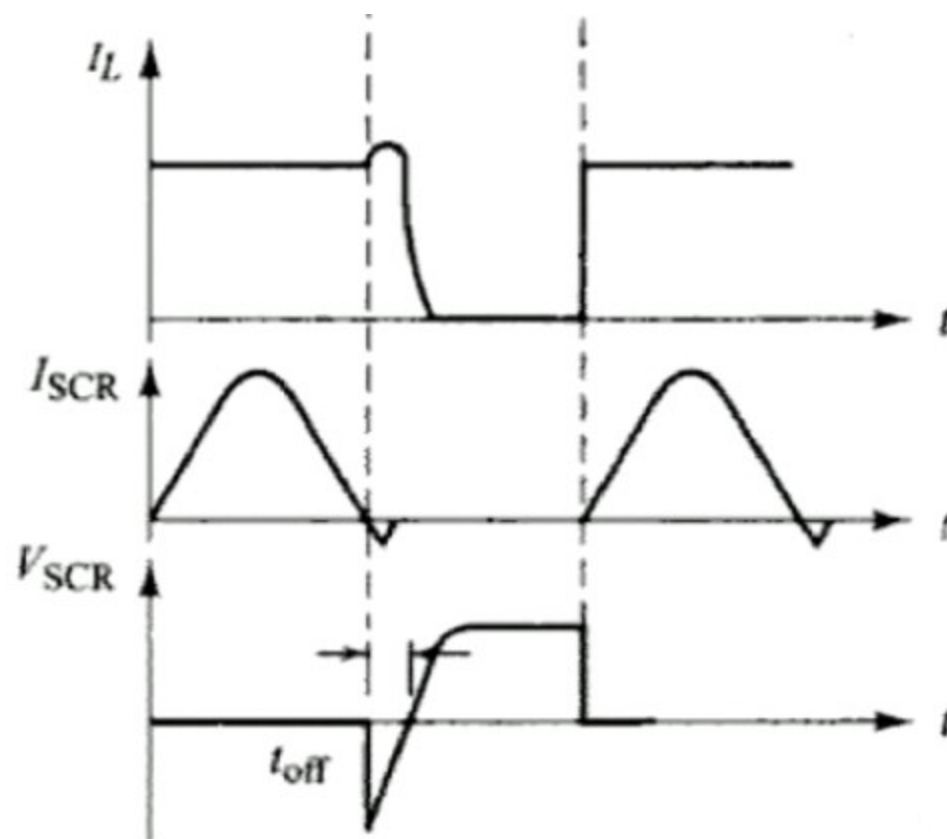


**Fig. 2.15** Class B commutation circuit



**Fig. 2.16** Associated waveforms

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Initially, as soon as the supply voltage  $E_{dc}$  is applied, the capacitor  $C$  starts

### **Design Considerations**

The circuit equations for the  $LC$  circuit are:

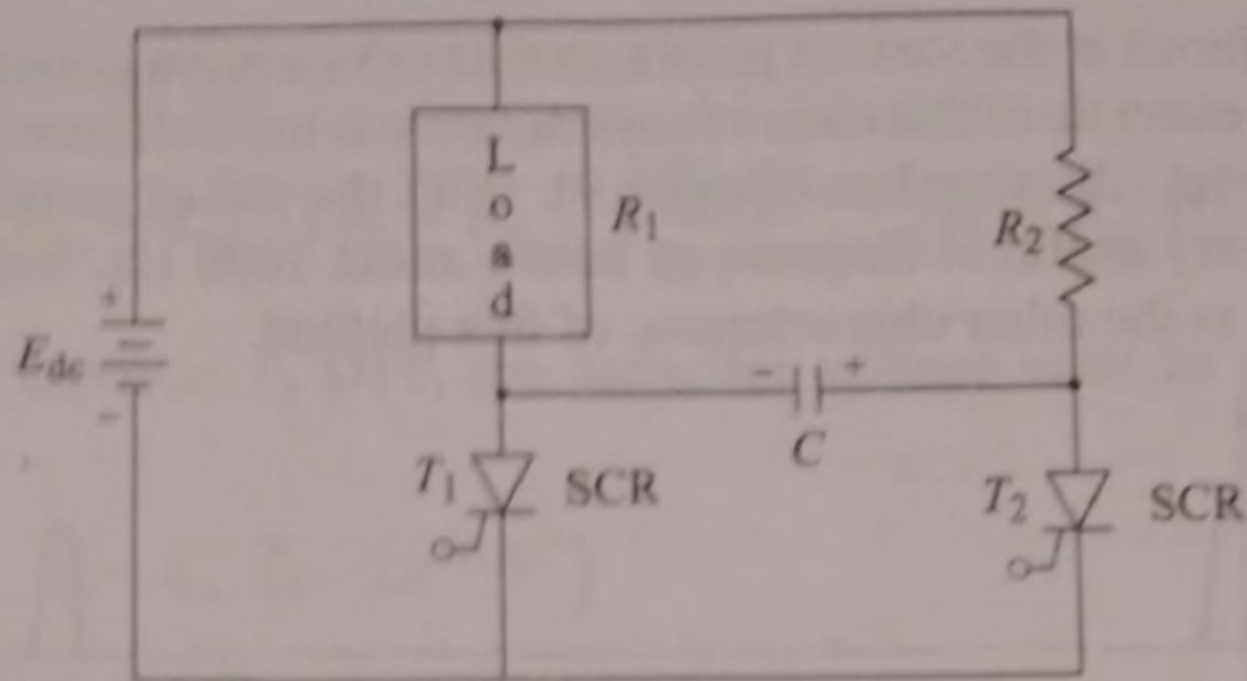
$$L \frac{di}{dt} + \frac{1}{C} \int i dt = 0$$

$$\therefore L \frac{d^2 i}{dt^2} + \frac{1}{C} i(t) = 0$$

Taking laplace transform of the above equation,  $\left( S^2 L + \frac{1}{C} \right) I(s) = 0$

$$\therefore i(t) = E_{dc} \sqrt{\frac{C}{L}} \sin \omega_0 t$$

where  $\omega_0 = \sqrt{\frac{1}{LC}}$



**Fig. 2.17** Class C-commutation circuit

### Circuit Operation

(a) *Mode 0: [Initial-state of circuit]* Initially, both the thyristors are OFF. Therefore, the state of the devices are –

**(c) Mode 2:** When a triggering pulse is applied to the gate of  $T_2$ ,  $T_2$  will be turned on. As soon as  $T_2$  is ON, the negative polarity of the capacitor  $C$  is applied to the anode of  $T_1$  and simultaneously, the positive polarity of capacitor  $C$  is applied to the cathode. This causes the reverse voltage across the main thyristor  $T_1$  and immediately turns it off.

Charging of capacitor  $C$  now takes place through the load and its polarity becomes reverse. Therefore, charging path of capacitor  $C$  becomes

$$E_{dc} \rightarrow R_1 \rightarrow C_1 \rightarrow C \rightarrow T_{2(a-k)} \rightarrow E_{dc}$$

Hence, at the end of Mode 2, the states of the devices are

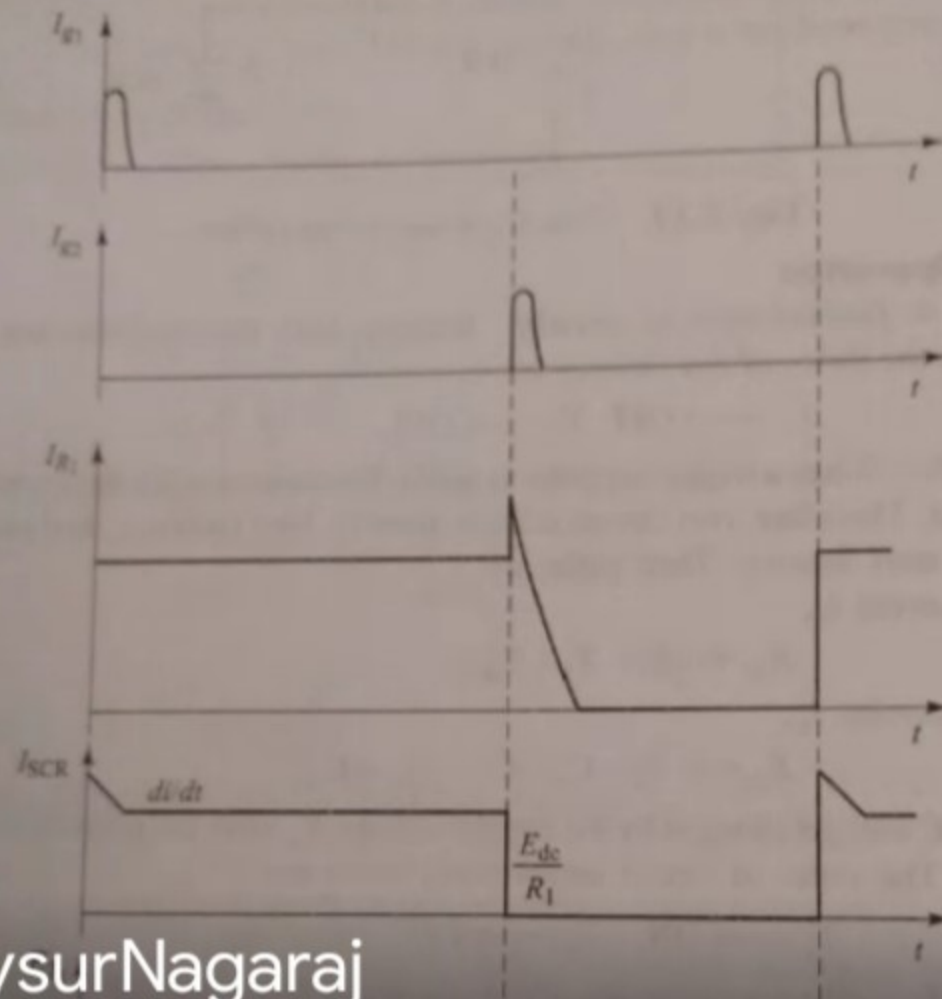
$$T_1 \longrightarrow \text{OFF}, \quad T_2 \longrightarrow \text{ON}, \quad E_{c1} = -E_{dc}$$

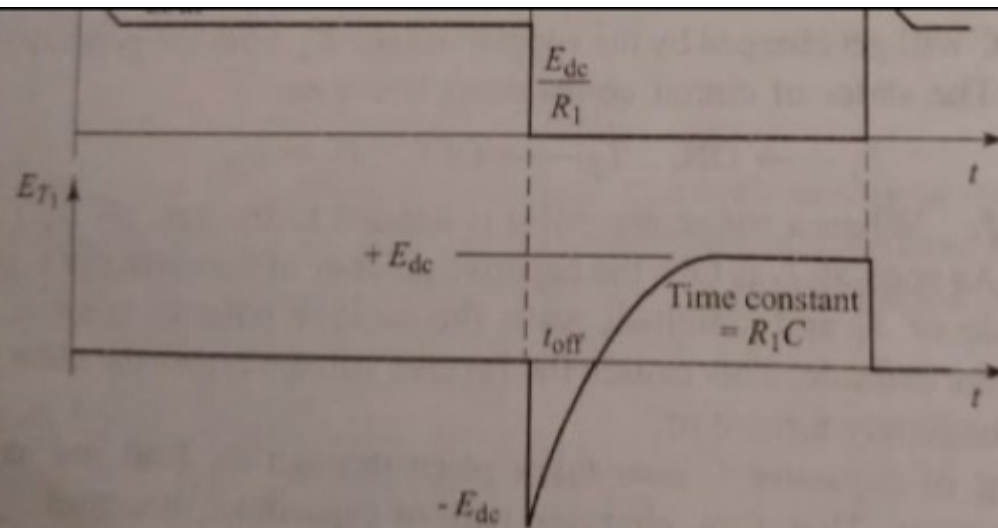
**(d) Mode 3:** Now, when thyristor  $T_1$  is triggered, the discharging current of capacitor turns the complementary thyristor  $T_2$  OFF. The state of the circuit at the end of this Mode 3 becomes

$$T_1 \longrightarrow \text{ON}, \quad T_2 \longrightarrow \text{OFF}, \quad E_{c1} = E_{dc}$$

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commutation is the other characteristic of this method.





**Fig. 2.18** Circuit waveforms

### **Design Considerations**

As explained previously, when thyristor  $T_1$  is conducting, capacitor  $C$  is charged to d.c. supply voltage  $E_{dc}$  through the resistor  $R_2$ . Now, when  $T_2$  is triggered, a voltage twice the d.c. supply voltage  $E_{dc}$  is applied to the  $R_1C$  series circuit so that current through the circuit is,

$$i = \frac{2E_{dc}}{R_1} e^{-t/R_1C} \quad (2.42)$$

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Therefore, the voltage across the thyristor  $T_1$  is

$$E_{T_1} = E_{dc} - i R_1 = E_{dc} - \frac{2E_{dc}}{R_1} e^{-t/R_1 C} \cdot R_1 = E_{dc} (1 - 2 e^{-t/R_1 C})$$

For making thyristor  $T_1$  OFF, the capacitor voltage must be equal to the voltage  $E_{T_1}$ .

$$\therefore E_c = E_{dc} (1 - 2 e^{-t/R_1 C}) \quad (2.43)$$

Let  $t = t_{off}$  when  $E_c = 0$ .

$\therefore$  Equation (2.43) becomes

$$0 = E_{dc} (1 - 2 e^{-t_{off}/R_1 C}) \quad \text{or} \quad 0 = 1 - 2 e^{-t_{off}/R_1 C} \quad (2.44)$$

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$$\therefore t_{\text{off}} = 0.6931 R_1 C \quad (2.45)$$

$$\text{or } C = 1.44 \frac{t_{\text{off}}}{R_1} \quad (2.46)$$

So from Eq. (2.45),  $R_1$  and  $C$  must be such that the turn-off time of SCR  $T_1$ ,  $t_{\text{off}}$  is satisfied.

The maximum allowable  $\frac{dV}{dt}$  rating for SCR  $T_1$  may be obtained from the SCR  $T_1$  data sheet.

The maximum  $\frac{dV}{dt}$  across  $T_1$  using the commutating components is given by

$$\frac{dV}{dt} > \frac{2 E_{\text{dc}}}{R_1 C} \quad (2.47)$$

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4. Class D—Auxiliary Commutation (An Auxiliary SCR Switching a

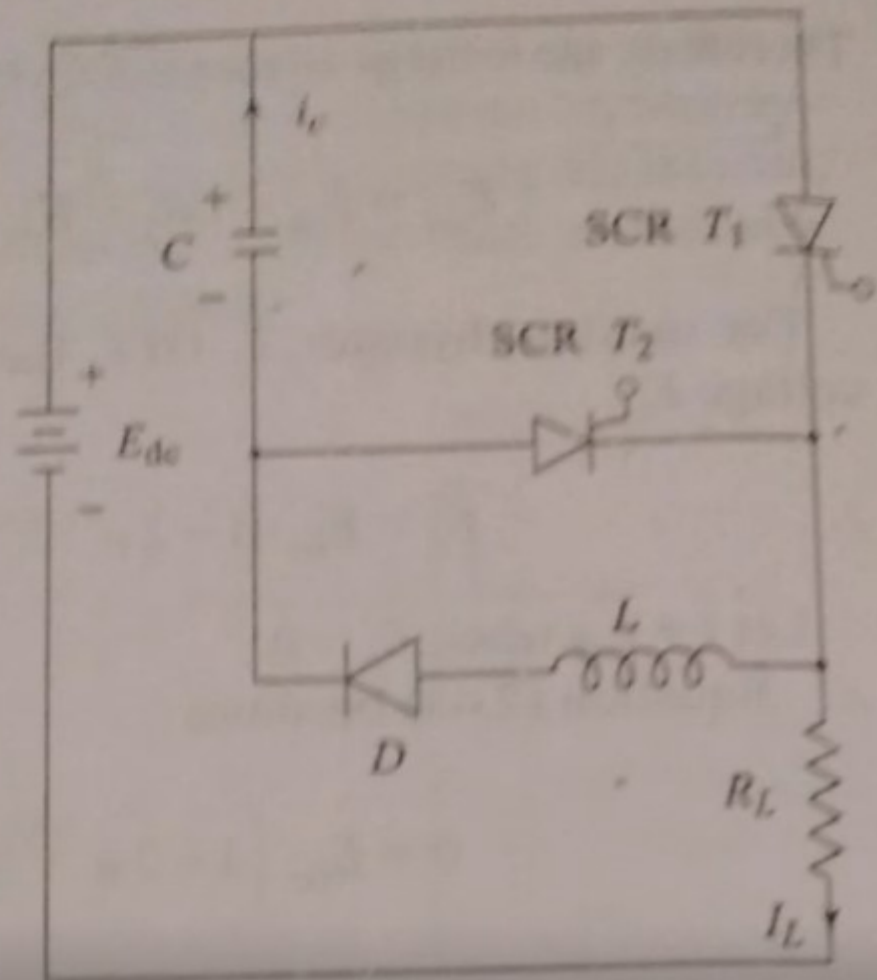


**(b) Mode 1:** Initially, SCR  $T_2$  must be triggered first in order to charge the capacitor  $C$  with the polarity shown. This capacitor  $C$  has the charging path  $E_{dc+} \rightarrow C_+ \rightarrow C_- \rightarrow T_2 \rightarrow R_L \rightarrow E_{dc-}$ . As soon as capacitor  $C$  is fully charged, SCR  $T_2$  turns-off. This is due to the fact that, as the voltage across the capacitor increases, the current through the thyristor  $T_2$  decreases since capacitor  $C$  and thyristor  $T_2$  form the series circuit.

Hence the state of circuit components at the end of Mode 1 becomes,

$T_1 \rightarrow \text{OFF}, T_2 \rightarrow \text{OFF}, E_C = E_{dc}$

**(c) Mode 2:** When thyristor  $T_1$  is



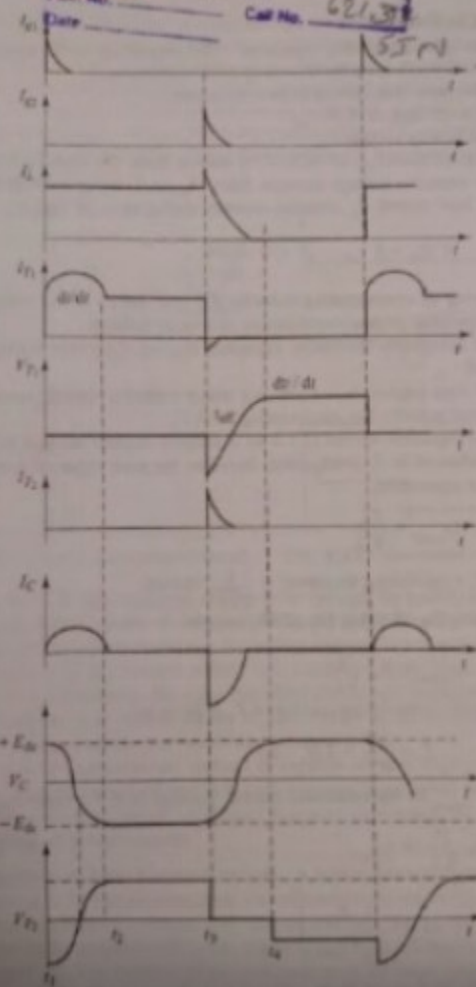


Fig. 2.20. Associated waveforms

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$$C E_{dc} = I_L t_{off} \quad \therefore C = \frac{I_L t_{off}}{E_{dc}} \quad (2.48)$$

(b) *Designing of commutating inductor L* The design of the inductor  $L$  is actually dependent on two contradictory criteria as follows:

- (i) The acceptable maximum capacitor current,  $I_C$ , when thyristor  $T_1$  is fired.
- (ii) The time interval  $(t_2 - t_1)$  during which capacitor voltage must reset to correct polarity for commutating SCR  $T_1$ .

Since the capacitor current ( $I_C$ ) is an oscillatory current through SCR  $T_1$ ,  $L$ ,  $D$ , and  $C$  when SCR  $T_1$  is triggered, therefore the peak value of current  $I_C$  is given by the expression,

$$I_{C(\text{peak})} = \frac{E_{dc}}{W_r L} \quad (2.49)$$

$$\text{PradeepmysurNagaraj} \quad \text{Resonant frequency} = \frac{1}{\sqrt{LC}} \text{ rad/sec.} \quad (2.50)$$