State variable Fralysis

Limitations of the Transfer function approach

- Obtaining pricise solution of any sim, loose their importance in conuntional approach
- (Omplete time domain solution of light order sim
- (8) It is not why much convenient for the analysis of MIHO SIMS
- 4) It gives onalysis of sin for some smufic types of into live step, Romp etc.
- E) It is only approache to linear Time Invariant sims.

 6) The classical methods like Root local, Bode pott etc are basically trail or effor procedures which fail to give the optimal solution required.
- all initial conclitions. This technique which was the concept of state is called state variable Analysis or state space Analysis.

Advantages of stak Vouiable Analysis

- 1) The nethod takes into account the effect of all
- 2) It can be applied to nonlinear as well as time varying
- 3) It can be conveniently applied to MIMO sims.

- 4) The sim our be designed for the optimal conditions preusely by using the modern method. S) Any type of the ip can be considered for designing the
- 6) As the nuthod involves matrix algebra, can be
- conveniently adopted for the digital computers 7) The State variables scheeked need not necessarily
- be the physical quantities of the slm
- 8) The vector matrix notation greatly simplifies the Hathematical approximation of the sim
- -> Initial conditions do ic memory affects the sim characterisation & subsequent behaviour.
- -> Initial conditions describe the status or state of the sim at t=to.
- The Stak can be regarded as a compact or concise reproventation of the past history of the s1m
- The state of the sim in brief separates the future from the past so that the state contains all the information contening the past history of the sim nte necessarily required to determine the response of the sim for any giwn type of isp.
- The state of the SIm at any time t'is actually to combined effect of the values of the different elements of the sim which are associated with the Initial conditions of Huslm
- > The complete state of the slm can be considered + a ventor having components which are the variable Of slm which are closely associated with initial cond

so state can be defined as untor xets called state unitor XCHD le stake at any time 't' is 'n' dominational rentor ie column matrix nxl

XCHD = [xich]

are called state variables of the slow

Definitions.

My

- as a minimal set of variables such that the knowledge of these variables at to to getter with the the knowledge of these variables at to to fogether with the knowledge of these variables at to completely determine the knowledge of the sim for to to to the determine the behaviour of the sim for to to.
- Destate variables: The variables involved in determining the state of a dynamic 81m xet), are called the state variables
- 3) Stake untor: The in stake Variables necessary to discribe the complete behaviour of the slow can be considued as in components of a untor xcto called the stake meter at time 't'
- Stake Space: The Space whose co-ordinate axes are nothing but the 'n' state variables with time as the implicit variable is called the State space.

Stake Hodel of Linear systems

Stake Hodel of Linear systems

Stake Hodel of Linear systems

Tonsidu Helio, ath order sim

HIHO

Sims

White of lips = m.

no: of lips = m.

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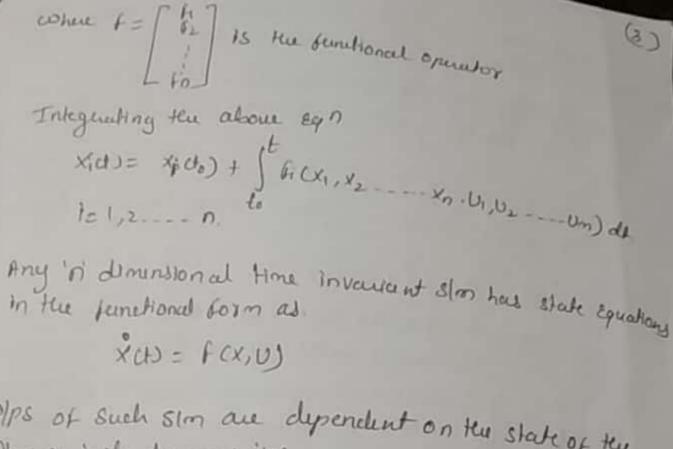
UCD: UCD | XID | XID | XID | YID | YID

The state variable representation can be arranged in the

$$\frac{dx_{1}(t)}{dt} = x_{1}(t) = f_{1}(x_{1}, x_{2} - \dots - x_{n}, v_{1}, v_{2} - \dots - v_{m})$$

$$\frac{dx_{2}(t)}{dt} = x_{2}(t) = f_{2}(x_{1}, x_{2} - \dots - x_{n}, v_{1}, v_{2} - \dots - v_{m})$$

$$\frac{dx_{n}(t)}{dt} = x_{n}(t) = f_{n}(x_{1}, x_{2} - \dots - x_{n}, v_{n}, v_{n}, v_{2} - \dots - v_{m})$$

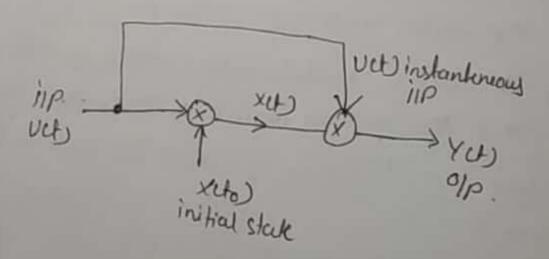


Olps of such sim are dependent on the state of the SIM a instantaneous ilps.

-- functional of Egn can be written as YCH) = g(X,U) where g'is the functioned operator

For time variant SIM, the Same Equations can be written as X(1) = f(x, U, t) --- Stak Egn

YCU = g(x, v,t) olp Egn



The functional Egry can be expressed intoms of linear xi = anxi + a12x2+ --- + a inxo + bin Ui + bi2 U2 + --- bim Um x2 = a21x1 + a22x2+ ---+ a2nxn+b21U1+b22U2+ -- bankn xn = anix1 + anix2+ - - + annxn + bn14 + bn2 V21 - - bnnun (LUU & + CHX A = CH)X XCH) = Stak Keetor meetric of order nx 1 U(1) = Ilp neutor matrix of order mx1 A = SIM matrix or Evaluation mutrix of ordunan B = 118 matrix or control matrix of ordu nxm 11/4 O/P Variables Yet) = C11 x1(1)+----- Cin xn(1)+d11 yet) ----+dimunty Yect) = (p1 x10+ - - - - - + checker) + dq 40) - - - + checker YUS CXUS + DUCK) YUS= 018 mutor matrix of order px1 C = O/P matrix or observation matrix of ordu Pro D = direct transmission matrix of ordu pxm The two nector eggs together is called the State model of the linear slm (4) = AxU) + BUL) YUS = CXUS + DUCK) This is the Stak model of a sim

Fox Drew time variant sims, the matrices A, B, CAO

X4) = ACD X4) + BOD OCH)
YCD = CCD X4) + BOD OCH)

Stak Hodel of single Input single output sim

XLH) = AXLH) + BUCH)

YUS = CXUS+ ducy

A = nxn onatix

B = nx1 matrix

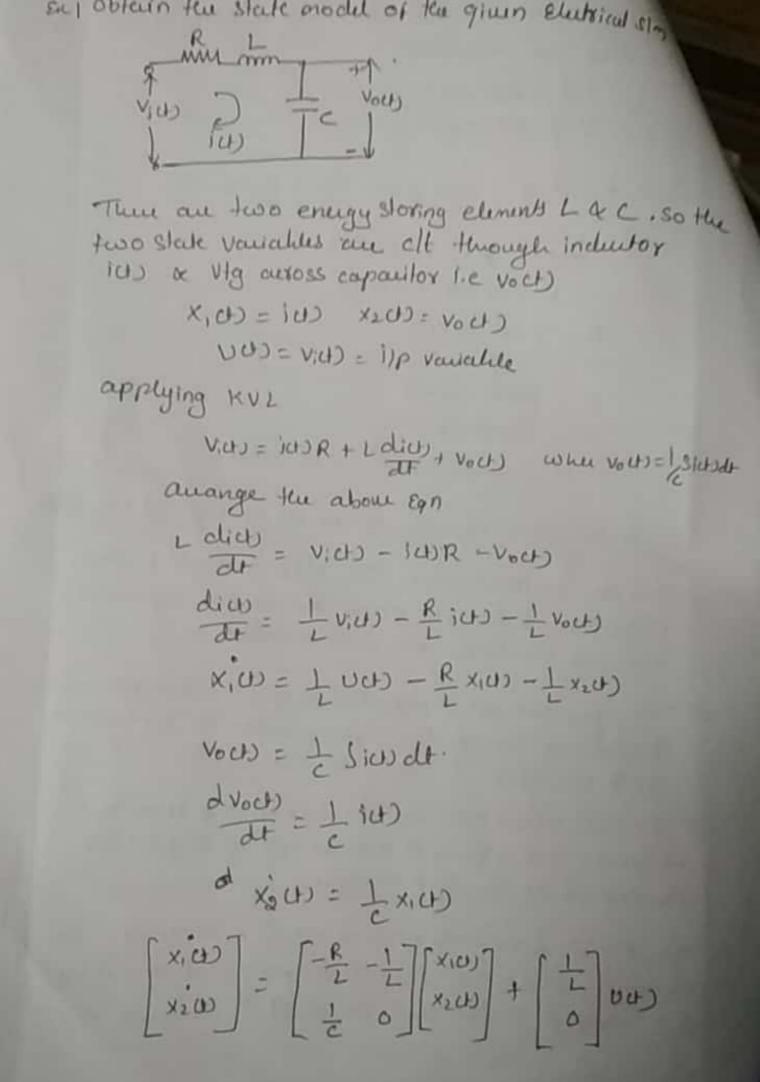
C = Ixn matrix

d = constart.

UCt) = Single Scalar ilp variable.

State Variable Representation using Physical variables

- inclustors & the vig across the various capacitors are selected to be the state variables.
- The Equation for differentiation of one state variable should not involve the differentiation of any other state variable
- of Energy storing elements such as spring & friction are selected as the state volumble
- The Physical variables associated with energy storing elements, which are responsible for initial conditions, are selected as the state variables of the given stm.



$$X(t) = A \times (t) + B \times (t)$$

$$B[P \ Vanishle \ Y(t)] = V_0(t) = V_0(t) = V_2(t)$$

$$Y(t) = C \times (t) \quad V_0 = C \times (t) \quad V_0 = C \times (t)$$

$$Y(t) = C \times (t) \quad V_0 = C \times (t) \quad V_0 = C \times (t)$$

$$Y(t) = C \times (t) \quad V_0 = C \times (t) \quad V_0 = C \times (t) \quad V_0 = C \times (t)$$

$$V[D] = C \times (t) \quad V_0 = C \times (t) \quad V_0 = C \times (t)$$

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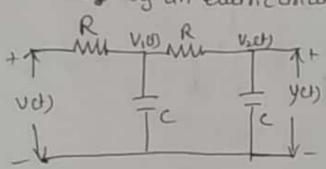
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$$V[D] = V[D]$$

Yet
$$V_0(t) = R_2 i_R(t)$$
 $C \frac{dV_0(t)}{dt} = i_1(t) - i_R(t)$
 $Y_0(t) = R_2 x_2(t)$ $Y_0(t) = \frac{1}{2} (x_1(t)) - \frac{1}{2} (x_1(t))$
 $X_1(t) = \frac{1}{2} (x_1(t)) - \frac{1}{2} (x_1(t))$
 $X_2(t) = \frac{1}{2} (x_1(t)) - \frac{1}{2} (x_1(t))$
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 $X_1(t) = \frac{1}{2} (x_1(t)) - \frac{1}{2} (x_1(t))$
 $X_2(t) = \frac{1}{2} (x_1(t)) - \frac{1}{2} (x_1(t))$
 $X_2(t) = \frac{1}{2} (x_1(t)) - \frac{1}{2} (x_1(t))$

(3) obtain an appropriate state model for a sim



801") Victo & vecto are state variables

with apply ockel at node

$$\frac{(2d) - V_1(t)}{R} + \frac{1}{C} \frac{dV_1(t)}{dt} + \frac{1}{C} \frac{V_1(t) - V_2(t)}{R} = 0$$

$$\frac{(2d) \frac{dV_1(t)}{dt} - \left(-\frac{(2d) + V_1(t)}{R}\right) - \left(-\frac{(2d) - V_2(t)}{R}\right) - \left(-\frac{(2d) - V_2(t)}{R}\right) = 0$$

$$\frac{(2d) \frac{dV_1(t)}{dt} - \frac{1}{R} \frac{(2d) + \frac{1}{R} \frac{V_2(t)}{R} + \frac{2}{R} \frac{V_1(t)}{R} + \frac{2}{R} \frac{V_1(t)}$$

choice of state variable is generally output variable Yet itself and other state variables are duivatives of the selected State Variable yers xich) = YCt) X2(1)= y'(1)=xi(1) Y3CH)= Y(U) = X(U) = X(U) Thus the various State Egns are XILL) = XICH) XU) = X34) ×n-1ch = xnch Xnet = ? Thus we have Yet = x1, YU) = X2 y'cs=x3, ... Yn-14)= xn(1), Yn(1) = xn(1) Xn(t) + an-1 xn(t) + an-2 xn-1(t) ...- + a1x1(t) + x0x1(t) = b000) Xn(+) = - aoxic+) - aix2el) - --- - an-2×n-1(+)-an-1×na) + bouch $\begin{bmatrix} x_1 \\ x_2 \\ -a_0 - a_1 - a_{n+1} \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 1 & -a_{n+1} & 0 \\ -a_0 & -a_1 & -a_{n+1} & a_n \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ -a_0 \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \end{bmatrix} U(1)$ X = Axct) + Buct) Y4)= x,4) Y(4) = [100 --- 0] (x(4)) Y(4) = (x4)
D = 0

$$x_{1}(t) = -\frac{1}{Re}v(t) + \frac{1}{Re}x_{2}(t)$$

$$Ke \perp at node v_{\perp}$$

$$c \frac{dv_{2}(t)}{dt} + v_{2}(t) - v_{1}(t) = 0$$

$$c \frac{dv_{2}(t)}{dt} = -\frac{v_{2}(t)}{R} + \frac{v_{1}(t)}{R}$$

$$c \frac{dv_{2}(t)}{dt} = -\frac{1}{Re}v_{2}(t) + \frac{1}{Re}v_{1}(t)$$

$$x_{2}(t) = -\frac{1}{Re}x_{2}(t) + \frac{1}{Re}x_{1}(t)$$

$$x_{2}(t) = -\frac{1}{Re}x_{1}(t) + \frac{1}{Re}x_{2}(t)$$

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$$x_{2}(t) = -\frac{1}{Re}x_{2}(t) + \frac{1}{Re}x_{2}(t)$$

$$x_{2}(t) = -\frac{$$

554. constant the state model on using Phase variables if the sim is described by the differential egn.

$$\begin{bmatrix} \dot{x}_1 (L) \\ \dot{x}_2 (L) \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ x_3 (L) \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -2 & -7 & -4 \end{bmatrix} \begin{bmatrix} x_1 (L) \\ x_2 (L) \\ x_3 (L) \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 5 \end{bmatrix} (U_{4})$$

$$A = \begin{cases} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -2 & -7 & -4 \end{cases} \quad B = \begin{cases} 0 \\ 5 \end{cases} \quad C = \begin{bmatrix} 1 & 0 & 0 \end{bmatrix} \quad D = 0$$

Transfer function from State model Considu a Standard State model durud tor linear time invaviant sm as. XCH) = AXCH) + BUCH) YUS= CXUS+ DUUS Taking laplace Fransform on both side Sxy) = Axcs) + BUCS) Yess = exes) + Dues) -> SX(S) - AX(S) = BU(S) -> SIXU) - AXU) = BUO) (SI-A] x(S) = BUC) XCS) = [SI-A] BUCG) Y (S) = C x(S) + D U(S) = C (SI-A] BUCS) + DUCS) Y(S) = [C [SI-A]B+D] U(S) $T\vec{F} = \frac{Y(S)}{U(S)} = C[SI - A]B + D$ $[SI - A] = \frac{AdJ[SI - A]}{|SI - A|}$ T(S) = C Adi[SI-A]B D

Sx1 5) consider a slm having state model.

$$\begin{bmatrix}
x_1 \\
x_2
\end{bmatrix} = \begin{bmatrix} -2 & -3 \\
4 & 2 \end{bmatrix} \begin{bmatrix} x_1 \\
x_2
\end{bmatrix} + \begin{bmatrix} 3 \\
5 \end{bmatrix} 0 & y = \begin{bmatrix} 1 \\
5 \end{bmatrix} \begin{bmatrix} 4 \\
5 \end{bmatrix}$$
with $0 = 0$. Obtain TF

Solf)
$$TF = C[SI - A] + B$$

$$\begin{bmatrix}
SI - A] = \begin{bmatrix} 1 & 0 \\
0 & 1 \end{bmatrix} s - \begin{bmatrix} -2 & -3 \\
4 & 2 \end{bmatrix} = \begin{bmatrix} 5 + 2 & 3 \\
-4 & 5 - 2 \end{bmatrix}$$
add $\begin{bmatrix} SI - A] = \begin{bmatrix} 1 & 0 \\
0 & 1 \end{bmatrix} s - \begin{bmatrix} -2 & -3 \\
4 & 5 + 2 \end{bmatrix}$

$$\begin{bmatrix}
SI - A] = \begin{bmatrix} 1 & 0 \\
0 & 1 \end{bmatrix} s - \begin{bmatrix} -2 & -3 \\
4 & 5 + 2 \end{bmatrix}$$

$$\begin{bmatrix}
SI - A] = \begin{bmatrix} 1 & 0 \\
0 & 1 \end{bmatrix} s - \begin{bmatrix} -2 & -3 \\
4 & 5 + 2 \end{bmatrix}$$

$$\begin{bmatrix}
SI - A\end{bmatrix} = \begin{bmatrix} 1 & 0 \\
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0 & 1 \end{bmatrix} s + \begin{bmatrix} 3$$

6) Find the T.f. of the Slm having stake model

$$\dot{X} = \begin{bmatrix} 0 & 1 \\ -2 & -3 \end{bmatrix} \times + \begin{bmatrix} 0 \end{bmatrix} U \times Y = \begin{bmatrix} 1 & 0 \end{bmatrix} X$$
Soln)

$$A = \begin{bmatrix} 0 & 1 \\ -2 & -3 \end{bmatrix} \quad B = \begin{bmatrix} 0 \\ 0 \end{bmatrix} \quad C = \begin{bmatrix} 1 & 0 \end{bmatrix} \quad D = 0$$

$$TF = C \begin{bmatrix} SI - AJB + D \\ SI - AJ = S \begin{bmatrix} 0 & 1 \\ -2 & 3 \end{bmatrix} = \begin{bmatrix} S & -1 \\ 2 & S+3 \end{bmatrix}$$

$$adj \begin{bmatrix} SI - AJ = \begin{bmatrix} S+3 & +1 \\ -2 & S \end{bmatrix} \\
|SI - AJ = S(S+3) + 2 = S^2 + 3S + 2 = (S+1)(S+2)$$

$$TF = \begin{bmatrix} 0 & adj \begin{bmatrix} SI - AJB \\ 1 & SI - AJ \end{bmatrix}$$

$$= \begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} S+3 & 1 \\ -2 & S \end{bmatrix} \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

$$(S+1)(S+2)$$

$$= \underbrace{S+3}_{(S+1)(S+2)}$$

solution of state Equation

considu the state Egn of linea Home invavour story

X (1) = A X(1) + B UCH)

The matrices A & B are constent matrices. This state

1) Homogenious (2) Non homogenous.

Homogeneous equation

Non Homogeneous Equation

The sa constant matrix & matrix vels is non zero

X CD = A XCD + BUCH)

Classical Huthor of solution

Considur a scalar differential egn or

dx = ax coher x co) = 10

ho no geneous egn without the ilp rentor
assume the solution of this egn or

x4) = bo + bit + bit + - - - bx tk

t=0 xco) = x0 = bo.

The solution has to sutisfy the original diffurition d [bo +bit 1 --- +bxtk] = a [bo + bit 1 -- +bxtk] bi + 2bit 1 - - - k bikt = abol abit 1 - - abit bi = abo 2b2 = abi KbK = abK-1 b== abi = 1 a a abo = a2bo = 1 a2bo $b_3 = \frac{ab_2}{3} = \frac{1}{3k_2}a^3b_0 = \frac{1}{3!}a^3b_0$ bic = 1 ak bo & x(0) = 60 1- XU) = bo + abot+ la2bot+ la3bd3 --- + lakb + = [1 +at + 1 a2t2 + 1 a3t3 + ---+ 1 axtk/10) 1+at+ = 1 a2 +2+ = a3+3, --+ = eat X(1)= e x(0) X(1) = AX(t) x(1) = ex(0) -- pc+)= eAt = state transition matrix At 1+At+ = 1 A2+2+ - - - - HAEK If instead of initial time t=0, it is selected as t=to tun the state transition matrix is du) = pA(t-to)

Zero Input Response -> The solution of the homogeneous state egn is under the condition of zero ilp. such response is called zero Input Suponse (ZIR) Solution of Nonhomogeneous egn lonsider a non homogeneous state Egn as XCD = AXU) + BUCH xu)-Axu)=Buch) Premuliplying both sides by EAt enfx(+)-Ax(+)] = ent Bu(+) EAT x (4) - EATA X (1) = d[EAT X (1)] where dileAtxu) = eAtBUCH) Assuming initial time as t= 0 a integrating both side from t=0 to to except = SeBUCOde exu)-x(0) = Ste-AZBUWdz

Premultiplying both sides by eat

x(+) = ex(0) + fe(t-z) B v(0) dz

Solution of nonhomogeneous Egn

Properties of State Transition Matrix () \$(0) = eAXO] 2) pu) = et = (et) = [p(-t)] \$ (4) = 0 (-t) 3) OCH + (2) = en(title) = entinely = QCHOQUED = QCHOQUED 4) eA(t+s) = eAt eAs 5) eA+B)t = eAt B+ only if AB=BA 6) [pors = Left] = ent pont 7) \$ (+2-t1). \$ (t1-t0) = \$ (t2-t0) Solution of state Egn by laplace Transform Luthod consider the nonhomogeneous State Egn as XUD= AXUD+BUCH Taking leplen Transform on both sides Sx(s) = Ax(s) + Bx(s) SX(S) - AX(S) = BUG) SXIS) - X(0) = AXIS) +BUU) SX(S) - AX(S) = X(O) + BU(S) (SI-A)X(S) = X(O) + BU(S) XLS) = [SI-NIXLO) + [SI-NIBUC) -(2) = ZIR + ZSR Comparing zero input response obtained earlier

(11)

$$\phi(s) : \left[sI-AJ = \left[\frac{s+3}{(s+1)(s+2)} \frac{-1}{(s+1)(s+2)}\right]$$

$$e^{AT} = \frac{1}{2} \left[sI-AJ = \frac{1}{2} \frac{s+3}{(s+1)(s+2)} \frac{-1}{(s+1)(s+2)}\right]$$

$$using partial feation expression for all the stand elevels
$$e^{At} = \left[\frac{2}{s+1} - \frac{1}{s+2} \frac{-1}{s+1} + \frac{1}{s+2}\right]$$

$$e^{At} = \left[\frac{2}{s+1} - \frac{1}{s+2} \frac{-1}{s+1} + \frac{1}{s+2}\right]$$

$$e^{At} = \left[\frac{2}{s+1} - \frac{1}{s+2} \frac{-1}{s+1} + \frac{1}{s+2}\right]$$

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$$e^{At} = \left[\frac{2}{s+1} - \frac{1}{s+2} + \frac{1}{s+2} + \frac{1}{s+2}\right]$$

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$$e^{At} = \left[\frac{2}{s+1} - \frac{1}{s+2} + \frac{1}{s+2} + \frac{1}{s+2}\right]$$

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$$e^{At} = \left[\frac{2}{s+1} - \frac{1}{s+2} + \frac{1}{s+2} + \frac{1}{s+2}\right]$$

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$$e^{At} = \left[\frac{2}{s+1} - \frac{1}{s+2} + \frac{1}{s+2} + \frac{1}{s+2}\right]$$

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$$e^{At} = \left[\frac{2}{s+1} - \frac{1}{s+2} + \frac{1}{s+2} + \frac{1}{s+2}\right]$$

$$e$$$$

$$x(t) = \begin{bmatrix} e^{3t} \\ -8e^{3t} \end{bmatrix} \quad \dot{x}(t) = \begin{bmatrix} -8e^{3t} \\ 9e^{3t} \end{bmatrix}$$

$$\dot{x}(t) = \begin{bmatrix} -1 \\ -8 \end{bmatrix} \quad \dot{x}(t) = \begin{bmatrix} -3 \\ 9 \end{bmatrix}$$

$$\dot{x}(t) = A \times (0)$$

$$\begin{bmatrix} -3 \\ 9 \end{bmatrix} = \begin{bmatrix} A_1 & A_2 \\ A_3 & A_4 \end{bmatrix} \begin{bmatrix} -1 \\ -3 \end{bmatrix}$$

$$A_1 - 3A_2 = -3$$

$$A_3 - 3A_4 = 9$$

$$A_1 + A_2 = \begin{bmatrix} A_1 & A_2 \\ A_3 & A_4 \end{bmatrix} \begin{bmatrix} -1 \\ 1 \end{bmatrix}$$

$$A_1 + A_2 = \begin{bmatrix} A_1 & A_2 \\ A_3 & A_4 \end{bmatrix} \begin{bmatrix} -1 \\ 1 \end{bmatrix}$$

$$A_1 + A_2 = \begin{bmatrix} A_1 & A_2 \\ A_3 & A_4 \end{bmatrix} \begin{bmatrix} -1 \\ 1 \end{bmatrix}$$

$$A_1 + A_2 = \begin{bmatrix} A_1 & A_2 \\ A_3 & A_4 \end{bmatrix} \begin{bmatrix} -1 \\ 1 \end{bmatrix}$$

$$A_1 + A_2 = \begin{bmatrix} A_1 & A_2 \\ A_3 & A_4 \end{bmatrix} \begin{bmatrix} -1 \\ 1 \end{bmatrix}$$

$$A_1 + A_2 = \begin{bmatrix} A_1 & A_2 \\ A_3 & A_4 \end{bmatrix} \begin{bmatrix} -1 \\ A_4 & A_4 \end{bmatrix} \begin{bmatrix} -1 \\ A_4$$

$$A = \begin{bmatrix} 0 & 1 \\ 3 & -2 \end{bmatrix}$$

$$(SI - A) = \begin{bmatrix} S & -1 \\ -3 & S+2 \end{bmatrix}$$

$$ads [SI - A] = \begin{bmatrix} S+2 & 1 \\ 3 & S \end{bmatrix}$$

$$|SI - A| = \begin{bmatrix} S+2 & 1 \\ 3 & S \end{bmatrix}$$

$$(SI - A) = ads [SI - A] = \begin{bmatrix} S+2 \\ (S+3)(S-1) \end{bmatrix}$$

$$(SI - A) = \begin{bmatrix} SI - A \end{bmatrix}$$

$$= \begin{bmatrix} 1 & 0.25 + 0.75 \\ S+3 & S-1 \end{bmatrix}$$

$$= \begin{bmatrix} 0.25 + 0.75 \\ S+3 & S-1 \end{bmatrix}$$

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$$= \begin{bmatrix} 0.25 + 0.75 \\ S-13 & S-1 \end{bmatrix}$$

$$(3) = \frac{\text{add}[s_1 - A]}{|s_1 - A|} = \frac{\text{add}[s_1 - A]}{|s_2 - a|} = \frac{\text{add}[s_1 - A]}{|s_$$

homogeneous state eqn is characterised by the homogeneous state eqn

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ 1 & 1 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$$
Compatte the solution of homogeneous eqn, assume the initial state vector
$$x_0 = \begin{bmatrix} 1 \\ 0 \end{bmatrix}$$

$$\begin{bmatrix} S_1 - A \end{bmatrix} = \begin{bmatrix} 8 - 1 & 0 \\ -1 & 8 - 1 \end{bmatrix}$$

$$\begin{bmatrix} S_1 - A \end{bmatrix} = \begin{bmatrix} 8 - 1 & 0 \\ -1 & 8 - 1 \end{bmatrix}$$

$$\begin{bmatrix} S_1 - A \end{bmatrix} = \begin{bmatrix} S - 1 & 0 \\ 1 & 1 \end{bmatrix}$$

$$\begin{bmatrix} S_1 - A \end{bmatrix} = \begin{bmatrix} S - 1 & 0 \\ 1 & S - 1 \end{bmatrix}$$

$$\begin{bmatrix} S_1 - A \end{bmatrix} = \begin{bmatrix} S - 1 & 0 \\ 1 & S - 1 \end{bmatrix}$$

$$\begin{bmatrix} S_1 - A \end{bmatrix} = \begin{bmatrix} S_1 - 1 & 0 \\ 1 & S - 1 \end{bmatrix}$$

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$$\begin{bmatrix} S_1 - A \end{bmatrix} = \begin{bmatrix} S_1 - 1 & 0 \\ 1 & S - 1 \end{bmatrix}$$

$$\begin{bmatrix} S_1 - A \end{bmatrix} = \begin{bmatrix} S_1 - 1 & 0 \\ 1 & S -$$

16) obtain the time response of the following sim

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ 1 & 1 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 1 \\ 1 \end{bmatrix} \text{ but}$$

Cohom with is the unit skep occurring at t=0 4.

Solf)

$$A = \begin{bmatrix} 1 & 0 \\ 1 & 1 \end{bmatrix} \quad B = \begin{bmatrix} 1 \\ 1 \end{bmatrix} \quad x(0) = \begin{bmatrix} 1 \\ 0 \end{bmatrix}$$

ZIR

Zeno lip response = $x(1) = \begin{bmatrix} 1 \\ 1 \end{bmatrix} \quad x(0) = \begin{bmatrix} 1 \\ 0 \end{bmatrix}$

ZIR

Zeno lip response = $x(1) = \begin{bmatrix} 1 \\ 1 \end{bmatrix} \quad x(0) = \begin{bmatrix} 1 \\ 0 \end{bmatrix}$

ZER

ZENO State response = $x(1) = \begin{bmatrix} 1 \\ 1 \end{bmatrix} \quad x(0) = \begin{bmatrix} 1$

Using partial frontion

$$ZSR = [[\phi cs) B ucs] = [[\frac{1}{5H} - \frac{1}{5}]]$$
 $= [\frac{1}{5H} - \frac{1}{5}]$
 $= [\frac{1}{5H} - \frac{1}{5H}]$
 $= [\frac{1}{5H} - \frac{1}{5$

$$[S1-n] = \frac{ads[S1-n]}{|S1-n|} = \frac{s+3}{(s+1)(s+2)}$$

$$= \frac{s+3}{(s+1)(s+2)} = \frac{s+3}{(s+1)(s+2)}$$

$$= \frac{s+3}{(s+1)(s+2)} = \frac{s}{(s+1)(s+2)}$$

$$= \frac{s+1}{s+1} - \frac{1}{s+2} = \frac{1}{s+1} + \frac{1}{s+2}$$

$$= \frac{s+1}{s+2} + \frac{1}{s+2} + \frac{1}{s+2}$$

$$= \frac{s+1}{s+2} + \frac{1}{s+2} + \frac{1}{s+2}$$

$$= \frac{s+1}{s+2} + \frac{1}{s+2} + \frac{1}{s+2}$$

$$= \frac{s+1}{s+2} + \frac{s+1}{s+2}$$

$$= \frac{s+3}{(s+1)(s+2)} + \frac{s+3}{(s+1)(s+2)} + \frac{s+3}{(s+1)(s+2)} = \frac{s+3}{(s+1)(s+2)}$$

$$= \frac{s+3}{(s+1)(s+2)} + \frac{s+3}{(s+1)(s+2)} + \frac{s+3}{(s+1)(s+2)} = \frac{s+3}{(s+3)(s+2)} = \frac{s+3}{(s+3)(s+2)} = \frac{s+$$

$$2SR = \begin{bmatrix} \begin{cases} \frac{2(5+3)}{(5+1)(5+2)} & \frac{5+4}{(5+1)(5+2)} \\ \frac{-4}{(5+1)(5+2)} & \frac{8-2}{(5+1)(5+2)} \\ \frac{-4}{(5+1)(5+2)} & \frac{8-2}{(5+1)(5+2)(5+3)} \\ \frac{-4}{(5+1)(5+2)} & \frac{4}{(5+1)(5+2)(5+3)} \\ \frac{-4}{(5+3)} & \frac{4}{(5+4)(5+2)(5+3)} \\ \frac{-4}{(5+3)} & \frac{4}{(5+2)(5+3)} & \frac{5^{2}+65+9}{(5+2)(5+3)} \\ \frac{-4}{(5+3)} & \frac{4}{(5+2)(5+3)} & \frac{5^{2}+65+9}{(5+2)(5+3)} \\ \frac{-4(5+3)}{(5+2)(5+2)(5+3)} & \frac{2^{2}+65+9}{(5+2)(5+3)} \\ \frac{-4(5+2)}{(5+2)(5+2)(5+3)} & \frac{3^{2}+65+9}{(5+2)(5+3)} \\ \frac{-4(5+2)}{(5+2)(5+3)} & \frac{3^{2}+165+18}{(5+2)(5+3)} \\ \frac{-4(5+1)(5+2)(5+3)}{(5+2)(5+3)} & \frac{3^{2}+165+18}{(5+2)(5+3)} \\ \frac{-4(5+1)(5+2)(5+3)}{(5+2)(5+3)} & \frac{3}{(5+2)(5+2)} \\ \frac{-4(5+1)(5+2)(5+3)}{(5+2)(5+3)} & \frac{3}{(5+2)(5+3)} \\ \frac{-4(5+1)(5+2)(5+3)}{(5+2)(5+3)} & \frac{3}{(5+2)(5+2)} \\ \frac{-4(5+1)(5+2)(5+3)}{(5+2)(5+3)} & \frac{3}{(5+2)(5+2)} \\ \frac{-4(5+1)(5+2)(5+3)}{(5+2)(5+3)} & \frac{3}{(5+2)(5+2)} \\ \frac{-4(5+1)(5+2)(5+3)}{(5+2)(5+3)} & \frac{3}{(5+2)(5+2)(5+3)} \\ \frac{-4(5+1)(5+2)(5+3)}{(5+2)(5+3)} & \frac{3}{(5+2)(5+2)} \\ \frac{-4(5+1)(5+2)(5+3)}{(5+2)(5+3)} & \frac{4}{(5+2)(5+2)} \\ \frac{-4}{(5+2)(5+2)(5+3)} & \frac{3}{(5+2)(5+2)(5+3)} \\ \frac{-4}{(5+2)(5+2)(5+3)} & \frac{3}{(5+2)(5+2)(5+2)} \\ \frac{-4}{(5+2)(5+2)(5+2)(5+2)} \\ \frac{-4}{(5+2)(5+2)(5+2)(5+2)(5+2)(5+2)} \\ \frac{-4}{(5+2)(5+2)(5+2)(5+2)(5+2)} \\ \frac{-4}{(5+2)(5+2)(5+2)(5+2)(5+2)(5+2)} \\$$

$$S = -1.$$

$$3 - 16 + 18 = -B(-1+2)(-1+3)$$

$$5 = -2B \quad B = -\frac{5}{2} = -2.5.$$

$$S = -2$$

$$12 - 32 + 18 = -2 \cdot C(-2+1)(-2+3)$$

$$-20 + 18 = -2 \cdot C(-1+1)(1)$$

$$-2 = -2 \cdot C \cdot C(-1+1)(1)$$

$$-2 = -2 \cdot C \cdot C(-1+1)(1)$$

$$-3 = -6D.$$

$$D = -\frac{3}{6} = \frac{1}{2} = 0.5$$

$$S^{2} - 6S - 12 = A(S+1)(S+2)(S+3) + BS(S+2)(S+3) + CS(S+1)(S+3) + DS(S+1)(S+3) + DS(S+1)$$

$$\frac{3}{8} = \frac{2.5}{5+1} = \frac{1}{5+2} + \frac{0.5}{5+3}$$

$$= \frac{2}{8} + \frac{2.5}{5+1} + \frac{1}{5+2} - \frac{2.5}{5+3}$$

$$= \frac{2}{8} + \frac{2.5}{5+1} + \frac{1}{5+2} - \frac{2.5}{5+3}$$

$$= \frac{2}{8} + \frac{2.5}{5+1} + \frac{1}{5+2} - \frac{2.5}{5+3}$$

$$= \frac{2}{8} + \frac{2.5}{5+1} + \frac{1}{5+2} + \frac{0.5}{5+3}$$

$$= \frac{2}{8} + \frac{2.5}{5+1} + \frac{1}{5+2} + \frac{0.5}{5+3}$$

$$= \frac{2}{8} + \frac{2.5}{5+3} + \frac{2.5}{5+3}$$

$$= \frac{2}{1} + \frac{2}{1} + \frac{2.5}{5+3}$$

$$= \frac{2}{1} + \frac{2.5$$

18) When
$$x(t) = \begin{bmatrix} 0 & 1 \\ -2 & -3 \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \end{bmatrix} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} \cot t$$

Find the unit step response column $x(t) = \begin{bmatrix} 1 \\ 1 \end{bmatrix}$

Sof) $A = \begin{bmatrix} 0 & 1 \\ -2 & -3 \end{bmatrix} B = \begin{bmatrix} 0 \\ 1 \end{bmatrix} x(t) = \begin{bmatrix} 1 \\ 1 \end{bmatrix}$

$$\begin{bmatrix} 52 - A \end{bmatrix} = \begin{bmatrix} 9 & -1 \\ +2 & 8+3 \end{bmatrix}$$

and $\begin{bmatrix} 51 - A \end{bmatrix} = \begin{bmatrix} 5+3 & 1 \\ -2 & 5 \end{bmatrix}$

$$\begin{bmatrix} 51 - A \end{bmatrix} = \begin{bmatrix} 5+3 & 1 \\ (5+1)(5+2) \end{bmatrix} = \begin{bmatrix} 1 & 1 \\ 1 & 5+1 \end{bmatrix} = \begin{bmatrix} 1 & 1 \\ 1 & 5+1 \end{bmatrix} = \begin{bmatrix} 1 & 1 \\ 1 & 5+1 \end{bmatrix} = \begin{bmatrix} 1 & 1 \\ 1 & 5+1 \end{bmatrix} = \begin{bmatrix} 1 & 1 \\ 1 & 1$$

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Yet) = ZIR + ZSR
=
$$\begin{cases} 8e^{\frac{1}{2}} - 2e^{\frac{1}{2}t} \\ -3e^{\frac{1}{2}} + 4e^{\frac{1}{2}t} \end{cases}$$
 = $\begin{cases} 6 \cdot s + 2e^{\frac{1}{2}} - 2e^{\frac{1}{2}t} \\ -2e^{\frac{1}{2}} + 3e^{\frac{1}{2}t} \end{cases}$
= $\begin{cases} 6 \cdot s + 2e^{\frac{1}{2}} - 1se^{\frac{1}{2}t} \\ -2e^{\frac{1}{2}} + 3e^{\frac{1}{2}t} \end{cases}$
= $\begin{cases} 6 \cdot s + 2e^{\frac{1}{2}} - 1se^{\frac{1}{2}t} \\ -2e^{\frac{1}{2}} + 3e^{\frac{1}{2}t} \end{cases}$ = $\begin{cases} 6 \cdot s + 2e^{\frac{1}{2}} - 1se^{\frac{1}{2}t} \\ -3e^{\frac{1}{2}} + 1e^{\frac{1}{2}} - 1e^{\frac{1}{2}} \end{cases}$ = $\begin{cases} 6 \cdot s + 2e^{\frac{1}{2}} - 1e^{\frac{1}{2}} \\ -3e^{\frac{1}{2}} + 1e^{\frac{1}{2}} - 1e^{\frac{1}{2}} \end{cases}$ = $\begin{cases} 6 \cdot s + 2e^{\frac{1}{2}} - 1e^{\frac{1}{2}} \\ -3e^{\frac{1}{2}} - 1e^{\frac{1}{2}} - 1e^{\frac{1}{2}} \end{cases}$ = $\begin{cases} 6 \cdot s + 2e^{\frac{1}{2}} - 1e^{\frac{1}{2}} \\ -3e^{\frac{1}{2}} - 1e^{\frac{1}{2}} - 1e^{\frac{1}{2}} \end{cases}$ = $\begin{cases} 6 \cdot s + 2e^{\frac{1}{2}} - 1e^{\frac{1}{2}} \\ -3e^{\frac{1}{2}} - 1e^{\frac{1}{2}} - 1e^{\frac{1}{2}} \end{cases}$ = $\begin{cases} 6 \cdot s + 2e^{\frac{1}{2}} - 1e^{\frac{1}{2}} - 1e^{\frac{1}{2}} \\ -3e^{\frac{1}{2}} - 1e^{\frac{1}{2}} - 1e^{\frac{1}{2}} \end{cases}$ = $\begin{cases} 6 \cdot s + 2e^{\frac{1}{2}} - 1e^{\frac{1}{2}} - 1e^{\frac{1}{2}} \\ -3e^{\frac{1}{2}} - 1e^{\frac{1}{2}} - 1e^{\frac{1}{2}} \end{cases}$ = $\begin{cases} 6 \cdot s + 2e^{\frac{1}{2}} - 1e^{\frac{1}{2}} - 1e^{\frac{1}{2}} \\ -3e^{\frac{1}{2}} - 1e^{\frac{1}{2}} - 1e^{\frac{1}{2}} \end{cases}$ = $\begin{cases} 6 \cdot s + 2e^{\frac{1}{2}} - 1e^{\frac{1}{2}} - 1e^{\frac{1}{2}} - 1e^{\frac{1}{2}} - 1e^{\frac{1}{2}} - 1e^{\frac{1}{2}} \end{cases}$ = $\begin{cases} 6 \cdot s + 2e^{\frac{1}{2}} - 1e^{\frac{1}{2}} -$

$$\frac{18}{18} = \frac{18}{18} = \frac{1$$

Yet) =
$$\begin{bmatrix} 0.5 & \text{e}^{\frac{1}{2}} = 0.5 & \text{e}^{\frac{1}{2}} + \int_{-0.5}^{0.5} & \text{e}^{\frac{1}{2}} - 0.25 & \text{e}^{\frac{1}{2}} + \int_{-0.5}^{0.5} & \text{e}^{\frac{1}{2}} & \text{e}^{\frac{1}$$

your following Egn defines a sepurately excited oc motor in the form of differential Egn W+ (B) dw + (K) W = (K) V The above Egn in state space form as follows w = P [w + Q V find P matrix, if v is vtg ip k wis orgalar knowly (1) w= do dw = d20 do + 円 do + につか = (に)レ $x_1 = 0$, $x_1 = 0$ $x_2 = \frac{d^20}{dt^2}$ × ×2+ (=) ×2+ (=) ×2= [=] V (B) x2 = [K] V - 12 + K2 x2 $\dot{x}_2 = \frac{\dot{x}}{BL} V - \left[\frac{\dot{x}^2 + L3}{BL}\right] \dot{x}_2$ $\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ - \begin{bmatrix} k^2 + L5 \\ BL \end{bmatrix} \begin{bmatrix} \chi_1 \\ \chi_2 \end{bmatrix} + \begin{bmatrix} 0 \\ k \\ BL \end{bmatrix} V$ W.K.T XI=0 XI=do = w

$$\begin{bmatrix}
\omega \\
\dot{\omega}
\end{bmatrix} = \begin{bmatrix}
0 \\
0
\end{bmatrix} - (\frac{k^2 + L5}{BL}) \begin{bmatrix}
0 \\
0
\end{bmatrix} = QV$$

$$22) Considu a sim qiun by
$$\dot{y}' + q\dot{y} + 26\dot{y} + 24\dot{y} = 60 \text{ obtain state model}$$

$$\dot{y}'' + 26\dot{y} + 24\dot{y} = 60 \text{ obtain state model}$$

$$\dot{y}'' + 26\dot{y} + 26\dot{y} + 24\dot{y} = 60$$

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$$\dot{y}'' + 26\dot{y} + 26\dot{y} + 26\dot{y} + 24\dot{y} = 60$$

$$\dot{y}'$$$$

 $\begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -24 & -26 & -9 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 6 \end{bmatrix} v(t)$

Ya>= [100][x]

on obtain the state model for the gluin

$$\frac{3}{3} \times (3) + 9 + 3 \times (3) + 26 \times (3) + 24 \times (3) = 24 \times (3)$$

$$\frac{3}{3} \times (3) + 9 + 3 \times (3) + 26 \times (3) + 24 \times (3) = 24 \times (3)$$

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$$\frac{3}{3} \times (3) + 2$$

$$\frac{1}{\sqrt{100}} = \frac{1}{\sqrt{3}+9\sqrt{5}+265+24}$$

$$s^{3}(c(5)) + 9\sqrt{5}(c(5)) + 26\sqrt{5}(c(5)) + 24\sqrt{6}(c(5)) = U(5)$$

$$c'' + 9c' + 26\sqrt{6} + 24\sqrt{6} = U$$

$$c = \times 1$$

$$\dot{x}_{1} = \times 2$$

$$\dot{x}_{2} = \times 3$$

$$\dot{x}_{3} + 9 \times_{3} + 26 \times_{2} + 24 \times_{1} = U$$

$$\begin{bmatrix} \dot{x}_{1} \\ \dot{x}_{2} \\ \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -24 - 26 & -9 \end{bmatrix} \begin{bmatrix} \dot{x}_{1} \\ \dot{x}_{2} \\ \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ \end{bmatrix} U$$

$$\begin{cases} \dot{x}_{1} \\ \dot{x}_{2} \\ \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -24 - 26 & -9 \end{bmatrix} \begin{bmatrix} \dot{x}_{1} \\ \dot{x}_{2} \\ \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ \end{bmatrix} U$$

$$\begin{cases} \dot{x}_{1} \\ \dot{x}_{2} \\ \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -24 - 26 & -9 \end{bmatrix} \begin{bmatrix} \dot{x}_{1} \\ \dot{x}_{2} \\ \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ \end{bmatrix} U$$

$$\begin{cases} \dot{x}_{1} \\ \dot{x}_{2} \\ \dot{x}_{3} \\ \end{cases}$$

$$\begin{cases} \dot{x}_{1} \\ \dot{x}_{2} \\ \dot{x}_{3} \\ \end{cases}$$