CMPE 185 Autonomous Mobile Robots

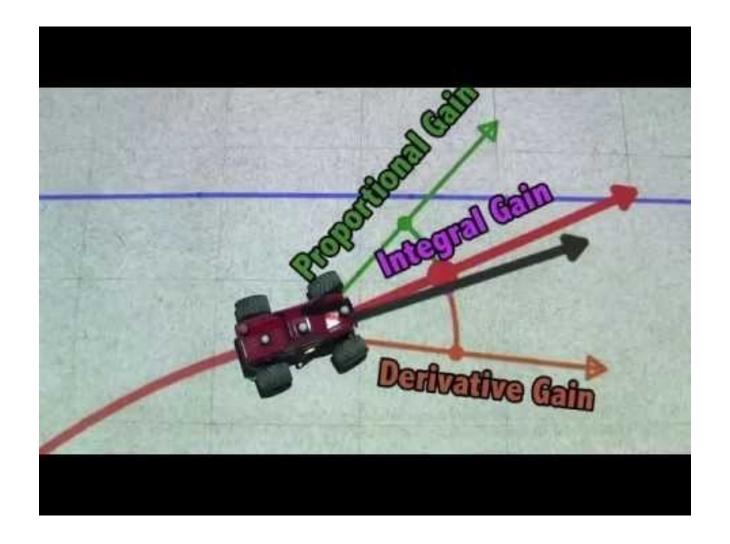
Navigation and Control Part 2

Dr. Wencen Wu

Computer Engineering Department

San Jose State University

PID Controller Explained



P Control

- Let us start with a simple controller: P controller
- Proportional Feedback Control (P Control)
 - Uses the error between the desired and measured sate to determine the control signal
- If $x_{desired}$ is the desired state, and x is the actual state, we define the error as

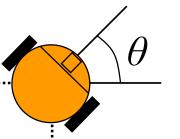
$$e = x_{desired} - x$$

• The control signal u is calculated as $u = K_P e$

where K_P is called the proportional gain

Consider the orientation control of a mobile robot

$$\begin{aligned} \dot{\theta} &= w \\ \theta_{k+1} &= \theta_k + w \Delta t \end{aligned}$$



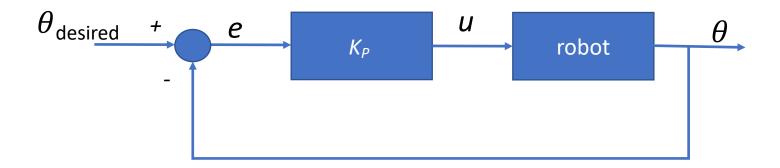
 The control signal u is the angular velocity w, and is calculated as

$$u = K_P(\theta_{desired} - \theta)$$

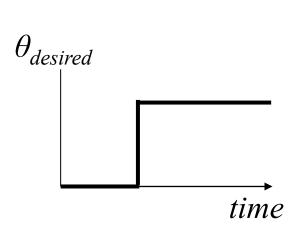
- Note:
 - If $\theta_{desired} = \theta$, the control signal is 0
 - If $\theta_{desired} < \theta$, the control signal is negative, resulting in an decrease in θ
 - If $\theta_{desired} > \theta$, the control signal is positive, resulting in an increase in θ
 - The magnitude of the increase/decrease depends on K_P

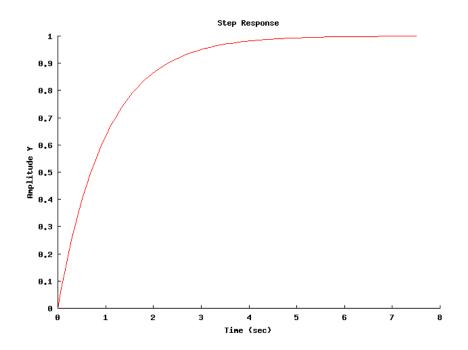
Block Diagram

$$u = K_P(\theta_{desired} - \theta)$$

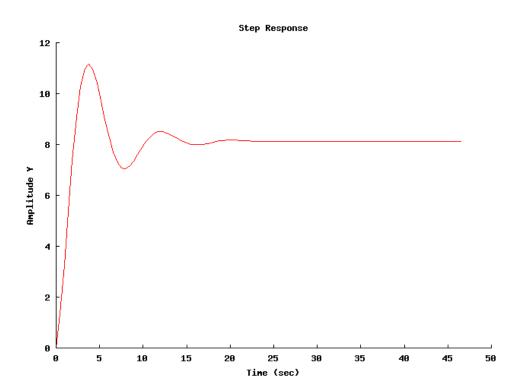


- Time Domain Response of Step Response
- Step from $\theta_{\text{desired}} = 0$ to $\theta_{\text{desired}} = 1$





- Time Domain Response of Step Response
- Step from $\theta_{desired} = 0$ to $\theta_{desired} = 8$



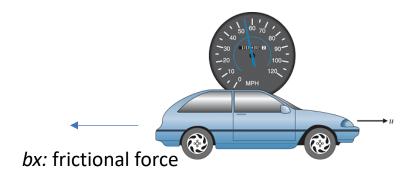
Another Example: Cruise Controllers

- Make a car drive at a desired, reference speed r
- Newton's Second Law: F = ma
- State: velocity x
- Input: gas/brake u
- Dynamics:

$$m\dot{x} = cu - bx$$

$$\dot{x} = \frac{c}{m}u - \gamma x$$

$$\gamma = \frac{b}{m}$$



c = electro-mechanical transmission coefficient

Cruise Controllers

- Assume that we measure the velocity y = x
- The control signal should be a function of

$$r - y (= e)$$

- What properties should the control signal have?
 - Small *e* gives small *u*
 - u should not be "jerky"
 - u should not depend on us knowing c and m exactly
- Car model: $\dot{x} = \frac{c}{m}u \gamma x$
- Want:

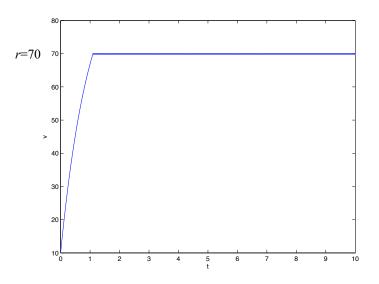
$$x \rightarrow r$$
 as $t \rightarrow \infty$ ($e = r - x \rightarrow 0$)

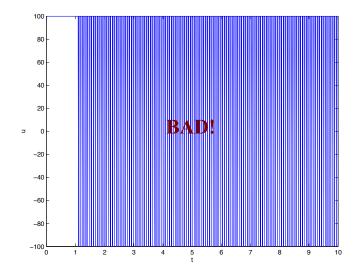
Bang-Bang Control

Attempt 1: Bang-Bang control

$$u = \begin{cases} u_{max} & if \ e > 0 \\ -u_{max} & if \ e < 0 \\ 0 & if \ e = 0 \end{cases}$$

Bumpy ride
Burns out actuators





Problem: the controller over-reacts to small errors

Proportional Control

Attempt 2: P Control

$$u(t) = K_P e(t)$$

- Intuition: if e(t) > 0, the goal velocity is larger than the current velocity. So, command a larger acceleration
- Small error yields small control signals
- Nice and smooth

Proportional Control

 At steady state (x does not change any more)

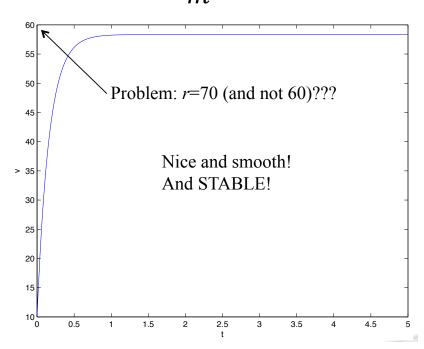
$$\dot{x} = 0 = \frac{c}{m}u - \gamma x$$

$$= \frac{c}{m}k(r - x) - \gamma x$$

$$\to (ck + m\gamma)x = ckr$$

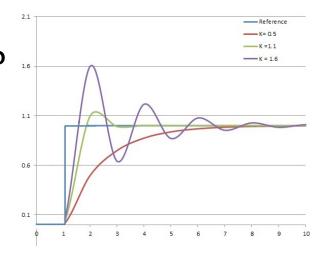
$$x = \frac{ck}{ck + m\gamma}r < r$$

$$\dot{x} = \frac{c}{m}u - \gamma x$$



Proportional Control

- We want to drive error to zero quickly
 - This implies large gains
- We want to get rid of steady-state error
 - If we're close to desired output, proportional output will be small. This makes it hard to drive steady-state error to zero.
 - This implies large gains.
- What's wrong with really large gains?
 - Oscillations

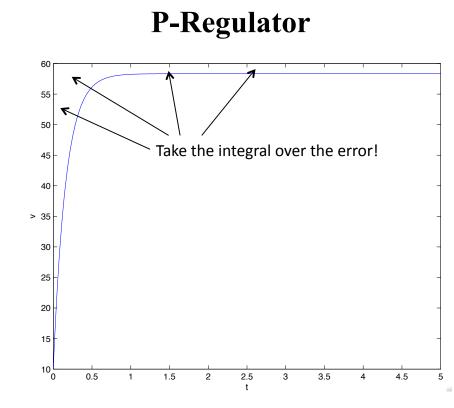


PI Controller

Attempt 3: PI-Controllers

$$u(t) = K_P e(t) + K_I \int_0^t e(\tau) d\tau$$

- If we have error for a long period of time, it argues for additional correction
- The integral term in the controller is the sum of the instantaneous error over time and gives the accumulated offset
- Force average error to zero (in steady state)



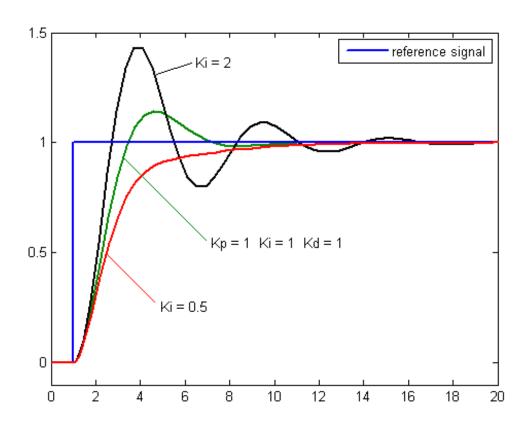
PI Controller

• Pros:

- accelerates the movement of the process towards setpoint
- eliminates the residual steady-state error

• Cons:

may result in overshooting the setpoint



Derivative Controller

- Damping friction is a force opposing motion, proportional to velocity
- Try to prevent overshoot by damping controller response
- Derivative term:

$$K_D \dot{e}(t)$$

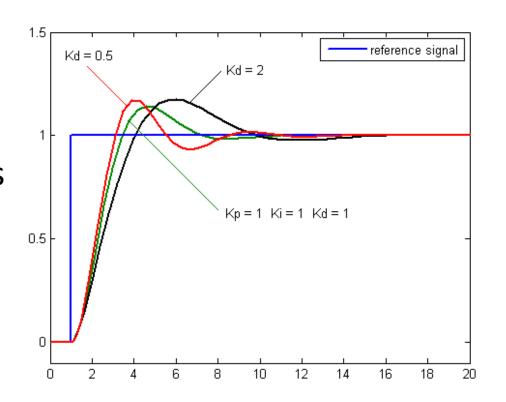
- Derivative control is "happy" the error is not changing
 - Things not getting better, but not getting worse either
- Estimating a derivative from measurements is fragile, and amplifies noise
- The Derivative term is rarely used along

PD Controller

Attempt 4: PD controller

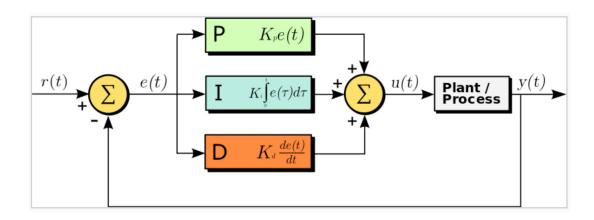
$$u(t) = K_P e(t) + K_D \dot{e}(t)$$

- Combine P and D terms
 - D term helps us avoid oscillation, allowing us to have bigger P terms
 - Faster response
 - Less oscillation



PID Control

$$u(t) = K_P e(t) + K_I \int_0^t e(\tau) d\tau + K_D \frac{de(t)}{dt}$$



PID Control

$$u(t) = K_P e(t) + K_I \int_0^t e(\tau) d\tau + K_D \frac{de(t)}{dt}$$

- P: contributes to stability, medium-rate responsiveness
- I: tracking and disturbance rejection, slow-rate responsiveness. May cause oscillations
- D: fast-rate responsiveness. Sensitive to noise
- PID: by far the most used low-level controller.
 - However, stability is not guaranteed

PID Control

- Note: we often won't use all three terms
 - Each type of term has downsides
 - Use only the terms you need for good performance

 Feedback has a remarkable ability to fight uncertainty in model parameters!

$$u(t) = K_P e(t) + K_I \int_0^t e(\tau) d\tau + K_D \frac{de(t)}{dt}$$

PID Controller Parameter Tuning

 If the parameters of the PID controller are chosen incorrectly, the controlled process input can be unstable, i.e., its output diverges, with or without oscillation.

Where do PID gains come from?

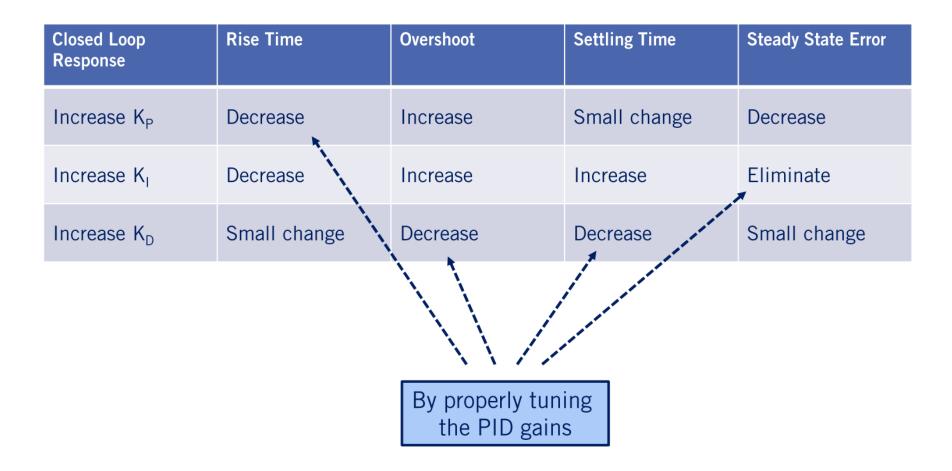
- Analysis
 - Carefully model system in terms of underlying physics and PID controller gains
 - Compute values of PID controller so that system is 1) stable and 2) performs well
- Empirical experimentation
 - Hard to make models accurate enough: many parameters
 - Often, easy to tune by hand.

PID Controller Parameter Tuning

- Parameter tuning is very important for PID controller
 - Manual tuning
 - 1. Increase P term until performance is adequate or oscillation begins
 - 2. Increase D term to dampen oscillation
 - 3. Go to 1 until no improvements possible.
 - 4. Increase I term to eliminate steady-state error.
 - Ziegler-Nichols method
 - Software

-

Characteristics of P, I, and D Gains



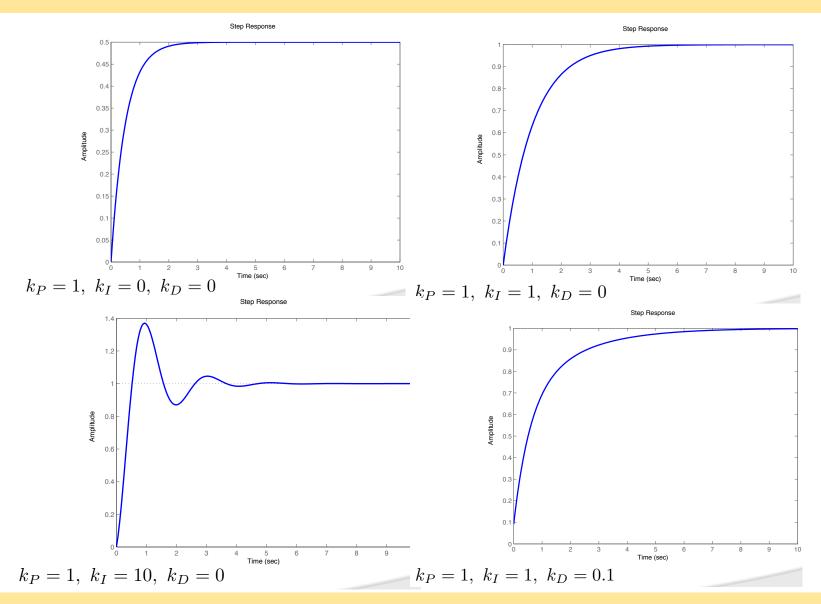
Cruise Controller

Let's consider the simplified model

$$\dot{x} = \frac{c}{m}u - \gamma x$$
 $c = 1, m = 1, \gamma = 0.1, r = 1$



Cruise Controller



Example: Go To Goal

- How to drive a robot to a goal location?
- Heading error: $e=\theta_{\mathrm{d}}$ θ

$$\begin{cases} \dot{x} = v \cos \theta \\ \dot{y} = v \sin \theta \\ \dot{\theta} = \omega \end{cases}$$

ullet In this case, the desired heading $heta_{
m d}$ is time-varying

$$(x_g, y_g)$$

$$\phi_d = \arctan\left(\frac{y_g - y}{x_g - x}\right)$$

$$(x, y)$$

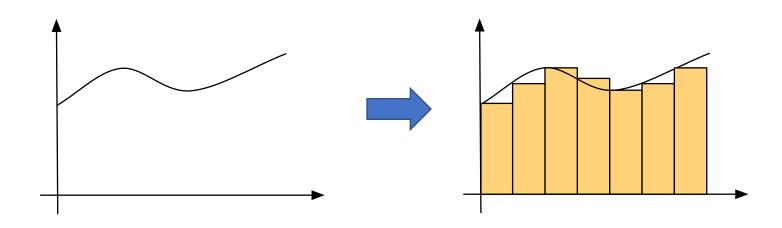
• Control: $\omega = PID(e)$

PID Controller Implementation

$$u(t) = K_P e(t) + K_I \int_0^t e(\tau) d\tau + K_D \frac{de(t)}{dt}$$

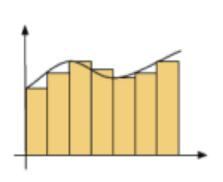
$$\Delta t$$
 (sample time)

$$\dot{e} \approx \frac{e_{new} - e_{old}}{\Delta t}$$



PID Controller Implementation

$$u(t) = K_P e(t) + K_I \int_0^t e(\tau) d\tau + K_D \frac{de(t)}{dt}$$



$$\Delta t \ (sample \ time) \quad \dot{e} \approx \frac{e_{new} - e_{old}}{\Delta t}$$

$$\int_0^t e(\tau)d\tau \approx \sum_{k=0}^N e(k\Delta t)\Delta t = \Delta t E$$

$$\Delta t E_{new} = \Delta t \sum_{k=1}^{N+1} e(k\Delta t) = \Delta t e((N+1)\Delta t) + \Delta t E_{old}$$

$$E_{new} = E_{old} + e$$

PID Controller Implementation

Each time the controller is called

```
read e;
e_dot=e-old_e;
E=E+e;
u=kP*e+kD*e_dot+kI*E;
old_e=e;
Note: The coefficients now include the sample time
and must be scaled accordingly
```

• Thank You!