

# Impedance and Windkessels

Leif Rune Hellevik

Department of Structural Engineering  
Norwegian University of Science and Technology  
Trondheim, Norway

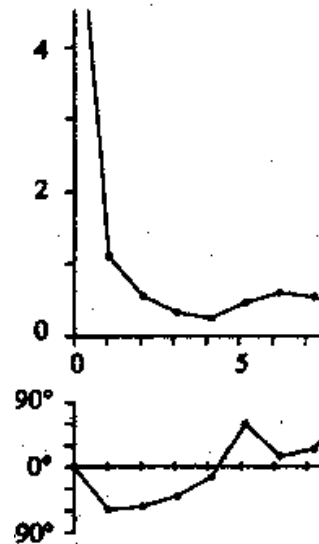
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## Outline

# Arterial input impedance

- ▶ Provides a (complete) and comprehensive description of the arterial system <sup>a</sup>
- ▶ Impedance
  - ▶ A measure of opposition to flow
  - ▶ Frequency dependent resistance
  - ▶ Resistance for non-oscillatory or steady motion
- ▶ Definition
  - ▶ The ratio of harmonic terms of pressure and corresponding harmonic terms of flow

$$p = |\hat{p}|e^{i(\omega t + \phi)}, \quad q = |\hat{q}|e^{i(\omega t + \beta)}$$
$$Z_i = \frac{|\hat{p}|}{|\hat{q}|}e^{j\theta}, \quad \theta = \phi - \beta$$



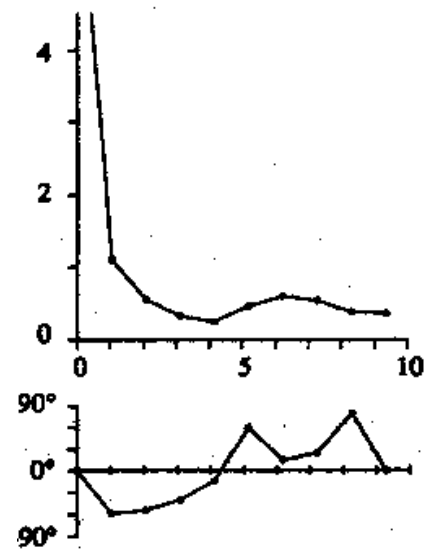
<sup>a</sup>Snapshots of hemodynamics

## Applicability of Fourier analysis

- ▶ Used to related hemodynamic variables such as pressure and flow
- ▶ Not meaningful to related time signals
  - ▶ Diastolic pressure and flow
  - ▶ Division of pressure by zero flow does not provide meaningful information
- ▶ Produce a mean and multiples of the heart rate
- ▶ Each harmonic has an amplitude and a phase angle
- ▶ Impedance
  - ▶ Relate pressure and flow
  - ▶ Ohm's law is applied for each frequency
  - ▶ Only valid for a linear relation between pressure and flow
- ▶ Aortic input impedance
  - ▶ Venous pressure may be neglected
  - ▶ Aortic pressure and flow gives a sufficiently accurate approximation of the input impedance

# Limitations to the use of Fourier analysis

- ▶ May only be used for periodic signals. The value of the signal at start and end should be the same.
- ▶ The relation of two signals should be linear.
- ▶ OK in many cases for pressure and flow despite the nonlinear relation
- ▶ The scatter in modulus and phase has been attributed to nonlinearities
- ▶ High frequency information should be considered with care.



## Reflection factor

- ▶ Occur at any point where there is an abrupt change in characteristic impedance (mismatch in impedance)
- ▶ Oscillations at origin: the reflections will mix with the original pulse
- ▶ Spatial variations in amplitude and different wave pattern in flow and pressure are indicators for reflections
- ▶ Wave separation

$$p = p_f + p_b$$

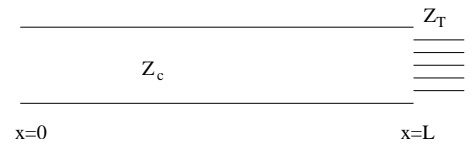
- ▶ Reflection factor

$$\Gamma \equiv \frac{p_b}{p_f} = -\frac{Q_b}{Q_f}$$

- ▶ Easy to show

$$\Gamma = \frac{Z_{in} - Z_c}{Z_{in} + Z_c}$$

# The quarter wavelength formula



- ▶ Forward waves

$$p_f = p_0 e^{j\omega t}, \quad Q_f = \frac{p_0}{Z_c} e^{j\omega t}$$

- ▶ Reflected waves ( $\Gamma = 1$ )

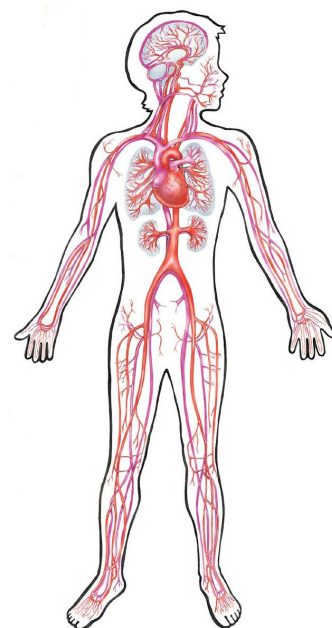
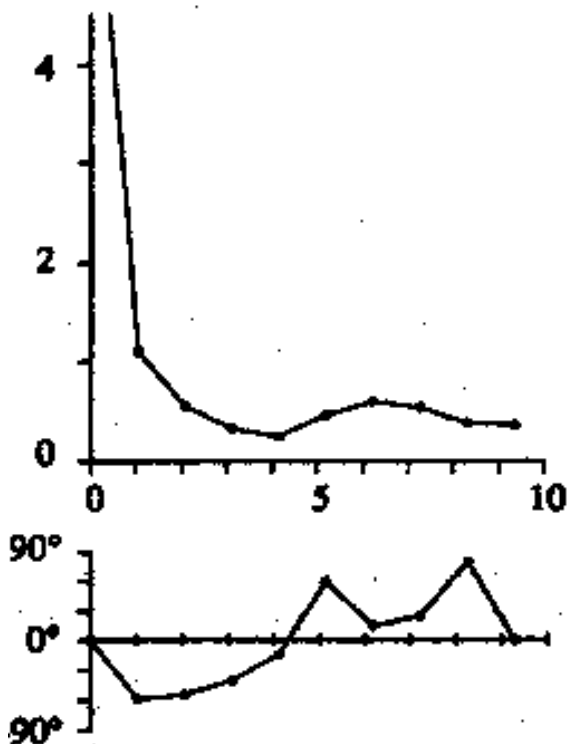
$$p_b = p_0 e^{j\omega(t-2L/c)}, \quad Q_b = -\frac{p_0}{Z_c} e^{j\omega(t-2L/c)}$$

- ▶ Input impedance

$$Z_{in} = \frac{p_f + p_b}{Q_f + Q_b} = Z_c \frac{e^{j\omega t} + e^{j\omega(t-2L/c)}}{e^{j\omega t} - e^{j\omega(t-2L/c)}}$$

- ▶  $Z_{in} = 0 \Rightarrow \frac{2\omega L}{c} = \pi \Rightarrow L = \frac{\lambda}{4}$

## Example: The quarter wavelength formula and $Z_{in}$



$$\min |Z_{in}| \text{ at } f = 3.8 \text{ Hz} \\ \Rightarrow L \approx 0.33 \text{ m}$$

# Characteristic impedance

## ► Governing equations

$$c \frac{\partial p}{\partial t} = - \frac{\partial Q}{\partial x}$$
$$\frac{\partial Q}{\partial t} = - \frac{A}{\rho} \frac{\partial p}{\partial x}$$

## ► Solutions

$$p = p_0 f(x - ct) + p_0^* g(x + ct)$$
$$Q = Q_0 f(x - ct) + Q_0^* g(x + ct)$$

## ► By subst in momentum equation and collection of terms

$$\left( \frac{A}{\rho} p_0 - c Q_0 \right) f' + \left( \frac{A}{\rho} p_0^* + c Q_0^* \right) g' = 0$$

## ► Must hold for arbitrary $f'$ and $g'$

$$Z_c = \frac{p_0}{Q_0} = - \frac{p_0^*}{Q_0^*} = \frac{\rho c}{A}$$

## Practical estimation of $Z_c$

### ► Average of $Z_i$

- Higher frequencies cancel and are damped
- Average between 4th and 10th harmonic

### ► Slope of $p$ and $Q$

- In early part of systole/ejection phase

$$Z_c = \frac{\Delta p / \Delta t}{\Delta Q / \Delta t}$$

- Both methods rely on the fact that  $Z_c$  is a p-Q relation in absence of reflections
- Reflections are small in early systole and at high frequencies

# Explanations of the input impedance

## ▶ The Windkessels

- ▶ Two-element Windkessel
  - ▶ The original
  - ▶ Peripheral resistance  $R_p$
  - ▶ Total arterial compliance  $C$
- ▶ Three-element Windkessel
  - ▶ Aortic characteristic impedance  $Z_c$
  - ▶  $\bar{p}/\bar{q} = R_p + R_c \neq R_p$
  - ▶ Leads to errors for estimates of  $C$
- ▶ Four-element Windkessel
  - ▶ Corrects for the above shortcomings
  - ▶ Total arterial inertance  $L$

## ▶ Wave transmission

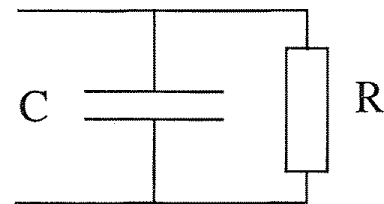
- ▶  $Z_i = Z_c$  for reflectionless system
- ▶  $Z_i \neq Z_c$  in the aorta for low frequencies
- ▶ Reflections at bifurcations and locations of impedance mismatch
- ▶ Waves with high frequencies return out of phase and cancel
- ▶ Damping is also stronger for high frequencies
- ▶ Apparently no reflections for high frequencies

## The Windkessel model<sup>1</sup>

- ▶ Peripheral resistance:  $R_p$
- ▶ Total arterial compliance:  $C = \frac{\partial V}{\partial p}$
- ▶ Flow split
  - ▶  $Q_a = \frac{\partial V}{\partial p} \frac{\partial p}{\partial t} = C \frac{\partial p}{\partial t}$
  - ▶  $Q_p = \frac{p}{R_p}$
- ▶ Mass:  $Q = C \frac{\partial p}{\partial t} + \frac{p}{R_p}$
- ▶ In diastole

$$\frac{\partial p}{\partial t} = -\frac{p}{RC}$$

$$p = p_0 e^{-t/RC}, \quad R = \frac{\bar{p}}{\bar{Q}}$$



## ▶ Problems

- ▶ Cannot fit exp decay to whole diastole
- ▶ When  $c \uparrow$  for old, 2-elt WK does better

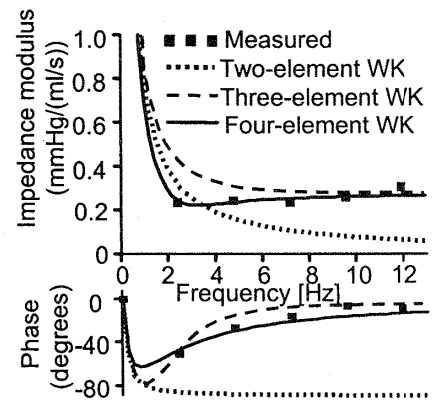
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<sup>1</sup>Otto Frank 1899

## Impedance for the Windkessel model

- ▶ Mass:  $Q = C \frac{\partial p}{\partial t} + \frac{p}{R_p}$
- ▶ Fourier:  $p = \hat{p} e^{j\omega t}$ ,  $Q = \hat{Q} e^{j\omega t}$
- ▶ By substitution

$$\hat{Q} = j\omega C \hat{p} + \frac{\hat{p}}{R_p}$$



- ▶ Impedance

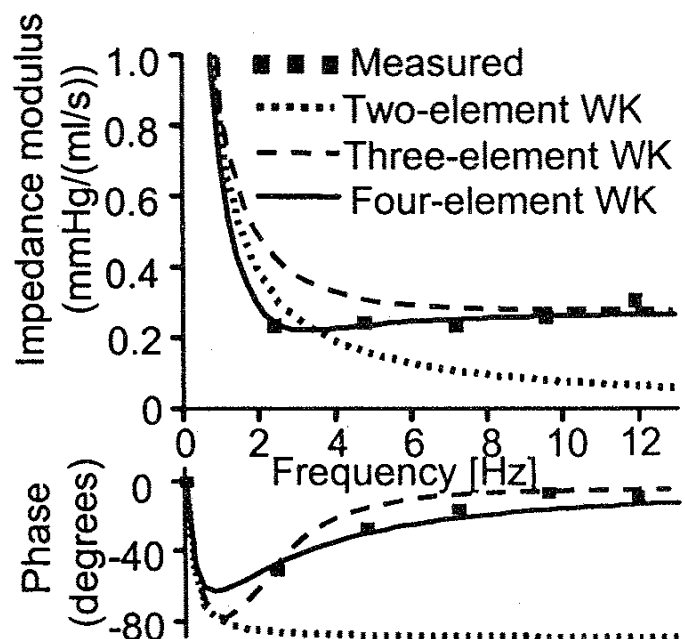
$$Z = \frac{\hat{p}}{\hat{Q}} = \frac{R_p}{1 + j\omega R_p C} = \frac{R_p}{1 + (\omega R_p C)^2} (1 - j\omega R_p C)$$

$$|Z| = \frac{R_p}{1 + (\omega R_p C)^2} \sqrt{1 + (\omega R_p C)^2} = \frac{R_p}{\sqrt{1 + (\omega R_p C)^2}}$$

$$\angle Z = -\arctan \omega R_p C$$

## Limitations of the Windkessel

- ▶ At high frequencies  $|Z| \rightarrow 0$ , not  $Z_c$
- ▶ At high frequencies  $\angle Z \rightarrow -90^\circ$ , not 0
- ▶ High frequency information not captured

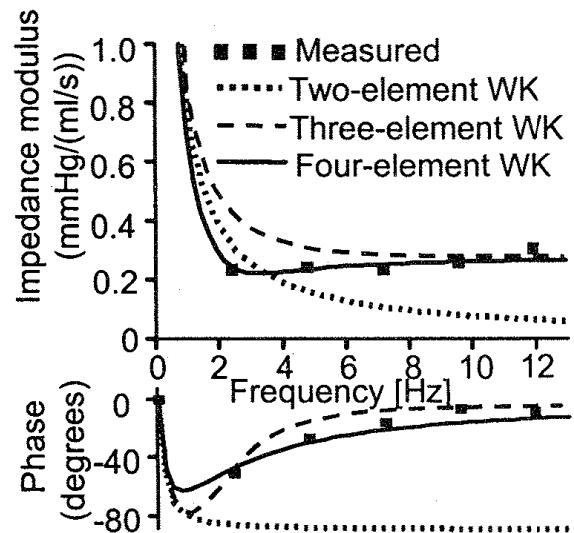
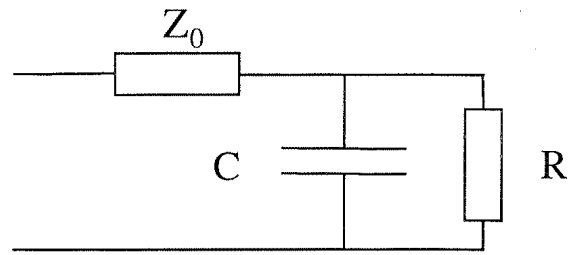


# The Westkessel model<sup>2</sup> (3-elt WK)

- ▶ To correct for high frequency problems
- ▶ Impedance

$$Z = Z_c + \frac{R_p}{1 + j\omega R_p C}$$

- ▶ Pros
  - ▶ Good high frequency  $|Z|$
  - ▶ Good high frequency  $\angle Z$
  - ▶ Good fit of  $p$  and  $Q$
- ▶ Cons
  - ▶ Bad compliance estimates
  - ▶ Bad low frequency est
  - ▶ Only monotonous decay in  $|Z|$



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<sup>2</sup>Westerhof

## Summary