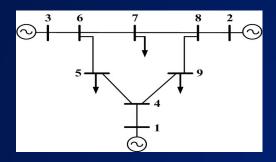
# IEEE-9 BUS Load Flow Analysis

**Course Code: EE 308** 

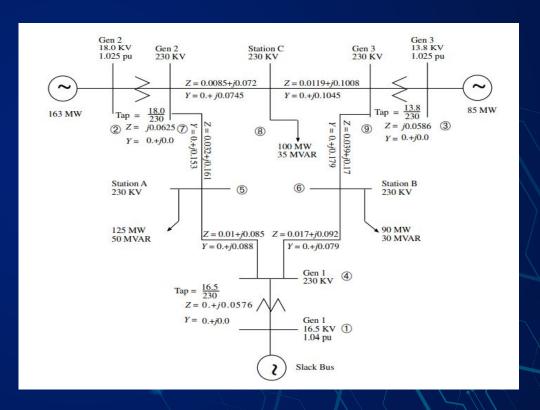
Comparison of different non-linear solution techniques in PowerWorld Simulator



IEEE 9 bus system consists of 3 synchronous generators, nine buses, six transmission lines, three transformers & three P-Q loads. The interconnection of these devices is depicted in the figure.

We have performed load flow analysis to determine the steady-state operating characteristics of the power system for a given load and generator real power and voltage conditions.

#### **IEEE 9 BUS SYSTEM**



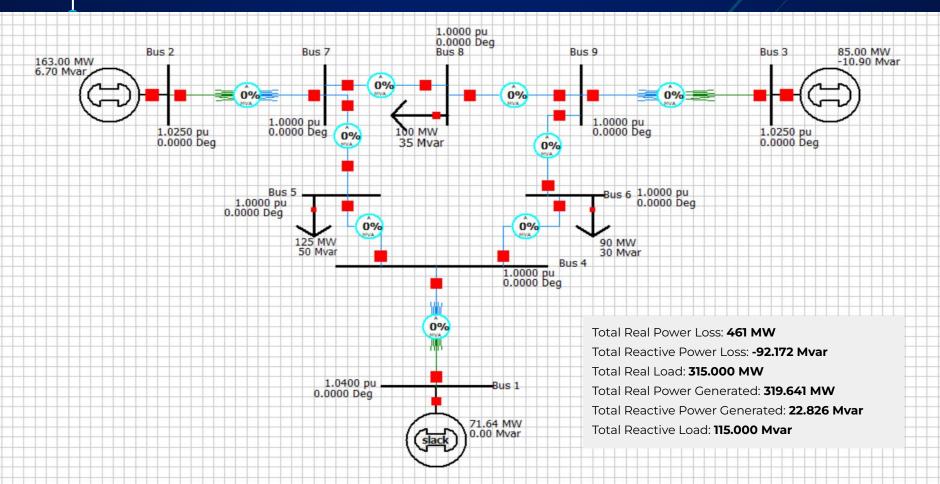
### Bus data of the 9 bus system

| Bus<br>No. | Bus Type | Per unit<br>Voltage | Voltage<br>(KV) | Generation<br>(MW) | Generation<br>(Mvar) | Load(MW) | Load(Mvar) |
|------------|----------|---------------------|-----------------|--------------------|----------------------|----------|------------|
| 1          | Slack    | 1.04                | 16.5KV          | 0                  | 0                    | 0        | 0          |
| 2          | PV       | 1.025               | 18.0KV          | 163                | 6.7                  | 0        | 0          |
| 3          | PV       | 1.025               | 13.8KV          | 85                 | -10.9                | 0        | 0          |
| 4          | PQ       | 1                   | 230KV           | 0                  | 0                    | 0        | 0          |
| 5          | PQ       | 1                   | 230KV           | 0                  | 0                    | 125      | 50         |
| 6          | PQ       | 1                   | 230KV           | 0                  | 0                    | 90       | 30         |
| 7          | PQ       | 1                   | 230KV           | 0                  | 0                    | 0        | 0          |
| 8          | PQ       | 1                   | 230KV           | 0                  | 0                    | 100      | 35         |
| 9          | PQ       | 1                   | 230KV           | 0                  | 0                    | 0        | 0          |

#### Line and branch data of the 9 bus system

| Line From | Line To | R      | Х      | В     |
|-----------|---------|--------|--------|-------|
| 1         | 4       | 0      | 0.0576 | 0     |
| 4         | 5       | 0.01   | 0.085  | 0.176 |
| 4         | 6       | 0.017  | 0.092  | 0.158 |
| 6         | 9       | 0.039  | 0.17   | 0.358 |
| 5         | 7       | 0.032  | 0.161  | 0.306 |
| 9         | 3       | 0      | 0.0586 | 0     |
| 7         | 2       | 0      | 0.0625 | 0     |
| 9         | 8       | 0.0119 | 0.1008 | 0.209 |
| 7         | 8       | 0.0085 | 0.072  | 0.149 |

#### **IEEE-9 Bus simulation in PowerWorld**



#### Y Bus Matrix

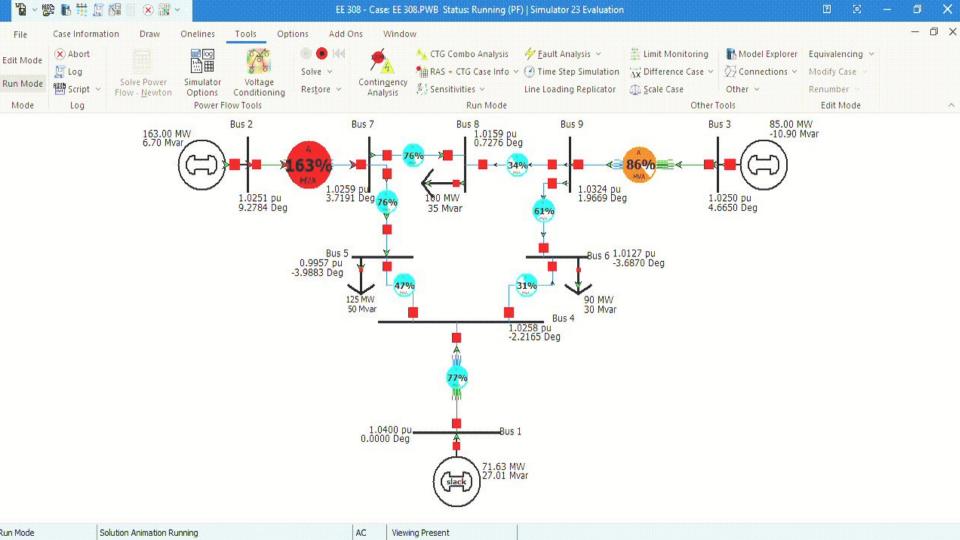
| No. | Name  | Bus1         | Bus2         | Bus3         | Bus4         | Bus5         | Bus6         | Bus7         | Bus8         | Bus9         |
|-----|-------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|
| 1   | Bus 1 | 0.00-j17.36  |              |              | -0.00+j17.36 |              |              |              |              |              |
| 2   | Bus 2 |              | 0.00-j16.00  |              |              |              |              | -0.00+j16.00 |              |              |
| 3   | Bus 3 |              |              | 0.00-j17.06  |              |              |              |              |              | -0.00+j17.06 |
| 4   | Bus 4 | -0.00+j17.36 |              |              | 3.31-j39.31  | -1.37+j11.60 | -1.94+j10.51 |              |              |              |
| 5   | Bus 5 |              |              |              | -1.37+j11.60 | 2.55-j17.34  |              | -1.19+j5.98  |              |              |
| 6   | Bus 6 |              |              |              | -1.94+j10.51 |              | 3.22-j15.84  |              |              | -1.28+j5.59  |
| 7   | Bus 7 |              | -0.00+j16.00 |              |              | -1.19+j5.98  |              | 2.80-j35.45  | -1.62+j13.70 |              |
| 8   | Bus 8 |              |              |              |              |              |              | -1.62+j13.70 | 2.77-j23.30  | -1.16+j9.78  |
| 9   | Bus 9 |              |              | -0.00+j17.06 |              |              | -1.28+j5.59  |              | -1.16+j9.78  | 2.44-j32.15  |

### **Load flow analysis**

**Load flow studies** are performed on power system to understand the nature of the installed network. Load flow is used to determine the **static performance** of the system.

It is commonly used to investigate:

- Component or circuit loading
- Bus voltage profiles (magnitude, phase angle, etc)
- Real and reactive power flow
- Power system losses
- Proper transformer tap settings



# Load Flow Analysis for the 9 Bus System

| • | Bus No. | Generation |       | Load |      | Bus Voltage   |               |  |
|---|---------|------------|-------|------|------|---------------|---------------|--|
|   |         | MW         | Mvar  | MW   | Mvar | Voltage (p.u) | Angle(degree) |  |
|   | 1       | 71.6       | 27    | 0    | 0    | 1.04          | 0             |  |
|   | 2       | 163        | 6.7   | 0    | 0    | 1.025         | 9.3           |  |
| • | 3       | 85         | -10.9 | 0    | 0    | 1.025         | 4.7           |  |
|   | 4       | 0          | 0     | 0    | 0    | 1.026         | -2.2          |  |
|   | 5       | 0          | 0     | 125  | 50   | 0.996         | -4            |  |
|   | 6       | 0          | 0     | 90   | 30   | 1.013         | -3.7          |  |
|   | 7       | 0          | 0     | 0    | 0    | 1.026         | 3.7           |  |
|   | 8       | 0          | 0     | 100  | 35   | 1.016         | 0.7           |  |
|   | 9       | 0          | 0     | 0    | 0    | 1.032         | 2             |  |

#### **Line to Line Losses and Power Transfer Data**

|      | Line | Р     | Q     | Line Los | SS     |
|------|------|-------|-------|----------|--------|
| From | То   | MW    | Mvar  | MW       | Mvar   |
| 1    | 4    | 70.53 | 27    | 0        | 3.23   |
| 4    | 5    | 40.88 | 22.9  | 0.3      | -15.8  |
| 4    | 6    | 30.7  | 1     | 0.2      | -15.43 |
| 6    | 9    | 59.6  | -13.6 | 1.4      | -31.5  |
| 5    | 7    | 84.3  | -11.3 | 2.3      | -19.8  |
| 9    | 3    | 85    | 15    | 0        | 4.1    |
| 7    | 2    | 163   | 9.1   | 0        | 15.8   |
| 9    | 8    | 24.2  | 3.1   | 0.1      | -21.2  |
| 7    | 8    | 76.4  | -0.8  | 0.5      | -11.5  |

### **Gauss- Seidel Method**

With the slack bus voltage assumed (usually V1 = 1.0 p.u.), the remaining **(n-1)** bus voltages are found through **iterative process** as follows

$$P_{i} = \sum_{j=1}^{n} |V_{i}| |V_{j}| |Y_{ij}| \cos(\theta_{ij} - \delta_{i} + \delta_{j})$$

$$Q_{i} = -\sum_{j=1}^{n} |V_{i}| |V_{j}| |Y_{ij}| sin(\theta_{ij} - \delta_{i} + \delta_{j})$$

The equation 1 and 2 are called static load flow equations.

$$I_i = \frac{P_i - jQ_i}{V_i^*}$$

$$V_i = \frac{1}{Y_{ii}} \left( I_i - \sum_{\substack{j=1 \ j \neq 1}}^n Y_{ij} V_j \right) \quad i = 2, 3, 4 \dots n$$

For  $(k+1)^{th}$  iteration, the voltage equation becomes

$$V_i^{(k+1)} = \frac{1}{Y_{ii}} \left[ \frac{P_i - jQ_i}{(V_i^k)^*} - \sum_{j=1}^{i-1} (Y_{ij} V_j^{k+1}) - \sum_{j=i+1}^{n} (Y_{ij} V_j^k) \right]$$

### **Newton- Raphson method**

- The Jacobian matrix gives the linearized relationship between small changes in voltage angle  $\Delta \delta$  and voltage magnitude  $\Delta V$  with the small changes in active and reactive power  $\Delta P$  and  $\Delta Q$ .
- The terms **ΔPir and ΔQir** are the difference between the scheduled and calculated valued, known as **mismatch** vector or power residuals, given by

$$P_i$$
 (scheduled)  $-P_i^r$  calculated  $= \Delta P_i^r$ 

$$Q_i \text{ (scheduled)} - Q_i^r \text{ calculated} = \Delta Q_i^r$$

$$|V|^{(r+1)} = |V|^r + |\Delta V|^r \qquad \left[ \begin{array}{c} \Delta P \\ \Delta Q \end{array} \right] = \begin{bmatrix} J \end{bmatrix} \begin{bmatrix} \Delta \delta \\ \Delta V \end{bmatrix}$$

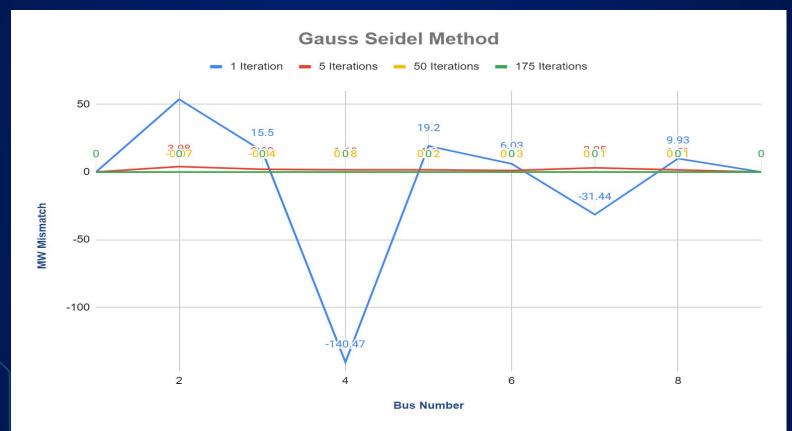
$$\delta(r+1) = \delta r + \Delta \delta r$$
where  $r = \text{no. of iteration}$ 
here  $[J] = \begin{bmatrix} J1 & J2 \\ J3 & J4 \end{bmatrix}$ 

# Initial Mismatches (Flat Start)

| X | Mism   | natches X Yb | us X Genera | tors X OPF Bu | ses X Mismato | hes X Buses   |                 |                               |
|---|--------|--------------|-------------|---------------|---------------|---------------|-----------------|-------------------------------|
| : |        | 00. 4k ∰     | .00 AM ABCD | ### Records ▼ | Geo * Set * C | olumns 🕶 🖼 🕶  | AUXB - AUXB - P | # ▼ SORT   f(x) ▼   Options ▼ |
| : | Filter | Advanced +   | Bus         | *             |               |               | → Find Remov    | re Quick Filter *             |
|   |        | Number       | Name        | Area Name     | Mismatch MW   | Mismatch Mvar | Mismatch M\ ▼   |                               |
|   | 1      | 2            | Bus 2       | 1             | 163.00        | 6.70          | 163.14          |                               |
|   | 2      | 5            | Bus 5       | 1             | -125.00       | -25.90        | 127.66          |                               |
|   | 3      | 8            | Bus 8       | 1             | -100.00       | -17.10        | 101.45          |                               |
|   | 4      | 6            | Bus 6       | 1             | -90.00        | -4.20         | 90.10           |                               |
|   | 5      | 4            | Bus 4       | 1             | 0.00          | 86.14         | 86.14           |                               |
|   | 6      | 3            | Bus 3       | 1             | 85.00         | -10.90        | 85.70           |                               |
|   | 7      | 9            | Bus 9       | 1             | 0.00          | 28.35         | 28.35           |                               |
|   | 8      | 7            | Bus 7       | 1             | 0.00          | 22.75         | 22.75           |                               |
|   | 9      | 1            | Bus 1       | 1             | 0.00          | 0.00          | 0.00            |                               |

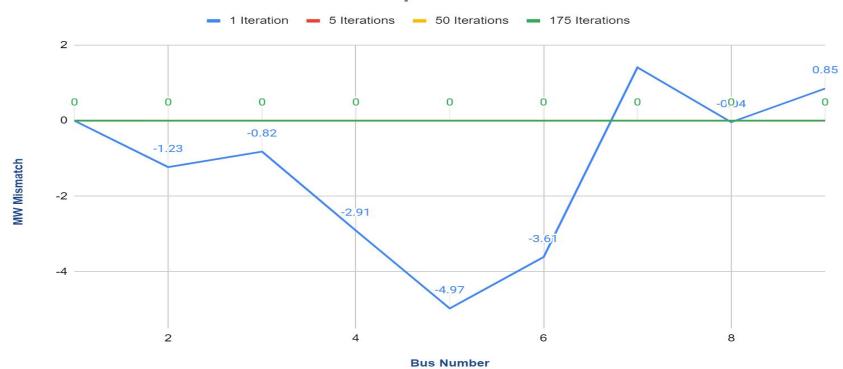
| 910 N 100            | 100 100 110 | Gauss Seidel |               |              | Newton Raphson     |               |                     |
|----------------------|-------------|--------------|---------------|--------------|--------------------|---------------|---------------------|
| Number of Iterations | Bus Number  | MW Mismatch  | Mvar Mismatch | MVA Mismatch | <b>MW Mismatch</b> | Mvar Mismatch | <b>MVA Mismatch</b> |
|                      | 1           | 0            | 0             | 0            | 0                  | 0             | 0                   |
|                      | 2           | 53.69        | 18.51         | 56.79        | -1.23              | -21.18        | 21.21               |
|                      | 3           | 15.5         | 2.59          | 15.71        | -0.82              | -5.35         | 5.41                |
|                      | 4           | -140.47      | -0.15         | 140.47       | -2.91              | 4.17          | 5.08                |
| 1                    | 5           | 19.2         | -2.88         | 19.41        | -4.97              | -8.31         | 9.68                |
| 50                   | 6           | 6.03         | 2.7           | 6.61         | -3.61              | -5.03         | 6.19                |
|                      | 7           | -31.44       | -12.57        | 33.86        | 1.41               | -0.53         | 1.51                |
|                      | 8           | 9.93         | 5.9           | 11.55        | -0.04              | 0.22          | 0.22                |
|                      | 9           | 0            | 0             | 0            | 0.85               | -0.62         | 1.05                |
|                      | 1           | 0            | 0             | 0            | 0                  | 0             | 0                   |
|                      | 2           | 3.98         | 8.28          | 9.18         | 0                  | -0.01         | 0.01                |
|                      | 3           | 2.02         | -7.28         | 7.55         | 0                  | 0             | 0                   |
|                      | 4           | 1.65         | 1.06          | 1.96         | 0                  | 0             | 0                   |
| 5                    | 5           | 1.6          | -0.08         | 1.6          | 0                  | 0             | 0                   |
|                      | 6           | 1.06         | 0.88          | 1.38         | 0                  | 0             | 0                   |
|                      | 7           | 3.05         | 1.94          | 3.61         | 0                  | 0             | 0                   |
|                      | 8           | 1.51         | 1.8           | 2.35         | 0                  | 0             | 0                   |
|                      | 9           | 0            | 0             | 0            | 0                  | 0             | 0                   |
|                      | 1           | 0            | 0             | 0            | 0                  | 0             | 0                   |
|                      | 2           | -0.07        | 7.02          | 7.02         | 0                  | -0.01         | 0.01                |
|                      | 3           | -0.04        | -10.58        | 10.58        | 0                  | 0             | 0                   |
|                      | 4           | 80.0         | 0.27          | 0.28         | 0                  | 0             | 0                   |
| 50                   | 5           | 0.02         | 0.12          | 0.12         | 0                  | 0             | 0                   |
|                      | 6           | 0.03         | 0.1           | 0.11         | 0                  | 0             | 0                   |
|                      | 7           | 0.01         | 0.28          | 0.28         | 0                  | 0             | 0                   |
|                      | 8           | 0.01         | 0.18          | 0.18         | 0                  | 0             | 0                   |
|                      | 9           | 0            | 0             | 0            | 0                  | 0             | 0                   |
|                      | 1           | 0            | 0             | 0            | 0                  | 0             | 0                   |
|                      | 2           | 0            | 6.7           | 6.7          | 0                  | -0.01         | 0.01                |
|                      | 3           | 0            | -10.9         | 10.9         | 0                  | 0             | 0                   |
|                      | 4           | 0            | 0             | 0            | 0                  | 0             | 0                   |
| 175                  | 5           | 0            | 0             | 0            | 0                  | 0             | 0                   |
|                      | 6           | 0            | 0             | 0            | 0                  | 0             | 0                   |
|                      | 7           | 0            | 0             | 0            | 0                  | 0             | 0                   |
|                      | 8           | 0            | 0             | 0            | 0                  | 0             | 0                   |
|                      | 9           | 0            | 0             | 0            | 0                  | 0             | 0                   |

# **Comparing the results**

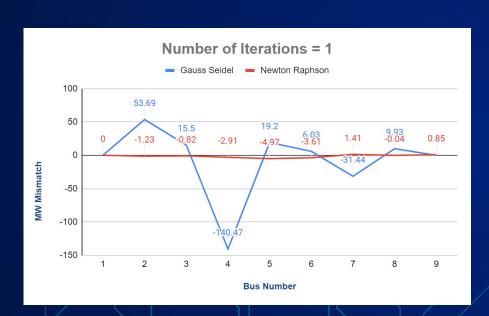


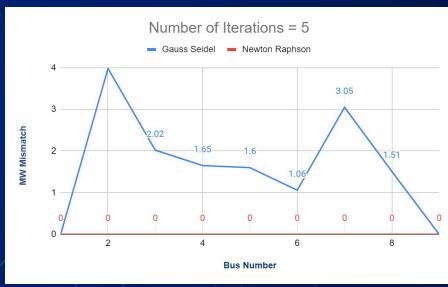
### **Comparing the results**





# **Comparing the results**





### **Observations**

The **Gauss-Siedel** method requires more iterations to converge for the same values of |V|, angle, active and reactive power. Furthermore, with less iterations, the **Newton Raphson** approach outperforms the **GS** method.

The **results** show that the **Gauss-Siedel** approach is straightforward and easy to implement, but gets slower as the number of buses **increases**. The **Newton Raphso**n approach is more accurate than any other methods and yields better results in fewer iterations.

| Method<br>Bus No.↓ | Used→ | Gauss-Siedel<br>Method | Newton - Raphson<br>method |
|--------------------|-------|------------------------|----------------------------|
| 6                  |       | 24                     | 11                         |
| 9                  |       | 182                    | 11                         |
| 14                 | 20    | 384                    | 7                          |
| 30                 |       | 648                    | 5                          |
| 57                 |       | 864                    | 11                         |

### System Data Changes

The following alterations are made on the IEEE 9 Standard Bus System model

#### Loads:

Load on Bus 5 is changed to **50 MW, 0 MVA**R Load on Bus 6 is changed to **150 MW, 50 MVAR** Load on Bus 8 is changed to **200 MW, 50 MVAR** 

#### **Generators:**

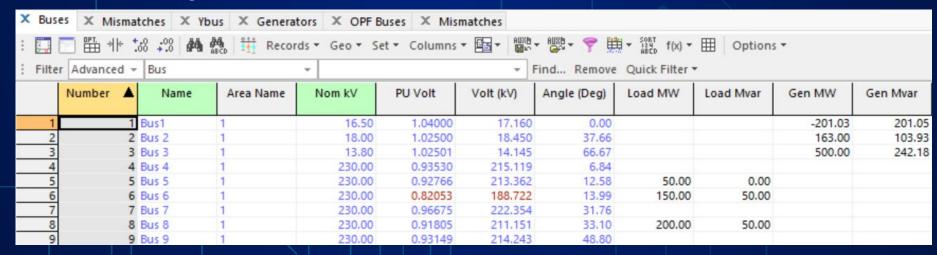
Real and Reactive Power of all generators are made equal to 500MW and 10MVAR

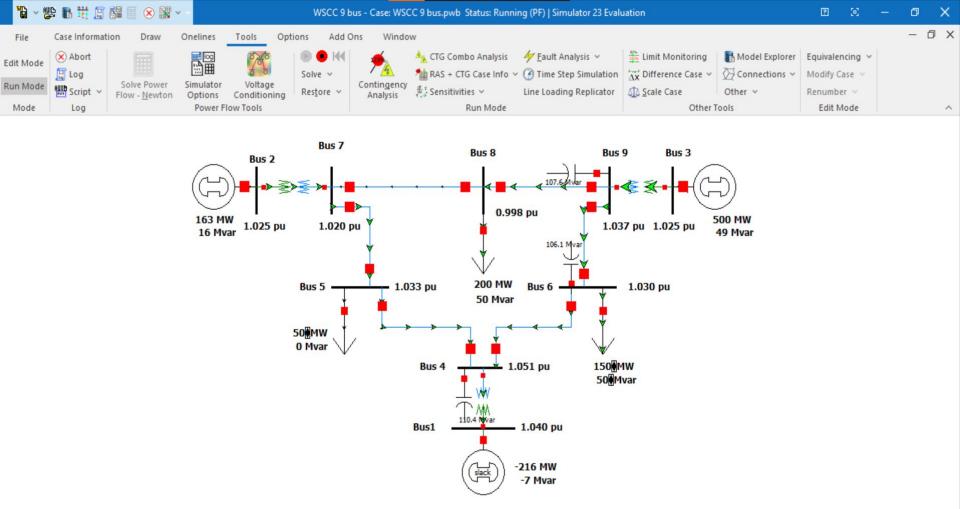
### Under normal system conditions the voltages need to be maintained between **95%** and **105%** of the nominal

Low Voltage condition results in equipment malfunctions:

- •Load will stall, overheat or damage
- •Reactive power output of capacitor is exponentially reduced
- •Generating units may trip

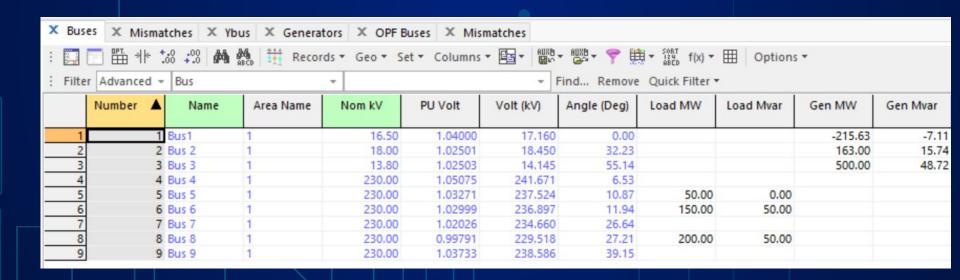
#### Here, Per Unit Voltage of Bus 6 = 0.82053





#### **Shunt Capacitor is Installed**

- When Capacitor of 100MVar rating is connected at Bus 6, Bus 9 and Bus 4
- This leads to per unit Voltage correction
- Now, Per Unit Voltage of Bus 6 = **1.02999**



### **Need for capacitor**

The generation of **reactive power** affects the total generation cost due to increase in the transmission losses.

TCSC (Thyristor controlled series capacitor) introduces a number of important benefits:

- Sub synchronous resonance risks elimination
- Real power oscillations damping
- Improvement in post contingency stability
- Increased power flow through the lines

TCSC provides a cost effective alternative capable of boosting the degree of overall power flow.

Utilization of TCSC in real world power problems between any buses can help overcome the issues of **reactive power losses** and poor power quality.



### Conclusion

Thus we have performed the load flow analysis of IEEE-9 Bus system by:

- Simulating the IEEE-9 Bus system on powerWorld simulator.
- Analysing the Gauss-Seidel and Newton-Raphson methods.
- Comparing the results of both these methods.
- Finding methods to improve the overall performance of the system.

#### Resources

- https://www.pscad.com/knowledge-base/article/25
- https://ieeexplore.ieee.org/document/8358277
- https://www.ripublication.com/irph/ijee16/ijeev9n2\_01.pdf
- https://www.omazaki.co.id/en/load-flow-study-analysis/
- https://scholarworks.calstate.edu/downloads/xg94hv83w
- https://www.powerworld.com/WebHelp/Content/MainDocumentation\_HTM L/Limit\_Monitoring\_Settings\_and\_Limit\_Violations\_Dialog.htm
- https://www.researchgate.net/publication/338345486\_Power\_Flow\_Analysis\_ using\_Power\_World\_Simulator
- https://www.irjet.net/archives/V3/i3/IRJET-V3I323.pdf
- https://www.powerworld.com/files/12Weber\_DFACTS.pdf

