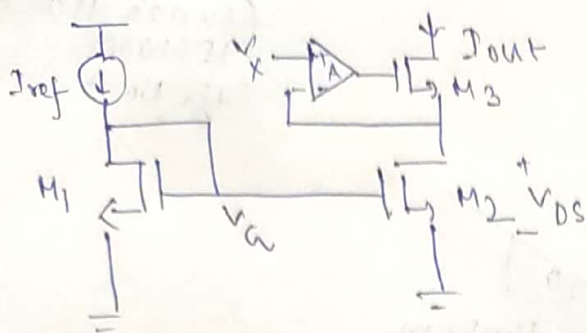


iii)



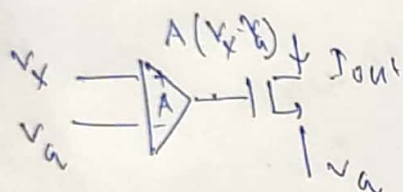
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$$I_{ref} = \frac{1}{2} \mu_n C_{ox} \left(\frac{W}{L} \right)_1 (V_G - V_{th})^2 (1 + \lambda V_{DS})$$

$$I_{out} = \frac{1}{2} \mu_n C_{ox} \left(\frac{W}{L} \right)_2 (V_G - V_{th})^2 (1 + \lambda V_{DS})$$

We wish $I_{ref} = I_{out}$

$$\therefore V_{DS} = V_G$$



$$I_{out} = \frac{1}{2} \mu_n C_{ox} \left(\frac{W}{L} \right)_3 [A(V_x - V_G) - V_G - V_{th}]^2 (1 + \lambda V_{DS3})$$

$$I_{out} = \frac{1}{2} \mu_n C_{ox} \left(\frac{W}{L} \right)_3 [A(V_x - V_G) - V_G - V_{th}]^2 (1 + \lambda V_{DS3})$$

$$I_{out} = \frac{1}{2} k_{n3} [AV_x - (A+1)V_G - V_{th}]^2 (1 + \lambda V_{DS3})$$

$$\frac{I_{out}}{1 + \lambda V_{DS3}} = \frac{1}{2} k_{n3} [AV_x - (A+1)V_G - V_{th}]^2$$

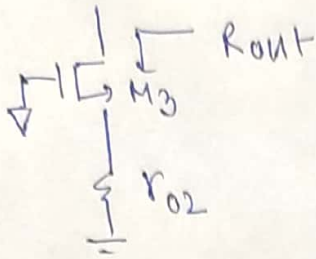
$$\frac{2I_{out}}{k_{n3}(1 + \lambda V_{DS3})} = (AV_x - (A+1)V_G - V_{th})^2$$

$$V_x = \frac{1}{A} \left[\sqrt{\frac{2I_{ref}}{k_{n3}(1 + \lambda V_{DS3})}} + V_{th} + (A+1)V_{GS1} \right] \quad \text{since } V_G = V_{GS1}$$

This value guarantees $I_{out} = I_{ref}$

For deriving R_{out}

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$$\begin{aligned} R_{out} &= r_{o3} + (1 + g_{m3} r_{o3}) R_s \quad R_s = \text{source resistance} \\ &= r_{o3} + r_{o2} (1 + g_{m3} r_{o3}) \\ &= r_{o2} + r_{o3} + g_{m3} r_{o2} r_{o3} \quad (\text{Ans}) \end{aligned}$$

Since for finding the out output resistance V_{in} is shorted

$$r_{o2} = \frac{\frac{r}{\lambda I_{Dref}}}{\lambda I_{out}}$$

$$r_{o3} = \frac{1}{\lambda I_{out}}$$

$$\begin{aligned} g_{m3} &= k_{n3} V_{ov3} \\ &= k_{n3} (V_{GS3} - V_{th}) \end{aligned}$$

All the parameters are for the time when I_{out} current flows