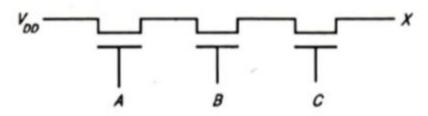
## The Pass Transistor



Pass transistor And gate.

$$X = A.B.C$$
 (Logic 1 =  $V_{OO} - V_I$ )

The output conductance gds can be expressed by

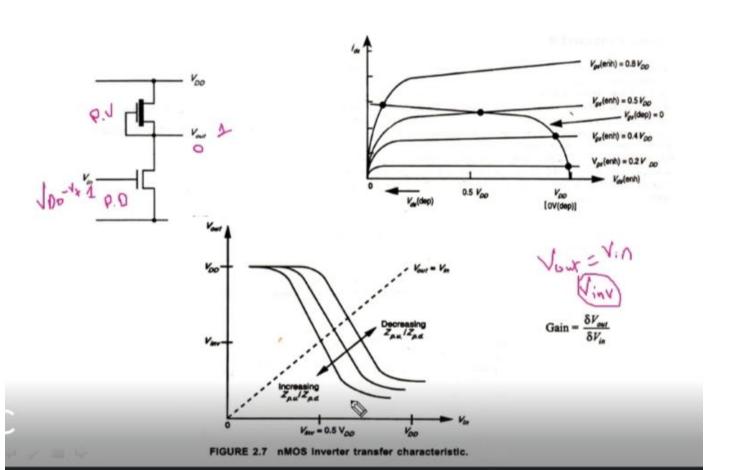
$$g_{ds} = \frac{\delta I_{ds}}{\delta V_{gs}} = \lambda . I_{ds} \alpha \left(\frac{1}{L}\right)^2$$

Here the strong dependence on the channel length is demonstrated as

$$\lambda \alpha \left(\frac{1}{L}\right)$$
 and  $I_{ds} \alpha \left(\frac{1}{L}\right)$ 

for the MOS device.

## The nMOS Inverter



## DETERMINATION OF PULL-UP TO PULL-DOWN RATIO (Zp.u) Zp.d.) FOR AN nMOS INVERTER DRIVEN BY ANOTHER nMOS INVERTER

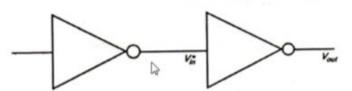


FIGURE 2.8 nMOS inverter driven directly by another inverter.

For equal margins around the inverter threshold, we set  $Vinv = 0.5 \ VDD$ . At this point both transistors are in saturation and

$$I_{ds} = K \frac{W}{L} \frac{(V_{gs} - V_t)^2}{2}$$

In the depletion mode

$$I_{ds} = K \frac{W_{p.u.}}{L_{p.u.}} \frac{(-V_{td})^2}{2} \text{ since } V_{gs} = 0$$

and in the enhancement mode

$$I_{ds} = K \frac{W_{p.d.}}{L_{p.d.}} \frac{(V_{inv} - V_i)^2}{2} \text{ since } V_{gs} = V_{inv}$$

Equating (since currents are the same) we have

$$W_{p.d.}(V - V)^2 =$$

$$\frac{W_{p.d.}}{L_{p.d.}} (V_{inv} - V_t)^2 = \frac{W_{p.u.}}{L_{p.u.}} (-V_{td})^2$$

$$Z_{p.d.} = \frac{L_{p.d.}}{W_{p.d.}}; Z_{p.u.} = \frac{L_{p.u.}}{W_{p.u.}}$$

whence

$$V_{p.d.} = W_{p.d.}$$
,  $V_{p.u.} = W_{p.u.}$ 

thus, from equation (2.9)

Now we can substitute typical values as follows:

$$Z_{p.d.} = \frac{L_{p.d.}}{W_{p.d.}}; Z_{p.}$$

 $\frac{1}{Z_{p.d.}} (V_{inv} - V_t)^2 = \frac{1}{Z_{p.u.}} (-V_{td})^2$ 

 $V_{inv} = V_t - \frac{V_{td}}{\sqrt{Z_{nu}/Z_{nd}}}$ 

 $V_{t} = 0.2V_{DD}$ ;  $V_{td} = -0.6V_{DD}$ 

 $0.5 = 0.2 + \frac{0.6}{\sqrt{Z_{2n}/Z_{pd}}}$ 

 $V_{inv} = 0.5 V_{DD}$  (for equal margins)

(2.9)

## PULL-UP TO PULL-DOWN RATIO FOR AN nMOS INVERTER DRIVEN THROUGH ONE OR MORE PASS TRANSISTORS

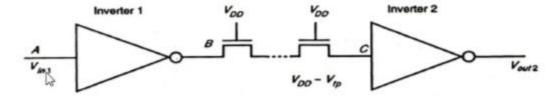


FIGURE 2.9 Pull-up to pull-down ratios for inverting logic coupled by pass transistors.

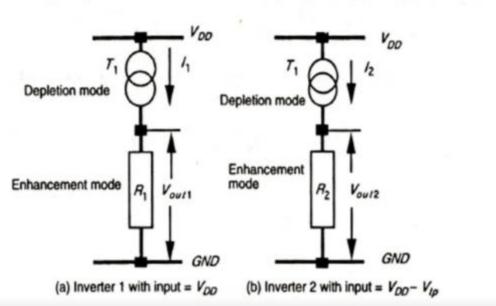


FIGURE 2.10 Equivalent circuits of inverters 1 and 2.

$$I_{ds} = K \frac{W_{p.d.1}}{L_{p.d.1}} \left( (V_{DD} - V_t) V_{ds1} - \frac{V_{ds1}^2}{2} \right)$$

Therefore

$$R_1 = \frac{V_{ds1}}{I_{ds}} = \frac{1}{K} \frac{L_{p.d.1}}{W_{p.d.1}} \left[ \frac{1}{V_{DD} - V_t - \frac{V_{ds1}}{2}} \right]$$

Note that  $V_{ds1}$  is small and  $V_{ds1}/2$  may be ignored. Thus

$$R_1 \neq \frac{1}{K} Z_{p.d.1} \left( \frac{1}{V_{DD} - V_t} \right)$$

Now, for depletion mode p.u. in saturation with  $V_{gs} = 0$ 

$$I_1 = I_{ds} = K \frac{W_{p.u.1}}{L} \cdot \frac{(-V_{ul})^2}{2}$$

The product

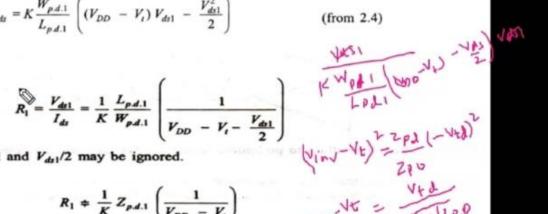
$$I_1R_1 = V_{out}$$

Thus

$$V_{out1} = I_1 R_1 = \frac{Z_{p.d.1}}{Z_{p.d.1}} \left( \frac{1}{V_{DD} - V_t} \right) \frac{(V_{td})^2}{2}$$

Consider inverter 2 (Figure 2.10(b)) when input =  $V_{DD} - V_{tp}$ . As for inverter 1

$$R_2 = \frac{1}{K} Z_{pd,2} \frac{1}{((V_{DD} - V_{pp}) - V_t)}$$



VIN - 45 = (20/LP.0

(from 2.5)

If inverter 2 is to have the same output voltage under these conditions then 
$$V_{out 1} = V_{out 2}$$
. That is

$$I_1R_1 = I_2R_2$$
Therefore

$$\frac{Z_{pu2}}{Z_{pd2}} = \frac{Z_{pu1}}{Z_{pd.1}} \frac{(V_{DD} - V_t)}{(V_{DD} - V_{tp} - V_t)}$$
Taking typical values

$$V_t = 0.2V_{DD}$$

 $I_2 = K \frac{1}{Z_{p,u,2}} \frac{(-V_{ud})^2}{2}$ 

 $V_{out2} = I_2 R_2 = \frac{Z_{pd.2}}{Z_{nu.2}} \left( \frac{1}{V_{DD} - V_{to} - V_t} \right) \frac{(-V_{td})^2}{2}$ 

 $V_t = 0.2 V_{DD}$ 

 $V_{tp} = 0.3 V_{DD}^*$ 

 $\frac{Z_{p.u.2}}{Z_{p.d.2}} = \frac{Z_{p.u.1}}{Z_{p.d.1}} \frac{0.8}{0.9}$ 

 $\frac{Z_{p.u.2}}{Z_{p.d.2}} \neq 2 \frac{Z_{p.u.1}}{Z_{p.d.1}} = \frac{8}{1}$ 

whence

Therefore