

(1)

ENPM 667

NAME - SUHAS NAGARAJ  
UID - 199505373

PROBLEM SET - 4

## PROBLEM - 1

Given :-  $\dot{x}(t) = \frac{1}{12} \begin{bmatrix} 5 & 1 \\ 1 & 5 \end{bmatrix} x(t) + e^{t/2} \begin{bmatrix} 1 \\ 1 \end{bmatrix} u(t)$

To show :- If the system is controllable or not

→ The given system is of the form

$$\dot{x}(t) = A(t)x(t) + B(t)u(t)$$

$$\therefore A(t) = \begin{bmatrix} \frac{5}{12} & \frac{1}{12} \\ \frac{1}{12} & \frac{5}{12} \end{bmatrix} \quad \text{and} \quad B(t) = \begin{bmatrix} e^{t/2} \\ e^{t/2} \end{bmatrix}$$

The gramian of ~~matrix~~ is controllability, it is represented by  $w_c(t_0, t_f)$  determines the controllability of the system. If the matrix is fully ranked (or invertible) then the system is controllable.

The gramian of controllability for a LTV system is given by :-

$$w_c(t_0, t_f) = \operatorname{tr} \int_{t_0}^{t_f} \Phi(t_0, \tau) B(\tau) B^T(\tau) \bar{\Phi}^T(t_0, \tau) d\tau.$$

(2)

Here, as A matrix is constant (not time dependent)  
 the state transition matrix  $\Phi(t_0, \tau)$  is given by

$$\underline{\Phi}(t_0, \tau) = \begin{bmatrix} e^{A_{11}(t_0 - \tau)} & e^{A_{12}(t_0 - \tau)} \\ e^{A_{21}(t_0 - \tau)} & e^{A_{22}(t_0 - \tau)} \end{bmatrix}$$

$$\therefore \underline{\Phi}(t_0, \tau) = \begin{bmatrix} e^{\frac{5}{12}(t_0 - \tau)} & e^{\frac{1}{12}(t_0 - \tau)} \\ e^{\frac{1}{12}(t_0 - \tau)} & e^{\frac{5}{12}(t_0 - \tau)} \end{bmatrix}$$

$$\begin{aligned} \therefore \underline{\Phi}(t_0, \tau) \cdot B(\tau) &= \begin{bmatrix} e^{\frac{5}{12}(t_0 - \tau)} & e^{\frac{1}{12}(t_0 - \tau)} \\ e^{\frac{1}{12}(t_0 - \tau)} & e^{\frac{5}{12}(t_0 - \tau)} \end{bmatrix} \begin{bmatrix} e^{\frac{\tau}{2}} \\ e^{\frac{\tau}{2}} \end{bmatrix} \\ &= \begin{bmatrix} e^{\frac{5}{12}t_0 + \frac{\tau}{12}} + e^{\frac{t_0}{12} - \frac{5}{12}\tau} \\ e^{\frac{t_0}{12} - \frac{5}{12}\tau} + e^{\frac{5}{12}t_0 + \frac{\tau}{12}} \end{bmatrix} \\ \underline{\Phi}(t_0, \tau) \cdot B(\tau) &= \left( e^{\frac{5}{12}t_0 + \frac{\tau}{12}} + e^{\frac{t_0}{12} - \frac{5}{12}\tau} \right) \begin{bmatrix} 1 \\ 1 \end{bmatrix} \end{aligned}$$

Taking the transpose of the above matrix

$$\begin{aligned} [\underline{\Phi}(t_0, \tau) \cdot B(\tau)]^T &= B^T(\tau) \cdot (\underline{\Phi}(t_0, \tau))^T \\ &= \left( e^{\frac{5}{12}t_0 + \frac{\tau}{12}} + e^{\frac{t_0}{12} - \frac{5}{12}\tau} \right) \begin{bmatrix} 1 & 1 \end{bmatrix} \end{aligned}$$

(3)

Substituting the values

$$W_C(t_0, t_f) = \frac{t_f}{t_0} \left( \left( e^{\frac{5}{12}t_0 + \frac{5}{12}\tau} + e^{\frac{t_0}{12} - \frac{5}{12}\tau} \right) \begin{bmatrix} 1 \\ 1 \end{bmatrix} + \left( e^{\frac{5}{12}t_0 + \frac{5}{12}\tau} + e^{\frac{t_0}{12} - \frac{5}{12}\tau} \right) \begin{bmatrix} 1 \\ 1 \end{bmatrix} d\tau \right)$$

$$W_C(t_0, t_f) = \frac{t_f}{t_0} \left\{ \left( e^{\frac{5}{12}t_0 + \frac{5}{12}\tau} + e^{\frac{t_0}{12} - \frac{5}{12}\tau} \right)^2 \begin{bmatrix} 1 & 1 \\ 1 & 1 \end{bmatrix} \right\}$$

Here we can observe that, even after integration, the 2 columns of the grammian matrix will be linearly dependent [as column 1 = column 2]

This shows that the grammian matrix  $W_C(t_0, t_f)$  is not invertible and hence the system is uncontrollable

★

ALTERNATE PROOF FOR PROBLEM - 1 USING

$$\text{Matrix } C = [B : AB : \dots : A^{n-1}B]$$

$$\text{We know that } A = \begin{bmatrix} \frac{5}{12} & \frac{1}{12} \\ \frac{1}{12} & \frac{5}{12} \end{bmatrix} \text{ and } B(t) = \begin{bmatrix} e^{\frac{t}{12}} \\ e^{\frac{5t}{12}} \end{bmatrix}$$

$$\text{Matrix } C = [B : AB : \dots : A^{n-1}B]$$

Here As  $n=2$ , only  $B$  and  $AB$  ~~is~~ column vectors exist

(4)

$$B = \begin{bmatrix} e^{\frac{t}{2}} \\ e^{\frac{t}{2}} \end{bmatrix}$$

$$AB = \begin{bmatrix} \frac{5}{12} & \frac{1}{12} \\ \frac{1}{12} & \frac{5}{12} \end{bmatrix} \begin{bmatrix} e^{\frac{t}{2}} \\ e^{\frac{t}{2}} \end{bmatrix}$$

$$= \begin{bmatrix} \frac{5}{12}e^{\frac{t}{2}} + \frac{1}{12}e^{\frac{t}{2}} \\ \frac{1}{12}e^{\frac{t}{2}} + \frac{5}{12}e^{\frac{t}{2}} \end{bmatrix}$$

$$AB = \begin{bmatrix} \frac{e^{\frac{t}{2}}}{2} \\ \frac{e^{\frac{t}{2}}}{2} \end{bmatrix}$$

Substituting

$$C = \begin{bmatrix} B : AB \end{bmatrix}$$

$$C = \begin{bmatrix} e^{\frac{t}{2}} & \frac{e^{\frac{t}{2}}}{2} \\ e^{\frac{t}{2}} & \frac{e^{\frac{t}{2}}}{2} \end{bmatrix}$$

The system is said to be controllable if this matrix  $C$  is fully ranked. In this case, column 2 of matrix  $C$  is  $\frac{1}{2}$  of column 1 of the matrix. Hence, the columns are linearly dependent. Therefore, the system is not controllable.

(5)

## PROBLEM - 2

$$\text{Given : } \begin{bmatrix} \dot{x}_1(t) \\ \dot{x}_2(t) \end{bmatrix} = \begin{bmatrix} 8_1(t) & 8_2(t) \\ -8_2(t) & 8_1(t) \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \end{bmatrix}$$

To solve :- Compute  $\Phi(t_0, t_f)$  and solution to the state space equation.

→ The given state space equation is of the form

$$\vec{\dot{x}}(t) = A(t) \vec{x}(t)$$

$$\text{Hence } A(t) = \begin{bmatrix} 8_1(t) & 8_2(t) \\ -8_2(t) & 8_1(t) \end{bmatrix}$$

The solution to this state space equation is given by

$$\vec{x}(t) = \Phi(t_0, t_f) \vec{x}_0$$

where  $\vec{x}_0$  is the initial state of the system

This can be solved by eigen value - eigenvector method where the state transition matrix is given by

$$\Phi(t_0, t_f) = V \Lambda V^{-1} \quad \text{--- (1)}$$

where  $V$  is a matrix of eigen vectors of  $A$  as its columns and  $\Lambda$  is a <sup>diagonal</sup> matrix given by  $\Lambda = \begin{bmatrix} e^{\frac{8_1}{2} T_1 dt} & 0 \\ 0 & e^{\frac{8_1}{2} T_2 dt} \end{bmatrix}$

where  $T_1$  and  $T_2$  are eigen values of  $A$

⑥

To find the eigen values and eigen vectors of A,

consider  $|A - \tau I| = 0$

$$\left| \begin{bmatrix} g_1(t) & g_2(t) \\ -g_2(t) & g_1(t) \end{bmatrix} - \begin{bmatrix} \tau & 0 \\ 0 & \tau \end{bmatrix} \right| = 0$$

$$\begin{vmatrix} g_1(t) - \tau & g_2(t) \\ -g_2(t) & g_1(t) - \tau \end{vmatrix} = 0$$

$$(g_1(t) - \tau)^2 + (g_2(t))^2 = 0$$

$$g_1^2(t) - 2g_1(t)\tau + \tau^2 + g_2^2(t) = 0.$$

$$\therefore \tau^2 - 2\tau(g_1(t)) + [g_1^2(t) + g_2^2(t)] = 0.$$

Taking roots of this equation

$$a=1 \quad b=-2g_1(t) \quad c=g_1^2(t) + g_2^2(t)$$

$$\tau_{1,2} = \frac{-b \pm \sqrt{b^2 - 4ac}}{2a}$$

$$= \frac{2g_1(t) \pm \sqrt{4g_1^2(t) - 4g_1^2(t) + 4g_2^2(t)}}{2}$$

$$= \frac{2g_1(t) \pm 2ig_2(t)}{2}$$

$$\tau_{1,2} = g_1(t) \pm i g_2(t)$$

(7)

$$\begin{aligned} \therefore \tau_1 &= \gamma_1(t) + i\gamma_2(t) \\ \tau_2 &= \gamma_1(t) - i\gamma_2(t) \end{aligned} \quad \left. \right\} - \textcircled{2}$$

Now, to find the eigen vectors, consider the equation

$$Ax = \tau x, \text{ For } \tau_1 :-$$

$$\begin{bmatrix} \gamma_1(t) & \gamma_2(t) \\ -\gamma_2(t) & \gamma_1(t) \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} (\gamma_1(t) + i\gamma_2(t)) x_1 \\ (\gamma_1(t) + i\gamma_2(t)) x_2 \end{bmatrix}$$

$$\cancel{\gamma_1(t)x_1 + \gamma_2(t)x_2} = \cancel{\gamma_1(t)x_1} + i\cancel{\gamma_2(t)x_1}$$

$$\cancel{\gamma_2(t)x_2} = i\cancel{\gamma_2(t)x_1}$$

$$x_2 = ix_1$$

$$\text{If } x_1 = 1, x_2 = i$$

$$\therefore V_1 = \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} 1 \\ i \end{bmatrix} \longrightarrow \text{for } \tau_1, \textcircled{3}$$

Now, for  $\tau_2$  :-

$$\begin{bmatrix} \gamma_1(t) & \gamma_2(t) \\ -\gamma_2(t) & \gamma_1(t) \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} (\gamma_1(t) - i\gamma_2(t)) x_1 \\ (\gamma_1(t) - i\gamma_2(t)) x_2 \end{bmatrix}$$

$$\cancel{\gamma_1(t)x_1 + \gamma_2(t)x_2} = \cancel{\gamma_1(t)x_1} - i\cancel{\gamma_2(t)x_1}$$

$$\cancel{\gamma_2(t)x_2} = -i\cancel{\gamma_2(t)x_1}$$

(8)

$$x_2 = -i x_1$$

$$\text{If } x_1 = 1, \quad x_2 = -i$$

$$\therefore V_2 = \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} 1 \\ -i \end{bmatrix} \quad \text{--- (4) for } T_2$$

Now, the matrix  $V$  is given by

$$V = \begin{bmatrix} V_1 & | & V_2 \end{bmatrix}$$

$$V = \begin{bmatrix} 1 & | & 1 \\ i & | & -i \end{bmatrix} \quad \text{--- (5)}$$

$$V^{-1} = \frac{\text{Adj } V}{|V|} = \frac{1}{-i-i} \begin{bmatrix} -i & -1 \\ -i & 1 \end{bmatrix} = \frac{1}{-2i} \begin{bmatrix} -i & -1 \\ -i & 1 \end{bmatrix}$$

$$V^{-1} = \begin{bmatrix} \frac{1}{2} & \frac{1}{2i} \\ \frac{1}{2} & -\frac{1}{2i} \end{bmatrix} \quad \text{--- (6)}$$

Substituting (2), (5) and (6) in equation (1)

$$\bar{\Phi}(t_0, t_f) = V \wedge V^{-1}$$

$$= \begin{bmatrix} 1 & 1 \\ i & -i \end{bmatrix} \begin{bmatrix} e^{\int_{t_0}^{t_f} T_1 dt} & 0 \\ 0 & e^{\int_{t_0}^{t_f} T_2 dt} \end{bmatrix} \begin{bmatrix} \frac{1}{2} & \frac{1}{2i} \\ \frac{1}{2} & -\frac{1}{2i} \end{bmatrix}$$

Here let  $e^{\int_{t_0}^{t_f} T_1 dt} = \Lambda_1$  and  
 $e^{\int_{t_0}^{t_f} T_2 dt} = \Lambda_2$

(9)

$$\therefore \Phi(t_0, t) = \begin{bmatrix} 1 & 1 \\ i & -i \end{bmatrix} \begin{bmatrix} 1 & 0 \\ 0 & \lambda_2 \end{bmatrix} \begin{bmatrix} \frac{1}{2} & \frac{1}{2i} \\ \frac{1}{2} & -\frac{1}{2i} \end{bmatrix}$$

$$= \begin{bmatrix} 1 & \lambda_2 \\ \lambda_1 i & -\lambda_2 i \end{bmatrix} \begin{bmatrix} \frac{1}{2} & \frac{1}{2i} \\ \frac{1}{2} & -\frac{1}{2i} \end{bmatrix}$$

$$\Phi(t_0, t) = \begin{bmatrix} \frac{\lambda_1}{2} + \frac{\lambda_2}{2} & \frac{\lambda_1}{2i} - \frac{\lambda_2}{2i} \\ \frac{\lambda_1 i}{2} - \frac{\lambda_2 i}{2} & \frac{\lambda_1}{2} + \frac{\lambda_2}{2} \end{bmatrix}$$

$$\Rightarrow \text{Here } \frac{1}{i} = -i$$

$$\therefore \Phi(t_0, t_f) = \begin{bmatrix} \frac{\lambda_1}{2} + \frac{\lambda_2}{2} & -\left(\frac{\lambda_1 i}{2} - \frac{\lambda_2 i}{2}\right) \\ \frac{\lambda_1 i}{2} - \frac{\lambda_2 i}{2} & \frac{\lambda_1}{2} + \frac{\lambda_2}{2} \end{bmatrix}$$

$$\text{where } \lambda_1 = e^{\int_{t_0}^{t_f} \gamma_1 dt} \quad \text{and} \quad \lambda_2 = e^{\int_{t_0}^{t_f} \gamma_2 dt}$$

$$\text{where } \gamma_1 = \varphi_1(t) + i\varphi_2(t) \quad \text{and} \quad \gamma_2 = \varphi_1(t) - i\varphi_2(t)$$

Hence, the solution to the system is given by

$$\vec{x}(t) = \Phi(t_0, t_f) \cdot \vec{x}(t_0)$$

$$\begin{bmatrix} x_1(t) \\ x_2(t) \end{bmatrix} = \begin{bmatrix} \frac{\lambda_1}{2} + \frac{\lambda_2}{2} & -\left(\frac{\lambda_1 i}{2} - \frac{\lambda_2 i}{2}\right) \\ \frac{\lambda_1 i}{2} - \frac{\lambda_2 i}{2} & \frac{\lambda_1}{2} + \frac{\lambda_2}{2} \end{bmatrix} \begin{bmatrix} x_1(t_0) \\ x_2(t_0) \end{bmatrix}$$

## PROBLEM - 3

Given :-

The moment of inertia of the space shuttle robot arm =  $J_1$

The moment of inertia of the space shuttle =  $J_2$

Equations of motion :-

$$J_1 \ddot{q}_1 = \tau \quad \text{--- (1)}$$

$$J_2 \ddot{q}_2 = \tau \quad \text{--- (2)}$$

Here  $\tau$  is the input

Selection of state :-

$$\vec{x} = \begin{bmatrix} q_1 \\ \dot{q}_1 \\ q_2 \\ \dot{q}_2 \end{bmatrix}$$

[As equations (1) and (2) are 2<sup>nd</sup> order differential equation wrt  $q$ , we select  $q^{(1)}$  and  $q^{(0)}$  as the state variables]

State space equation :-

general form :-

$$\vec{\dot{x}} = A \vec{x} + B \vec{u}$$

$$\text{ie } \begin{bmatrix} \ddot{q}_1 \\ \dot{q}_1 \\ q_2 \\ \dot{q}_2 \end{bmatrix} = \begin{bmatrix} \ddot{q}_1 \\ \tau/J_1 \\ q_2 \\ \dot{q}_2 \end{bmatrix} = \begin{bmatrix} \ddot{q}_1 \\ 0 \\ \dot{q}_2 \\ 0 \end{bmatrix} + \begin{bmatrix} 0 \\ \tau/J_1 \\ 0 \\ \tau/J_2 \end{bmatrix}$$

(11)

$$\therefore \begin{bmatrix} \dot{q}_1 \\ \ddot{q}_1 \\ \dddot{q}_2 \\ \vdots \\ \ddot{q}_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 \\ 0 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} q_1 \\ q_2 \\ \dot{q}_1 \\ \dot{q}_2 \end{bmatrix} + \begin{bmatrix} 0 \\ \frac{1}{J_1} \\ 0 \\ \frac{1}{J_2} \end{bmatrix} \begin{bmatrix} \text{not T} \end{bmatrix}$$

This is the system in state space form

\* Checking the controllability of the system :-

A LTI system is said to be controllable if

$$\text{rank} [B : AB : A^2B : \dots : A^{n-1}B] = n$$

where  $n$  is number of state variables.

$\therefore$  Here,  $n = 4$

$$\therefore B = \begin{bmatrix} 0 \\ \frac{1}{J_1} \\ 0 \\ \frac{1}{J_2} \end{bmatrix} \quad AB = \begin{bmatrix} 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 \\ 0 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} 0 \\ \frac{1}{J_1} \\ 0 \\ \frac{1}{J_2} \end{bmatrix} = \begin{bmatrix} \frac{1}{J_1} \\ 0 \\ \frac{1}{J_2} \\ 0 \end{bmatrix}$$

$$A^2B = \begin{bmatrix} 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 \\ 0 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 \\ 0 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} 0 \\ \frac{1}{J_1} \\ 0 \\ \frac{1}{J_2} \end{bmatrix}$$

$$= \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} 0 \\ \frac{1}{J_1} \\ 0 \\ \frac{1}{J_2} \end{bmatrix}$$

$$A^3B = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \end{bmatrix}$$

(12)

$$A^3 B = A \cdot A^2 B$$

$$\text{Here as } A^2 = \vec{0}, A^3 B = \vec{0}$$

Plugging the values in the controllability matrix

$$C = [B : AB : A^2 B : A^3 B]$$

$$C = \begin{bmatrix} 0 & \frac{1}{\zeta_1} & 0 & 0 \\ \frac{1}{\zeta_1} & 0 & 0 & 0 \\ 0 & \frac{1}{\zeta_2} & 0 & 0 \\ \frac{1}{\zeta_2} & 0 & 0 & 0 \end{bmatrix}_{n \times n}$$

Here, column 3 = column 4. So all the columns of matrix C are not linearly independent

Hence the rank of C is less than 4

As  $\text{rank}[C] < n$  ie  $\text{rank}[C] < 4$ , the system is uncontrollable

The system given above is not controllable, but it can still be stabilizable. There can be gain matrix K such that the eigen values of  $A + B_K K$  have negative real part, making the system stable.

(13)

As the system is not controllable, it is possible to separate the controllable part of the system by appropriate similarity transformation.

⇒ In our case  $\text{rank} [B : AB] = 2$  is the controllable subspace with dimension 2

The similarity transformation matrix is defined as

$$S = \begin{bmatrix} B & AB & S_{n-2} \end{bmatrix} = \begin{bmatrix} B & AB & S_2 \end{bmatrix}$$

$$S_{n-2} = \begin{bmatrix} V_1 & V_2 & S_{n-2} \end{bmatrix} = \begin{bmatrix} V_1 & V_2 & S_2 \end{bmatrix}$$

where  $S_{n-2}$  or  $S_2$  is a matrix contains 2 linearly independent vectors chosen so that  $S$  is non singular.

Hence, there exist a non singular matrix  $S$  such

that  $\hat{A} = S^{-1}AS = \begin{bmatrix} A_1 & | & A_{12} \\ \hline 0 & + & A_2 \end{bmatrix}_{n \times n \rightarrow 2 \times 2}$

$$\hat{B} = S^{-1}B = \begin{bmatrix} B_1 \\ \hline 0 \end{bmatrix}_{n \times m \rightarrow 2 \times m}$$

Here the pair  $A_1, B_1$  is controllable and the pair  $\hat{A}, \hat{B}$  is the standard form of uncontrollable system

(14)

## PROBLEM - 4

Given: - 2<sup>nd</sup> order system

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} 1 & -3 \\ 1 & -2 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 1 \\ -2 \end{bmatrix} u$$

Find  $u = k_1 x_1 + k_2 x_2$  such that the closed loop system has poles at  $s = -2, 2$ 

Comparing the given equation with

$$\vec{\dot{x}} = A\vec{x} + B\vec{u}$$

we get  $A = \begin{bmatrix} 1 & -3 \\ 1 & -2 \end{bmatrix}$  and  $B = \begin{bmatrix} 1 \\ -2 \end{bmatrix}$

Number of state variables =  $n = 2$ 

Controllability of the system:-

$\det C = [B : AB : A^2B : \dots : A^{n-1}B]$  Here  $C$  is the controllability matrix

if  $\text{rank}[C] = n$ , then system is controllableHere as  $n = 2$ ,  $C = [B : AB]$ 

$$B = \begin{bmatrix} 1 \\ -2 \end{bmatrix}$$

$$AB = \begin{bmatrix} 1 & -3 \\ 1 & -2 \end{bmatrix} \begin{bmatrix} 1 \\ -2 \end{bmatrix} = \begin{bmatrix} 1+6 \\ 1+4 \end{bmatrix} = \begin{bmatrix} 7 \\ 5 \end{bmatrix}$$

(15)

$$\therefore C = \begin{bmatrix} 1 & 7 \\ -2 & 5 \end{bmatrix}$$

The matrix is said to be fully ranked if it has linearly independent rows. The above matrix C is fully ranked as the 2 columns are linearly independent ie there is no straight relationship between the columns.

Therefore the matrix C is fully ranked making the given system controllable and we can place the poles wherever we want

\* Now, to determine  $U = k_1 x_1 + k_2 x_2$  so that the closed loop system poles are at  $s = -2, 2$ , consider the closed loop system of the form

$$\vec{x}(t) = (A + B_D k) \vec{x}(t) + B_D \vec{U}_D(t)$$

$$\vec{y}(t) = (C + Dk) \vec{x}(t)$$

~~stability of the system is~~

Now the  $(A + B_D k)$  represent the A matrix of closed loop system.

(16)

Consider

$$A_{\text{closed}} = A + BK$$

$$A_{\text{closed}} = \begin{bmatrix} 1 & -3 \\ 1 & -2 \end{bmatrix} + \begin{bmatrix} 1 \\ -2 \end{bmatrix} \begin{bmatrix} k_1 \\ k_2 \end{bmatrix} \quad \boxed{\begin{bmatrix} k_1 \\ k_2 \end{bmatrix}}$$

$$= \begin{bmatrix} 1 & -3 \\ 1 & -2 \end{bmatrix} + \begin{bmatrix} k_1 & k_2 \\ -2k_1 & -2k_2 \end{bmatrix}$$

$$A_{\text{closed}} = \begin{bmatrix} 1+k_1 & -3+k_2 \\ 1-2k_1 & -2k_2-2 \end{bmatrix}$$

To find the poles, consider

$$\det(\tau I - A_{\text{closed}}) = 0 \quad [\text{Given as hint}]$$

$$\left| \begin{bmatrix} \tau & 0 \\ 0 & \tau \end{bmatrix} - \begin{bmatrix} 1+k_1 & -3+k_2 \\ 1-2k_1 & -2k_2-2 \end{bmatrix} \right| = 0$$

$$\left| \begin{array}{cc} \tau - 1 - k_1 & 3 - k_2 \\ -1 + 2k_1 & \tau + 2k_2 + 2 \end{array} \right| = 0$$

$$(\tau - 1 - k_1)(\tau + 2k_2 + 2) - (3 - k_2)(-1 + 2k_1) = 0$$

$$\tau^2 + 2\tau k_2 + 2\tau - \tau - 2k_2 - 2 - \tau k_1 - 2k_1 k_2 \dots$$

$$\dots - 2k_1 - (-3 + 6k_1 + k_2 - 2k_1 k_2) = 0$$

(17)

$$\therefore \tau^2 + \tau(2k_2 + 2 - 1 - k_1) + (-2k_2 - 2 - 2k_1k_2 - 2k_1 + 3 - 6k_1 - k_2 + 2k_1k_2) = 0$$

$$\tau^2 + \tau(2k_2 - k_1 + 1) + (-3k_2 - 8k_1 + 1) = 0$$

$\Rightarrow$  Substituting the values of  $\tau$  ie  $\tau_1 = -2$  &  $\tau_2 = 2$

~~we get~~ when  $\tau = -2$ ,

$$(-2)^2 - 2(2k_2 - k_1 + 1) + (-3k_2 - 8k_1 + 1) = 0$$

~~$4 - 4k_2 + 2k_1 - 2 - 3k_2 - 8k_1 + 1$~~

$$4 - 4k_2 + 2k_1 - 2 - 3k_2 - 8k_1 + 1 = 0$$

$$3 - 7k_2 - 6k_1 = 0$$

$$\therefore 6k_1 + 7k_2 = 3 \quad -\textcircled{1}$$

when  $\tau = 2$ ,

$$2^2 + 2(2k_2 - k_1 + 1) + (-3k_2 - 8k_1 + 1) = 0$$

$$4 + 4k_2 - 2k_1 + 2 - 3k_2 - 8k_1 + 1 = 0$$

$$k_2 - 10k_1 + 7 = 0$$

$$10k_1 - k_2 = 7 \quad -\textcircled{2}$$

Solving equations ① and ②, we get,

$$k_1 = \frac{13}{19} \quad \text{and} \quad k_2 = -\frac{3}{19}$$

$\therefore$  The state feedback control is given by

$$U = k_1 x_1 + k_2 x_2$$

$$U = \frac{13}{19} x_1 - \frac{3}{19} x_2$$


---

### PROBLEM - 5

Given :  $\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} -1 & 0 \\ 0 & 2 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} U$

Comparing the above equation with

$$\vec{\dot{x}} = A \vec{x} + B \vec{U}$$

we get  $A = \begin{bmatrix} -1 & 0 \\ 0 & 2 \end{bmatrix} \quad B = \begin{bmatrix} 0 \\ 1 \end{bmatrix}$

Number of state variables = 2

Checking for controllability :-

$$\text{rank } [B : AB] = ?$$

(19)

$$AB = \begin{bmatrix} -1 & 0 \\ 0 & 2 \end{bmatrix} \begin{bmatrix} 0 \\ 1 \end{bmatrix} = \begin{bmatrix} 0 \\ 2 \end{bmatrix}$$

$$\text{rank} \begin{bmatrix} B & AB \end{bmatrix} = \text{rank} \begin{bmatrix} 0 & 0 \\ 1 & 2 \end{bmatrix} = 1$$

Here, the 2 columns are linearly dependent, hence  
the  $\text{rank} \begin{bmatrix} B & AB \end{bmatrix} < n$

So, the system is uncontrollable

Closed loop system :-

$$\dot{\vec{x}} = (A + BK) \vec{x}$$

Characteristic equation to find the poles,

$$\det \begin{bmatrix} T I - A_{\text{closed}} \end{bmatrix} = 0$$

where  $A_{\text{closed}} = A + BK$

$$= \begin{bmatrix} -1 & 0 \\ 0 & 2 \end{bmatrix} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} [k_1 \ k_2]$$

$$= \begin{bmatrix} -1 & 0 \\ 0 & 2 \end{bmatrix} + \begin{bmatrix} 0 & 0 \\ k_1 & k_2 \end{bmatrix}$$

$$A_{\text{closed}} = \begin{bmatrix} -1 & 0 \\ k_1 & k_2 + 2 \end{bmatrix}$$

Substituting,

$$\left| \begin{bmatrix} \tau & 0 \\ 0 & \tau \end{bmatrix} - \begin{bmatrix} -1 & 0 \\ k_1 & k_2+2 \end{bmatrix} \right| = 0$$

$$\left| \begin{array}{cc} \tau + 1 & 0 \\ -k_1 & \tau - k_2 - 2 \end{array} \right| = 0$$

$$(\tau + 1)(\tau - k_2 - 2) = 0$$

~~$$\tau^2 - k_2 \tau - 2\tau + \tau - k_2 - 2 = 0$$~~

~~$$\tau^2 - \tau(k_2 + 1) - (k_2 + 2) = 0$$~~

$$\therefore \tau + 1 = 0$$

$$\tau = -1 \quad \text{--- (1)}$$

$$\text{Also } \tau - k_2 - 2 = 0$$

$$\tau = k_2 + 2 \quad \text{--- (2)}$$

Therefore one of the poles of the system is always at  $-1$  whereas the other pole can be placed anywhere by controlling the value of  $k_2$

- \* Can be closed loop poles can be placed at -2 ?
- One of the pole of the closed loop system is at -1 and this cannot be changed. But the other pole can be placed at -2 by selecting  $k_2$  as

$$k_2 = -4$$

Therefore the system poles can be placed at -1, -2 but it cannot be placed at -2, -2

- \* Can this system be stabilized ?

Yes, this system can be stabilized as one pole is already at left half plane as it has a fixed value of -1 (-ve real value) and the other pole can be placed at left half plane by selecting appropriate values of  $k_2$

If  ~~$k_2$~~   $k_2 < -2$  then the system is stable as the poles will have -ve real parts.

Problem 6

$$\text{Given: } \begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ 0 & 2 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u$$

Comparing the above equation with

$$\dot{\vec{x}} = A\vec{x} + B\vec{u}$$

$$A = \begin{bmatrix} 1 & 0 \\ 0 & 2 \end{bmatrix} \quad \text{and} \quad B = \begin{bmatrix} 0 \\ 1 \end{bmatrix}$$

Number of state variables,  $n = 2$

Checking for controllability :-

$$\text{rank } [B : AB] = ?$$

$$B = \begin{bmatrix} 0 \\ 1 \end{bmatrix}$$

$$AB = \begin{bmatrix} 0 \\ 2 \end{bmatrix}$$

$$\text{rank } [B : AB] = \text{rank } \begin{bmatrix} 0 & 0 \\ 1 & 2 \end{bmatrix} = 1$$

The 2 columns of the above matrix are linearly dependent, hence the matrix is not fully ranked

$\therefore$  The system is not controllable

\* closed loop system :-

$$\dot{\vec{x}} = (A + BK) \vec{x}$$

(23)

Equation to find poles of the closed loop system:-

$$\det(\tau I - A_{\text{closed}}) = 0$$

$$\text{where } A_{\text{closed}} = A + BK$$

$$= \begin{bmatrix} 1 & 0 \\ 0 & 2 \end{bmatrix} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} [k_1 \ k_2]$$

$$= \begin{bmatrix} 1 & 0 \\ 0 & 2 \end{bmatrix} + \begin{bmatrix} 0 & 0 \\ k_1 & k_2 \end{bmatrix}$$

$$= \begin{bmatrix} 1 & 0 \\ k_1 & k_2 + 2 \end{bmatrix}$$

$$\therefore \det(\tau I - A_{\text{closed}}) = \det \left[ \begin{bmatrix} \tau & 0 \\ 0 & \tau \end{bmatrix} - \begin{bmatrix} 1 & 0 \\ k_1 & k_2 + 2 \end{bmatrix} \right] = 0$$

$$= \begin{vmatrix} \tau - 1 & 0 \\ -k_1 & \tau - k_2 - 2 \end{vmatrix} = 0$$

$$\therefore (\tau - 1)(\tau - k_2 - 2) = 0$$

$$\therefore \tau = 1 \text{ and } \tau = k_2 + 2$$

Here, one of the poles of the system is fixed at 1 and it cannot be changed by varying the values of  $k_1$  or  $k_2$

(24)

Hence the system is unstable and is also unstabilizable as it has one pole in right half plane and it cannot be changed.

Can one pole be placed at -2?

Yes one of the pole can be placed at -2 by selecting the value of  $k_2$  as -4. But the other pole is fixed at +1, hence the poles can be ~~(1, -2)~~ but cannot be (-2, -2)

### PROBLEM 7

Given :-  $y(t)$  is output of an LTI system with input  $v(t)$ .  $x(t_0) = 0$ .

To prove :-  $\dot{y}(t)$  is the output of the LTI system when input is  $\dot{v}(t)$

$\Rightarrow$  ~~The~~ geno The state space representation of an LTI system is given by :-

$$\vec{\dot{x}}(t) = A \vec{x}(t) + B \vec{v}(t)$$

$$y(t) = C \vec{x}(t) + D \vec{v}(t)$$

Taking Laplace transform of the state space equations,

$$L(\vec{\dot{x}}(t)) = L(A \vec{x}(t)) + L(B \vec{u}(t))$$

$$[S\vec{x}(s) - \vec{x}(0)] = A\vec{x}(s) + B\vec{u}(s)$$

$$\therefore S\vec{x}(s) = A\vec{x}(s) + B\vec{u}(s)$$

$$S\vec{x}(s) - A\vec{x}(s) = B\vec{u}(s).$$

~~$\vec{x}(s)[SI - A] = B\vec{u}(s)$~~

~~$\vec{x}(s) = [SI - A]^{-1} B\vec{u}(s)$~~

~~SAX~~

$$[SI - A]\vec{x}(s) = B\vec{u}(s)$$

Multiplying  $[SI - A]^{-1}$  on left ~~side~~ on both sides.

$$[SI - A]^{-1}[SI - A]\vec{x}(s) = [SI - A]^{-1}B\vec{u}(s)$$

$$\vec{x}(s) = [SI - A]^{-1}B\vec{u}(s) \quad \text{--- ①}$$

(26)

$$\text{Now consider, } L(\vec{y}(t)) = L(C\vec{x}(t) + D\vec{u}(t))$$

$$\vec{Y}(s) = C\vec{X}(s) + D\vec{U}(s)$$

Substituting ①

$$\vec{Y}(s) = C [SI - A]^{-1} B \vec{U}(s) + D \vec{U}(s)$$

$$\vec{Y}(s) = [C [SI - A]^{-1} B + D] \vec{U}(s) \quad \text{--- ②}$$

Now consider the input as  ~~$\vec{u}$~~   $\vec{v}$  and output as

$\vec{y}$ , then the state space equation becomes

$$\dot{\vec{x}}(t) = A\vec{x}(t) + B\vec{v}(t)$$

$$\vec{y}(t) = C\vec{x}(t) + D\vec{v}(t)$$

Let  $\vec{y}(t) = \hat{y}^*(t) \rightarrow \text{estimated output}$

Now, take Laplace transforms of the modified state space equations,

$$L(\dot{\vec{x}}(t)) = L(A\vec{x}(t) + B\vec{v}(t))$$

$$s\vec{X}(s) - \vec{X}(0)^* = A\vec{X}(s) + B(s\vec{U}(s) - \vec{V}(0))$$

$$\therefore s\vec{X}(s) = A\vec{X}(s) + B s\vec{U}(s)$$

$$s\vec{X}(s) - A\vec{X}(s) = B s\vec{U}(s)$$

~~$$(SI - A) X(s) = BSU(s)$$~~

$$X(s) = (SI - A)^{-1} BSU(s) \quad \text{--- (3)}$$

Consider,  $L(\hat{y}(t)) = L(C\vec{x}(t) + D\vec{u}(t))$

$$\hat{y}(s) = CX(s) + DSU(s)$$

Substituting (3)

$$\hat{y}(s) = C(SI - A)^{-1} BS\vec{u}(s) + DS\vec{u}(s)$$

$$\hat{y}(s) = [C(SI - A)^{-1} B + D] S\vec{u}(s)$$

But from (2) we know that

$$y(s) = (C(SI - A)^{-1} B + D)\vec{u}(s)$$

$$\therefore \hat{y}(s) = y(s) \cdot s$$

Taking inverse laplace,

$\hat{y}(t) = \underline{\dot{y}(t)}$   $\rightarrow$  The estimated output is equal to  $\dot{y}(t)$ , hence proving the statement

Hence proved

## PROBLEM 8

Given :-  $\dot{\vec{x}}(t) = \begin{bmatrix} -1 & 0 & 0 \\ 0 & -4 & 4 \\ 0 & -1 & 0 \end{bmatrix} \vec{x}(t)$ ,  $\vec{x}(t_0) = \vec{x}_0$

To solve :- The solution for the linear state equation

The given equation is of the form

$$\dot{\vec{x}}(t) = A \vec{x}(t)$$

Taking Laplace transform on both sides,

$$L(\dot{\vec{x}}(t)) = L(A \vec{x}(t))$$

$$s\vec{x}(s) - \vec{x}(t_0) = A\vec{x}(s)$$

~~$$s\vec{x}(s) - A\vec{x}(s) = \vec{x}(t_0)$$~~

~~$$(sI - A)\vec{x}(s) = \vec{x}(t_0)$$~~

Here  $\vec{x}(t_0) = \vec{x}_0$ .

$$(sI - A)\vec{x}(s) = \vec{x}_0$$

$$\vec{x}(s) = (sI - A)^{-1} \vec{x}_0 \quad \text{--- (1)}$$

Here  $sI - A = \begin{bmatrix} s & 0 & 0 \\ 0 & s & 0 \\ 0 & 0 & s \end{bmatrix} - \begin{bmatrix} -1 & 0 & 0 \\ 0 & -4 & 4 \\ 0 & -1 & 0 \end{bmatrix}$

$$sI - A = \begin{bmatrix} s+1 & 0 & 0 \\ 0 & s+4 & -4 \\ 0 & 1 & s \end{bmatrix}$$

Finding inverse of  $(SI - A)$

$$(SI - A)^{-1} = \frac{\text{Adj } (SI - A)}{|SI - A|}$$

~~$(SI - A)^{-1} = \frac{\text{C}_1}{|SI - A|}$~~

$$\begin{aligned} |SI - A| &= \begin{vmatrix} s+1 & 0 & 0 \\ 0 & s+4 & -4 \\ 0 & 1 & s \end{vmatrix} \\ &= (s+1) [s(s+4) + 4] \\ &= (s+1) [s^2 + 4s + 4] \\ &= (s+1) \cdot (s+2)^2 \end{aligned}$$

$$\begin{aligned} \text{Adj } (SI - A) &= \begin{bmatrix} C_{11} & C_{21} & C_{31} \\ C_{12} & C_{22} & C_{32} \\ C_{13} & C_{23} & C_{33} \end{bmatrix} \\ &= \begin{bmatrix} s^2 + 4s + 4 & 0 & 0 \\ 0 & (s+1)s & 4(s+1) \\ 0 & -(s+1) & (s+1)(s+4) \end{bmatrix} \\ &= \begin{bmatrix} (s+2)^2 & 0 & 0 \\ 0 & s(s+1) & 4(s+1) \\ 0 & -(s+1) & (s+1)(s+4) \end{bmatrix} \end{aligned}$$

(30)

$$\therefore (SI - A)^{-1} = \frac{\text{Adj}(SI - A)}{|SI - A|}$$

$$= \frac{1}{(s+1)(s+2)^2} \begin{bmatrix} s+1 & 0 & 0 \\ 0 & s+4 & -4 \\ 0 & 1 & 1 \end{bmatrix}$$

$$(SI - A)^{-1} = \frac{1}{(s+1)(s+2)^2} \begin{bmatrix} (s+2)^2 & 0 & 0 \\ 0 & s(s+1) & 4(s+1) \\ 0 & -(s+1) & (s+1)(s+4) \end{bmatrix}$$

$$(SI - A)^{-1} = \begin{bmatrix} \frac{1}{s+1} & 0 & 0 \\ 0 & \frac{s}{(s+2)^2} & \frac{4}{(s+2)^2} \\ 0 & -\frac{1}{(s+2)^2} & \frac{s+4}{(s+2)^2} \end{bmatrix}$$

Substituting in equation ①

$$X(s) = \begin{bmatrix} \frac{1}{s+1} & 0 & 0 \\ 0 & \frac{s}{(s+2)^2} & \frac{4}{(s+2)^2} \\ 0 & -\frac{1}{(s+2)^2} & \frac{s+4}{(s+2)^2} \end{bmatrix} X_0$$

Taking inverse laplace transform on both sides

$$L^{-1}\{X(s)\} = L^{-1} \left\{ \begin{bmatrix} \frac{1}{s+1} & 0 & 0 \\ 0 & \frac{s}{(s+2)^2} & \frac{4}{(s+2)^2} \\ 0 & -\frac{1}{(s+2)^2} & \frac{s+4}{(s+2)^2} \end{bmatrix} X_0 \right\}$$

(31)

Consider  $L^{-1} \left\{ (sI - A)^{-1} \right\}$

$$= \begin{bmatrix} L^{-1} \left\{ \frac{1}{s+1} \right\} & 0 & 0 \\ 0 & L^{-1} \left\{ \frac{s}{(s+2)^2} \right\} & L^{-1} \left\{ \frac{4}{(s+2)^2} \right\} \\ 0 & L^{-1} \left\{ -\frac{1}{(s+2)^2} \right\} & L^{-1} \left\{ \frac{s+4}{(s+2)^2} \right\} \end{bmatrix}$$

Here  $L^{-1} \left\{ \frac{1}{s+1} \right\} = e^{-t}$

$$\begin{aligned} L^{-1} \left\{ \frac{s}{(s+2)^2} \right\} &= L^{-1} \left\{ \frac{1}{s+2} - \frac{2}{(s+2)^2} \right\} \\ &= L^{-1} \left\{ \frac{1}{s+2} \right\} - L^{-1} \left\{ \frac{2}{(s+2)^2} \right\} \\ &= e^{-2t} - 2t e^{-2t} \\ &= (1-2t) e^{-2t} \end{aligned}$$

$$\begin{aligned} L^{-1} \left\{ \frac{4}{(s+2)^2} \right\} &= e^{-2t} L^{-1} \left\{ \frac{4}{s^2} \right\} \quad \text{By considering} \\ &= e^{-2t} \cdot 4t \quad L^{-1} \left\{ F(s-a) \right\} = e^{at} f(t) \end{aligned}$$

$$\begin{aligned} L^{-1} \left\{ -\frac{1}{(s+2)^2} \right\} &= e^{-2t} L^{-1} \left\{ -\frac{1}{s^2} \right\} \\ &= -e^{-2t} t \end{aligned}$$

$$\begin{aligned} L^{-1} \left\{ \frac{s+4}{(s+2)^2} \right\} &= L^{-1} \left\{ \frac{1}{s+2} + \frac{2}{(s+2)^2} \right\} = e^{-2t} + e^{-2t} \cdot 2t \\ &= e^{-2t} (1+2t) \end{aligned}$$

(32)

Substituting,

$$L^{-1} \left\{ (sI - A)^{-1} \right\} = \begin{bmatrix} e^t & 0 & 0 \\ 0 & e^{-2t}(1-2t) & e^{-2t} \cdot 4t \\ 0 & -e^{-2t} \cdot t & e^{-2t}(1+2t) \end{bmatrix}$$

Substituting back in equation ①

$$x(t) = \begin{bmatrix} e^t & 0 & 0 \\ 0 & e^{-2t}(1-2t) & e^{-2t} \cdot 4t \\ 0 & -e^{-2t} \cdot t & e^{-2t}(1+2t) \end{bmatrix} x_0$$