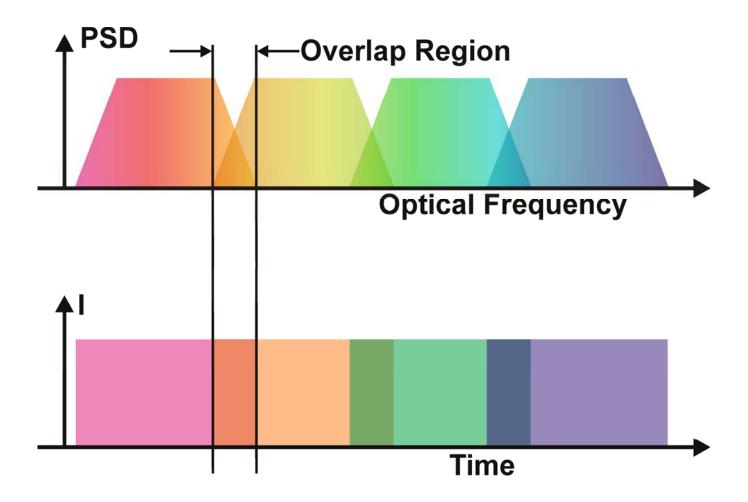




Experimental Configuration 150 GS/s continuous time ADC

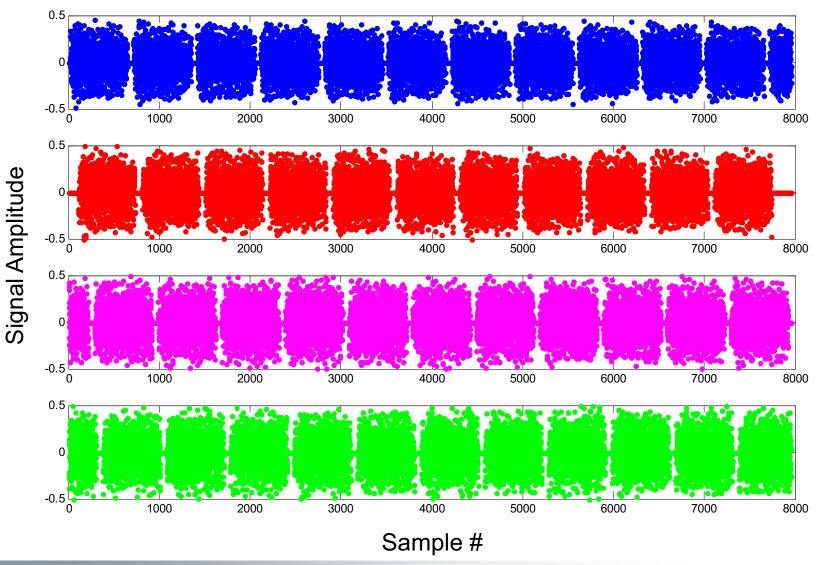


Overlap options



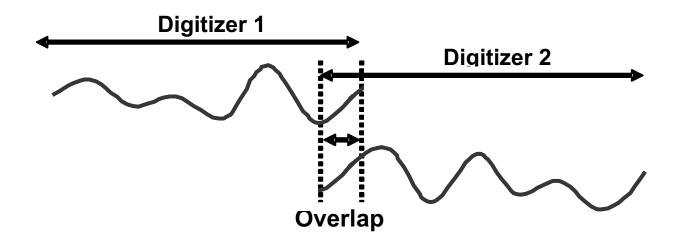


4 Channels at 150 GS/s



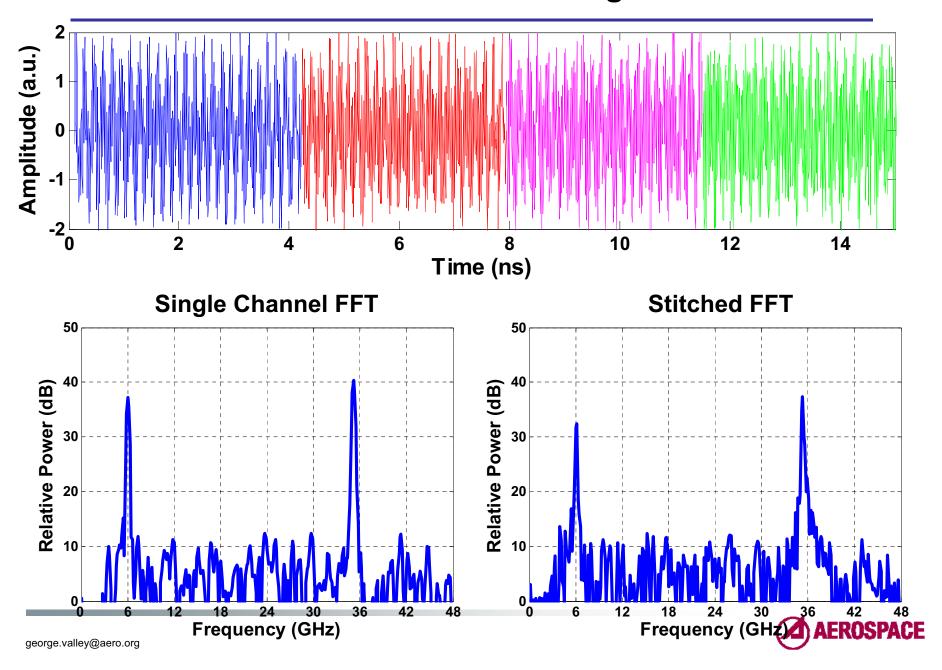
Segment-to-Segment Stitching

- Segments from all 4-channels are concatenated to form the continuous signal
- Out-of-band real-time calibration tone used to independently correct for gain and timing errors

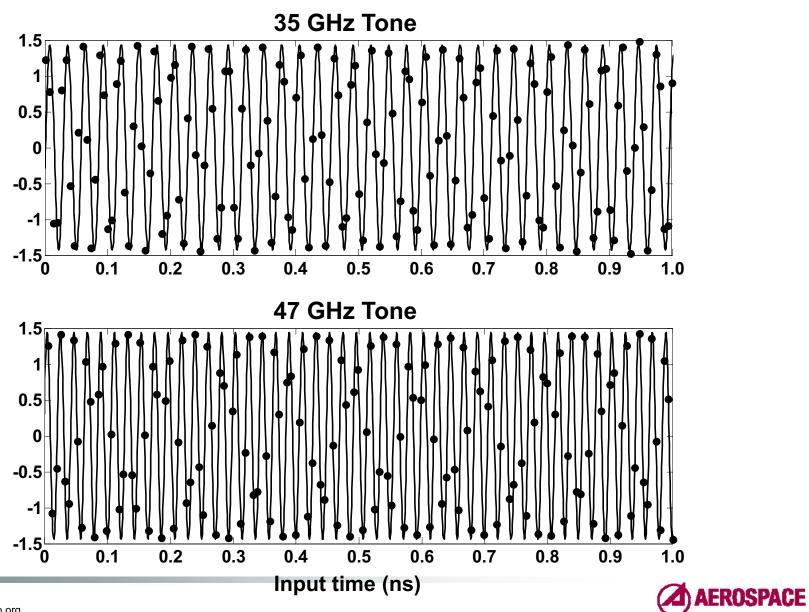




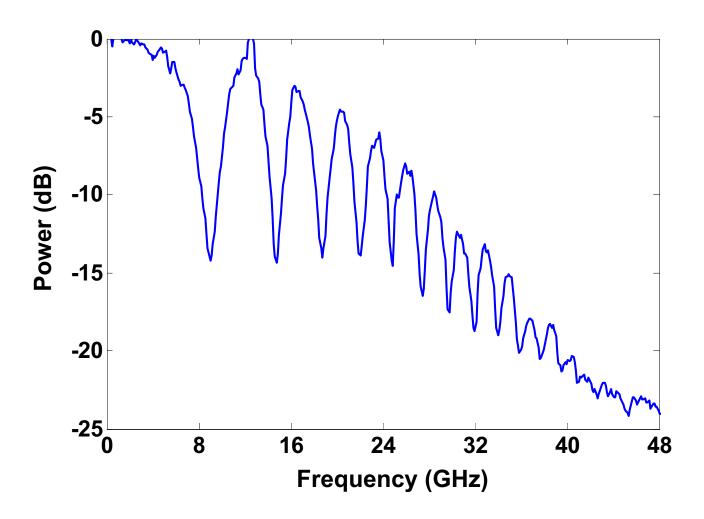
4 Channel Stitching



Reconstructed Signals at 150 GS/s



Dispersion Penalty and Roll-off in 150 GS/s system



Dispersion penalty is a big issue for ultra broadband time-stretch ADC Best solution is single-sideband operation



Summary

- Each new bit of ADC resolution requires an increase in signal-to-noiseand-distortion ratio (SNDR) of 6 dB
- ENOB without noise bandwidth is meaningless
- Decreasing the noise bandwidth by a factor of 4 increases ADC resolution by 1 ENOB
 - e.g. the Tektronix 50 GS/s digital oscilloscope has
 - 5 ENOB over 16 GHz
 - 7 ENOB over 1 GHz
- Every time you sneeze, you lose a few 1/10's of an ENOB
- Optical photons are very energetic compared to RF photons
 - Shot noise is irrelevant for electronic ADCs.
 - Shot noise is a fundamental limit in photonic ADCs
- Photonic ADCs usually contain a microwave photonic link
 - Standard analysis gives the SNR/CNR
 - Max ENOB over a given noise bandwidth readily estimated
- If commercialized, photonic ADCs will resemble data conversion modules and digital oscilloscopes rather than single chip ADCs



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