# Development of a Mobile Design Template for Substation Earthing System

Siow Chun Lim Faculty of Engineering Multimedia University Cyberjaya, Malaysia clsiow@mmu.edu.my

Mohamed Najib Harami Faculty of Engineering Multimedia University Cyberjaya, Malaysia mohammed.h 92@hotmail.com

Abstract—Electrical engineers often find the process of designing the earthing system of substations to be tedious, arduous and time consuming. Mobile apps development and usage has been on the rise of late due to the high availability of smart phones and Internet of Things. In terms of electrical earthing system design, there are very few applications available which are neither helpful nor informative. Hence, this paper outlines the development of a mobile application which is able to assist and ease electrical engineers' design process. Functionality and validity of the app has been verified by comparing calculations obtained manually and by the app. Hence, this app can be used for the design and verification of an earthing system.

Keywords—earthing system; substation; Javascript; mobile apps

## I. Introduction

Earthing system is an electrical network that is connected to the earth to provide safe return path for fault current as well as to operationalise the protective devices to protect the safety of equipment and human [1]. Substation is an essential part of the power system to ensure power delivery to the consumers. Hence, substation earthing system is crucial to ensure not only reliable power distribution but also the safety of workers and equipment. The IEEE 80 standard has been one of the most comprehensive advocate of the design of a sound earthing system for substations [2]. However, practicing electrical engineer involved in the design of a substation earthing system often find the design process to be arduous and tedious. Once designed, several rounds of verification usually take place to ensure the calculation is done without error.

There are several commercial software such as CDEGS, ETAP and AutoGrid Pro which offer help for engineers to design the substations earthing system. Unfortunately, the aforementioned software tends to require significant subscription charges which could be burdensome to small or even medium-scale consulting firms. In addition, such software usually requires additional training to meaningfully apply them to design a substation earthing system. As the result, many practicing engineers still prefer to fall back on the manual design methodology as per IEEE 80 standard.

The field of mobile application development has been growing on an exponential scale in the past decade. More than 5 million mobile applications have been developed and made available today. Despite the staggering figure, the number of mobile applications developed for engineering application remains to be relatively insignificant compared to healthcare, learning, gaming and lifestyle domain. It cannot be denied that mobile apps can be an extremely convenient tool due to the high portability of smartphones.

A quick survey in the major apps store reveals limited number of apps developed to assist the design of electrical earthing systems. Table I summarises few of the aforementioned apps:

TABLE I. COMPARISON OF AVAILABLE APPS

Application name	Electrical earthing	Electrical engineering practical	Electrical calculation
Description	Describe earthing product installation in general	Explains how electrical system works in general without any calculation.	The free version of the app calculates some basic value on electrical system such as voltage drop, current, active power, reactive power, etc. whereas the calculations of earthing system requires an amount of money to active the app.

With this motivation in mind, this paper shall outline the processes involved in developing a mobile app which has the capability to verify the design of a substation earthing system. It is desirable for the apps to have these characteristics:

- Perform calculation of all the needed values in a simple manner
- Simple User-Interface.
- Embedded user guide which briefly explains each parameter in a clear manner to the user
- Indicates whether the current earthing system design is safe or not after the calculation is complete.

Fig.1 depicts the fundamental working principle of a desirable app for the aforementioned purpose.

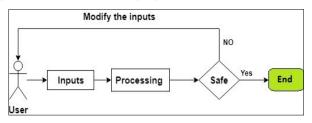


Fig. 1. Working flow of the desirable app

# II. METHODOLOGY

Fig. 2 illustrates the overall design philosophy of a substation earthing system according to IEEE 80 [2]. The desirable app shall be able to perform the logic and calculations according to the flow in Fig. 2 before eventually providing a conclusion on whether the current design meets the safety criteria or otherwise.

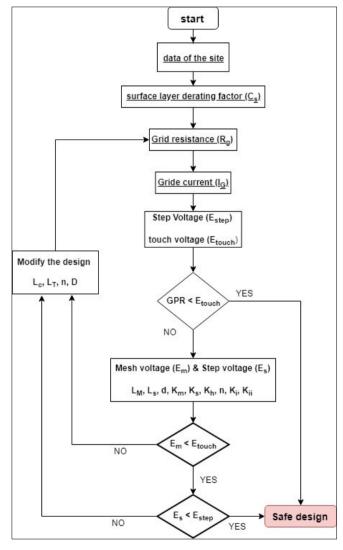


Fig. 2. Substation earthiig system design flow [2]

Before starting to design an earthing grid, it is paramount to ensure that the soil resistivity data is obtained via measurement method as recommended in IEEE 81 [3]. Due consideration has to be given to possible environmental factor which may affect the soil resistivity value [4].

A thin layer of high resistivity material such as gravel, is usually placed above the ground grid to increase the contact resistance between the ground and the human feet in the substation area. The thickness of the surface layer should be between 0.08m and 0.15m to help to protect person against dangerous step and touch voltages [2]. The surface layer derating factor is calculated by:

$$C_s = 1 - \frac{0.09 \left(1 - \frac{\rho}{\rho_s}\right)}{2 h_s + 0.09}$$
 (1)

where

 $C_s$  Surface layer derating factor.

 $\rho$  Soil Resistivity ( $\Omega$ .m)

 $\rho_s$  Resistivity of surface layer material ( $\Omega$ .m).

 $h_s$  Thickness of surface layer (m).

Minimizing the ground potential grid (GPR) can be done by the design of a good earthing grid with low resistance [1]. Grid resistance goes side by side with the earthing grid design and it can be calculated by [2]:

$$R_g = \rho \left[ \frac{1}{L_T} + \frac{1}{\sqrt{20 A}} \left( 1 + \frac{1}{1 + h \sqrt{20 / A}} \right) \right]$$
 (2)

where

 $R_g$  grid resistance  $(\Omega)$ 

 $L_T$  total buried length of conductors (m)

A area of grid  $(m^2)$ 

h depth of grid (m).

 $\rho$  Soil Resistivity ( $\Omega$ m)

The worst scenario where the earth fault current would flow through the earthing grid back to earth is known as maximum grid current and can be calculated by [2]:

$$I_G = I_g \times D_f \tag{3}$$

where

 $I_G$  grid current (A)

 $I_g$  symmetrical earth fault current (A).

 $D_f$  decrement factor.

The decrement factor used in conjugation with the symmetric ground fault current parameter is given by [2]:

$$D_f = \sqrt{1 + \frac{T_A}{t_f} + (1 - e^{\frac{-2t_f}{T_A}})}$$
 (4)

where

D<sub>f</sub> decrement factor

T<sub>A</sub> dc time offset constant

t<sub>f</sub> Fault duration (s)

The dc time offset constant is given by [2]:

$$T_A = \frac{X}{R} \times \frac{1}{2\pi f} \tag{5}$$

where

X/R ratio of fault location

f system frequency (Hz)

The reactance and resistance parameter in the fault location ratio is given by:

$$R = \frac{100 (Tx \ load \ loss - Tx \ no \ load \ loss)}{Tx \ rating \times 1000}$$
 (6)

$$X = \sqrt{Tx_{impedance}^2 + R^2}$$
 (7)

where

 $T_X$  transformer

Next, the safe touch and step voltages for human being weighing 50kg and 70kg can be calculated as follows [2]:

$$E_{touch,50kg} = (1000 + 1.5C_s \rho_s) \frac{0.116}{\sqrt{t_s}}$$
 (8)

$$E_{step,50kg} = (1000 + 6C_s \rho_s) \frac{0.116}{\sqrt{t_s}}$$
 (9)

$$E_{touch,70kg} = (1000 + 1.5C_s \rho_s) \frac{0.157}{\sqrt{t_s}}$$
 (10)

$$E_{step,70kg} = (1000 + 6C_s \rho_s) \frac{0.157}{\sqrt{t_s}}$$
 (11)

where

 $C_s$  surface layer derating factor

t<sub>s</sub> maximum fault clearing time

 $\rho_s$  soil resistivity ( $\Omega$ m)

Then, the ground potential rise, GPR can be calculated by:

$$GPR = I_G \times R_g$$
 (12)

The next step is crucial as it will determine whether the current earthing grid design is safe or otherwise. The design is deemed as safe if GPR does not surpass touch voltage limit. Conversely, the design is deemed as unsafe if GPR value exceeds the touch voltage limit. In such case, further calculation of mesh voltage  $E_m$  and step voltage  $E_s$  is required as follows [2]:

$$E_m = \frac{\rho_s \ K_m \ K_i \ I_G}{L_m} \tag{13}$$

where

 $\rho_s$  soil resistivity ( $\Omega$ m)

 $K_m$  geometric spacing factor

K<sub>i</sub> irregularity factor

 $L_m$  effective buried length of the grid

$$K_m = \frac{1}{2\pi} \left( ln \left[ \frac{D^2}{16h \times d} + \frac{(D+2h)^2}{8D \times d} - \frac{h}{4d} \right] + \frac{K_{ii}}{K_h} ln \left[ \frac{8}{\pi (2n-1)} \right] \right)$$
where

D spacing between parallel grid conductors (m)

h depth of buried grid conductors (m)

d diameter of grid conductor (m)

 $k_h$  weighting factor for burial depth =  $\sqrt{1+h}$ 

 $K_{ii}$  weighting factor for earth electrodes /rods on the corner mesh

 $K_{ii} = 1$  for grid with electrodes along the corner

 $K_{ii} = \frac{1}{\frac{n}{2n^2}}$  for grid with no electrodes on the corners

n geometrical factor

$$n = n_a \times n_b \times n_c \times n_d$$

where

$$n_a = \frac{2L_c}{L_p}$$

-  $n_b = 1$  for square grid otherwise

$$n_b = \sqrt{\frac{L_p}{4\sqrt{A}}}$$

-  $n_c = 1$  for square and rectangular grid, otherwise

$$n_c = \left[\frac{L_x L_y}{A}\right]^{\frac{0.7A}{L_x L_y}}$$

- n<sub>d</sub> = 1 for square, rectangular or L-shape, otherwise

$$n_d = \frac{D_m}{\sqrt{L_x^2 + L_y^2}}$$

where

L<sub>c</sub> total length of horizontal grid conductors (m)

L<sub>p</sub> grid perimeter (m)

A total area of grid (m<sup>2</sup>)

 $L_x$  and  $L_y$  maximum length of grid in x and y directions (m)

 $D_{m}$  maximum distance between any two points on the grid (m)

$$K_i = 0.644 + 0.148 n$$

For grid without earthing electrodes:

$$L_M = L_c + L_R$$

For grid with earthing electrodes on the corners:

$$L_M = L_c + \left[ 1.5 + 1.22 \left( \frac{L_r}{\sqrt{L_x^2 + L_y^2}} \right) \right] L_R$$

where

 $L_c$  total length of horizontal grid conductors (m)

 $L_R$  total length of earthing electrodes (m)

 $L_r$  length of each earthing electrodes (m)

 $L_x$  and  $L_y$  maximum length of the grid in x and y directions (m)

The step voltage can be calculated as follows [2]:

$$E_S = \frac{\rho_S \ K_S \ K_i \ I_G}{L_S} \tag{14}$$

where

 $\rho_s$  soil resistivity ( $\Omega$ m)

 $I_G$  maximum grid current (A)

 $K_s$  geometrical spacing factor

K<sub>i</sub> irregularity factor

 $L_s$  effective buried length of the grid

$$K_s = \frac{1}{\pi} \left[ \frac{1}{2h} + \frac{1}{D+h} + \frac{1}{D} (1 - 0.5^{n-2}) \right]$$

where

D spacing between parallel grid conductors (m)

h depth of buried grid conductors (m)

n geometrical factor

$$L_s = 0.75L_c + 0.85L_R$$

where

 $L_c$  total length of horizontal grid conductors (m)

 $L_R$  total length of earthing electrodes (m)

After mesh and step voltages have been found, their values will be compared with maximum allowable mesh and step voltages. If  $(E_m > E_{touch})$  and  $(E_s > E_{step})$  then the current design of earthing grid system needs to be modified possibly by increasing the grd area, reducing the grid spacing, burying additional ground conductor grid outside the vicinity or by increasing the thickness of surface materials. Otherwise, the current design is deemed as safe.

## III. APPLICATION DEVELOPMENT

The application has been developed by using the SCRUM model of app development. SCRUM model is an iterative process, whereby the development of the application is split into multiple stages. Agile SCRUM process helps the companies and developers in enhancing the quality of the products by being more adaptive to changes, requiring less time to create best estimates, thus allowing developers to more control over the project scheduling [5]. Fig. 3 shows how the flow of how an app is typically being developed.

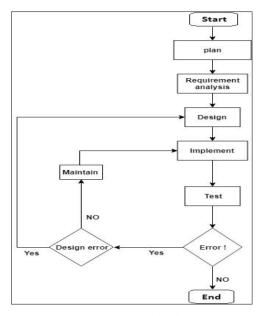


Fig. 3. Flow of application development

Planning requires identification of the objective of the mobile application, target users as well as the features of the app. Requirement analysis is to determine the users' expectations for the mobile application. These requirements have been detailed out in Section II of this paper. At the design stage, care has to be given to ensure that the design of each screen of the application is as detailed as possible to ease users' experience. Inclusion of short description for each input, placement of each screen button, navigation between screens and display of result have to be considered.

## IV. RESULTS AND DISCUSSIONS

Fig. 4 shows the home screen of the application. The current version of the application includes a user guide that briefly explains every parameter used in the calculation.



Fig. 4. Home screen of the app

Fig. 5 shows the first screen of the application. User has to input several parameters such as soil resistivity, grid dimensions and has to select the type of surface layer.

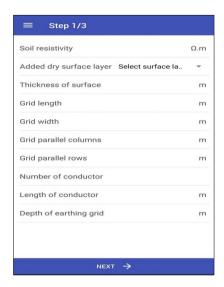


Fig. 5. First screen of the app

Fig. 6 illustrates the second screen of the app where the design engineer has to specify parameter such as system frequency, maximum fault duration and transformer rating.

Transformer load loss	W
Transformer no load loss	W
Transformer rating	kVA
Transformer impedance	%
System frequency	Hz
Max fault duration	s
Symmetrical grid current	Α
Body wieght Select body wieght:	*

Fig. 6. Second screen of the app

The third screen as shown in Fig. 7 requires the user to select the shape of the grid which is currently limited to either square or rectangular. If the safety criteria is not satisfied, a warning message will be displayed at the bottom of the screen.

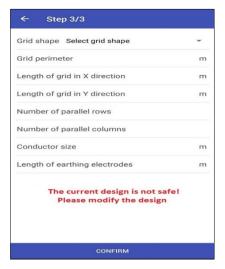


Fig. 7. Final screen of the app

Table II shows the comparison between manual calculation and apps calculation to verify the functionality of the apps.

TABLE II. VERIFICATION OF APPS

TABLE II. VERIFICATION OF AFFS					
Input values	Manual calculations	App calculations			
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$Pa = 400 \ \Omega.m$ $Ps = 5500 \ \Omega-m$ $Cs = 0.71614$ $Rg = 2.77569 \ \Omega$	$Pa = 400 \ \Omega.m$ $Ps = 5500 \ \Omega-m$ Cs = 0.716 $Rg = 2.776 \ \Omega$			
Tx load loss = 12300W Tx no load loss = 2800 W Tx rating = 1600 kVA Tx impedance = 6 Frequency = 50 Hz Fault duration = 0.5 sec Fault current = 3180 A Body weight = 70 kg	$\begin{array}{c} R = 0.59375~\Omega \\ X = 5.97055~\Omega \\ X/R = 10.05566\\ \Omega \\ TA = 0.03201 \\ Df = 1.031512 \\ IG = 3280.207~A \\ GPR = 9104.838 \\ V \\ E_{touch}  \   _{70} = \\ 1533.828~V \\ E_{step~70} = 5469.218 \\ V \\ (GPR > E_{touch}) \\ Continue \\ \end{array}$	$\begin{array}{c} R = 0.594 \ \Omega \\ X = 5.971 \ \Omega \\ X/R = 10.056 \ \Omega \\ TA = 0.0320 \\ Df = 1.0315 \\ IG = 3280.207 \ A \\ GPR = 9104.838 \\ V \\ E_{touch}  _{70} = \\ 1533.830 \ V \\ E_{step}  _{70} = \\ 5469.226 \ V \\ (GPR > E_{touch}) \\ Continue \end{array}$			
$\begin{array}{ccc} Grid & shape & = \\ rectangular & Lp = 280 \text{ m} \\ Length of grid in \\ X=70 \text{ m} & Y=70 \text{ m} \\ \\ n_r = 11 \\ n_c = 11 \\ d = 0.01 \text{ m} \\ Lr = 7.5 \text{ m} \end{array}$	$\begin{array}{c} n = 11 \\ D = 7 \\ K_m = 0.7687 \\ K_i = 2.3070 \\ L_m = 1540 \text{ m} \\ E_m = 1493.899 \text{ V} \\ K_s = 0.4061 \\ L_s = 1155 \text{ m} \\ E_s = 1048.23 \text{ V} \\ \\ E_m < E_{touch\_70} \\ E_s < E_{step\_70} \\ \\ Your \ design \ is \\ safe \end{array}$	$E_{m} = 1493.899 \\ E_{s} = 1048.234 \\ E_{m} < E_{touch\_70} \\ E_{s} < E_{step\_70} \\ Your \ design \ is \\ safe$			

It can be seen that the calculated values and the computed values are closely matched yielding similar conclusion that the current design is deemed as safe. Fig. 8 shows the output summary. Note that the user will only be able to reach the screen as shown in Fig. 8 if the design is safe.

← Result				
Soil Resistivity(R) 400.000 Ω.m				
Added Dry Surface Layer 5500				
Cs Value 0.716				
Earthing Grid Resistence 2.776 $\Omega$				
Max Grid Current 3280.207 A				
E Touch 1533.830 V				
E Step <b>5469.226</b> V				
GPR Value 9104.850 V				
Max Mesh Voltage 1493.899 V				
Max Allowable Step Voltage 1048.234 V				
Your design is safe				

Fig. 8. Final screen of the app

After further testing with several other scenarios, it can be deduced that the app is perfectly working and giving satisfactory results for the following conditions:

```
When (GPR \leq E<sub>touch</sub>) When (GPR \geq E<sub>touch</sub>)
```

```
When (E_m > E_{touch})
When (E_m < E_{touch})
```

## V. CONCLUSION

This paper has outlined the process involved in developing a mobile application capable to verify the safety level of a substation earthing system design. With the availability of this app, the time required for the design of a substation earthing system to be verified can be significantly shortened without the need for tedious manual calculation. This mobile application is expected to be made available at the apps store by the end of this year.

## ACKNOWLEDGMENT

Facilities and support provided by the Faculty of Engineering, Multimedia University is appreciated.

# REFERENCES

- S. C. Lim, C. Gomes, and M. Z. A. A. Kadir, "Electrical earthing in troubled environment", International Journal of Electrical Power & Energy Systems, 2013, 47, pp. 117-128
- [2] "IEEE Guide for Safety and AC Substation Grounding", IEEE Standard 80-2013 (Revision of IEEE Std.80-2000), 2013.
- [3] "IEEE Guide for measureing earth resistivity, ground impedance, and earth surface potentials of a grounding system,' IEEE Standard 81-2012.
- [4] S. C. Lim, G. Nourirad, C. Gomes, and M. Z. A. A. Kadir, "Significance of localized soil resistivity in designing a grounding system," IEEE 8th International Power Engineering and Optimization Conference, 2014.
- [5] "what is agile | what is scrum", by cPrime [online] Available: <a href="https://www.cprime.com/resources/what-is-agile-what-is-scrum/">https://www.cprime.com/resources/what-is-agile-what-is-scrum/</a>. [Accessed: Sep.2018]