# Ocean-Driven Melting near and within Ice Shelf Basal Channels and Crevasses



Sarah Villhauer<sup>1</sup>, Ken Zhao<sup>2</sup>, Peter Washam<sup>3</sup>, and Erin Pettit<sup>2</sup>

<sup>1</sup>University of California, Los Angeles <sup>2</sup>Oregon State University <sup>3</sup>Cornell University



#### Research Overview

- Goal is to investigate how different conditions and forcings within ice shelf cavities impact the near-boundary dynamics and thermodynamics, which drive disparate magnitudes and spatial patterns of melt.
- Use Large Eddy Simulations of circulation within ice shelf cavities to simulate a parameter regime including: (1) channel width, magnitude of (2) far-field temperature, (3) salinity, and (4) velocity, and (5) orientation of far-field velocity.

#### **Motivation**

- Ice shelves in West Antarctica and Northern Greenland have lost a significant amount of mass, thinned, and retreated over the past two decades.
- Gap in understanding: (1) How does 3D circulation within basal channels/crevasses influence melting and evolution of these morphologies? (2) Do basal geometries stabilize or destabilize ice shelves?

**PGIS Across Glacier** 

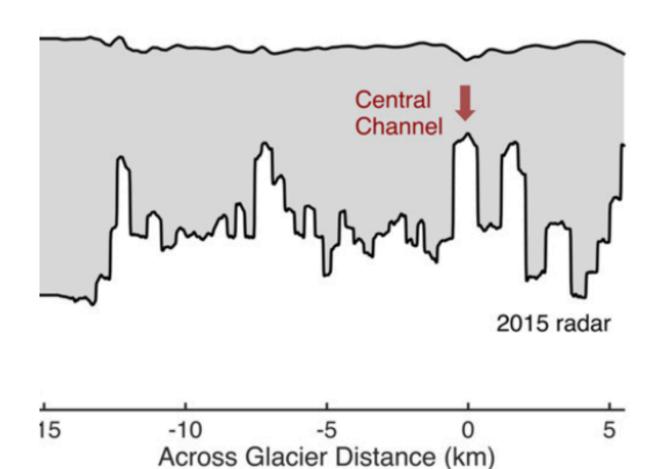


Figure 1: Radar profile across the Petermann Gletscher in Northwest Greenland. Credit: Washam et al (2018).



- Large Eddy Simulations of ocean circulation within basal geometries were developed using MITGCM with 3D Smagorinsky viscosity
- Sensitivities of melt to each control parameter can be predicted by using 3-eq. ice-ocean boundary layer parameterization.

$$m = C_{eddy}V(T - T_f) \tag{1}$$

Definitions: T is the ambient temperature,  $T_f$  is the local freezing temperature at the ambient salinity S (which can be calculated using the liquidus condition).  $C_{\text{eddy}}$  is the turbulent transfer of heat by small-scale ocean boundary layer eddies.

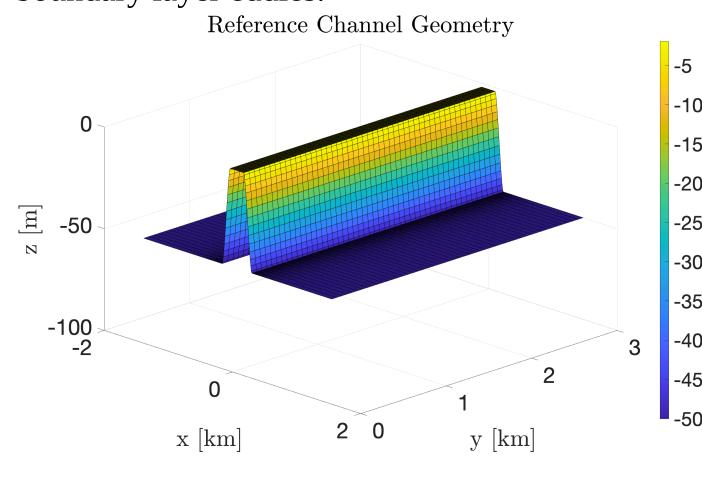


Figure 2: Channel geometry of reference case, with a height of 50m and width of 500m.

Channel width [m]	70, 125, <b>500</b>
$T_{\infty}$ [°C]	-1.8, -1.2, <b>-0.25</b>
$S_{\infty}$ [psu]	29, <b>34.15</b> , 34.6
$V_{\infty}$ [m/s]	0.05, <b>0.1</b> , 0.2
$\theta$	<b>0</b> , 45, 90

Table 1: Parameter regime chosen to represent a range of Greenlandic and Antarctic conditions. **Reference case values in bold.** 

## Reference Case Dynamics & Thermodynamics

Western boundary upwelling/Coriolis-favored circulation

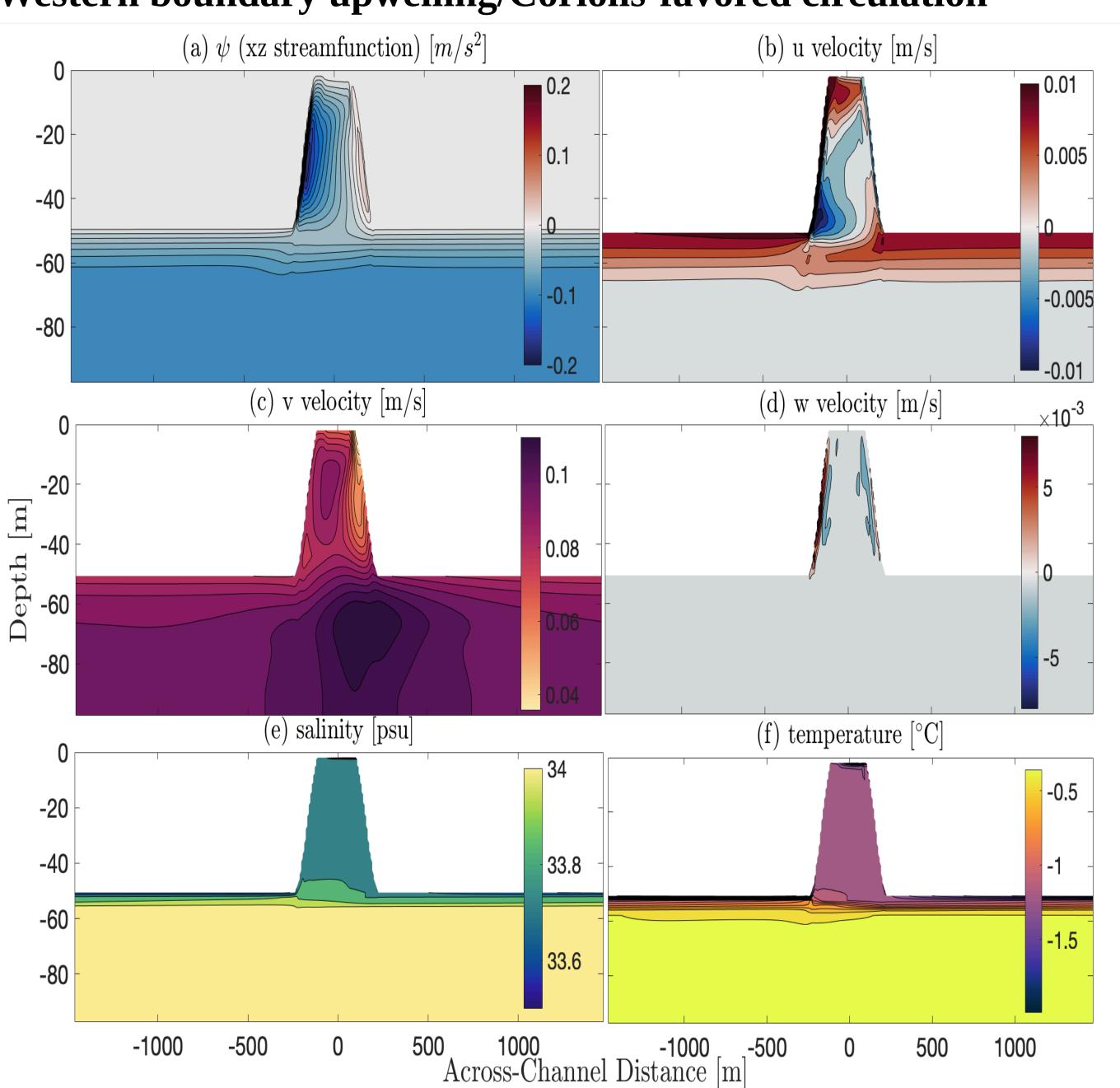


Figure 3: Y-averaged profile of (a) xz streamfunction, (b) u velocity, (c) v velocity, (d) w velocity, (e) temperature, and (f) salinity at day 10 of simulation. Oriented facing the outflowing boundary to the North.

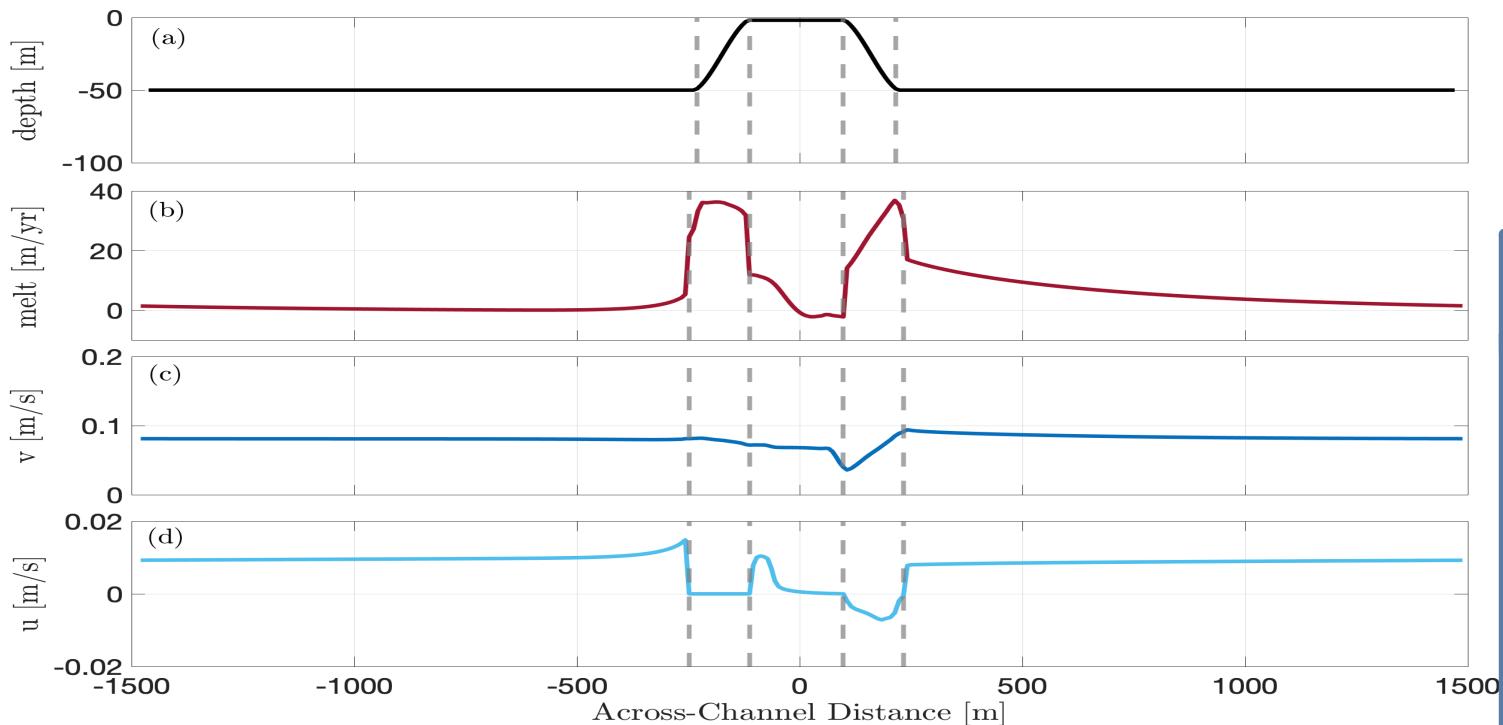


Figure 4: (a) Across-channel depth. Y-averaged profile of (b) melt (c) v velocity, and (d) u velocity at day 10 of simulation. Grey lines mark the sides and top of the channel.

### **Preliminary Melt Theory**

• Melt rates can be predicted within and near various geometries by analyzing nondimensionalized momentum  $\hat{V}$  and thermal forcing channel permeability  $\Delta \hat{T}$ , where

$$V = \frac{V_{\min}}{V_{\infty}}$$
 (2)

$$\hat{T} = \frac{T_{\min} - T_f}{T_{\infty} - T_f} \tag{3}$$

Definitions:  $V_{\infty}$  is the far-field velocity, and  $V_{\min}$  is the velocity at the top of the channel.  $T_{\infty}$  is the far-field temperature,  $T_{\min}$  is the temperature at the top of the channel, and  $T_f$  is the local freezing temperature at the ambient salinity S (which can be calculated using the liquidus condition).

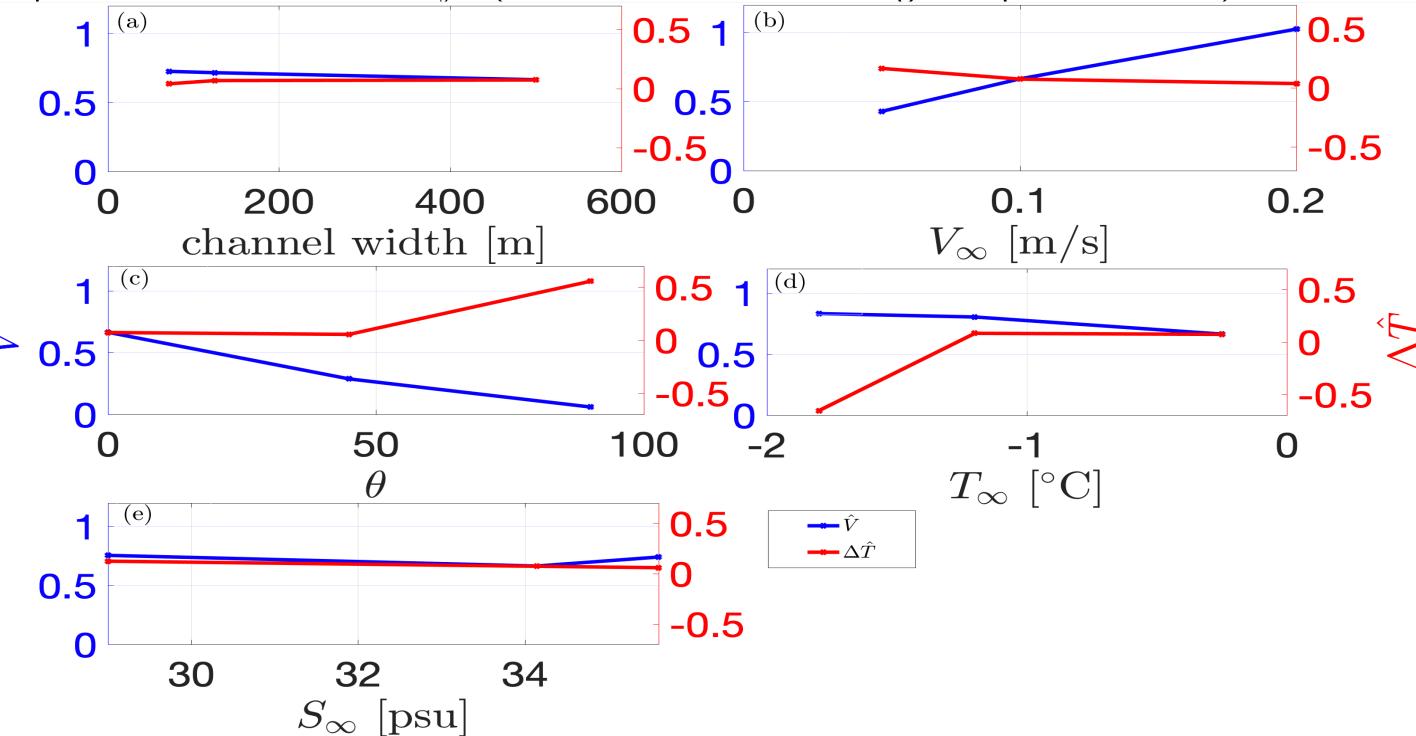


Figure 5:  $\hat{V}$  and  $\Delta \hat{T}$  as a function of control parameters.

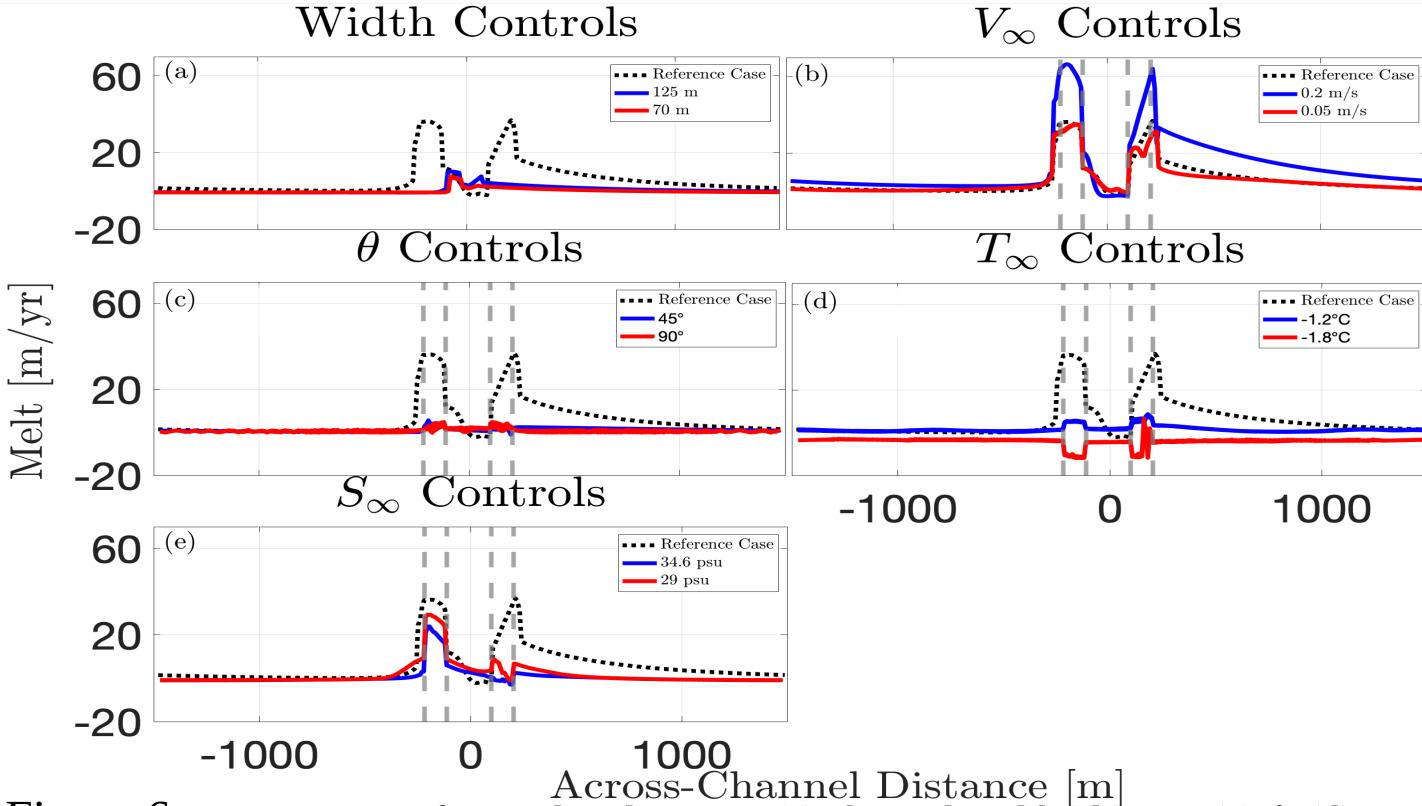


Figure 6: Sensitivities of annual melt rate to (a) channel width, (b)  $V_{\infty}$ , (c)  $\theta$ , (d)  $T_{\infty}$ , and (e)  $S_{\infty}$ .

# **Summary and Future Work**

- Higher melt rates are found on channel walls compared to the top of channels.
- Melt rate is most sensitive to increasing  $V_{\infty}$  and  $T_{\infty}$ .
- Use  $\hat{V}$  and  $\Delta \hat{T}$  to predict melt rates within and outside basal geometries

$$m \propto \left(\frac{V_{\infty} + V_{\min}}{2}\right) \left(\frac{T_{\infty} + T_{f}}{2}\right)$$