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## **UNIVERSITY OF CAMBRIDGE INTERNATIONAL EXAMINATIONS**

**GCE Advanced Subsidiary Level and GCE Advanced Level** 

## MARK SCHEME for the May/June 2010 question paper for the guidance of teachers

## 9702 PHYSICS

9702/41

Paper 4 (A2 Structured Questions), maximum raw mark 100

This mark scheme is published as an aid to teachers and candidates, to indicate the requirements of the examination. It shows the basis on which Examiners were instructed to award marks. It does not indicate the details of the discussions that took place at an Examiners' meeting before marking began, which would have considered the acceptability of alternative answers.

Mark schemes must be read in conjunction with the question papers and the report on the examination.

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| Page 2 | Mark Scheme: Teachers' version | Syllabus | Paper |
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|        | GCE AS/A LEVEL – May/June 2010 | 9702     | 41    |

## Section A

| 1 | (a) | _     | le (subtended) <u>at centre</u> of circle<br>arc equal in length to radius                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     | B1<br>B1             | [2]       |
|---|-----|-------|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|----------------------|-----------|
|   | (b) | (i)   | point S shown below C                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          | B1                   | [1]       |
|   |     | (ii)  | (max) force / tension = weight + centripetal force centripetal force = $mr\omega^2$<br>15 = 3.0/9.8 × 0.85 × $\omega^2$<br>$\omega$ = 7.6 rad s <sup>-1</sup>                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  | C1<br>C1<br>C1<br>A1 | [4]       |
| 2 | (a) | (i)   | 27.2 + 273.15 or 27.2 + 273.2<br>300.4 K                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | C1<br>A1             | [2]       |
|   |     | (ii)  | 11.6 K                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         | A1                   | [1]       |
|   | (b) | (i)   | ( $< c^2 >$ is the) mean / average square speed                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                | B1                   | [1]       |
|   |     | (ii)  | $\rho = Nm/V$ with $N$ explained<br>so, $\rho V = 1/3 Nm < c^2 >$<br>and $\rho V = NkT$ with $N$ explained<br>so mean kinetic energy $N < N$ = $N$ = | B1<br>B1<br>B1<br>B1 | [4]       |
|   | (c) | (i)   | pV = nRT<br>2.1 × 10 <sup>7</sup> × 7.8 × 10 <sup>-3</sup> = $n \times 8.3 \times 290$<br>n = 68  mol                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          | C1<br>A1             | [2]       |
|   |     | (ii)  | mean kinetic energy = $3/2 kT$<br>= $3/2 \times 1.38 \times 10^{-23} \times 290$<br>= $6.0 \times 10^{-21} J$                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  | C1<br>A1             | [2]       |
|   |     | (iii) | realisation that total internal energy is the total kinetic energy energy = $6.0 \times 10^{-21} \times 68 \times 6.02 \times 10^{23}$ = $2.46 \times 10^5$ J                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  | C1<br>C1<br>A1       | [3]       |
| 3 | (a) | (i)   | to-and-fro / backward and forward motion (between two limits)                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  | B1                   | [1]       |
|   |     | (ii)  | no energy loss or gain / no external force acting / constant energy / constant an                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              | nplitud<br>B1        | de<br>[1] |
|   | (   | (iii) | acceleration directed towards a fixed point acceleration proportional to distance from the fixed point / displacement                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          | B1<br>B1             | [2]       |
|   | (b) |       | eleration is constant (magnitude)<br>cannot be s.h.m.                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          | M1<br>A1             | [2]       |

| Page 3 |                                                                                                                 | Mark Scheme: Teachers' version                                                                                                                                                                  |                                     | Syllabus                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            | Paper               |                |     |
|--------|-----------------------------------------------------------------------------------------------------------------|-------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-------------------------------------|-------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|---------------------|----------------|-----|
|        |                                                                                                                 |                                                                                                                                                                                                 | GCE AS/A LEVEL – May/June 2010 9702 |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     | 9702                | 41             |     |
| 4      |                                                                                                                 | -                                                                                                                                                                                               | do work<br>ult of the               | position/shape, etc. of an object                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   |                     | B1<br>B1       | [2] |
|        | (b) (i)                                                                                                         | 1                                                                                                                                                                                               | $\Delta {\sf E}_{\sf gpe}$          | = $GMm/r$<br>= $(6.67 \times 10^{-11} \times \{2 \times 1.66 \times 10^{-27}\}^2) / (3.8 \times 10^{-49} \text{ J})$<br>= $1.93 \times 10^{-49} \text{ J}$                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          | 10 <sup>-15</sup> ) | C1<br>C1<br>A1 | [3] |
|        |                                                                                                                 | 2                                                                                                                                                                                               | $\Delta E_{	ext{epe}}$              | = $Qq / 4\pi\epsilon_0 r$<br>= $(1.6 \times 10^{-19})^2 / (4\pi \times 8.85 \times 10^{-12} \times 3.8 \times 10^{-12})^2 / (4\pi \times 8.85 \times 10^{-12} \times 3.8 \times 10^{-12})^2 / (4\pi \times 8.85 \times 10^{-12} \times 3.8 \times 10^{-12})^2 / (4\pi \times 8.85 \times 10^{-12} \times 3.8 \times 10^{-12})^2 / (4\pi \times 8.85 \times 10^{-12} \times 3.8 \times 10^{-12})^2 / (4\pi \times 8.85 \times 10^{-12} \times 3.8 \times 10^{-12})^2 / (4\pi \times 8.85 \times 10^{-12} \times 3.8 \times 10^{-12})^2 / (4\pi \times 8.85 \times 10^{-12} \times 3.8 \times 10^{-12})^2 / (4\pi \times 8.85 \times 10^{-12} \times 3.8 \times 10^{-12})^2 / (4\pi \times 8.85 \times 10^{-12} \times 3.8 \times 10^{-12})^2 / (4\pi \times 8.85 \times 10^{-12} \times 3.8 \times 10^{-12})^2 / (4\pi \times 8.85 \times 10^{-12} \times 3.8 \times 10^{-12})^2 / (4\pi \times 8.85 \times 10^{-12} \times 3.8 \times 10^{-12})^2 / (4\pi \times 8.85 \times 10^{-12} \times 3.8 \times 10^{-12})^2 / (4\pi \times 8.85 \times 10^{-12} \times 3.8 \times 10^{-12})^2 / (4\pi \times 8.85 \times 10^{-12} \times 3.8 \times 10^{-12})^2 / (4\pi \times 8.85 \times 10^{-12} \times 3.8 \times 10^{-12})^2 / (4\pi \times 8.85 \times 10^{-12} \times 3.8 \times 10^{-12})^2 / (4\pi \times 8.85 \times 10^{-12} \times 3.8 \times 10^{-12})^2 / (4\pi \times 8.85 \times 10^{-12} \times 3.8 \times 10^{-12})^2 / (4\pi \times 8.85 \times 10^{-12} \times 3.8 \times 10^{-12})^2 / (4\pi \times 8.85 \times 10^{-12} \times 3.8 \times 10^{-12})^2 / (4\pi \times 8.85 \times 10^{-12} \times 3.8 \times 10^{-12})^2 / (4\pi \times 8.85 \times 10^{-12} \times 3.8 \times 10^{-12})^2 / (4\pi \times 8.85 \times 10^{-12} \times 3.8 \times 10^{-12})^2 / (4\pi \times 8.85 \times 10^{-12} \times 3.8 \times 10^{-12})^2 / (4\pi \times 8.85 \times 10^{-12} \times 3.8 \times 10^{-12})^2 / (4\pi \times 8.85 \times 10^{-12} \times 3.8 \times 10^{-12})^2 / (4\pi \times 8.85 \times 10^{-12} \times 3.8 \times 10^{-12})^2 / (4\pi \times 8.85 \times 10^{-12} \times 3.8 \times 10^{-12})^2 / (4\pi \times 8.85 \times 10^{-12} \times 3.8 \times 10^{-12})^2 / (4\pi \times 8.85 \times 10^{-12} \times 3.8 \times 10^{-12})^2 / (4\pi \times 8.85 \times 10^{-12} \times 3.8 \times 10^{-12})^2 / (4\pi \times 8.85 \times 10^{-12} \times 3.8 \times 10^{-12})^2 / (4\pi \times 8.85 \times 10^{-12} \times 3.8 \times 10^{-12})^2 / (4\pi \times 8.85 \times 10^{-12} \times 3.8 \times 10^{-12})^2 / (4\pi \times 8.85 \times 10^{-12} \times 3.8 \times 10^{-12})^2 / (4\pi \times 8.85 \times 10^{-12} \times 3.8 \times 10^{-12})^2 / (4\pi \times 8.85 \times 10^{-12} \times 3.8 \times 10^{-12})^2 / (4\pi \times 8.85 \times 10^{-12} \times 3.8 \times 10^{-12})^2 / (4\pi \times 8.85 \times 10^{-12} \times 3.8 \times 10^{-12})^2 / (4\pi \times 8.85 \times 10^{-12} \times 3.8 \times 10^{-12})^2 / (4\pi \times 8.85 \times 10^{-12} \times 3.8 \times 10^{-12})^2 / (4\pi \times 8.85 \times 10^{-12} \times 10^{-12})^2 / (4\pi \times 8.85 \times 10^{-12} \times 10^{-12})^2 / (4\pi \times 8.85 \times 10^{-12} \times 10^{-12})^2$ | ) <sup>–15</sup> )  | C1<br>C1<br>A1 | [3] |
|        | (ii) idea that $2E_K = \Delta E_{\text{epe}} - \Delta E_{\text{gpe}}$<br>$E_K = 3.03 \times 10^{-14} \text{ J}$ |                                                                                                                                                                                                 |                                     |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     |                     | B1             |     |
|        |                                                                                                                 |                                                                                                                                                                                                 | 3.03 × 10<br>.19 MeV                | $(0^{-14}) / 1.6 \times 10^{-13}$                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   |                     | M1<br>A0       | [2] |
|        | (iii)                                                                                                           | fusio                                                                                                                                                                                           | on may o                            | occur / may break into sub-nuclear particles                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        |                     | B1             | [1] |
| 5      | (a) (i)                                                                                                         | (a) (i) $V_H$ depends on angle between (plane of) probe and $B$ -field either $V_H$ max when plane and $B$ -field are normal to each other or $V_H$ zero when plane and $B$ -field are parallel |                                     |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     |                     |                |     |
|        |                                                                                                                 | or                                                                                                                                                                                              | V <sub>H</sub> de                   | epends on sine of angle between plane and <i>B</i> -                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                | field               | B1             | [2] |
|        | (ii)                                                                                                            |                                                                                                                                                                                                 | to 1 s.f.                           | es $V_H r$ at least three times constant so valid s.f., not constant so invalid                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     |                     | M1<br>A1       | [2] |
|        |                                                                                                                 | 2                                                                                                                                                                                               | straight                            | line passes through origin                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          |                     | B1             | [1] |
|        | .,.,                                                                                                            | rate<br>cons                                                                                                                                                                                    | of chan<br>stant fiel               | ed is proportional / equal to<br>ge of (magnetic) flux (linkage)<br>d in <u>coil</u> / flux (linkage) of <u>coil</u> does not change<br>rrent (in wire) / switch current on or off / use a.                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         |                     | M1<br>A1<br>B1 | [3] |
|        |                                                                                                                 |                                                                                                                                                                                                 | te coil<br>e coil <u>to</u>         | wards / away from wire (1 mark each, max 3)                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         |                     | ВЗ             | [3] |
| 6      |                                                                                                                 | a) all four diodes correct to give output, regardless of polarity connected for correct polarity                                                                                                |                                     |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     |                     |                | [2] |
|        | $V_0$                                                                                                           | = √2                                                                                                                                                                                            | $= V_{S} / V_{rms}$                 |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     |                     | C1<br>C1       |     |
|        | rati                                                                                                            |                                                                                                                                                                                                 |                                     | $(\sqrt{2} \times 240)$ or 1/37 or 0.027                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            |                     | A1             | [3] |

|      | ugc ¬                                                                                                    |              | Mark General: reactions version                                                                                                                                       | Cynabas | i apci         |     |
|------|----------------------------------------------------------------------------------------------------------|--------------|-----------------------------------------------------------------------------------------------------------------------------------------------------------------------|---------|----------------|-----|
|      |                                                                                                          |              | GCE AS/A LEVEL – May/June 2010 9702                                                                                                                                   |         |                |     |
| 7 (a | ) arro                                                                                                   | ow po        | inting up the page                                                                                                                                                    |         | B1             | [1] |
| (b   | ) (i)                                                                                                    | V            | = $Bqv$<br>= $(12 \times 10^3) / (930 \times 10^{-6})$<br>= $1.3 \times 10^7 \text{ m s}^{-1}$                                                                        |         | C1<br>C1<br>A1 | [3] |
|      | (ii)                                                                                                     | q/m          | = $mv^2 / r$<br>= $(1.3 \times 10^7) / (7.9 \times 10^{-2} \times 930 \times 10^{-6})$<br>$8 \times 10^{11} \text{ C kg}^{-1}$                                        |         | C1<br>C1<br>A1 | [3] |
| 8 (a | (a) momentum conservation hence momenta of photons are equal (but opposite) same momentum so same energy |              |                                                                                                                                                                       |         |                | [2] |
| (b   | ) (i)                                                                                                    | (Δ) <i>E</i> | $= (\Delta)mc^{2}$ = 1.2 × 10 <sup>-28</sup> × (3.0 × 10 <sup>8</sup> ) <sup>2</sup> = 1.08 × 10 <sup>-11</sup> J                                                     |         | C1<br>A1       | [2] |
|      | (ii)                                                                                                     | E<br>λ       | = $hc / \lambda$<br>= $(6.63 \times 10^{-34} \times 3.0 \times 10^{8}) / (1.08 \times 10^{-11})$<br>= $1.84 \times 10^{-14}$ m                                        |         | C1<br>A1       | [2] |
|      | (iii)                                                                                                    | λ<br>p       | = $h/p$<br>= $(6.63 \times 10^{-34}) / (1.84 \times 10^{-14})$<br>= $3.6 \times 10^{-20}$ N s                                                                         |         | C1<br>A1       | [2] |
|      |                                                                                                          |              | Section B                                                                                                                                                             |         |                |     |
| 9 (a | ) (i)                                                                                                    | poin         | t X shown correctly                                                                                                                                                   |         | B1             | [1] |
|      | (ii)                                                                                                     | non-         | mp has <u>very large</u> / infinite gain<br>inverting input is at earth (potential) / earthed / at 0 V<br>iplifier is not to saturate, inverting input must be (almos | st)     | M1<br>M1       |     |
|      |                                                                                                          |              | arth potential / 0 (V) same potential as inverting input                                                                                                              |         | A1             | [3] |
| (b   | ) (i)                                                                                                    | (amp         | input resistance = $1.2 \text{ k}\Omega$<br>blifier) gain (= $-4.2 / 1.2$ ) = $-3.5$<br>meter) reading = $-3.5 \times -1.5$                                           |         | C1<br>C1       |     |
|      |                                                                                                          | `            | = 5.25 V<br>I disregard of signs or incorrect sign in answer, max 2                                                                                                   | marks)  | A1             | [3] |
|      | (ii)                                                                                                     | (amp         | s bright so) resistance of LDR increases<br>blifier) gain decreases<br>meter) reading decreases                                                                       |         | M1<br>M1<br>A1 | [3] |

Mark Scheme: Teachers' version

Syllabus

Paper

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| Pag | ge 5                                          | M                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                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                                                                                                                                                    | Syllabus                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              | Paper                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         |                                     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|     |                                               | GC                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             | CE AS/A LEVEL – May/June 2010                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     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   | 41                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            |                                            |
| (a) | repeated images / combine repeated to build u | I at different<br>data is pro<br>d / added to<br>I for succes<br>up a 3-D im                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   | t angles<br>cessed<br>o give (2-D) image of slice<br>sive slices<br>age                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           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   | B1<br>B1<br>B1<br>B1<br>B1<br>B1<br>max 6                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     | [6]                                        |
| (b) | (i) 16                                        |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  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   | A1                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            | [1]                                        |
|     | ` '                                           |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                | ducting 16 then dividing by 3                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     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   | C1<br>A1                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      | [2]                                        |
| (a) |                                               |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  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   | M1<br>A1                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      | [2]                                        |
| (b) | (1 each,<br>disadvar                          | max 2)<br>itages e.g.                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          | less noise / less interference greater bandwidth / better quality short range / more transmitters / line of sig more complex circuitry greater expense                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            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   | B4                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            | [4]                                        |
| (a) | 190 = 1 or $-190$                             | $0 \lg(18 \times 10) = 10 \lg P_2 /$                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | $0^3 / P_2$ ) $(18 \times 10^3)$                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  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   | C1<br>C1<br>A1                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                | [3]                                        |
|     | (i) 11 (ii) e.g.                              | SHz / 12 GF<br>so that inpu                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    | dz<br>ut signal to satellite will not be 'swamped'                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         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   | B1<br>B1                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      | [1]                                        |
|     | (a) (b) (a)                                   | repeated images / combine repeated to build usimage can be image can be image.  (a) frequency (in synchronic can be image can be image.  (b) (ii) advantage (1 each, disadvar can be image can be image.  (b) (ii) advantage (1 each, disadvar can be image can be image.  (b) (ii) advantage can be image can be image.  (b) (ii) advantage can be image can be image.  (b) (ii) advantage can be image ca | (a) X-ray taken of slice repeated at different images / data is procombined / added to repeated for success to build up a 3-D imitimage can be viewed.  (b) (i) 16  (ii) evidence of decto give  3 2 6 5  (a) frequency of carrier (in synchrony) with give (in synchrony) with | (a) X-ray taken of slice / plane / section repeated at different angles images / data is processed combined / added to give (2-D) image of slice repeated for successive slices to build up a 3-D image image can be viewed from different angles / rotated  (b) (i) 16  (ii) evidence of deducting 16 then dividing by 3 to give  3 2 6 5  (a) frequency of carrier wave varies (in synchrony) with signal (in synchrony) with displacement of signal  (b) advantages e.g. less noise / less interference greater bandwidth / better quality (1 each, max 2) disadvantages e.g. short range / more transmitters / line of signal (1 each, max 2)  (a) gain / loss/dB = 10 lg(P <sub>1</sub> /P <sub>2</sub> ) 190 = 10 lg(18 × 10 <sup>3</sup> / P <sub>2</sub> ) or -190 = 10 lg P <sub>2</sub> / 18 × 10 <sup>3</sup> ) power = 1.8 × 10 <sup>-15</sup> W  (b) (i) 11 GHz / 12 GHz | (a) X-ray taken of slice / plane / section repeated at different angles images / data is processed combined / added to give (2-D) image of slice repeated for successive slices to build up a 3-D image image can be viewed from different angles / rotated  (b) (i) 16  (ii) evidence of deducting 16 then dividing by 3 to give 3 2 6 5  (a) frequency of carrier wave varies (in synchrony) with signal (in synchrony) with displacement of signal  (b) advantages e.g. less noise / less interference greater bandwidth / better quality (1 each, max 2) disadvantages e.g. short range / more transmitters / line of sight more complex circuitry greater expense (1 each, max 2)  (a) gain / loss/dB = 10 lg(P <sub>1</sub> /P <sub>2</sub> ) 190 = 10 lg(18 × 10 <sup>3</sup> / P <sub>2</sub> ) or -190 = 10 lg P <sub>2</sub> / 18 × 10 <sup>3</sup> ) power = 1.8 × 10 <sup>-15</sup> W  (b) (i) 11 GHz / 12 GHz  (ii) e.g. so that input signal to satellite will not be 'swamped' | GCE AS/A LEVEL - May/June 2010   9702   41 |