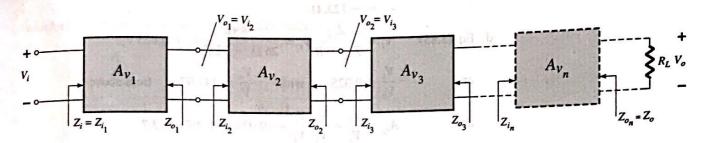
No matter how perfect the system design, the application of a load to a two-port system will affect the voltage gain. Therefore, there is no possibility of a situation where A_{ν_1} , A_{ν_2} , and so on, of Fig. 5.69 are simply the no-load values. The loading of each succeeding stage must be considered. The no-load parameters can be used to determine the loaded gains of Fig. 5.69, but Eq. (5.93) requires the loaded values.



Cascaded system.

EXAMPLE 5.14 The two-stage system of Fig. 5.70 employs a transistor emitter-follower configuration prior to a common-base configuration to ensure that the maximum percentage of the applied signal appears at the input terminals of the common-base amplifier. In Fig. 5.70, the no-load values are provided for each system, with the exception of Z_i and Z_o for the emitter-follower, which are the loaded values. For the configuration of Fig. 5.70, determine:

- a. The loaded gain for each stage.
- b. The total gain for the system, A_{ν} and A_{ν} .
- c. The total current gain for the system.
- d. The total gain for the system if the emitter-follower configuration were removed.

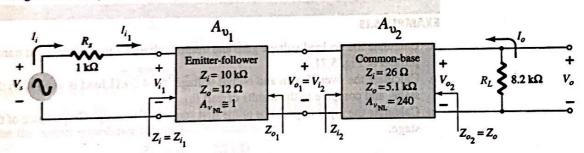


FIG. 5.70 Example 5.14.

Solution:

and

a. For the emitter-follower configuration, the loaded gain is (by Eq. (5.88))

emitter-follower configuration, the loaded gain is (by Eq. (3.66))
$$V_{o_1} = \frac{Z_{i_2}}{Z_{i_2} + Z_{o_1}} A_{v_{NL}} V_{i_1} = \frac{26 \Omega}{26 \Omega + 12 \Omega} (1) V_{i_1} = 0.684 V_{i_1}$$

$$A_{V_i} = \frac{V_{o_1}}{V_{i_1}} = 0.684$$

For the common-base configuration,

$$V_{o_2} = \frac{R_L}{R_L + R_{o_2}} A_{v_{\rm NL}} V_{i_2} = \frac{8.2 \text{ k}\Omega}{8.2 \text{ k}\Omega + 5.1 \text{ k}\Omega} (240) V_{i_2} = 147.97 V_{i_2}$$
 and
$$A_{v_2} = \frac{V_{o_2}}{V_{i_1}} = 147.97$$

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b. Eq. (5.93):
$$A_{\nu_1} = A_{\nu_1} A_{\nu_2}$$

= $(0.684)(147.97)$
= 101.20