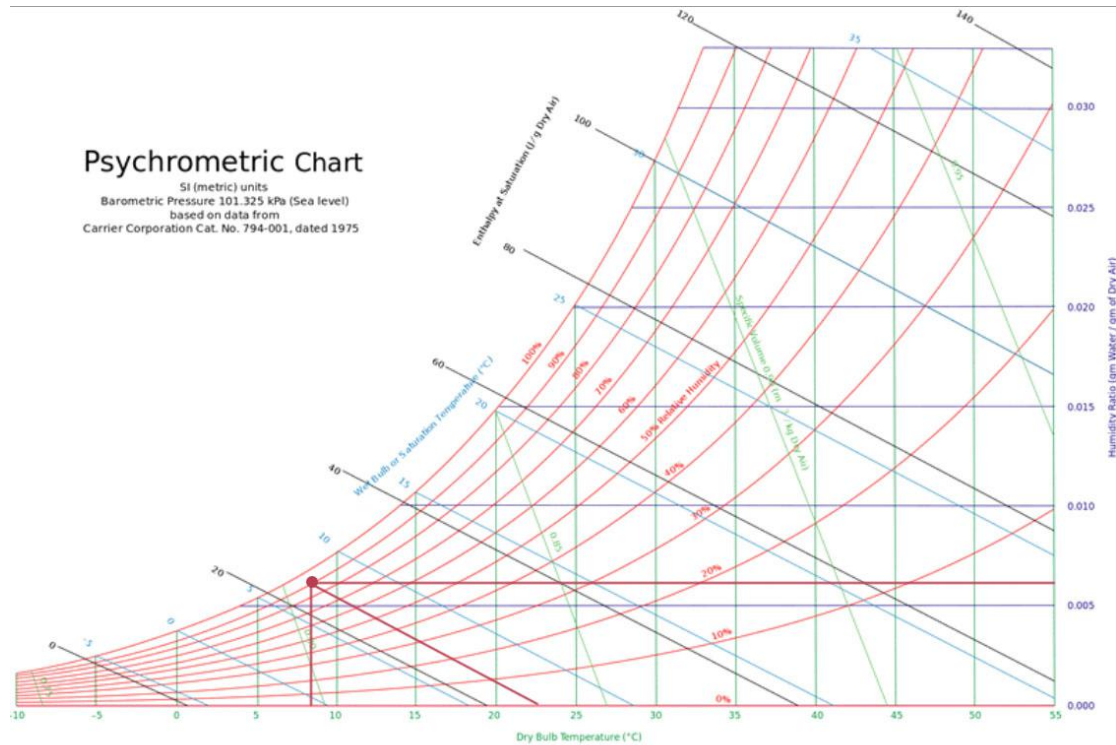


Task 1 Use a weather forecast website, and utilize the psychrometric chart and the formula we went through in the class to determine the absolute humidity, the wet-bulb temperature and the mass of water vapour in the air in Classroom A (Aula A) of Piacenza campus in the moment that you are solving this exercise (provide the inputs that you utilized)

Humidity: 90% = Relative humidity: $\phi = 90\%$

Pressione atmosferica: 1019 hPa = total air pressure $P = 101.9 \text{ kPa}$ Effective

temperature: $7^\circ\text{C} = 230 \text{ K}$



Utilizing the psychrometric chart, we can notice that

-The absolute humidity $\omega = 0.0055$

- $T_{wb} = 6^\circ\text{C}$

$$\omega = \frac{0.622 P_v}{P_a} = \frac{0.622 P_v}{P - P_v} = 0.0055$$

$$P_v = 0.893 \text{ circa}$$

$$\phi = \frac{m_v}{m_g} = 90\%$$

$$m \text{ (for gasses in general)} \frac{P_v}{R_{sp} \cdot T}$$

for water vapor $R_{sp} = 0.4615$

P_v (pressure of water vapor) = 0.893 kPa Volume(V) of classroom, where

$$m_v = \frac{0.893 V}{0.4615 \cdot 230} = 8.41 \cdot 10^{-3} V$$

$$m_g = \frac{m_v}{90\%} = 9.34 \cdot 10^{-3} V$$

Task 2 Utilize the same methodology we went through in the class and determine the sensible and latent load corresponding to internal gains, the ventilation, and the infiltration in a house with a *good* construction quality and with the same geometry as that of the example which is located in Brindisi, Italy

| BRINDISI, Italy | | | | | | | | | | | | | | WMO#: 163200 | | |
|--|------------------------|-----------------|----------------|-------------------------------|------|--------------------|------|---|------|-----------------------|------|-------------|------|-----------------------|------|--------------------------|
| Lat: 40.65N | | Long: 17.95E | | Elev: 10 | | StdP: 101.2 | | Time Zone: 1.00 (EUW) | | Period: 86-10 | | WBAN: 99999 | | | | |
| Annual Heating and Humidification Design Conditions | | | | | | | | | | | | | | | | |
| Coldest Month | Heating DB | | | Humidification DP/MCDB and HR | | | | | | Coldest month WS/MCDB | | | | MCWS/PCWD to 99.6% DB | | |
| | | | | 99.6% | | | 99% | | | 0.4% | | 1% | | | | |
| | 99.6% | 99% | | DP | HR | MCDB | DP | HR | MCDB | WS | MCDB | WS | MCDB | MCWS | PCWD | |
| (a) | (b) | (c) | (d) | (e) | (f) | (g) | (h) | (i) | (j) | (k) | (l) | (m) | (n) | (o) | | |
| 2 | 2.9 | 4.1 | -5.1 | 2.5 | 7.2 | -3.0 | 3.0 | 7.4 | 13.4 | 10.2 | 12.4 | 10.6 | 3.4 | 250 | | |
| (1) | | | | | | | | | | | | | | | | |
| Annual Cooling, Dehumidification, and Enthalpy Design Conditions | | | | | | | | | | | | | | | | |
| Hottest Month | Hottest Month DB Range | Cooling DB/MCWB | | | | | | Evaporation WB/MCDB | | | | | | MCWS/PCWD to 0.4% DB | | |
| | | 0.4% | | 1% | | 2% | | 0.4% | | 1% | | 2% | | | | |
| | | DB | MCWB | DB | MCWB | DB | MCWB | WB | MCDB | WB | MCDB | WB | MCDB | MCWS | PCWD | |
| (a) | (b) | (c) | (d) | (e) | (f) | (g) | (h) | (i) | (j) | (k) | (l) | (m) | (n) | (o) | (p) | |
| 8 | 7.1 | 32.8 | 23.6 | 31.1 | 24.3 | 29.9 | 24.3 | 27.2 | 29.7 | 26.3 | 29.0 | 25.6 | 28.3 | 4.2 | 180 | |
| (2) | | | | | | | | | | | | | | | | |
| Dehumidification DP/MCDB and HR | | | | | | | | | | | | | | Enthalpy/MCDB | | Hours 8 to 4 & 12.8/20.6 |
| 0.4% | | 1% | | 2% | | 0.4% | | 1% | | 2% | | | | | | |
| DP | HR | MCDB | DP | HR | MCDB | DP | HR | MCDB | Enth | MCDB | Enth | MCDB | Enth | MCDB | | |
| (a) | (b) | (c) | (d) | (e) | (f) | (g) | (h) | (i) | (j) | (k) | (l) | (m) | (n) | (o) | (p) | |
| 26.3 | 21.8 | 29.2 | 25.4 | 20.7 | 28.5 | 24.7 | 19.7 | 27.9 | 86.0 | 30.1 | 82.2 | 29.1 | 78.5 | 28.3 | 1236 | |
| (3) | | | | | | | | | | | | | | | | |
| Extreme Annual Design Conditions | | | | | | | | | | | | | | | | |
| Extreme Annual WS | | | Extreme Max WB | Extreme Annual DB | | | | n-Year Return Period Values of Extreme DB | | | | | | | | |
| | | | | Mean | | Standard deviation | | n=5 years | | n=10 years | | n=20 years | | n=50 years | | |
| | | | | Min | Max | Min | Max | Min | Max | Min | Max | Min | Max | Min | Max | |
| (a) | (b) | (c) | (d) | (e) | (f) | (g) | (h) | (i) | (j) | (k) | (l) | (m) | (n) | (o) | (p) | |
| 11.3 | 9.9 | 8.7 | 31.4 | 0.4 | 37.3 | 1.4 | 3.0 | -0.6 | 39.4 | -1.4 | 41.1 | -2.2 | 42.8 | -3.2 | 44.9 | |
| (4) | | | | | | | | | | | | | | | | |

Soln:

Number of occupants=2 Number of bed rooms=1

Height of the building=2.5m Area of the floor=200 m²

Internal gains:

$$Q_{\text{igsensible}} = 136 + 2.2A_{\text{cf}} + 22N_{\text{oc}} = 136 + 2.2 * (200) + 22 * 2 = 620 \text{ W}$$

$$Q_{\text{iglaten}} = 20 + 0.22A_{\text{cf}} + 12N_{\text{oc}} = 20 + 0.22 * 200 + 12 * 2 = 88 \text{ W}$$

Infiltrations

For a house with a good construction quality, unit leakage area $A_{\text{ul}} = 1.4 \text{ cm}^2 / \text{m}^2$

And the exposed surface $A_{\text{es}} = A_{\text{wall}} + A_{\text{roof}} = 200 + 144 = 344 \text{ m}^2$

cooling temperature $T_{\text{cooling}} = 24^\circ\text{C}$, and heating temperature $T_{\text{heating}} = 20^\circ\text{C}$ in Brindisi,

$$\Delta T_{\text{cooling}} = 31.1 - 24 = 7.1^\circ\text{C} = 7.1 \text{ K}$$

$$T_{\text{heating}} = 20 - (-4.1) = 24.1^\circ\text{C} = 24.1 \text{ K}$$

$$DR = 7.1^\circ\text{C} = 7.1$$

$$\text{Given that } IDF_{\text{heating}} = 0.073 \frac{L}{\text{s} * \text{Cm}^2}$$

$$IDF_{\text{cooling}} = 0.33 \frac{L}{\text{s} * \text{cm}^2}$$

Infiltration airflow rate

$$Q_{i, \text{heating}} = A_L * IDF_{\text{heating}} = 48.16 * 0.073 = 35.15 \frac{L}{s}$$

$$Q_{i, \text{cooling}} = A_L * IDF_{\text{cooling}} = 481.6 * 0.033 = 15.89 \frac{L}{s}$$

The required minimum whole - building ventilation rate is

$$Q_v = 0.05A_{\text{cf}} + 3.5(N_{\text{br}} + 1) = 0.05 * 200 + 3.5 * (1 + 1) = 17 \frac{L}{s}$$

$$Q_{i-v, \text{heating}} = Q_{i, \text{heating}} + Q_v = 35.157 + 17 = 52.15 \frac{L}{s}$$

$$Q_{i-v, \text{cooling}} = Q_{i, \text{cooling}} + Q_v = 15.893 + 17 = 32.89 \frac{L}{s}$$

Given that

$$C_{\text{sensible}} = 1.23$$

$$C_{\text{latent}} = 3010$$

$$\Delta \omega_{\text{cooling}} = 0.0039$$

$$q_{\text{inf - ventilation cooling sensible}} = C_{\text{sensible}} Q_{i-v, \text{cooling}} \Delta T_{\text{cooling}} = 1.23 * 32.89 * 7.1 = 287.25 \text{ W}$$

$$q_{\text{inf - ventilation cooling latent}} = C_{\text{latent}} Q_{i-v, \text{cooling}} \Delta \omega_{\text{cooling}} = 3010 * 32.89 * 0.0039 = 386.13 \text{ W}$$

$$q_{\text{ventilation heating latent}} = C_{\text{sensible}} Q_{i-v, \text{heating}} \Delta T_{\text{cooling}} = 1.23 * 52.15 * 24.1 = 546 \text{ W}$$