

Hearth Models

Biomechanics lecture

Anatomy of the human heart

- Heart chambers

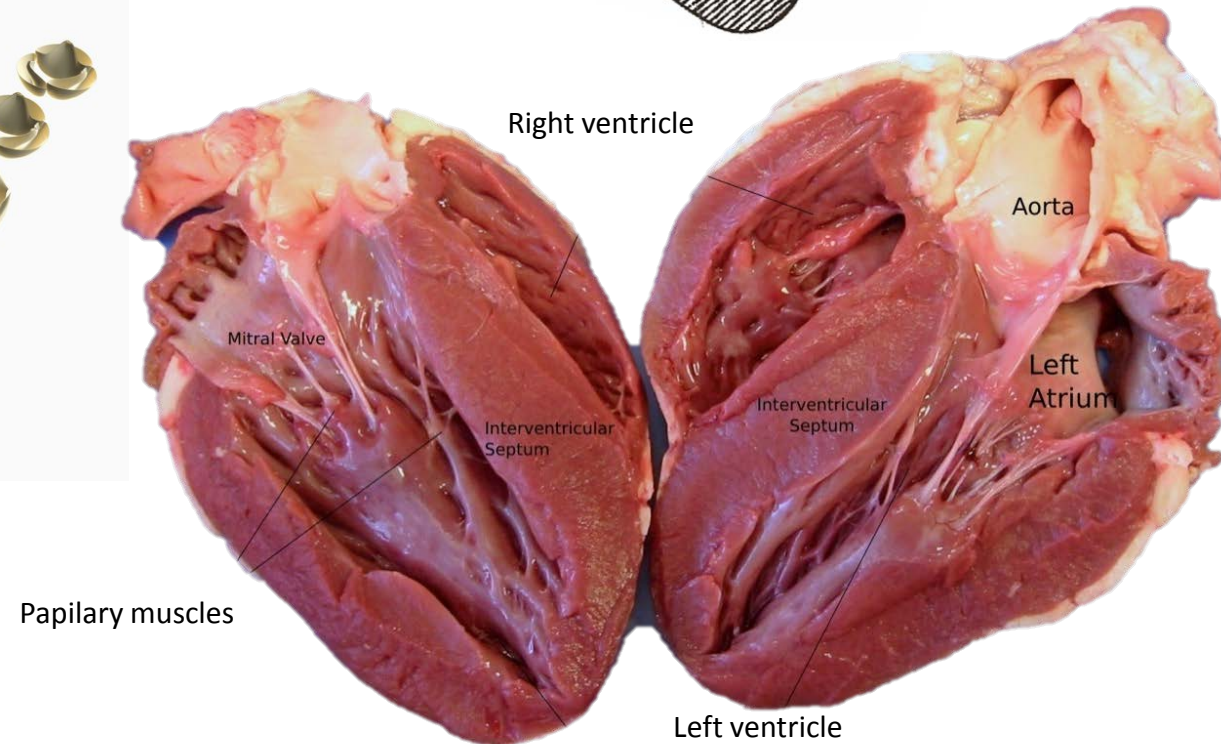
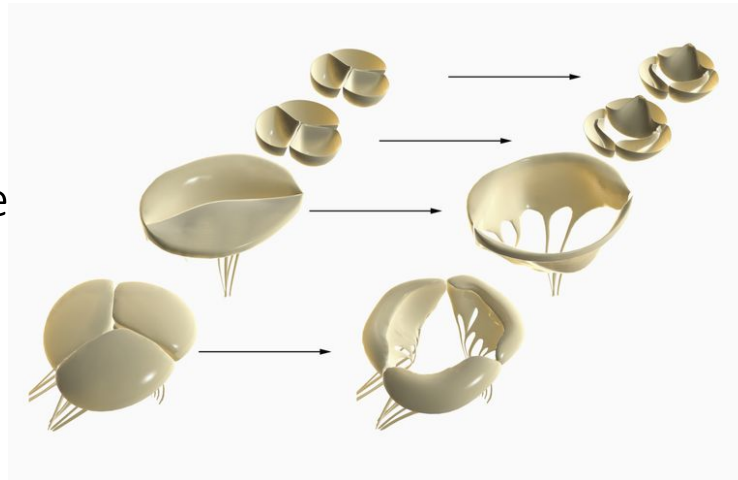
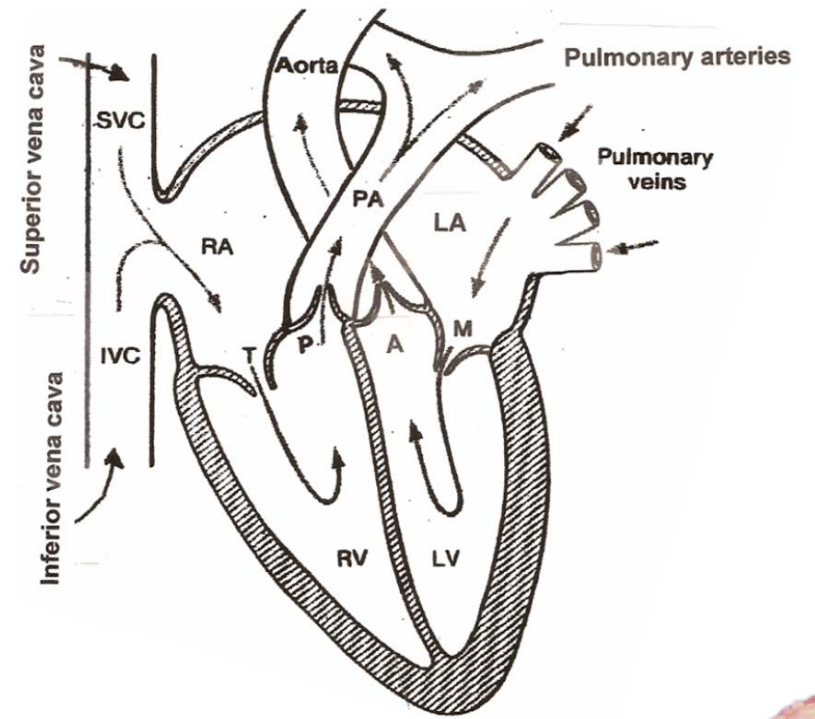
- Right atrium
- Left atrium
- Right ventricle
- Left ventricle

- Valves

- aortic valve
- pulmonary valve
- mitral valve
- tricuspid valve

- Main cycles

- Diastole (filling)
- Systole (ejection)



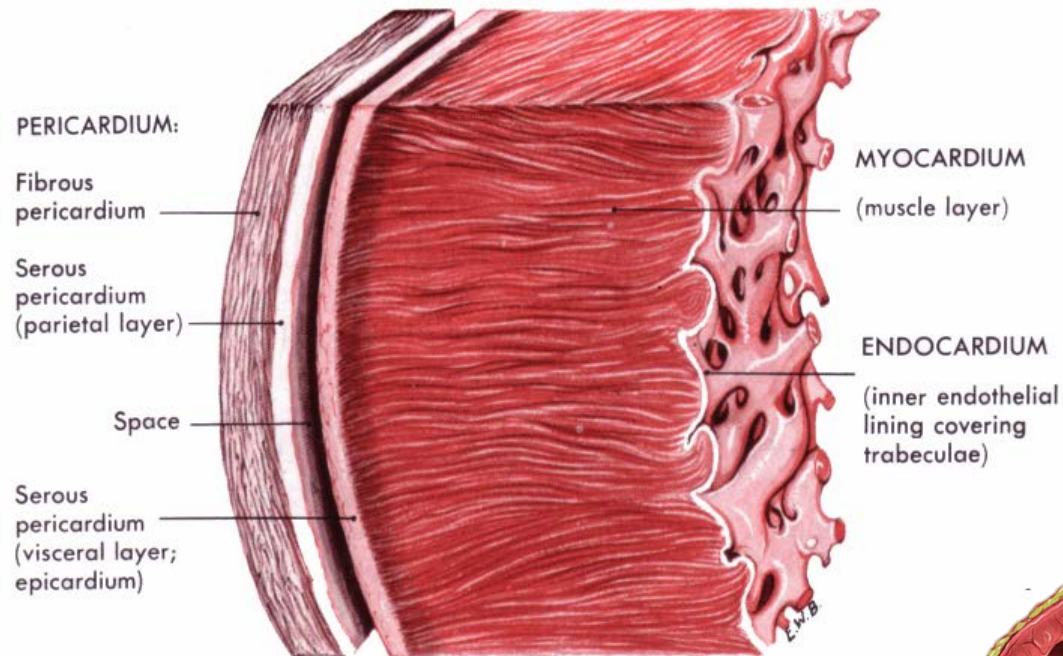
Anatomy of the human heart

- Thee layers

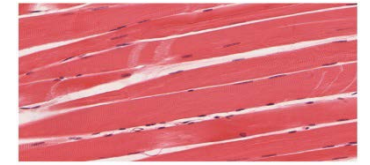
- Pericardium
- Myocardium
- Endocardium

- Hearth muscles

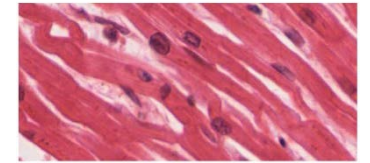
- Myocardium



Section of the heart wall showing the components of the outer pericardium (heart sac), muscle layer (myocardium), and inner lining (endocardium).



Skeletal muscle

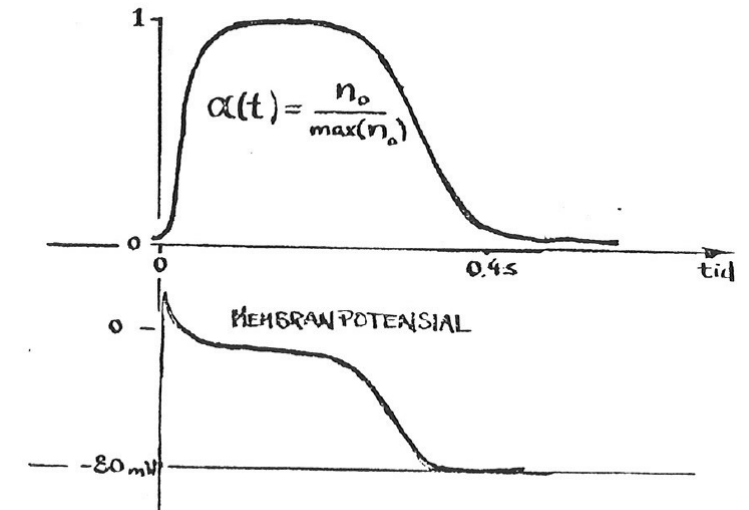
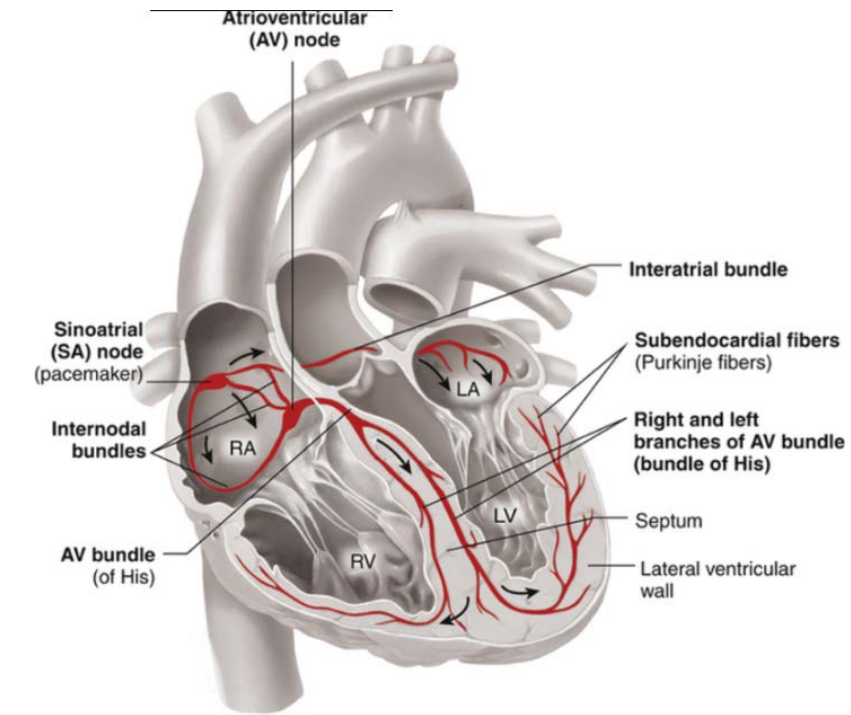
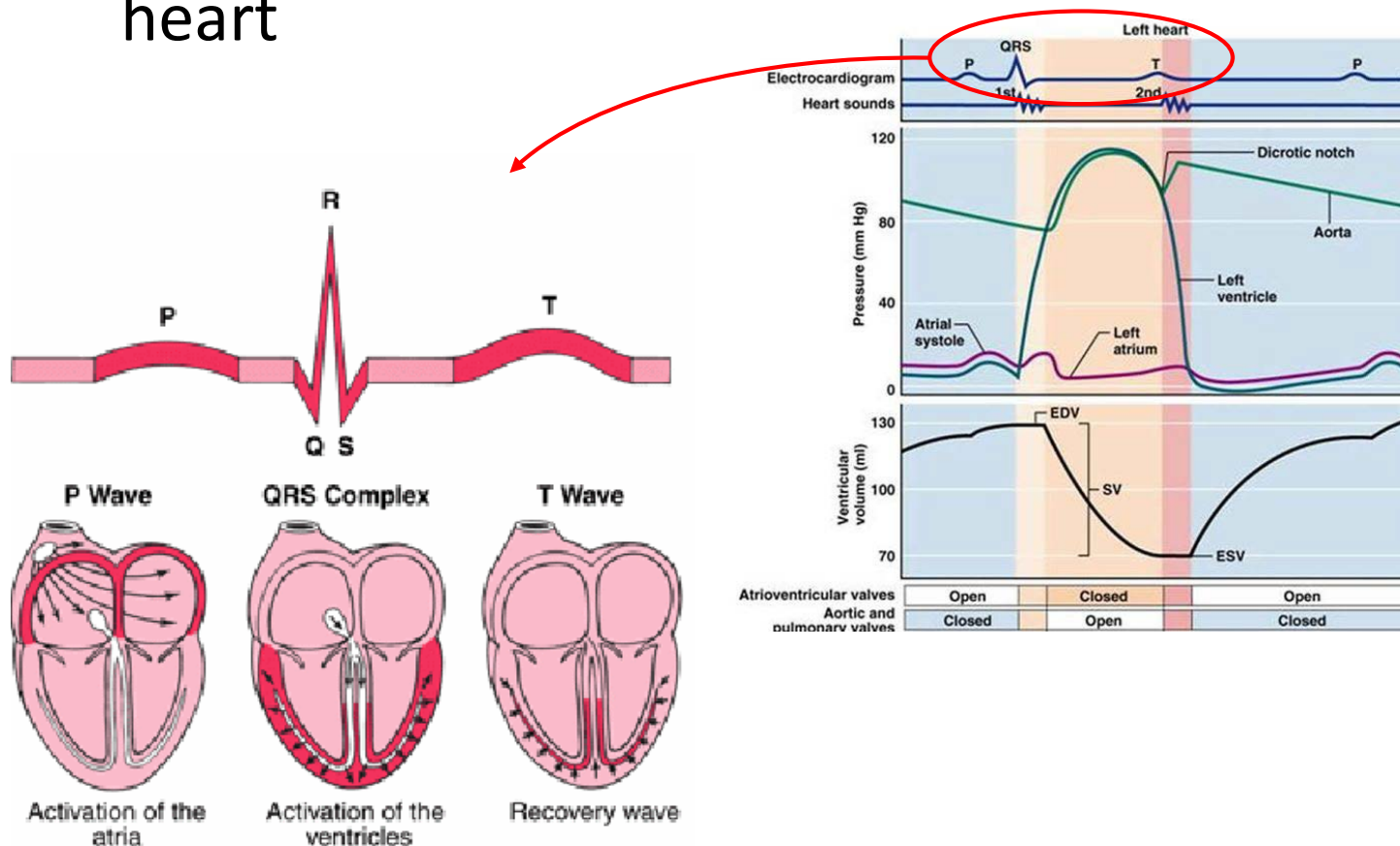


Myocardium



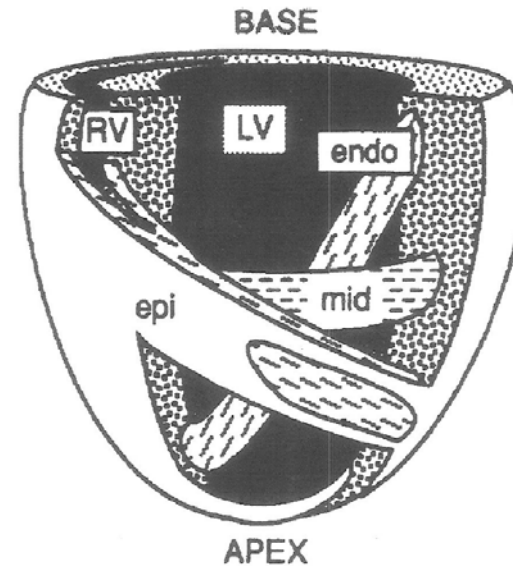
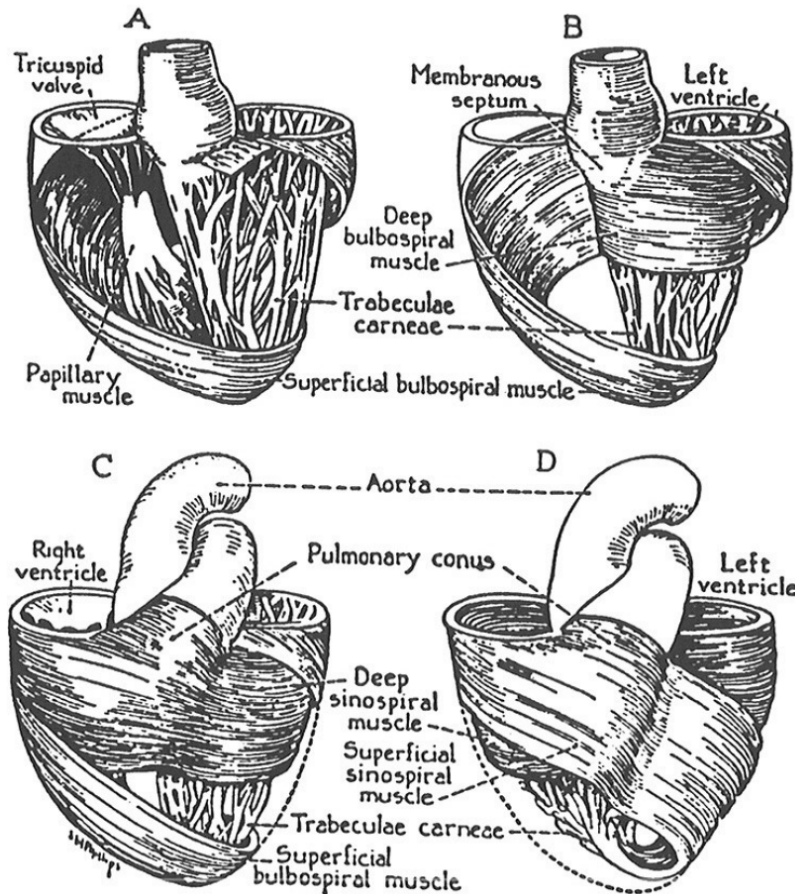
Anatomy of the human heart

- Electrical activity of the heart

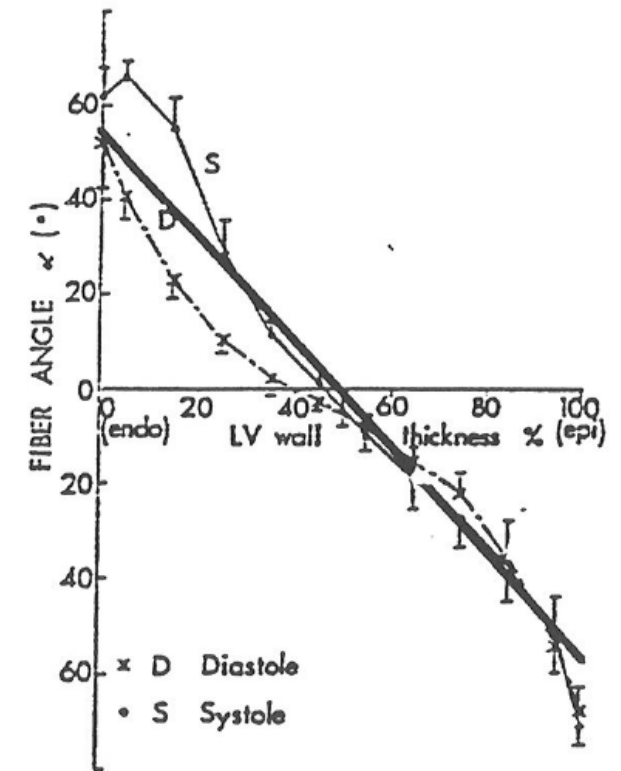
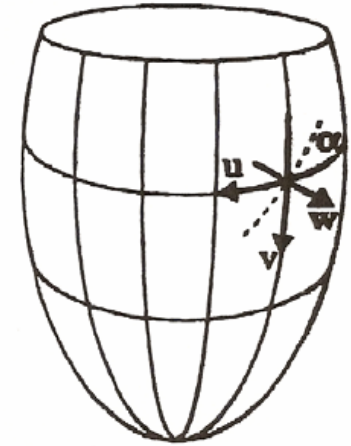


Anatomy of the human heart

- Myocardium fiber directions

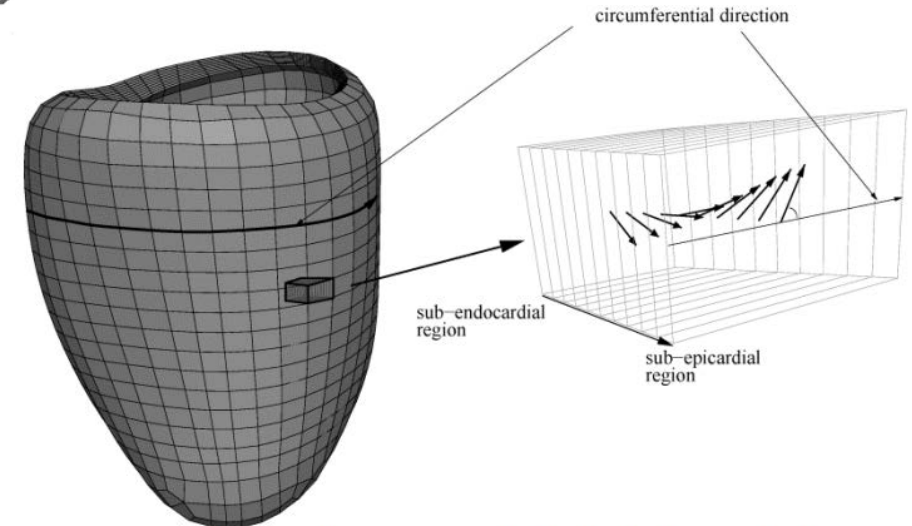
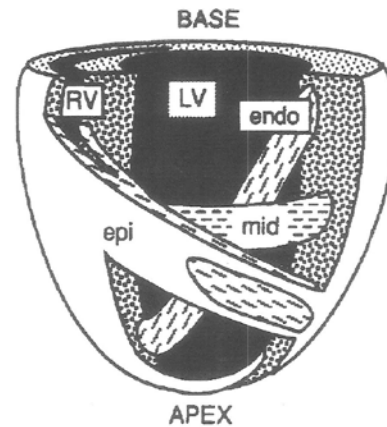
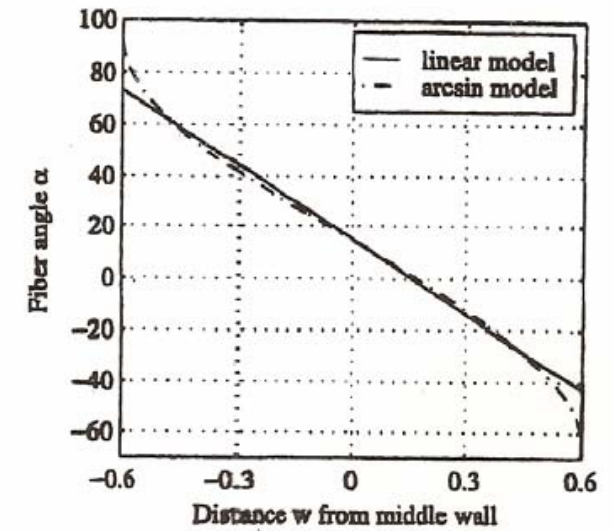


Arts et al, 1979.



Models of the left ventricle

- **The early, simple models** of the left ventricle assume a thin-walled chamber obeying Laplace's law
- **In a newer generation of models**, the left ventricle is considered to be a thick-walled spherical or ellipsoidal shell having isotropic material properties
- **A more accurate description** of the geometry of the LV requires the use of finite element methods, applied to an ellipsoidal or more realistic geometry with isotropic or anisotropic material properties



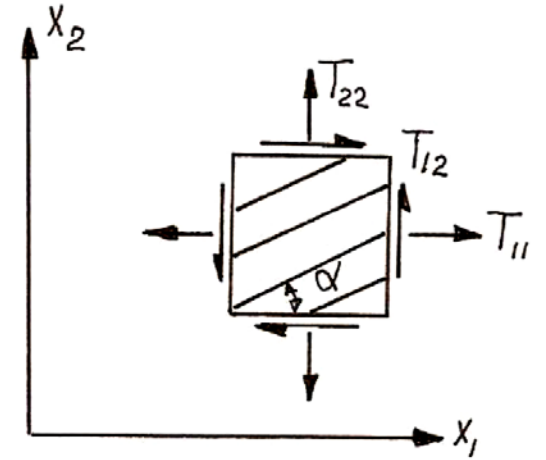
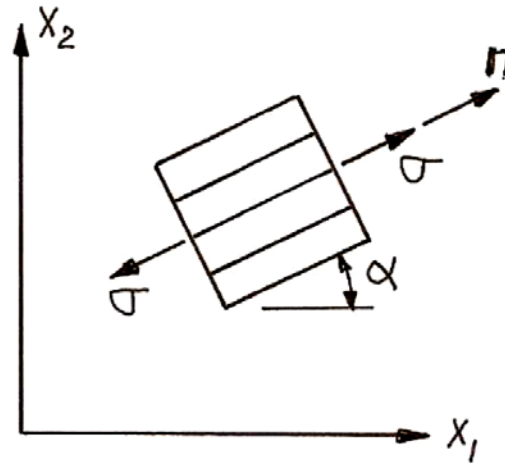
Finite element model of a left ventricle

The fluid-fiber continuum

- Chadwick et al, 1982, proposed a mechanical model of the LV in which he regarded the myocardium as a fluid-fiber continuum.

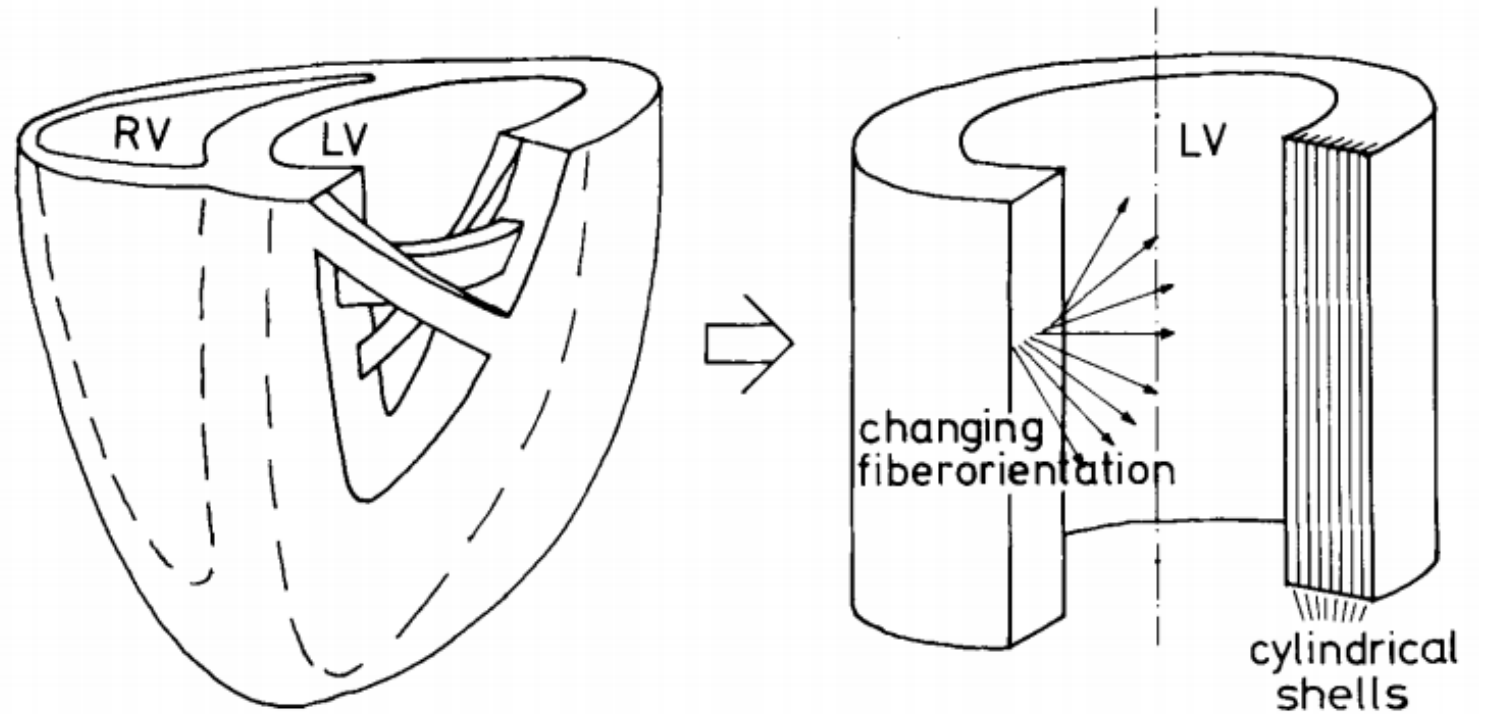
$$T_{ij} = -p \delta_{ij} + \sigma n_i n_j$$

$$T_{11} = -p + \sigma \cos^2 \alpha, \quad T_{22} = -p + \sigma \sin^2 \alpha, \quad T_{33} = -p, \quad T_{12} = \sigma \sin \alpha \cos \alpha$$



The Arts model of the left ventricle

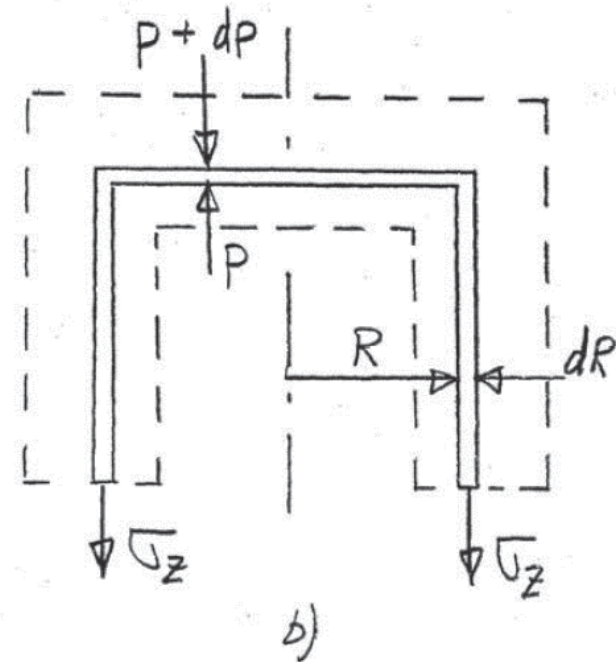
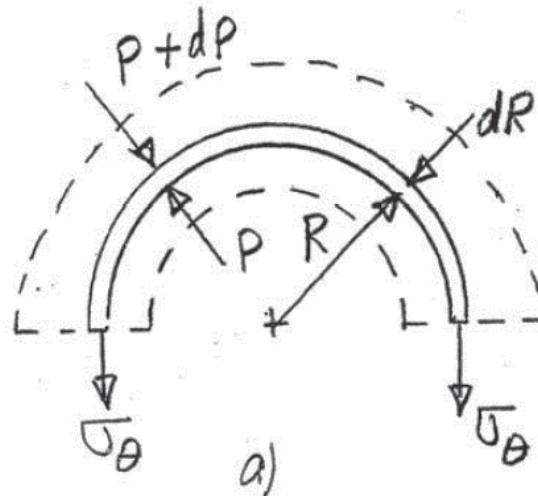
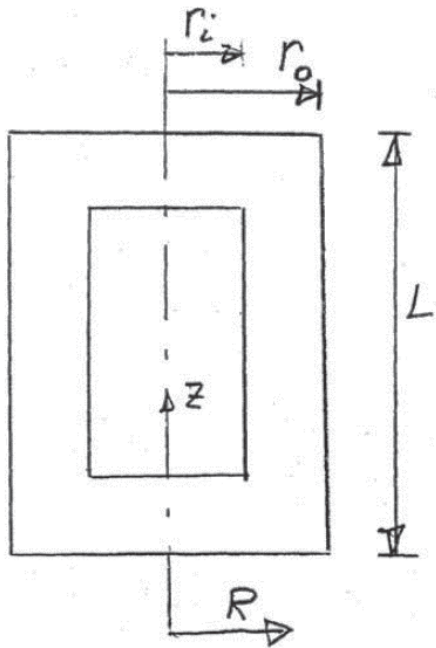
- Arts et al, 1979, the left ventricle is modeled as a thick-walled cylinder composed of 8 concentric cylindrical shells



The Arts model of the left ventricle

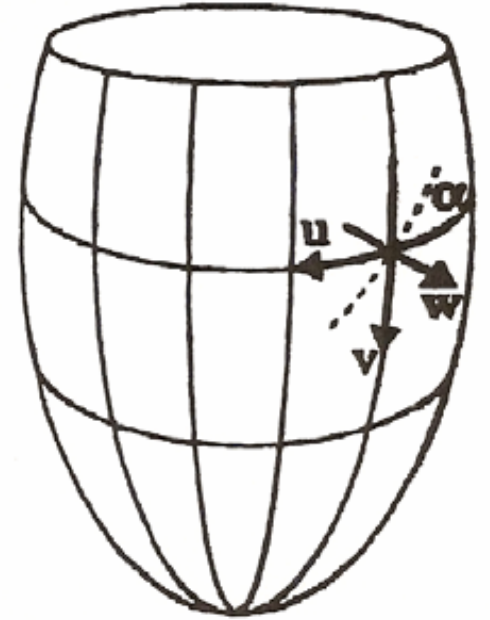
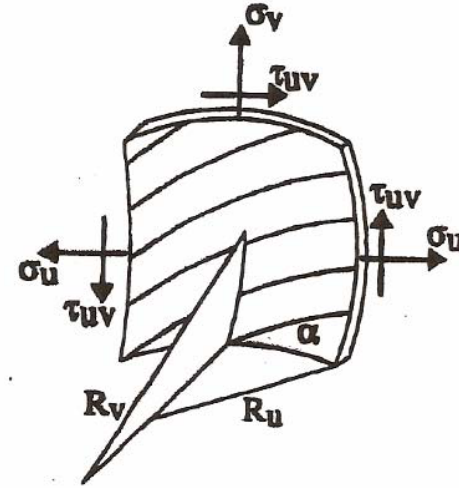
- Arts et al, 1979, the left ventricle is modeled as a thick-walled cylinder composed of many concentric cylindrical shells

$$\frac{p_{lv}}{\sigma} = \frac{1}{3} \ln \left(1 + \frac{V_w}{V_{lv}} \right)$$

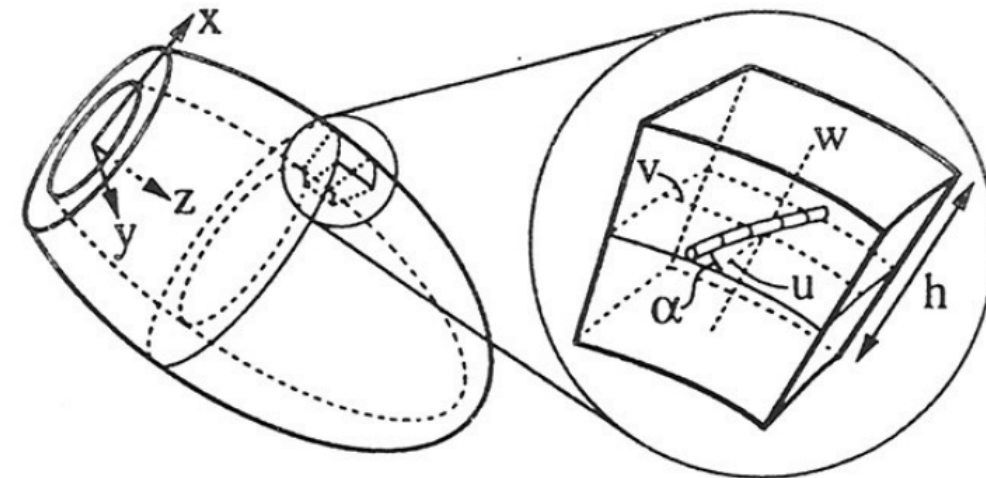


The ellipsoidal model

- Rabben et al, proposed an ellipsoidal model of where the left ventricle is modeled as a thick-walled shell. The middle surface of the thick-walled shell is an axisymmetric ellipsoid

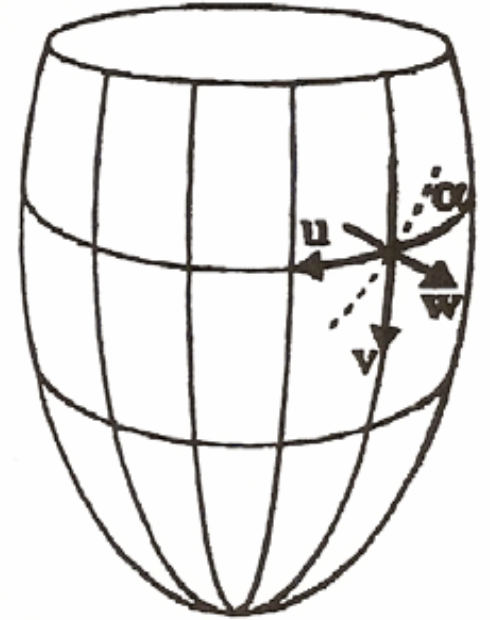
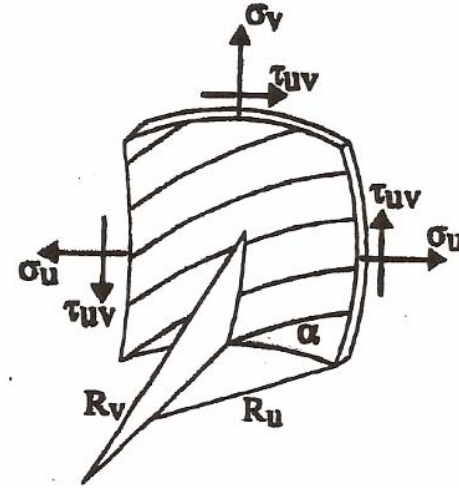


1. The surfaces $w = \text{constant}$ are isobars, i.e. surfaces of constant intra-myocardial pressure.
2. The u -lines and v -lines are along the principal curvature directions. The radii of curvature are R_u with respect to the u -lines and R_v with respect to the v -lines.
3. The w -coordinate is normal to the isobars.
4. The muscle fibers are parallel to the isobars.



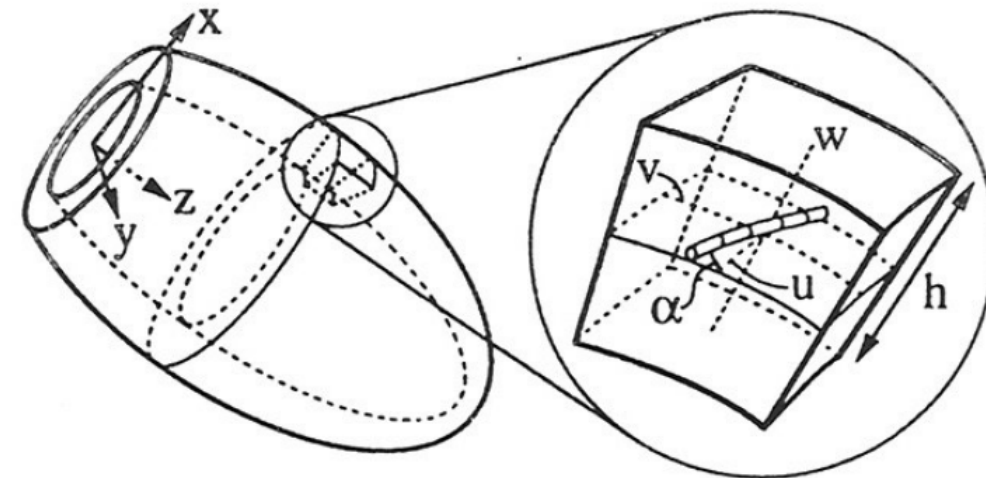
The ellipsoidal model

- Rabben et al, proposed an ellipsoidal model of where the left ventricle is modeled as a thick-walled shell. The middle surface of the thick-walled shell is an axisymmetric ellipsoid



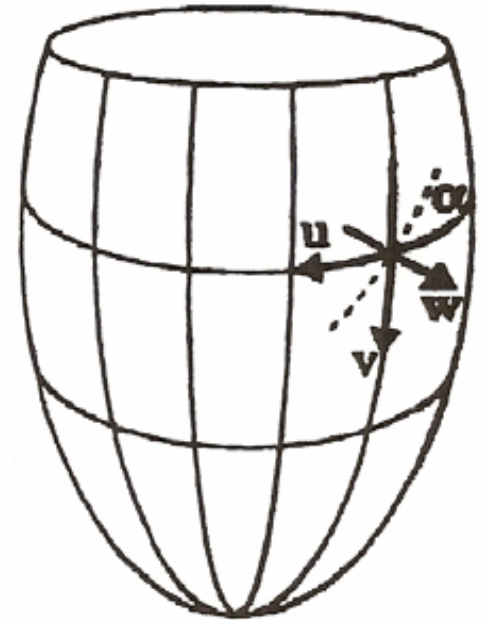
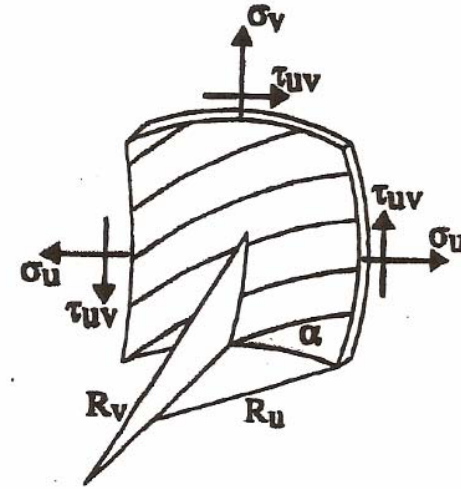
$$T_{11} = -p + \sigma \cos^2 \alpha, \quad T_{22} = -p + \sigma \sin^2 \alpha, \quad T_{33} = -p, \quad T_{12} = \sigma \sin \alpha \cos \alpha$$

$$\sigma_u = \sigma \cos^2 \alpha, \quad \sigma_v = \sigma \sin^2 \alpha, \quad \sigma_w = 0, \quad \tau_{uv} = \sigma \sin \alpha \cos \alpha$$



The ellipsoidal model

- Equilibrium



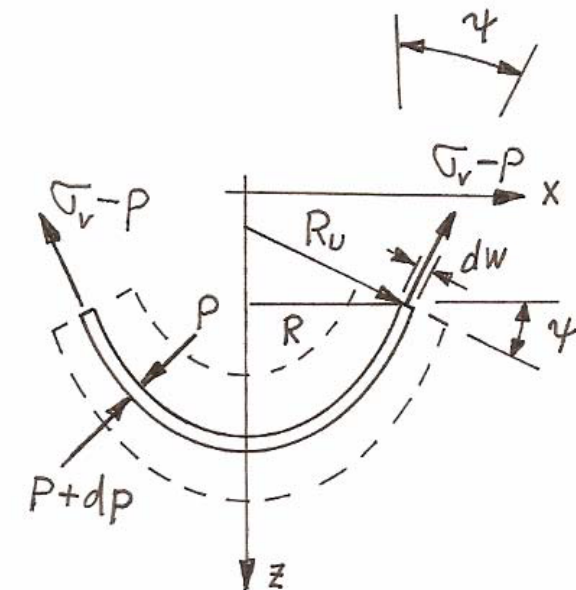
$$-\frac{dp}{dw} = \frac{2\sigma}{R_u(3 - R_u/R_v)}$$

$$\sigma_u = \sigma \cos^2 \alpha, \quad \sigma_v = \sigma \sin^2 \alpha$$

$$\sigma_u + \sigma_v = \sigma$$

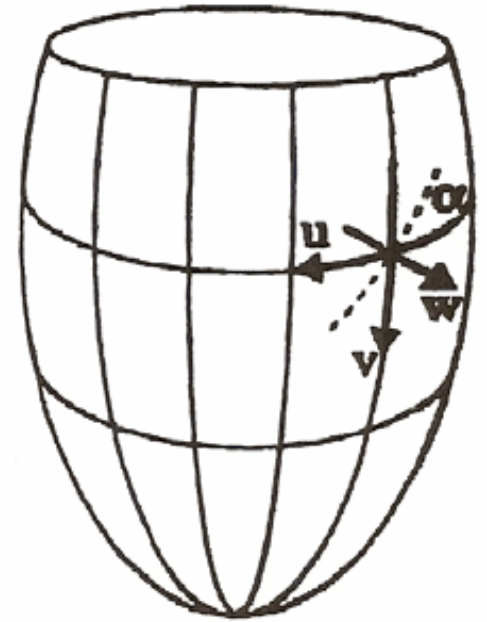
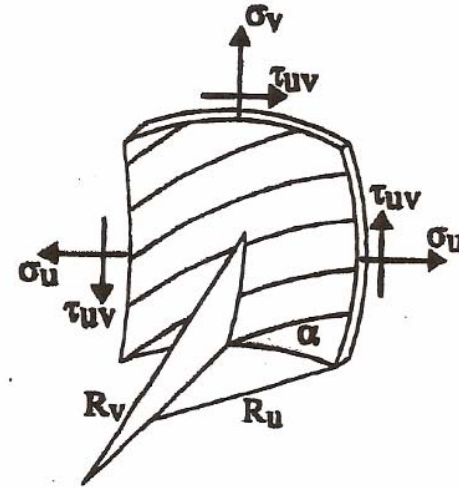
$$-\frac{dp}{dw} = \frac{\sigma_u}{R_u} + \frac{\sigma_v}{R_v} \quad (\text{Laplace law})$$

Equilibrium in z-direction



The ellipsoidal model

- Equilibrium



$$-\frac{dp}{dw} = \frac{2\sigma}{R_u(3 - R_u/R_v)}$$

$$\sigma_u = \sigma \cos^2 \alpha, \quad \sigma_v = \sigma \sin^2 \alpha$$

$$\sigma_u + \sigma_v = \sigma$$

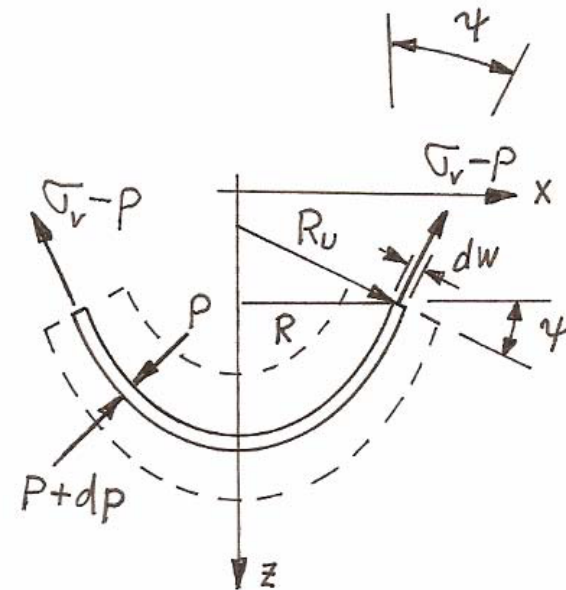
$$-\frac{dp}{dw} = \frac{\sigma_u}{R_u} + \frac{\sigma_v}{R_v} \quad (\text{Laplace law})$$

Equilibrium in z-direction

Integration through the thickness of the wall then gives:

$$\frac{\sigma}{p_{lv}} = \left[\frac{2}{3} \ln \left(\frac{R_{mu} + h/2}{R_{mu} - h/2} \right) + \frac{1}{3} \ln \left(\frac{3R_{mu} - R_{mv} + h}{3R_{mu} - R_{mv} - h} \right) \right]^{-1}$$

$$R_u = R_{mu} + w, \quad R_v = R_{mv} + w \quad \text{where} \quad -\frac{h}{2} \leq w \leq \frac{h}{2}$$



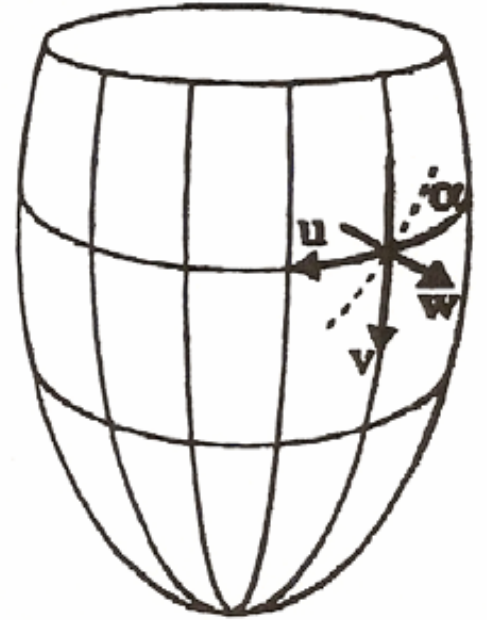
The ellipsoidal model

- Fiber directions

Balance equations

$$-\frac{dp}{dw} = \frac{\sigma \cos^2 \alpha}{R_{mu} + w} + \frac{\sigma \sin^2 \alpha}{R_{mv} + w}$$

$$\frac{\sigma}{p_{lv}} = \left[\frac{2}{3} \ln \left(\frac{R_{mu} + h/2}{R_{mu} - h/2} \right) + \frac{1}{3} \ln \left(\frac{3R_{mu} - R_{mv} + h}{3R_{mu} - R_{mv} - h} \right) \right]^{-1}$$



The ellipsoidal model

- Fiber directions

Balance equations

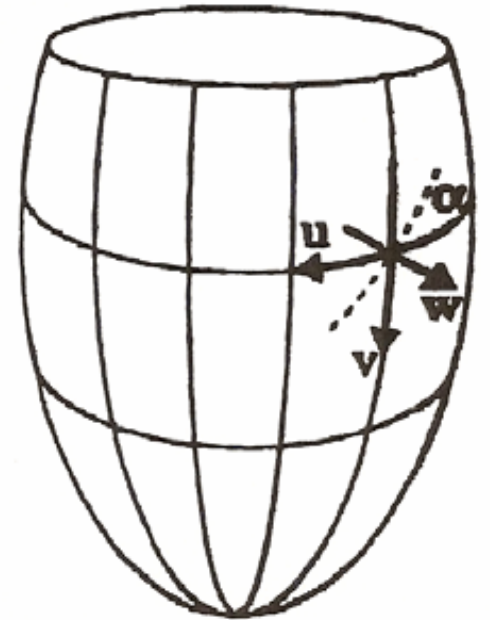
$$-\frac{dp}{dw} = \frac{\sigma \cos^2 \alpha}{R_{mu} + w} + \frac{\sigma \sin^2 \alpha}{R_{mv} + w}$$

$$\frac{\sigma}{p_{lv}} = \left[\frac{2}{3} \ln \left(\frac{R_{mu} + h/2}{R_{mu} - h/2} \right) + \frac{1}{3} \ln \left(\frac{3R_{mu} - R_{mv} + h}{3R_{mu} - R_{mv} - h} \right) \right]^{-1}$$

Constraints

$$\int_{-h/2}^{h/2} \left[\frac{\cos^2 \alpha}{R_{mu} + w} + \frac{\sin^2 \alpha}{R_{mv} + w} \right] dw = \frac{2}{3} \ln \left(\frac{R_{mu} + h/2}{R_{mu} - h/2} \right) + \frac{1}{3} \ln \left(\frac{3R_{mu} - R_{mv} + h}{3R_{mu} - R_{mv} - h} \right)$$

$$T = \int_{-h/2}^{h/2} (\tau_{uv} \cdot R) \cdot 2\pi R dw = \sigma \pi \cos^2 \psi_m \int_{-h/2}^{h/2} \sin 2\alpha (R_{mu} + w)^2 dw = 0$$



The ellipsoidal model

- Fiber directions

Constraints

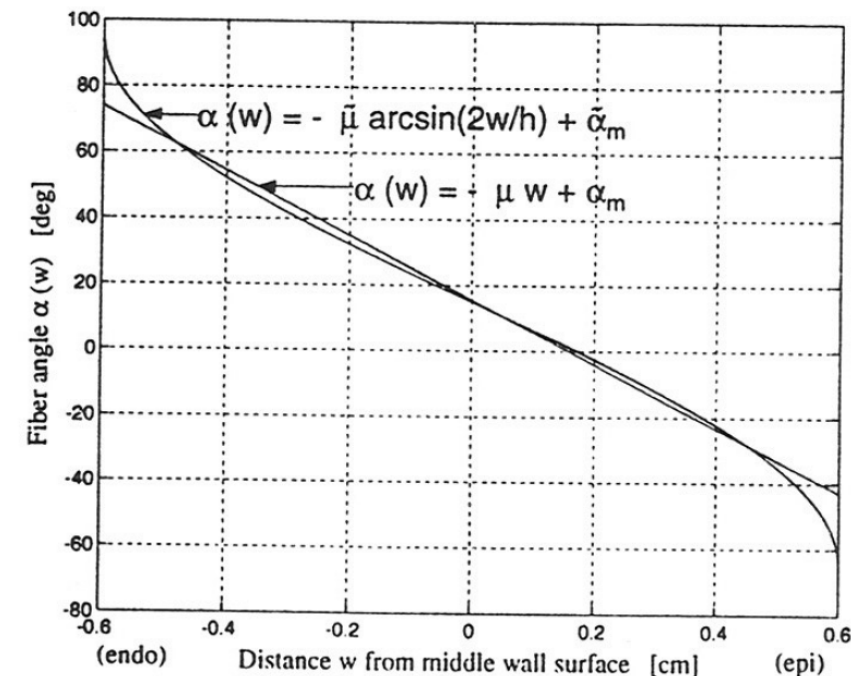
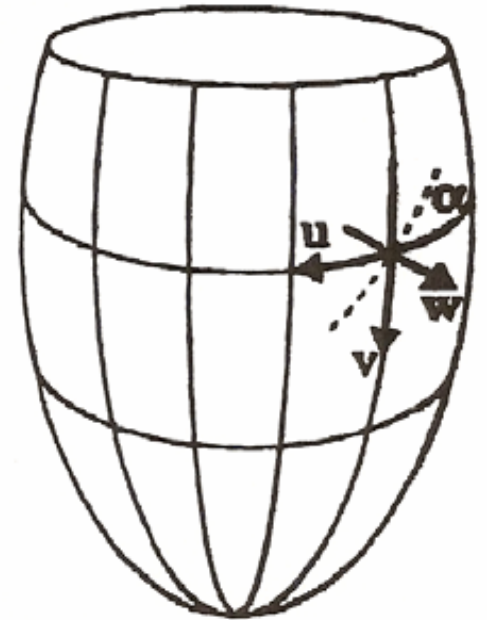
$$\int_{-h/2}^{h/2} \left[\frac{\cos^2 \alpha}{R_{mu} + w} + \frac{\sin^2 \alpha}{R_{mv} + w} \right] dw = \frac{2}{3} \ln \left(\frac{R_{mu} + h/2}{R_{mu} - h/2} \right) + \frac{1}{3} \ln \left(\frac{3R_{mu} - R_{mv} + h}{3R_{mu} - R_{mv} - h} \right)$$

$$T = \int_{-h/2}^{h/2} (\tau_{uv} \cdot R) \cdot 2\pi R dw = \sigma \pi \cos^2 \psi_m \int_{-h/2}^{h/2} \sin 2\alpha (R_{mu} + w)^2 dw = 0$$

Fiber directions models

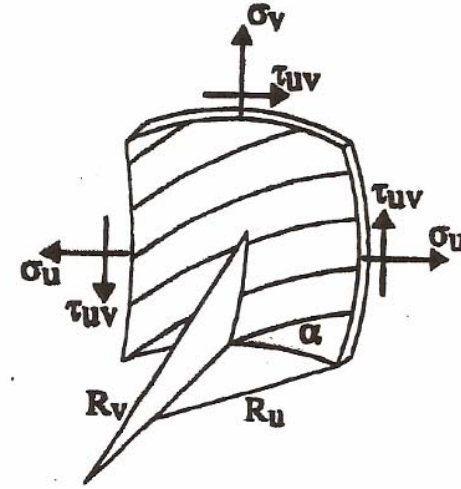
$$\alpha = -\mu w + \alpha_m \quad \text{linear model}$$

$$\alpha = -\hat{\mu} \arcsin \left(\frac{2w}{h} \right) + \hat{\alpha}_m \quad \text{arcsin model}$$



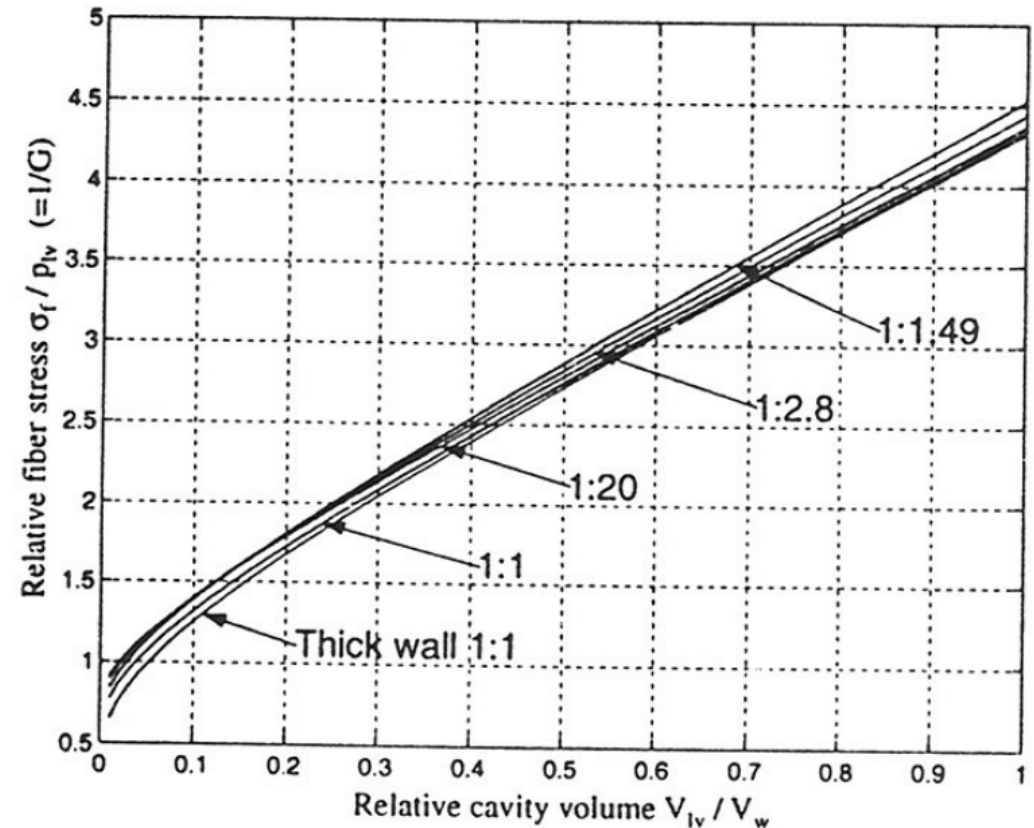
The ellipsoidal model

- Fiber stress



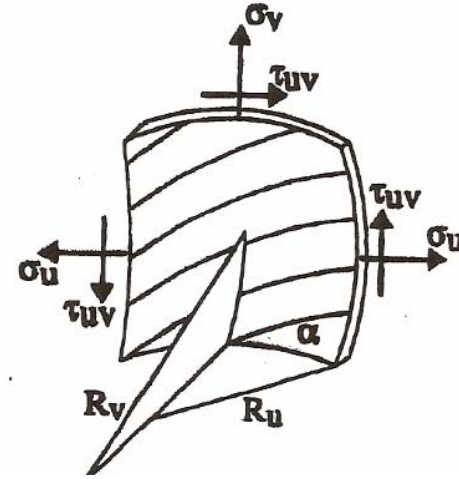
$$\frac{\sigma}{p_{lv}} = \left[\frac{2}{3} \ln \left(\frac{R_{mu} + h/2}{R_{mu} - h/2} \right) + \frac{1}{3} \ln \left(\frac{3R_{mu} - R_{mv} + h}{3R_{mu} - R_{mv} - h} \right) \right]^{-1}$$

$$\frac{\sigma}{p_{lv}} = \frac{2h}{R_{mu} \left(3 - \frac{R_{mu}}{R_{mv}} \right)} \quad \text{thin wall ventricle} \quad R_u \approx R_{mu}$$



The ellipsoidal model

- Fiber stress



$$\frac{\sigma}{p_{lv}} = \left[\frac{2}{3} \ln \left(\frac{R_{mu} + h/2}{R_{mu} - h/2} \right) + \frac{1}{3} \ln \left(\frac{3R_{mu} - R_{mv} + h}{3R_{mu} - R_{mv} - h} \right) \right]^{-1}$$

$$\frac{\sigma}{p_{lv}} = \frac{2h}{R_{mu} \left(3 - \frac{R_{mu}}{R_{mv}} \right)}$$

thin wall ventricle
 $R_u \approx R_{mu}$

$$\frac{p_{lv}}{\sigma} = \frac{1}{3} \ln \left[1 + \frac{V_w}{V_{lv}} \right]$$

Arts model

