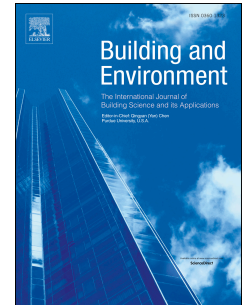


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# Study of thermal comfort in underground construction based on field measurements and questionnaires in China

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## ABSTRACT

Underground buildings have the potential to reduce energy demand in comparison to conventional aboveground buildings. In China, previous studies on thermal comfort have been mainly focused on the building environment, such as offices, residential and non-residential buildings, but rarely on underground construction, especially the air-defence basement. To investigate the thermal comfort conditions in the unique and complex underground construction, comparative thermal comfort surveys including field measurements and questionnaires have been carried out in different underground air-defence basement in 95 nationwide typical cities. As a result, the mean thermal sensation (AMTS) from questionnaires is compared with PMV calculated based on the field data in different cities, and significant discrepancies are found. The occupant's actual cool feeling is larger in the cooler side, but occupants may sense the warmth as being less severe than the PMV predicts in warmer side. In addition, the neutral temperature model for underground construction is developed, and the thermal acceptability and preference are discussed. It shows that thermal acceptable temperature range is unsymmetrically distributed with respect to the thermal neutral temperature and changes with the ground temperature. Ultimately, the recommend temperature ranges for different cities through thermal comfort model are discussed based on psychrometric chart.

Keywords: thermal sensation; underground construction; thermal neutral temperature; acceptable temperature ranges

## 1. Introduction

## 1.1 Need for study

Underground construction is perceived to be environmental friendly and sustainable as it is the higher protection against the climatic influences by constant surrounding soil temperature [1,2] and a pleasant thermal comfort can be ensured with less energy [3,4]. In recent years, there has been a great interest in underground construction (UC) including air-defence basement construction, subway, parking lots, shopping malls, exhibition halls and service facilities in China. At present, China's underground space development has entered a high-speed development period, the total quantity of air-defence basement ranks first in the world.

Thermal environment of underground construction is different from the aboveground buildings. In underground construction, since there is no direct influence from the solar radiation, the thermal sensation induced by direct solar radiation can be neglected. The mean ground temperature ( $T_g$ ) greatly affects the heat transfer of surrounding rock-soil [5], [6] and the average radiation temperature ( $T_R$ ), that plays an important role on the personal thermal sensation. Too high or low average radiation temperature generally causes bad effects on the thermal sensation [7]. Different  $T_g$  in different regions may cause different  $T_R$ . **Table.1** shows the  $T_R$  of the offices buildings measured by LSI thermal comfort device both in the aboveground and underground buildings in four typical cities. It could be seen that the  $T_R$  in aboveground building was generally 1-2 °C higher than the air temperature  $T_{in}$  in room. But the  $T_R$  in the underground construction is about 1 °C lower than that of air temperature, and different  $T_R$  is observed in different cities. Thermal comfort is defined as “that condition of mind which expresses satisfaction with the thermal environment”[8].

The variations of personal psychological state in underground facility would inevitably make the person's thermal sensation different from the aboveground.

There are no specific studies on thermal comfort of occupants in underground air defence basement in China. The occupants' thermal sensation in the underground construction needs to explore to provide a theoretical basis for the thermal environment design.

**Table.1** The measured  $T_R$  in underground construction and aboveground buildings in different cities

| Typical city | Test time                    | $T_o$<br>( $^{\circ}\text{C}$ ) | $T_{in}$ of the                                   | $T_R$ of the                                      | $T_g$<br>( $^{\circ}\text{C}$ ) | $T_{in}$ of the                                       | $T_R$ of the  |
|--------------|------------------------------|---------------------------------|---|---|---------------------------------|---|---|
|              |                              |                                 | Aboveground<br>building<br>( $^{\circ}\text{C}$ ) | Aboveground<br>building<br>( $^{\circ}\text{C}$ ) |                                 | underground<br>construction<br>( $^{\circ}\text{C}$ ) | underground<br>construction<br>( $^{\circ}\text{C}$ ) |
| BeiJing      | 15:00-16:00 in Aug. 23, 2008 | 32.6                            | 29.7  | 30.8  | 13.7                            | 24.3  | 22.2  |
| NanJing      | 11:15-12:15 in Jul.25, 2007  | 36.4                            | 28.7  | 30.5  | 17.4                            | 25.3  | 24.1  |
| Changsha     | 16:00-17:00 in Jul.26, 2008  | 33.7                            | 28.4  | 29.8  | 17.9                            | 26.5  | 24.8  |
| Guangzhou    | 14:30-15:30 in Aug. 4, 2008  | 36.2                            | 28.3  | 30.4  | 23.8                            | 27.4  | 25.6  |

## 1.2 Learning's from earlier thermal comfort studies

The theoretical basis for field study of thermal comfort could be classified in two categories: the predicted mean vote (PMV) and percentage of people dissatisfied (PPD) methods [7] developed by Fanger and adaptive model proposed by Nicol and Humphreys [9,10].

PMV model is used in practice in the ISO 7730 [11] and ASHRAE-55 [12] standards. More and more studies put PMV-PPD model into question [13,14,15] recently. The argument is that PMV-PPD model ignores the important parameters such as cultural, climatic, social and contextual dimensions of comfort and thus denying all processes of thermal adaptation [16], especially in free-running buildings. An extension of the PMV model that includes an expectancy factor is also introduced by Fanger et.al [17] for using in non-air-conditioned buildings in warm climates. Subsequent thermal comfort models [18,19,20] based on PMV model have been developed.

The adaptive thermal comfort model is a paradigm shift versus the predicted mean vote (PMV) approach. According to the field studies, linear regressions relating indoor operative temperatures to prevailing outdoor air temperatures are established. It is being widely accepted in the thermal comfort research community that state of mind is widely driven by perception and expectation of the occupants. The adaptive model was first included in the ASHRAE standard 55 [21] in 2004 as an optional method for evaluating naturally ventilated buildings. In 2007 the adaptive model was also included in EN 152515 [22]. Recently, Humphreys M et.al [23] updated the adaptive model through the new insights and an extended database.

Many field studies for thermal comfort have been carried out in different continents (Europe[24,25,26,27], Asia[28,29,30,31], Africa[32], etc.) and involves a variety of building types such as office buildings [33], residential building [34,35], educational building [36,37,38]. However, most of them are for aboveground buildings and there has been limited study on underground construction.

Considering the complex underground thermal environment, Agus P. Sasmito et.al [39] found that the virgin rock temperature ( $T_g$ ) had a great relation with the thermal comfort. Maidment G et.al [40] studied the thermal comfort conditions in underground railway environments in the UK. It shows that the acceptable thermal comfort criteria for an office may not be achievable in an underground railway environment. Based on the building information model of the subways, Mohamed Marzouk et.al (2014)[41] gave the ways to track the thermal comfort problems. In China, Hu Songtao et.al [42] performed the field test of thermal environment parameters and the subjective questionnaire in underground railway trains in different cities. Gang Liu [43] studied on thermal comfort of passenger at high-speed railway station in transition season. The air-defence basement is the underground building with large space and high density of people in wartime, the thermal comfort of the occupants in air-defence basement should be a concern. It is not possible to obtain a generalized thermal comfort model for all climatic zone because adaptation process, expectation and perception of people are region specific [44]. Toe and Kubota [45] found that the typical adaptive actions, occupants' ability and avenues for adaptation, and comfort temperatures differed with climate. Manoj Kumar Singh et.al [46] developed the thermal comfort models for various climatic zones of North-East India. Recently, based on field studies and laboratory studies from different climate zones in China, the Chinese evaluation standard for the indoor thermal environment for aboveground buildings was proposed [47]. However, the widely used design standard for air defence basement in China is the *Design Code for Civil air defence basement (GB50038-2005)* [48], which recommends same thermal comfort zones for underground engineering in different regions. It ignores thermal environment difference and occupant adaptability in different regions and may lead to the usage of the standard be widely limited. China has a very broad geographical area and therefore having large differences of thermal environment

parameters in different regions. The large variations can also be seen from the annual mean ground temperature  $T_g$ , which are 5.4 °C, 13.4 °C and 23.8 °C in Harbin, Beijing and Guangzhou, respectively. The thermal environment particularity and different psychological and physiological reactions of occupants in the underground would make the acceptable thermal comfort criteria for different areas may be different. But the reasonable thermal comfort model for different climatic zones in underground environment has not been discussed.

### 1.3. Aims and objectives

Accordingly, the aims of this study are as follows: a) Comparing the actual mean thermal sensation (AMTS) from questionnaires with PMV calculated from the field measurements to find the 'acceptable' thermal comfort criteria for underground environment in different cities; b) Establishing thermal neutral temperature model and acceptable temperature ranges to provide a design basis for thermal environment of underground environment; c) Comparing and exploring the recommend temperature ranges through new thermal comfort model with the original temperature ranges for underground environment in different areas.

## 2. Methodology

The field studies were conducted in different air-defence basement in 95 nationwide typical cities over a period of 6 years in China. The methodology for this work consists of both subjective and objective study. The subjective study consists of administering questionnaire to subjects during the field study. During the process of filling up the questionnaire, other micro-climatic parameters are measured simultaneously and discussed in the objective study. Field investigations on thermal environment are mainly carried out in the air-defence basement or the underground store offices in different cities as shown in **Fig.1**. Until October 2014, 825 data samples and 1318 effective questionnaires were recorded from field studies in 95 nationwide typical cities.



(a) Underground air-defence basement in Nanjing

(b) Underground air-defence basement in Beijing

Fig.1 The typical underground air-defence basement in Nanjing (a) and Beijing (b)

## 2.1. Subjective study

To assess the clothing, activity level, background information and thermal comfort of the occupants, a questionnaire was designed based on the Thermal Environment Survey of Standard 55 [49]. The questionnaire consists of two main parts: I: Basic information, which includes the height, weight and age and the clothing and level of activity of subjects. II: Thermal comfort, which includes the thermal sensation, thermal preference, and thermal acceptance of subjects. The ASHRAE seven-point scale of thermal sensation (+3 (hot), +2 (warm), +1 (slightly warm), 0 (neutral), -1 (slightly cool), -2 (cool), -3 (cold)) are adopted in the subject questionnaires. Two persons were responsible for guiding people to fill-in thermal sensation questionnaires. The main contents of subjective questionnaire on thermal comfort Part II are included in **Appendix A**.

**Table.2** represents the different comfort survey indicators. The number of questionnaires filled depended on the geographical area, 432 copies in the area with ground temperature  $T_g < 12\text{ }^{\circ}\text{C}$ , 502 copies in the area with  $12\text{ }^{\circ}\text{C} < T_g < 20\text{ }^{\circ}\text{C}$  and 384 copies in the area with  $20\text{ }^{\circ}\text{C} < T_g$ . The gender, age, height and weight distributions of the investigated occupants are also shown in **Table 2**.

**Table 2** Comfort survey indicators

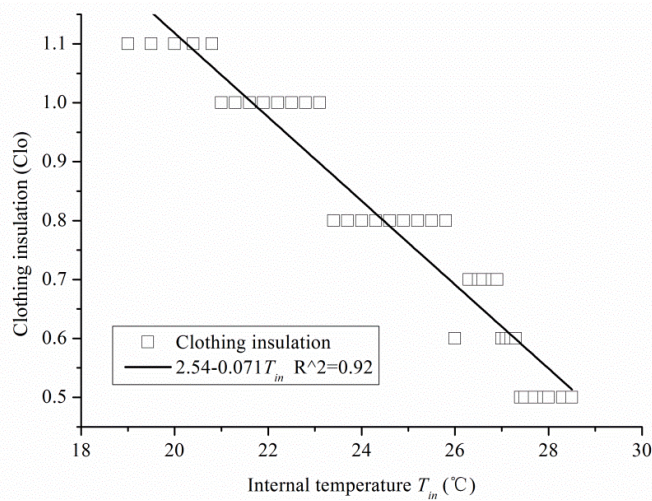
| $T_g$ in filed areas | $T_g < 12\text{ }^{\circ}\text{C}$ | $12\text{ }^{\circ}\text{C} < T_g < 20\text{ }^{\circ}\text{C}$ | $20\text{ }^{\circ}\text{C} < T_g$ |
|----------------------|------------------------------------|---|------------------------------------|
|----------------------|------------------------------------|---|------------------------------------|

|  |  |   |   |
|--|--|---|---|
| Cities                                     | Harbin, Changchun,<br>Xining, Urumq,<br>Datong, ShenYang,<br>Yinchuan, Taiyuan,<br>Lanzhou | Nanjing, Beijing, Zhengzhou,<br>Shanghai, Hangzhou, Hefei,<br>Anqing, Wuhan, Changsha,<br>Jinan | Fuzhou, Xiamen, Jinjiang,<br>Nanning, Guanghzou,<br>Qinzhou, Haikou |
| Subjects                                   | Male:316/432<br>female:116/432   | male:326/502<br>female:176/502  | male:282/384<br>female:102/384                                      |
| Respondent Age(%)                          | >60: 3%<br>40-60: 22.6%<br>20-40: 69.9%<br><20: 4.4%                                       | >60: 3.6%<br>40-60: 20.5%<br>20-40: 70.3%<br><20: 5.6%  | >60: 2.3%<br>40-60: 19.8%<br>20-40: 74.7%<br><20: 3.1%              |
| Respondent Age<br>mean (min. max.)         | 26 (16-61)   | 27 (18-63)  | 23 (19-63)  |
| Respondent height (m)<br>mean (min. max.)  | 174.6 (155-184)  | 171.4 (150-186)   | 170.5 (150-178)   |
| Respondent weight (kg)<br>mean (min. max.) | 67.8 (45-89)   | 62.8 (48-91)  | 62.3 (45-88)  |

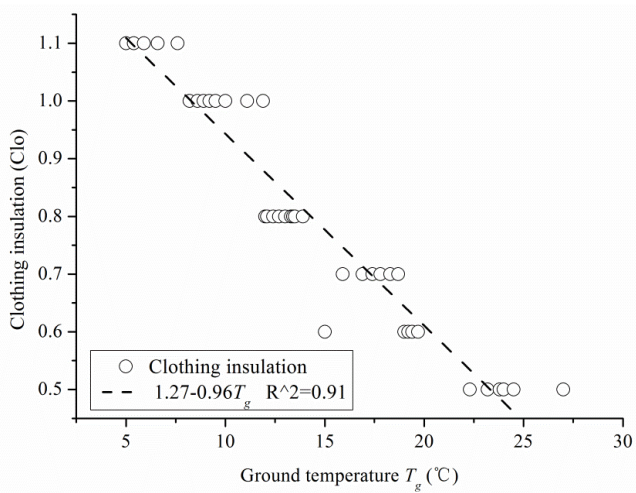
Individual clothing articles indicated in the survey responses are converted into their respective thermal insulation values using the garment values according to ASHRAE Standard 55. **Fig.2** gives clothing thermal insulation values as function of the internal air temperature  $T_{in}$ . In **Fig.2**, the thermal insulation varies from 0.5 Clo to 1.2 Clo with the  $T_{in}$  ranging from 18.5 °C to 29.3 °C.

The annual mean ground temperature ( $T_g$ ) is the important regional factor, which influences the thermal load in underground construction. **Fig.3** shows the clothing thermal insulation values vary with  $T_g$ . It could find that the clothing thermal insulation changes with the  $T_g$ . The average clothing insulation value is 1.0 Clo when the  $T_g$  below 12 °C, while the  $T_g$  between 12 °C and 20 °C, the average value is 0.7 Clo, and when the  $T_g$  above 20 °C, the average value is only 0.5 Clo.



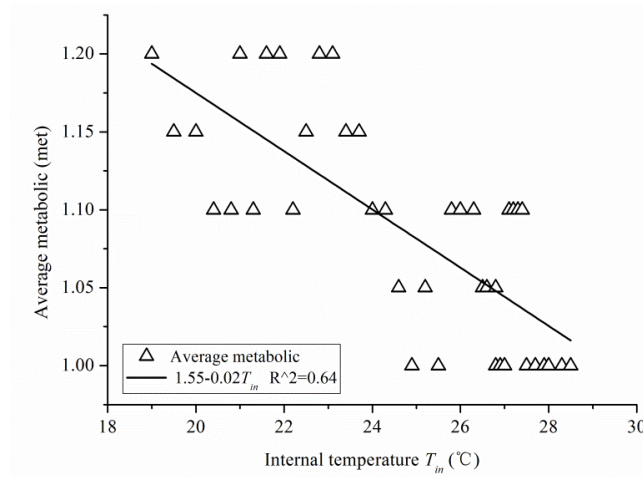


**Fig.2** Thermal clothing insulation values as function of the internal temperature.



**Fig.3** Thermal clothing insulation values as function of the ground temperature.

Metabolic rates are calculated from the descriptions of the activity of individuals in various questionnaires according to ISO 7730 [50]. In this study, activity levels vary from 1 met to 1.2 met and there is an average value equal to 1 met for the person in the underground construction. **Fig.4** confirms that metabolic rates slightly decrease with an increasing internal temperature.



**Fig.4** Average metabolic values as function of indoor operative temperature

## 2.2. Objective study

The variables measured contain internal air temperature ( $T_{in}$ ), radiation temperature ( $T_R$ ), ground temperature ( $T_g$ ), relative humidity ( $RH$ ), and the air velocity ( $V_A$ ). The instruments, range and accuracy of each measured parameter are shown in **Fig.5** and **Table.3**. Until October 2014, 825 data samples were recorded from different underground construction in 95 nationwide typical cities.



a. LSI thermal comfort device



b. CO<sub>2</sub>, O<sub>2</sub>, temperature and humidity instrument

**Fig.5** Thermal environment test instruments

**Table.3** Measuring range and accuracy of the instruments used in this study

| instrument                 | Parameters | Range     | Accuracy  |
|----------------------------|------------|-----------|-----------|
| LSI thermal comfort device | $T_{in}$   | 10-35°C   | ±0.5 °C   |
|                            | $T_R$      | 10-35°C   | ±0.5 °C   |
|                            | $RH$       | 20-80%    | ±1.6%     |
|                            | $V_A$      | 0-2m/s    | ±0.1 m/s  |
| Testo 425                  | $V_A$      | 0-20m/s   | ±0.03 m/s |
| Testo 425                  | $T_{in}$   | 0-70 °C   | ±0.5 °C   |
| HUMIPORT                   | $RH$       | 10-80%    | ±1.6%     |
| KIMO TM200                 | $T_R$      | 50-250 °C | ±0.2°C    |

The actual mean thermal sensation vote (AMTS) could be obtained from the field questionnaires and the predicted mean vote (PMV) values could be calculated through the measured thermal parameters. Then, the AMTS votes would compare with the PMV votes to find the thermal sensation variations in underground construction.

### 3 Results and analysis

#### 3.1 Average radiation temperature

Based on the field tests, the operative temperature  $T_{op}$  could be simplified as an average value of the internal air temperature ( $T_{in}$ ) and average radiation temperature ( $T_R$ ) ( $T_{op} = (T_R + T_{in})/2$ ) according to the conditions introduced in ASHRAE Standard55 [51]. The temperature difference ( $\Delta T = T_R - T_{in}$ ) between  $T_R$  and  $T_{in}$  varying with the  $T_{op}$  in Nanjing and Harbin is shown in Fig.6.

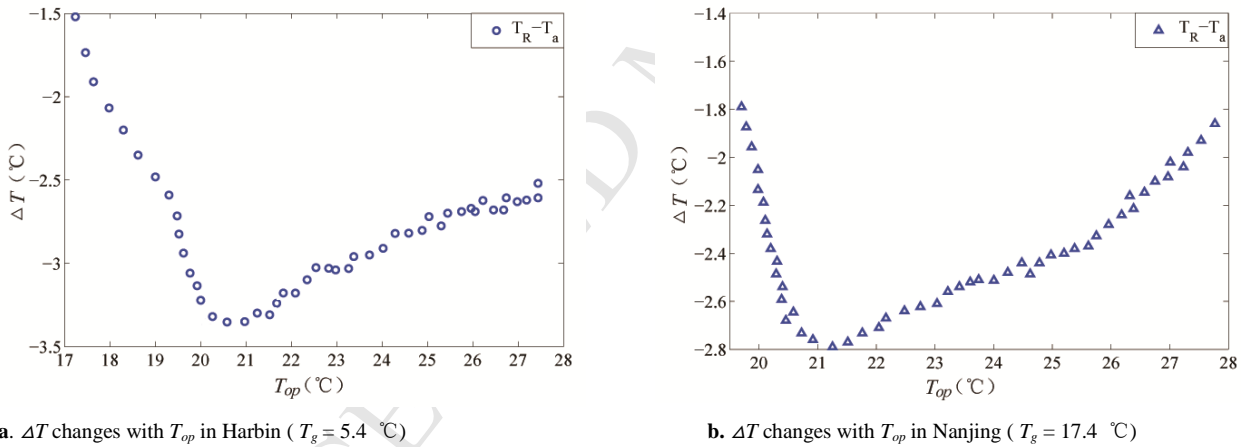


Fig.6  $\Delta T$  changes with  $T_{op}$  in cities of Harbin and Nanjing

In Fig.6, it could be found that the temperature difference ( $\Delta T$ ) between  $T_R$  and  $T_{in}$  in the typical cities: Harbin and Nanjing is negative, which means that  $T_R$  is lower than the internal air temperature. When the  $T_{op}$  is relative lower and varies in the range of 18 °C to 21 °C, the  $\Delta T$  decreases with increasing  $T_{op}$ . For example, in an underground construction in Harbin, the  $\Delta T$  is -1.5 °C corresponding  $T_{op}$  of 17 °C, however, the  $\Delta T$  changes to -3.4 °C when  $T_{op}$  is 20.5 °C. This may due to that when the  $T_{op}$  varies in the lower range from 18 °C to 21 °C. Although the  $T_{in}$  rises, wall temperature and  $T_R$  have smaller changes due the larger thermal storage capacity of the rock-soil surrounding and

relative lower  $T_g$ . This leads to the difference between the  $T_{in}$  and  $T_R$  becomes larger with the  $T_{op}$ . However, when the  $T_{op}$  varies in the higher range from 21 °C to 28 °C in **Fig.6**, the  $\Delta T$  increases with the  $T_{op}$ . In **Fig.6b**, for an underground construction in Nanjing, the  $\Delta T$  are found as -2.4 °C and -1.6 °C corresponding to the  $T_{op}$  22.5 °C and 28 °C, respectively. The temperature difference between the internal air and the wall become larger when the  $T_{op}$  above 22 °C, thus, the wall temperature and  $T_R$  rise quickly and the difference between the  $T_R$  and  $T_{in}$  becomes smaller.

In aboveground buildings, the  $T_R$  is about 2-3 °C higher than the indoor air temperature in summer. The relative higher  $T_R$  has bad effects on the occupants' thermal comfort. However, in underground construction, the  $T_R$  is always lower than  $T_{in}$  due to the relative lower  $T_g$ . This would cause different thermal sensation for the occupants in underground construction and the acceptable thermal comfort criteria for aboveground may not be achievable in underground environment. Meanwhile, the thermal environment of underground construction is also different in different regions. This would lead to regional differences of personal thermal sensation.

### 3.2 Thermal sensation

The actual mean thermal sensation (AMTS) values of occupants for half-degree operative temperature bin are obtained directly from the questionnaires. PMV values varying with internal temperature are also calculated based on the field tests and compared with the AMTS values in typical cities of Harbin, Nanjing and Guangzhou shown in **Fig.7**. The regression analysis of PMV and AMTS votes with  $T_{in}$  are performed through the line and logarithmic function, respectively. The fitted AMTS and PMV equations in the typical cities are:

Harbin with  $T_g=5.4$  °C :

$$AMTS=1.86\ln(T_{in}-14.4)-3.89 \quad R^2=0.82 \quad (1)$$

$$PMV=0.237T_{in}-5.37 \quad R^2=0.98 \quad (2)$$

Nanjing with  $T_g=17.4$  °C :

$$\text{AMTS}=2.2\ln(T_{in}-17.7)-4.6 \quad R^2=0.84 \quad (3)$$

$$\text{PMV}=0.311T_{in}-7.97 \quad R^2=0.98 \quad (4)$$

Guangzhou with  $T_g=23.6$  °C :

$$\text{AMTS}=3\ln(T_{in}-14.2)-7.48 \quad R^2=0.83 \quad (5)$$

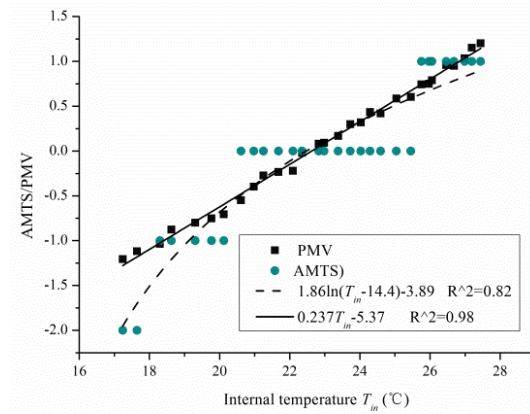
$$\text{PMV}=0.3T_{in}-7.8 \quad R^2=0.97 \quad (6)$$

The regression relationships indicate that AMTS does not agree with PMV. In the **Fig.7**, the values of AMTS are lower than PMV when the internal temperature below 21 °C, 23.5 °C and 24 °C in Harbin, Nanjing and Guangzhou, respectively. When the  $T_{in}$  is 20 °C, the values of PMV is obtained as -1.45 while the corresponding AMTS is -2.0 in an underground construction in the Nanjing. In the city of Guangzhou with the  $T_g$  of 23.6 °C in **Fig.7c**, AMTS is 0.5 lower than PMV when the  $T_{in}$  is 22 °C. It indicates that in the cooler side of the thermal sensation, the AMTS values are lower than PMV with the same  $T_{in}$ , the actual cool thermal sensation of the occupants is larger. This also indicates that the traditional PMV model may lead to some errors for evaluating the thermal environment of the underground construction.

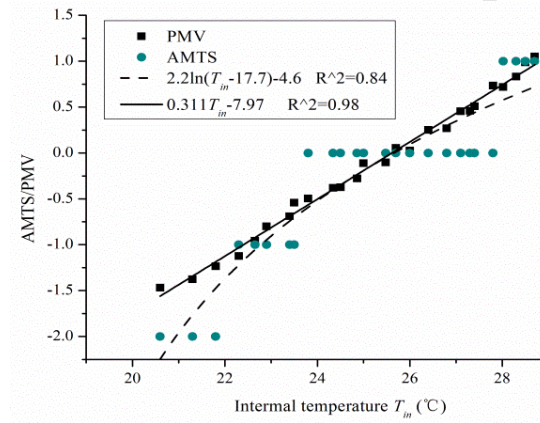
When the  $T_{in}$  varies from 21 °C to 25.5 °C in Harbin in **Fig.7a**, from 23.5 °C to 26.4 °C in Nanjing in **Fig.7b**, from 24 °C to 27 °C in Guangzhou in **Fig.7c**, the average AMTS values are 0, the occupants' thermal sensation is comfortable and the PMV values are in the range of -0.5 to 0.5. When the  $T_{in}$  increases further, the value of AMTS is lower than PMV. In Harbin in **Fig.7a**, when the  $T_{in}$  is 27 °C, the value of PMV is 0.3 larger than the AMTS, and the difference extends 0.5 when the  $T_{in}$  is 28 °C. This shows that the people actual thermal sensation values of warmth are smaller than the calculated PMV. The occupants may sense the warmth as being less severe than the PMV predicts.

From **Fig.7**, compared with the AMTS in different areas, it could be found that the values of occupants' AMTS are smaller in the areas with higher  $T_g$  under the same  $T_{in}$ . For example, When the  $T_{in}$  is 19 °C, the value of AMTS is found as -1.0 in the Harbin with  $T_g=5.4$  °C, whereas the AMTS value is -2.0 in Nanjing with  $T_g=17.4$  °C. When the  $T_{in}$  is 28 °C, the occupants' AMTS are 1.0 and 0.5 in Nanjing ( $T_g=17.4$  °C) and Guangzhou ( $T_g=23.8$  °C), respectively. This

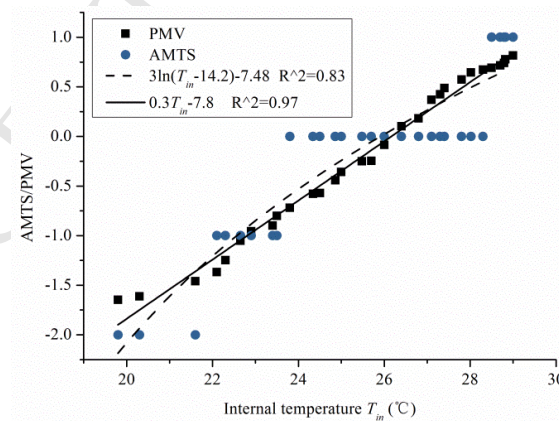
is due to the thermal environment characteristic difference and adaption processes in different regions.



a. PMV and AMTS changes with  $T_{in}$  in Harbin



b. PMV and AMTS changes with  $T_{in}$  in Nanjing



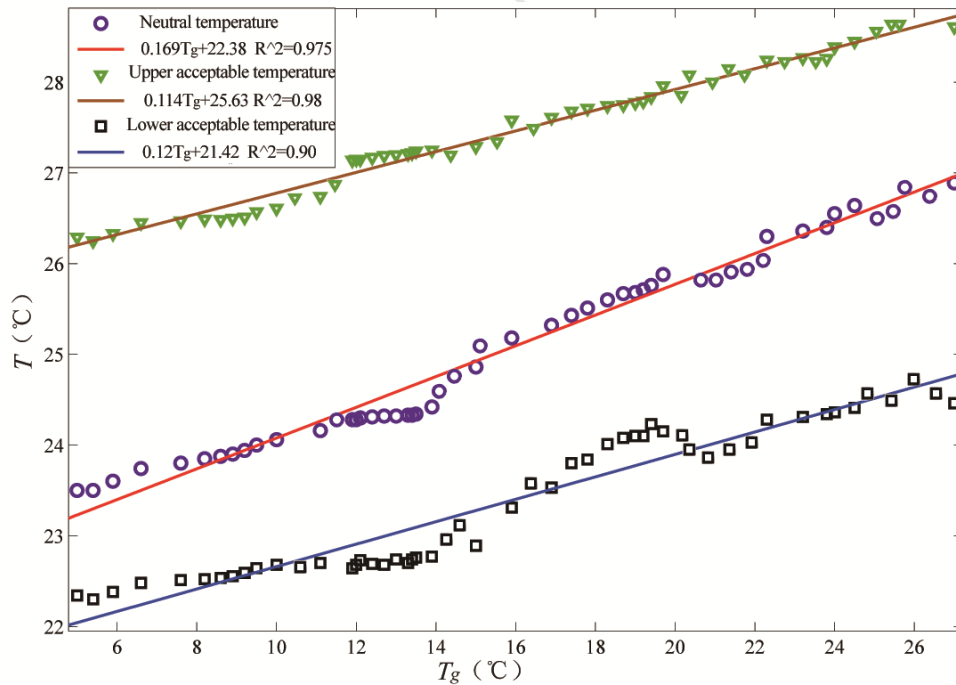
c. PMV and AMTS changes with  $T_{in}$  in Guangzhou

**Fig.7** PMV and AMTS changes with  $T_{in}$  in typical cities

### 3.3 Thermal neutral temperature and acceptable temperature range

Based on the thermal sensation questionnaires, the regression relationship between AMTS votes and  $T_{in}$  were given by logarithmic function in different cities. For example, in Harbin:  $AMTS=1.86\ln(T_{in}-14.4)-3.89$ . The internal air temperature  $T_{in}$  corresponding to  $AMTS=0$  in different cities with different  $T_g$  can be used to represent the neutral temperature  $T_{neu}$  in the underground construction. Therefore, the  $T_{neu}$  for different cities with different ground temperature  $T_g$  could be obtained. The annual mean ground temperature ( $T_g$ ) are the main regional factors influence the thermal load in different cities in underground construction. Considering the  $T_g$  as a typical representative and stable in the underground construction, the temperature frequency method and weighted linear regression are used to obtain the fitting relationships between the  $T_{neu}$  and  $T_g$  shown as **Eq.7**. This could be taken as the new thermal comfort model for underground construction in China. **Fig.8** gives the  $T_{neu}$  varying with the  $T_g$ .

$$T_{neu} = 0.169T_g + 22.38 \quad R^2 = 0.975 \quad (7)$$



**Fig.8** Neutral temperature model and acceptable temperature ranges for underground construction

It could be found that thermal neutral temperature models reflect linear relationship between the  $T_{neu}$  and  $T_g$  with respect to different regions. The neutral temperature is higher in the area with higher  $T_g$  and lower in the regions with lower  $T_g$ .



For example, in the city of Changchun with  $T_g = 6.6$  °C, the neutral temperature for underground construction is 23.7°C. In the city of Beijing with  $T_g = 13.9$  °C, the neutral temperature is 24.3°C. The thermal neutral temperature models take into account the thermal environment characteristic difference and occupants' adaptability of different regions. It would be more suitable for underground construction and can be referred by designers for energy conservation designing. De Dear and Brager [52] indicated a range of  $\pm 3.5$  °C about the neutral temperature as the acceptable thermal comfort ranges. The temperatures corresponding to the votes between  $\pm 0.5$  on the 7-point scales are taken as the acceptable limits of temperature. Thermal comfort theory based on the PMV model [7] find that a comfort zone of 2-3 °C on either side of the neutral temperature is taken as acceptable. According to the ISO 7730 [53], the predicted mean vote between the limits of +0.85 and -0.85 corresponds to the point where 80% of the occupants feel satisfied. But in this paper the results from the questionnaires in underground construction did not conform to these conclusions. Thermal acceptability for this paper in underground construction is obtained directly from the occupants who answered 'acceptable' to the questionnaire, when asked whether their thermal conditions were acceptable or not. The percentage of actual acceptable votes for each half-degree operative temperature bin is recorded and analyzed. If the people acceptance ratio is 90% for the warmer side of thermal sensation, then the corresponding temperature is obtained as the upper limit of the acceptable temperature  $T_{com\_upper}$ . If the people acceptance ratio is 90% for cooler side of thermal sensation, the corresponding temperature is obtained as the lower limit of the acceptable temperature  $T_{com\_lower}$ . Based on the investigations, the  $T_{com\_upper}$  and  $T_{com\_lower}$  are estimated for different cities with different  $T_g$ . Then, the temperature frequency method and weighted linear regression are also used to obtain the fitting relationships between thermal acceptable upper, lower limits of temperatures and  $T_g$ :

$$T_{com\_upper} = 0.114T_g + 25.63 \quad R^2 = 0.98 \quad (8)$$

$$T_{com\_lower} = 0.12T_g + 21.42 \quad R^2 = 0.90 \quad (9)$$

**Fig.8** also gives the upper and lower limit of thermal acceptable temperature model varying with  $T_g$ . **Fig.9** give the AMTS values varying with  $T_g$  corresponding to acceptable upper and lower limits of temperatures.



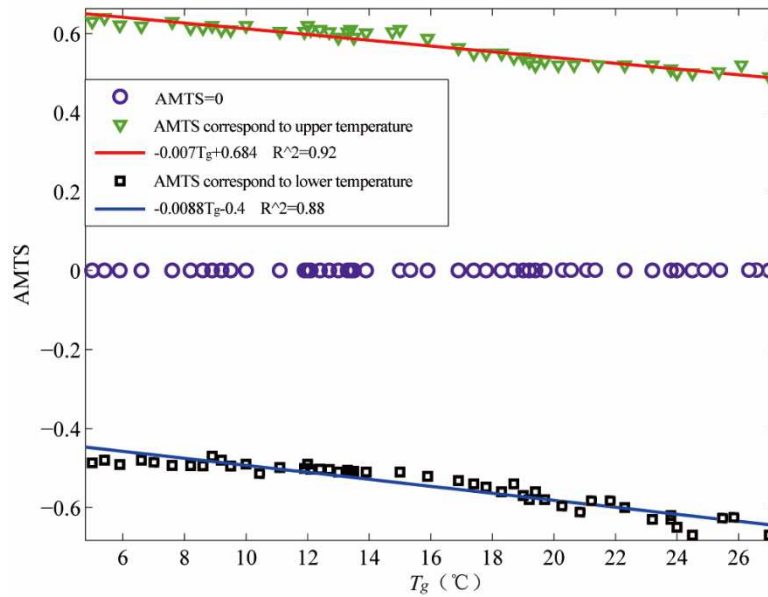


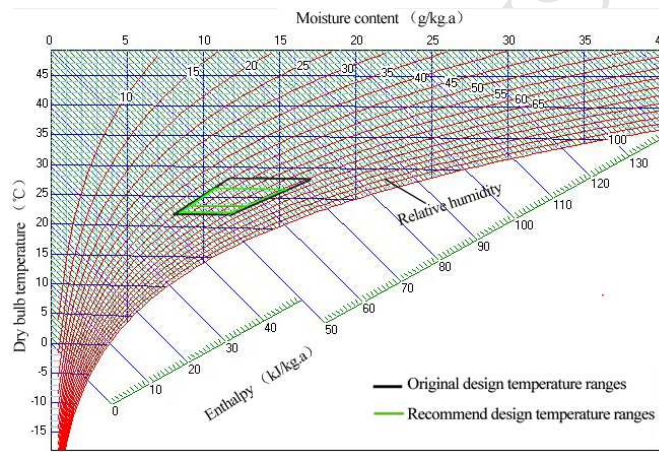
Fig.9. Neutral temperature model and acceptable temperature ranges for underground construction

It can be seen from Fig.8 and Fig.9 that the thermal acceptable temperature range is unsymmetrically distributed with respect to the thermal neutral temperature, and the AMTS corresponding to acceptable upper and lower limits of temperatures are not the same absolute value on either side of neutral temperature. When the  $T_g=5.4\text{ }^{\circ}\text{C}$ , the upper limit of the acceptable temperature is  $26.8\text{ }^{\circ}\text{C}$  and the corresponding the AMTS is  $+0.62$ . The neutral temperature is  $23.5\text{ }^{\circ}\text{C}$  corresponding with  $\text{AMTS}=0$ . The lower limit of the acceptable temperature is  $22.3\text{ }^{\circ}\text{C}$  corresponding the AMTS of  $-0.49$ . The acceptable temperature range in warmer side is about  $3.5\text{ }^{\circ}\text{C}$ , but the acceptable temperature range in the cooler side is only  $1.2\text{ }^{\circ}\text{C}$ . It also could be found that the acceptable temperature ranges vary with the  $T_g$ . **Table.4** gives the upper and lower limit of acceptable temperature in typical cities with different  $T_g$ . It shows that the acceptable temperature ranges in the warmer side is larger in the areas with lower  $T_g$ . For example, the acceptable temperature range in the warmer side of Harbin ( $T_g=5.4\text{ }^{\circ}\text{C}$ ) is  $3.5\text{ }^{\circ}\text{C}$ , but the acceptable temperature range in the warmer side of Hangzhou ( $T_g=13.9\text{ }^{\circ}\text{C}$ ) is only  $2.1\text{ }^{\circ}\text{C}$ . which is  $1.4\text{ }^{\circ}\text{C}$  lower than that of Harbin with the  $T_g$  of  $5.4\text{ }^{\circ}\text{C}$ . However, with the  $T_g$  increasing, the acceptable temperature range in the cooler side becomes larger. The acceptable temperature range in the cooler side of Guangzhou ( $T_g=23.8\text{ }^{\circ}\text{C}$ ) is only  $2.0\text{ }^{\circ}\text{C}$ , but the acceptable temperature range in the cooler side of Haikou ( $T_g=24.6\text{ }^{\circ}\text{C}$ ) extends to  $2.5\text{ }^{\circ}\text{C}$ .

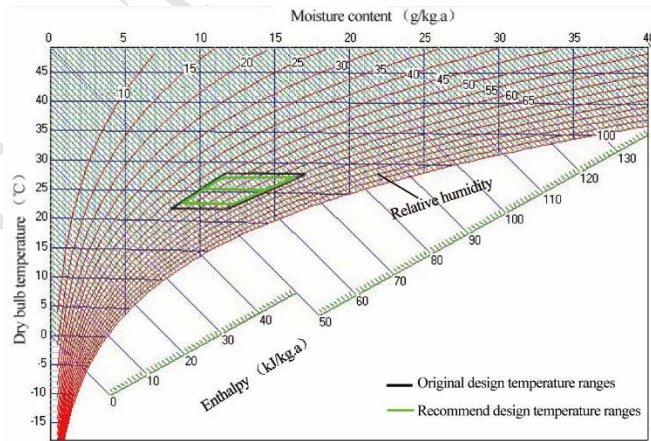
**Table.4** The upper and lower limit of acceptable temperature in typical cities

| Cities    | $T_g$ | $T_{com\_upper}$ | $T_{neu}$ | $T_{com\_lower}$ | $\Delta T_{upper}$ | $\Delta T_{lower}$ | AMTS <sub>upper</sub> | AMTS <sub>lower</sub> |
|-----------|-------|------------------|-----------|------------------|--------------------|--------------------|-----------------------|-----------------------|
| Harbin    | 5.4   | 26.25            | 23.5      | 22.3             | 2.75               | 1.2                | 0.64                  | -0.48                 |
| Hohhot    | 7.6   | 26.47            | 23.8      | 22.51            | 2.67               | 1.29               | 0.63                  | -0.49                 |
| Datong    | 9.2   | 26.51            | 23.94     | 22.59            | 2.57               | 1.35               | 0.61                  | -0.48                 |
| Shenyang  | 10    | 26.61            | 24.06     | 22.68            | 2.55               | 1.38               | 0.62                  | -0.49                 |
| Karamay   | 12.4  | 26.84            | 24.31     | 22.69            | 2.53               | 1.62               | 0.61                  | -0.50                 |
| Beijing   | 13.9  | 26.9             | 24.34     | 22.77            | 2.56               | 1.57               | 0.60                  | -0.51                 |
| Nanjing   | 17.4  | 27.65            | 25.43     | 23.8             | 2.22               | 1.63               | 0.55                  | -0.54                 |
| Hangzhou  | 18.3  | 27.7             | 25.6      | 24.01            | 2.1                | 1.59               | 0.55                  | -0.56                 |
| Wuhan     | 19.2  | 27.8             | 25.71     | 24.1             | 2.09               | 1.61               | 0.53                  | -0.58                 |
| Guangzhou | 23.8  | 28.26            | 26.4      | 24.34            | 1.86               | 2.06               | 0.51                  | -0.63                 |
| Haikou    | 27    | 28.85            | 27        | 24.5             | 1.85               | 2.54               | 0.5                   | -0.63                 |

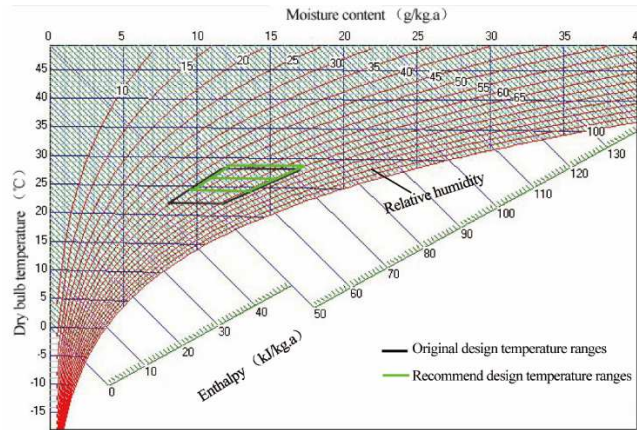
### 3.4 Applied analysis of thermal comfort model



a. the recommend thermal temperature range for Harbin



b. the recommend thermal temperature range for Nanjing



c. the recommend thermal temperature range for Guangzhou

Fig.10 the recommend thermal temperature range in psychrometric chart for different cities

Based on the psychrometric chart, **Fig.10** shows the recommend design temperature ranges for different cities through the thermal questionnaires and the original temperature ranges from the standard GB 50038-2005 [48]. The new thermal comfort model would be instrumental for researchers to formulate thermal standards and give the energy conservation design for underground construction in different areas.

In **Fig.10a**, the recommend design temperature is compared with the original temperature for the city of Harbin in psychrometric chart. It could be found that the recommend temperature is lower than the original temperature. The ground temperature in the Harbin is 5.4 °C and the lower recommend temperature could reduce lots of heating load for the underground construction in Harbin and save a larger number of energy consumption form equipment. This also could be found in the city of Guangzhou in **Fig.10c**, the higher recommend temperature ranges would reduce lots of cooling load and lots of passive energy conservation measures could be used.

#### 4 Conclusions

The purpose of this research is to establish the reasonable thermal comfort model for underground construction, especially air-defence basement in China. Thermal comfort surveys including field measurements and questionnaires have been carried out in different underground constructions in 95 nationwide typical cities. The conclusions drawn from this study are as follows:

- (1) In the underground construction, the occupant's actual cool feeling obtained from questionnaires is larger and the values of AMTS in cooler side of the thermal sensation are smaller in the areas with higher  $T_g$ . The values of PMV is obtained as -1.45 while the AMTS is -2 in an underground construction in the Nanjing, when the  $T_{in}$  is 20 °C, but the value of AMTS is found as -1.0 in the Harbin with  $T_g=5.4$  °C with the  $T_{in}$  of 20 °C.
- The occupants may sense the warmth as being less severe than the PMV predicts. For example, in Harbin, when the  $T_{in}$  is 27 °C, the value of PMV is 0.3 larger than the value of AMTS. People have lower thermal sensation of warmth in the regions with higher  $T_g$ . For example, for an underground construction in Nanjing ( $T_g=17.4$  °C), when the  $T_{in}$  is 28°C, the occupant's AMTS is about 1.0 while the occupant's AMTS is only about 0.5 in the Guangzhou ( $T_g=23.8$  °C) with the same  $T_{in}$  of 28°C.
- (2) The fitting relationships between the neutral temperature and  $T_g$  are obtained as:  $T_{neu}=0.169T_g+22.38$ . The thermal acceptable upper and lower limits of temperatures vary with the  $T_g$  for underground construction also developed as:  $T_{com\_upper}=0.114T_g+25.63$  and  $T_{com\_lower}=0.12T_g+21.42$ , respectively. It shows that the thermal acceptable temperature ranges are unsymmetrically distributed with respect to the thermal neutral temperature and change with the  $T_g$ . The acceptable temperature range in the warmer side of Hohhot ( $T_g=7.6$  °C), Hangzhou ( $T_g=13.9$  °C) and Guangzhou ( $T_g=23.8$  °C) are 2.5 °C, 2.1 °C and 1.86 °C, respectively.
- (3) Based on psychrometric chart, the recommended temperature ranges for different cities through thermal questionnaires are compared with the original temperature ranges. It shows that the recommend temperature ranges varying with the ground temperature could save lots of energy consumption.

|   |  |
|---|--|
| <b>Nomenclature</b>   | $T_{neu}$ thermal neutral temperature (°C)   |
| $T_g$ annual mean ground temperature (°C)                       | $AMTS_{upper}$ actual mean thermal sensation corresponding the upper limit of acceptable temperature |
| $T_{in}$ air temperature in underground construction (°C)       | $AMTS_{lower}$ actual mean thermal sensation corresponding the lower limit of acceptable temperature |
| $T_{op}$ operative temperature (°C)                             |  |
| $T_R$ average radiation temperature (°C)                        |  |
| $\Delta T$ Temperature difference between $T_R$ and $T_a$ (°C)  | <b>Acronyms</b>  |
| $T_{com\_lower}$ the lower limit of acceptable temperature (°C) | $AMTS$ actual mean thermal sensation   |
| $T_{com\_upper}$ the upper limit of acceptable temperature (°C) |  |

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# **Appendix. A:** Sample questionnaire

Thank you for your support for thermal environment survey in underground construction

|  |                            |                            |                          |                          |                          |                          |
|--|----------------------------|----------------------------|--------------------------|--------------------------|--------------------------|--------------------------|
| <b>subject detail</b>  |                            |                            |                          |                          |                          |                          |
| Name   | city name                  | Climatic zone              | Time                     | occupation               |                          |                          |
| Age  | Sex                        |                            | Height                   | Weight                   |                          |                          |
|  | M <input type="checkbox"/> | F <input type="checkbox"/> |                          |                          |                          |                          |
| <b>Cloths worn by occupants</b>  |                            |                            |                          |                          |                          |                          |
| Casualy  | At the time of voting      |                            | At social functions      |                          |                          |                          |
| <input type="checkbox"/>   | <input type="checkbox"/>   |                            | <input type="checkbox"/> |                          |                          |                          |
| <b>Thermal environment</b>   |                            |                            |                          |                          |                          |                          |
| Temperature  | Relative humidity          | Air velocity               | Underground details      |                          |                          |                          |
|  |                            |                            |                          |                          |                          |                          |
| <b>Thermal sensation</b>   |                            |                            |                          |                          |                          |                          |
| Cold   | Cool                       | Slightly Cool              | Neutral                  | Slightly Warm            | Warm                     | Hot                      |
| <input type="checkbox"/>   | <input type="checkbox"/>   | <input type="checkbox"/>   | <input type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/> |
| <b>How would you consider the room temperature?</b>                            |                            |                            |                          |                          |                          |                          |
| Acceptable   |                            |                            | Not acceptable           |                          |                          |                          |
| <input type="checkbox"/>   |                            |                            | <input type="checkbox"/> |                          |                          |                          |
| <b>How would you like to feel?</b>   |                            |                            |                          |                          |                          |                          |
| Much too cool  | Too cool                   | Comfortable Cool           | Comfortable              | Comfortable Warm         | Too Warm                 | Much too Warm            |
| <input type="checkbox"/>   | <input type="checkbox"/>   | <input type="checkbox"/>   | <input type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/> |
| <b>Level of Air movement should be:</b>  |                            |                            |                          |                          |                          |                          |
| Lesser   |                            | As it is                   |                          | More                     |                          |                          |
| <input type="checkbox"/>   |                            | <input type="checkbox"/>   |                          | <input type="checkbox"/> |                          |                          |
| <b>Level of Humidity should be:</b>  |                            |                            |                          |                          |                          |                          |
| Lesser   |                            | As it is                   |                          | More                     |                          |                          |
| <input type="checkbox"/>   |                            | <input type="checkbox"/>   |                          |                          |                          |                          |
| <b>other visions on thermal environment survey in underground construction</b> |                            |                            |                          |                          |                          |                          |

317 **Reference**

- [1] Andolsuna Simge, Culpa Charles H, Haberla Jeff, Witte Michael J. Energy plus vs. DOE-2.1e: the effect of ground-coupling on energy use of a code house with basement in a hot-humid climate. *Energy Build* July 2011;43(7): 1663-75.
- [2] Balaras CA, Drousa K, Dascalaki E, Kontoyiannidis S. Heating energy consumption and resulting environmental impact of European apartment buildings. *Energy Build* 2005; 37:429-42.
- [3] Casals Miquel, Gangoellsa Marta, Forcadaa Núria, et.al. A breakdown of energy consumption in an underground station. *Energy Build* 2014;78:89-97.
- [4] van Dronkelaar C, C\_ostola D, Mangkuto R, Hensen JLM. Heating and cooling energy demand in underground buildings: potential for saving compared to above ground buildings for various climates and building functions. *Energy Build* 2013:251-65.
- [5] Yuan Y, Cheng B, Mao J, et al. Effect of the thermal conductivity of building materials on the steady-state thermal behaviour of underground building envelopes. *Build. Environ.* 2006 41(3):330-335.
- [6] Barbaresi Alberto, Torreggiani Daniele, Benni Stefano, Tassinari Patrizia. Underground cellar thermal simulation: definition of a method for modeling performance assessment based on experimental calibration. *Energy Build* 2014;76:363-72.
- [7] P.O. Fanger. Thermal comfort-analysis and applications in environmental engineering. In: Fanger PO, editor. C.D.T. Press; 1970.
- [8] ANSI/ASHRAE Standard 55-2004, Thermal Environmental Conditions for Human Occupancy, American Society of Heating, Refrigeration and Air conditioning Engineers, Inc., 2004.
- [9] J.F. Nicol, M.A. Humphreys, Adaptive thermal comfort and sustainable thermal standards for buildings, *Energy Build.* *Energy* 34 (6) (2002) 563-572.
- [10] R.J. de Dear, G. Brager, Developing an adaptive model of thermal comfort and preference, *ASHRAE Trans.* 104 (1998) 145–167.
- [11] ISO 7730 Ergonomics of the thermal environment—analytical determination and interpretation of thermal comfort using calculation of the PMV and PPD indices and local thermal comfort criteria; 2005.
- [12] ASHRAE. Thermal environmental conditions for human occupancy. In: ANSI/ASHRAE standard 55-2013, American Society of heating, refrigerating and air-conditioning engineers, Atlanta, GA; 2013.
- [13] Katafygiotou, M. C., & Serghides, D. K.. Thermal comfort of a typical secondary school building in Cyprus. *Sustainable Cities and Society*, 2014 13:303–312.
- [14] Villadiego, K., & Velay-Dabat, M. A. Outdoor thermal comfort in a hot and humid climate of Colombia: A field study in Barranquilla. *Build. Environ.* 2014 75:142–152.
- [15] J.T. Kim, J.H. Lim, S.H. Cho, G.Y. Yun, Development of the adaptive PMV model for improving prediction performances, *Energy Build.* 2015 98:100–105.
- [16] C. Buratti, P. Ricciardi, Adaptive analysis of thermal comfort in university classrooms: correlation between

experimental data and mathematical models, *Build. Environ.* 2009 44:674–687.

[17] P.O. Fanger, J. Toftum, Extension of the PMV model to non-air-conditioned buildings in warm climates, *Energy Build.* 2002 34:533–536.

[18] L. Schellen, M.G.L.C. Loomans, B.R.M. Kingma, M.H. de Wit, a.J.H. Frijns. The use of a thermophysiological model in the built environment to predict thermal sensation, *Build. Environ.* 2013 59:10-22.

[19] J. Langevin, J. Wen, P.L. Gurian, Modeling thermal comfort holistically: Bayesian estimation of thermal sensation, acceptability, and preference distributions for office building occupants, *Build. Environ.* 2013 69:206–226.

[20] Yao R, Li B, Liu J. A theoretical adaptive model of thermal comfort—Adaptive Predicted Mean Vote (aPMV). *Build. Environ.* 2009 44(10): 2089-96.

[21] RAA-C.E, ANSI/ASHRAE Standard 55—Thermal Environmental Conditions for Human Occupancy, American Society of Heating, 2004.

[22] European Standard, EN 15251, Indoor Environmental Input Parameters for Design and Assessment of Energy Performance of Buildings—Addressing Indoor Air Quality, Thermal Environment, Lighting and Acoustics, 2007.

[23] Humphreys M, Rijal H, Nicol J. Updating the adaptive relation between climate and comfort indoors; new insights and an extended database. *Build. Environ* 2013 63:40-55.

[24] P. Ricciardi, C. Buratti, Thermal comfort in open plan offices in northern Italy: an adaptive approach, *Build. Environ.* 2012 56:314–320.

[25] Francesca Romana d'Ambrosio Alfano, Thermal comfort: design and assessment for energy saving, *Energy Build.* 2014 81:326-336.

[26] R. Van Gaeve, V.A. Jacobs, Thermal comfort of the surgical staff in the operating room, *Build. Environ.* 2014 81:7-41.

[27] G. Desogus, S. Di Benedetto, The use of adaptive thermal comfort models to evaluate the summer performance of a Mediterranean earth building, *Energy Build.* 2015 104:350-359.

[28] Asit Kumar Mishra, Maddali Ramgopal, A thermal comfort field study of naturally ventilated classrooms in Kharagpur, India, *Build. Environ.* 2015 92:396-406.

[29] Siti Aisyah Damiati, Sheikh Ahmad Zaki, Hom Bahadur Rijal, Surjamanto Wonorahardjo. Field study on adaptive thermal comfort in office buildings in Malaysia, Indonesia, Singapore, and Japan during hot and humid season. *Build. Environ.* 2016 109:208-223.

[30] Haoran Ning, Zhaojun Wang, Adaptive thermal comfort in university dormitories in the severe cold area of China, *Build. Environ.* 2016 99:161-169.

[31] Zhaojun Wang, Lin Zhang, Thermal comfort for naturally ventilated residential buildings in Harbin, *Energy Build.* 2010 42:2406-2415.

[32] Ogbonna AC, Harris DJ. Thermal comfort in sub-Saharan Africa: field study report in Jos-Nigeria. *Appl Energy* 2008;85:1–11.



- [33] M. Indraganti, R. Ooka, H.B. Rijal, G.S. Brager, Adaptive model of thermal comfort for offices in hot and humid climates of India, *Build. Environ.* 2014 74:39-53.
- [34] J. Han, W. Yang, J. Zhou, G. Zhang, Q. Zhang, D.J. Moschandreas, A comparative analysis of urban and rural residential thermal comfort under natural ventilation environment, *Energy Build.* 2009 41:139-145.
- [35] Veronica Soebarto, Helen Bennetts, Thermal comfort and occupant responses during summer in a low to middle income housing development in South Australia, *Build. Environ.* 2014 75:19-29.
- [36] L. DiasPereira, D. Raimondo, Assessment of indoor air quality and thermal comfort in Portuguese secondary classrooms: methodology and results, *Build. Environ.* 2014 81:69-80.
- [37] Despoina Teli, Mark F. Jentsch, The role of a building's thermal properties on pupils' thermal comfort in junior school classrooms as determined in field studies, *Build. Environ.* 2014 82:640-654.
- [38] Bin Cao, Maohui Luo, Min Li, Yingxin Zhu, Too cold or too warm? A winter thermal comfort study in different climate zones in China. *Energy and Buildings* 133 (2016) 469–477
- [39] Agus P. Sasmito, Jundika C. Kurnia, Erik Birgersson, Arun S. Mujumdar. Computational evaluation of thermal management strategies in an underground mine. *Applied Thermal Engineering* 90 (2015) 1144-1150.
- [40] Maidment G, Missenden J, Ampofo F. Underground railway environment in the UK Part 1: Review of thermal comfort[J]. *Applied Thermal Engineering*, 2004, 24(5):611-631.
- [41] Mohamed Marzouk, Ahmed Abdelaty. Monitoring thermal comfort in subways using building information modeling. *Energy and Buildings* 84 (2014) 252–257.
- [42] Hu Songtao, Jiang Yameng, WangGang et.al. Investigation on indoor thermal environment of underground railway trains. *HV&AC*, 2015,45(7):23-27. (in chinese).
- [43] Gang Liu, Chao Cen, Qi Zhang, Kuixing Liu, Rui Dang. Field study on thermal comfort of passenger at high-speed railway station in transition season. *Build. Environ.* 2016 108:220-229.
- [44] Manoj Kumar Singh, Sadhan Mahapatra, Jacques Teller. Development of thermal comfort models for various climatic zones of North-East India. *Sustainable Cities and Society* 14 (2015) 133–145
- [45] Toe DHC, Kubota T. Development of an adaptive thermal comfort equation for naturally ventilated buildings in hot-humid climates using ASHRAE RP-884 database. *Front Archit Res* 2013;2:278-91.
- [46] Manoj Kumar Singh, Sadhan Mahapatra, Jacques Teller. Development of thermal comfort models for various climatic zones of North-East India. *Sustainable Cities and Society* 14 (2015) 133–145
- [47] B. Li, R. Yao, Q. Wang, Y. Pan, An introduction to the Chinese Evaluation Standard for the indoor thermal environment, *Energy Build.* 2014 82:27–36.
- [48] Code for design of civil air defence basement, GB 50038-2005, Ministry of Housing and Urban-Rural Development of the People's Republic of China, Beijing, China, 2005 (in Chinese).
- [49] ASHRAE. ASHRAE 55-1992, Thermal Environmental Conditions for Human Occupancy, Atlanta American Society of Heating, Refrigerating and Air-Conditioning Engineers, 1992.
- [50] UNI EN ISO 7730. Ergonomics of the thermal environment—analytical determination and interpretation of thermal comfort using calculation of the PMV and PPD indices and local thermal comfort criteria; 2006.
- [51] Thermal Environmental Conditions for Human Occupancy, ASHRAE Standard 55-2013, American Society of Heating, Refrigerating and Air-Conditioning Engineers, Atlanta, Georgia, 2013.
- [52] de Dear RJ, Brager GS. Thermal comfort in naturally ventilated buildings: revisions to ASHRAE Standard 55.



Energy Build. 2002 34(6):549-61.

[53] ISO. International standard 7730: moderate thermal environments e determination of the PMV and PPD indices and the specification of the conditions for thermal comfort. International Standards Organization; 1994.

**Highlights**

- ▶ Comparative thermal comfort surveys have been carried out in underground constructions.
- ▶ The mean thermal sensation (AMTS) is compared with PMV in different cities
- ▶ Neutral temperature models and the acceptable limit temperature model are established.
- ▶ The recommend temperature ranges could save energy consumption in different areas.