

on Ione [8-(1.3)3] exp[-(1.3)(a-3)] + e-3(1.3)[.(4+3)8+(1+3)] e-301.i) [{e301.i) (4.3i)}- a(1.j)} a Jenc 63011)[8-(1.1)2] exb[-(1.1)(0.2)] + (1.1)-(1.13)8 on B. 2/19 e 3(1.1) [6-(1.1)] exp [-(1.1)(a-5)] + (1.1) - (4.13)8 8 / 0 e 3(1.3) - (4.3) / - a(1.j) [e3(1.j) - 1] 1 = [2 2 2 2] g + 3 g 11 1 0 + 3 2 2 200] - 10 In the region as gsab-38 mpet of on B. M. T. 1 - [(2-10) ((-1) =] qx3 & 5113 - 10 In the region a+b-38 < 8 ≤ a+b B= [- (1.1) [8-(1.1) [8-(1.1) (0.46-8)] + (1.1) - (1.43) [8]

B= [- (1.1) (0.46-8)] + (1.1) - (1.43) [8] In the region 0+659 x 200 ((6108-9-1)10170 x 8 18 B= 0 with changing frequency the skin depth would change. However the expressions would remain same. Charly the decay would be fonter with increasing frequency and decay would be fonter with increasing frequency and magnetic field would be confined more and more tworks the surface and in between conductors. (ii) Lext = 18.42 1.5 b) (100) = 3 d (100) = 10 d (100) = or year = / 1/20 1 2 x dg dt or foxt ohrhat ling on Lext = more In & - Mil In a finductor.

for internal inductance of second conductor dy = dy Jene $I_{ene} \approx 1 - \frac{g \exp \left[-\frac{(1+j) \log - g)}{g}\right]}{(6+0)\left[1-e^{-3(1+j)}\right]}$ B. Ing sene (to)) (con) forday is sind o on B: Tene dr. Bogdt Jenc on Lines - Ships (Tene) de (des) NI Land de Mille or Line : Arthook St 1- gexp [- (10) (a-6-8)]) de on Lines = Mynod $\int_{0}^{1} \int_{0}^{1} \int_{0}^{$ a fine = without $\frac{3x6!}{2\pi} = \frac{3(1+3)[1-e^{-3(1+3)}]}{(\alpha+b)[1-e^{-3(1+3)}]} + 8 \frac{(\alpha+b)[1-e^{-3(1+3)}]}{(\alpha+b)[1-e^{-3(1+3)}]^2}$ $\frac{a + b + b}{(a + b)^{2}(1 - e^{-3(1+i)})} = \frac{a + b}{(a + b)^{2}(1 - e^{-3(1+i)})} = \frac{b}{(a + b)^{2}(1 - e^{-3(1+i)})}$ a Lines 2/10/ [1 (a+b-3d) - a+b + 8(a+b)2[1-e-3(1+j)]2 -2(1+j)(a+b)(e((1-5)-1))7 on Ling ≈ Mul [-IN (1-30) + 8(1-j) 1-e-8(1.1)] [1-e-3(1.1)]] on Line ? " Mot In (a+b-3d) or - Mot In (1-38)

For internal inductance of first conductor da = dy Tene Since the expression is very complicated we can make approximations Tene = e 30 +1) [8-(1+3) [8-(1+3) [8-(1+3) (e3(1+1)-(4+3))] - a(1+j) (e3(1+1)-(4+3)) or <u>fonc</u> ≈ -e 3(1.1) (1.1) g exp [-(1.1)(a-9)] + (1.1) -aci,j) [e30,1)-1] or Tenc & 6 +3(1,1) 3 6 x b [- (1,1) (0,2)] +1 a [e+3(j+1)-1] a fenc $\approx g \exp\left[-\frac{(1+j)(\alpha-g)}{8}\right] - 1$ $\approx g \exp\left[-\frac{(1+j)(\alpha-g)}{8}\right]$ $= a \left[1-e^{-3(1+i)}\right]$ B ~ Mr/2018 ~ Mr/201 2xp [= (1+1)(a-9)]-1/9 or B & M/2010 (1-e-3(1+j)) exp [- (1+j)(a-9)] dr. Baldt Jene or dr. harroz de gt sexb [-\frac{8}{5}(1+9)(a-8)] on >= [27702(1-10-3(11))]2 [Sexp[-2(1+j)(a-3)] dg

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on Limi = Myhor 6-6(1+1) 8 [6 ((1)) - (++6)) 8 - 2(11) a (e6(11)) on Limi & Maror 6-6(11) 8 -2(11) a [6(11)] a lini1 & Myhologe-e-6(1+3)] (1+3) a HMI 20 (cincl 8 ska) i. Thus the net internal inductance is Lint = Lint + Lint 2 er Line & Mal In (a+b-38) or Lint & My IN (a+p) For different frequencies the value of inductances can be determined. We assume the wire thickness Lint = $\frac{ML}{2\pi} \ln \left(\frac{3.5a}{3.5a-36} \right) = \left(1.02 \frac{MH}{M} \right) L$ Lext. MI IN 0 = 1/21/122 = (0.183 MH) Y tor 1 = 10 OHF Lint: 1/211 In (3.50-38) = (0.32 nH) & 1 (0.183 MH) 8 tor 1=100 WHS Fint = Tre IN (3.50-36) = (0.101 NH) 8 Text = fr 12 - [0.183 mH) 8