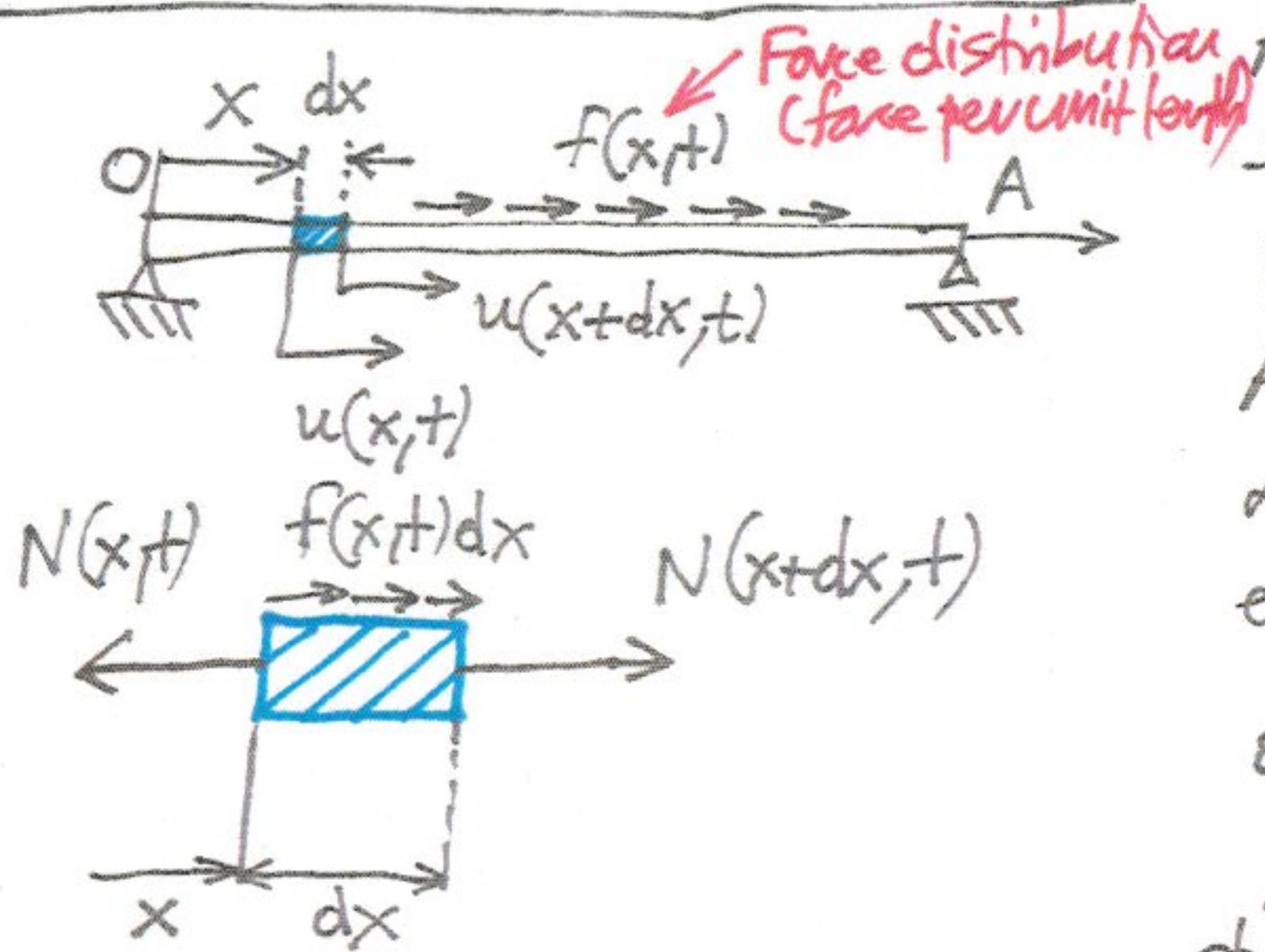


B. Axial vibrations of elastic rods



Assume modulus of elasticity E and cross section $A(x)$. Assume $m(x) = A(x)\rho$ mass per unit length of rod, ρ is density

Assuming linearly elastic material and small axial oscillations \Rightarrow Infinitesimal linear elasticity in x -direction \Rightarrow

$$\epsilon(x,t) = \frac{\partial u(x,t)}{\partial x}, \quad \sigma(x,t) = E \epsilon(x,t) \Rightarrow$$

↑
strain

Assume uniform distribution of stresses at each cross section

$$\Rightarrow \text{Local axial force at position } x \text{ is equal to } N(x,t) = \sigma(x,t) A(x) = EA(x) \frac{\partial u(x,t)}{\partial x}$$

At position $x+dx$, the local axial force is then given by,

$$N(x+dx,t) = EA(x+dx) \frac{\partial u(x+dx,t)}{\partial x}$$

Considering the differential element of length dx we write balance of forces in the x -direction $\Rightarrow m(x)dx \frac{\partial^2 u(x,t)}{\partial t^2} = N(x+dx,t) - N(x,t) + f(x,t)dx \Rightarrow$

$$\Rightarrow m(x)dx \frac{\partial^2 u(x,t)}{\partial t^2} = \frac{EA(x+dx) \frac{\partial u(x+dx,t)}{\partial x} - EA(x) \frac{\partial u(x,t)}{\partial x}}{dx} + f(x,t)dx \Rightarrow \text{As } dx \rightarrow 0,$$

$$m(x) \frac{\partial u(x,t)}{\partial t} = \frac{\partial}{\partial x} \left[EA(x) \frac{\partial u(x,t)}{\partial x} \right] + f(x,t) + O(\Delta x^2) \Rightarrow$$

$$\Rightarrow m(x) \frac{\partial^2 u(x,t)}{\partial t^2} = \frac{\partial}{\partial x} \left[EA(x) \frac{\partial u(x,t)}{\partial x} \right] + f(x,t)$$

Generalized wave equation!

If $m(x)=m$, $EA(x)=EA$, $f(x,t)=0$ \Rightarrow We get the classical wave equation

$$\boxed{\frac{\partial^2 u}{\partial x^2} = \frac{1}{c^2} \frac{\partial^2 u}{\partial t^2}} \quad c^2 = \frac{E}{\rho}, \quad c \text{ is the speed of sound in the rod.}$$

↑ classical wave equation

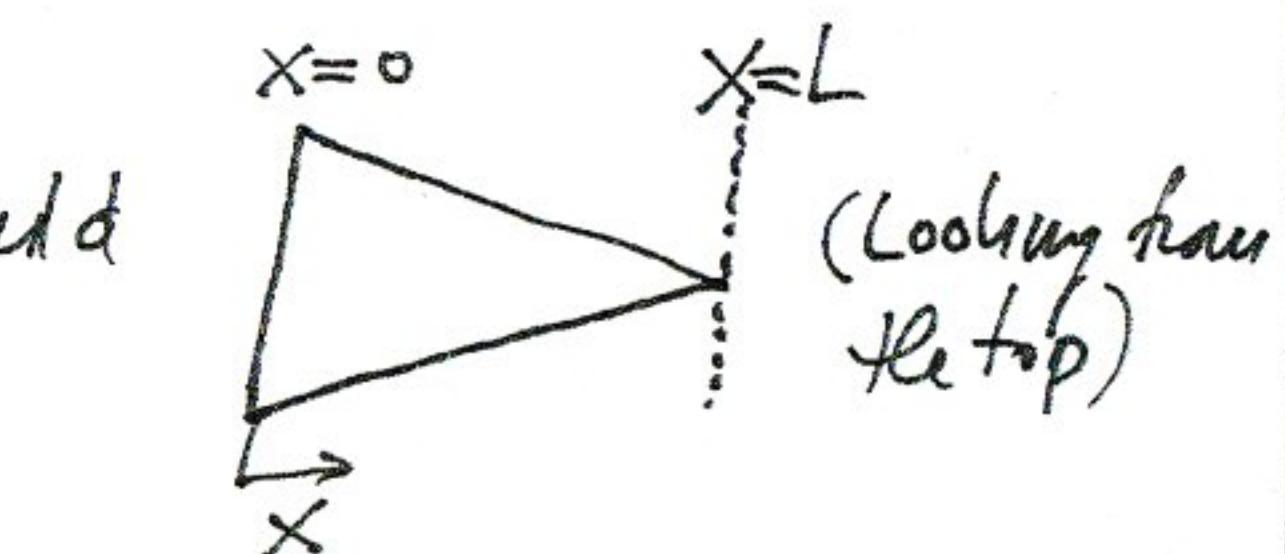
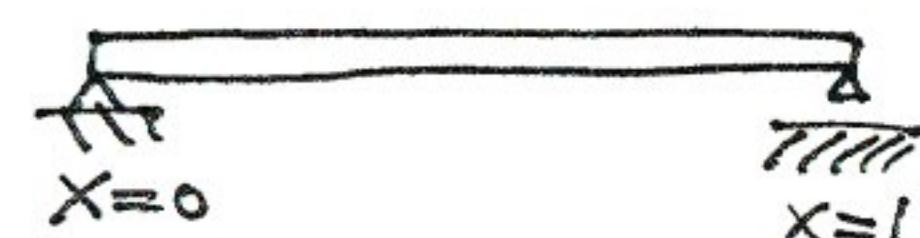
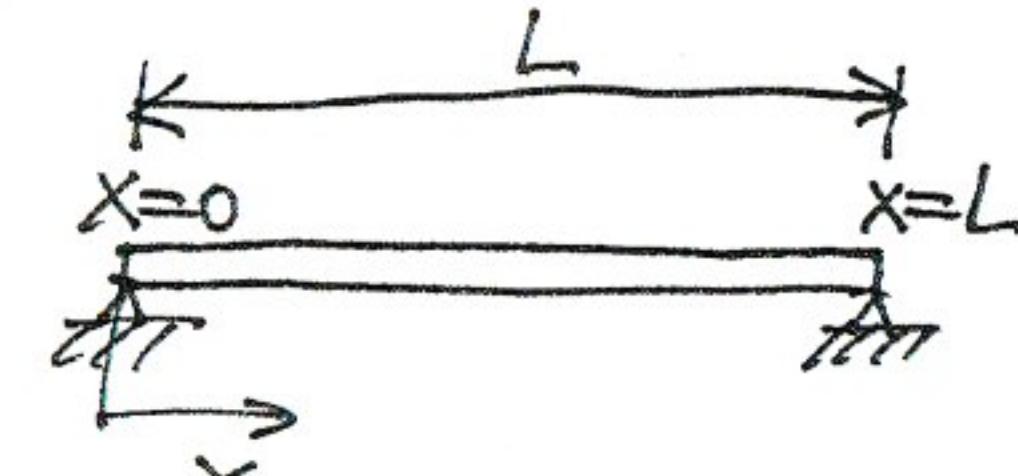
Discussing briefly boundary conditions,

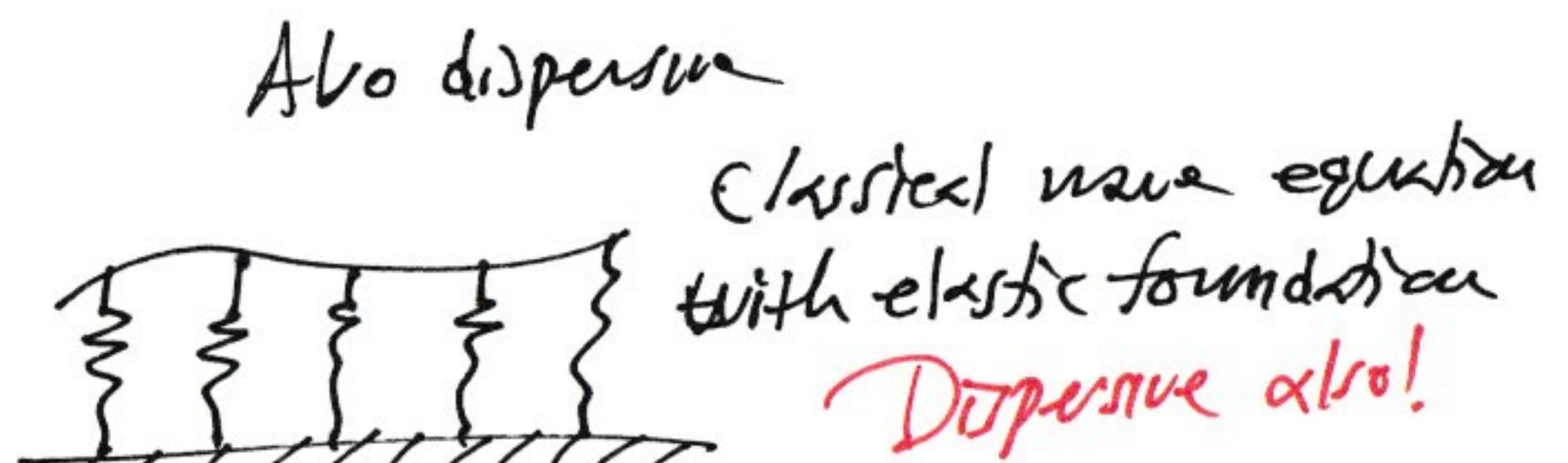
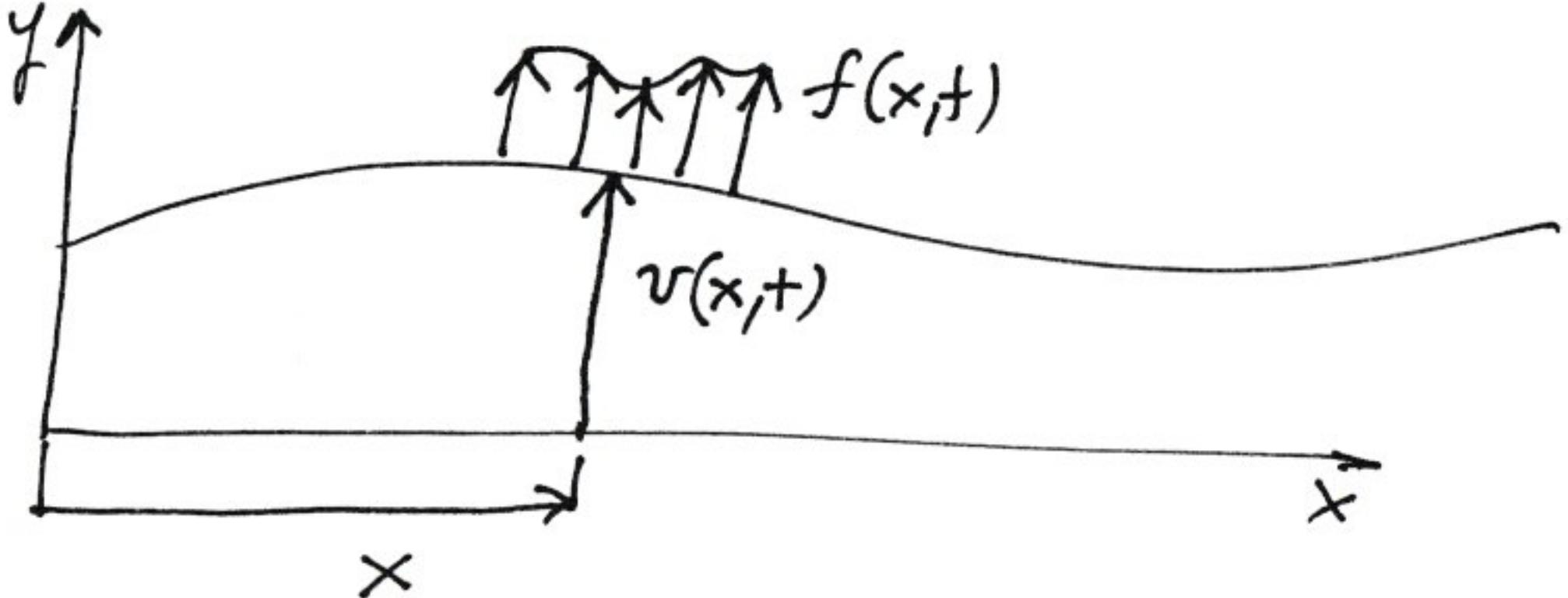
fixed end $\Rightarrow u(0,t)=0$ or $u(L,t)=0$

free end $\Rightarrow \lim_{x \rightarrow L} \left[EA(x) \frac{\partial u(x,t)}{\partial x} \right] = 0 \Rightarrow$

\Rightarrow If $EA(L) \neq 0 \Rightarrow \frac{\partial u(L,t)}{\partial x} = 0$

But if $\lim_{x \rightarrow L} EA(x) = 0 \Rightarrow$ The full boundary condition should be taken into account





Non Dispersive medium

Generalized wave equation, $m(x) \frac{\partial^2 v}{\partial t^2} = \frac{\partial}{\partial x} \left[T(x) \frac{\partial v}{\partial x} \right] + f(x,t) = 0$

If $m(x)=m$, $T(x)=T$, $f(x,t)=0$, \rightarrow Classical wave equation

$$m \frac{\partial^2 v}{\partial t^2} = T \frac{\partial^2 v}{\partial x^2} \Rightarrow \frac{\partial^2 v}{\partial t^2} = \left(\frac{T}{m} \right) \frac{\partial^2 v}{\partial x^2}$$

~~$v \approx c$~~

for the classical wave equation, any applied disturbance propagates with the same velocity c .

for example, consider traveling wave Ansatz

$$v(x,t) = A \cos(\omega t - kx) \quad \begin{matrix} \text{frequency} \\ \text{wavenumber} \end{matrix}$$

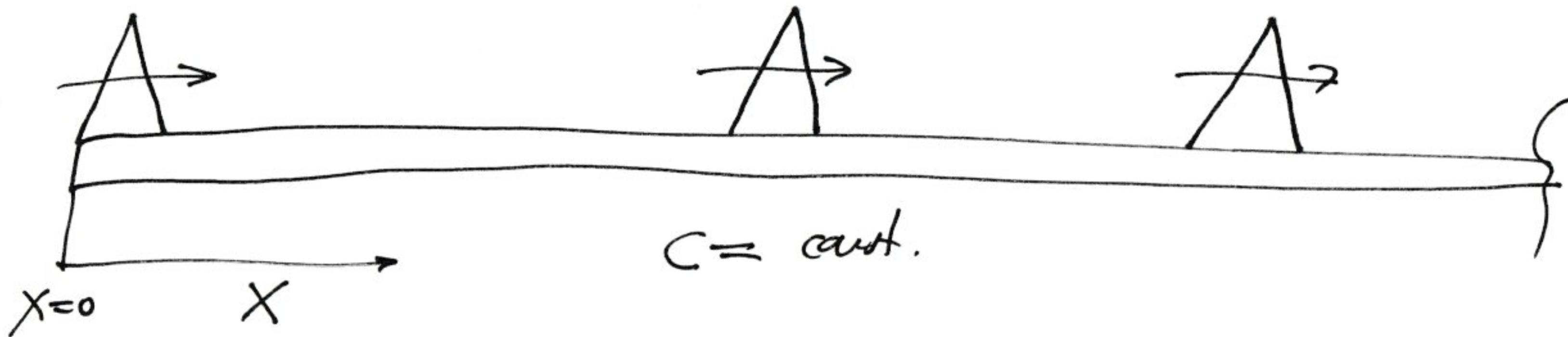
$$\Rightarrow \frac{\partial v}{\partial t} = -\omega A \sin(\omega t - kx) \Rightarrow \frac{\partial^2 v}{\partial t^2} = -\omega^2 A \cos(\omega t - kx)$$

$$\frac{\partial v}{\partial x} = -kA \sin(\omega t - kx) \Rightarrow \frac{\partial^2 v}{\partial x^2} = -k^2 A \cos(\omega t - kx)$$

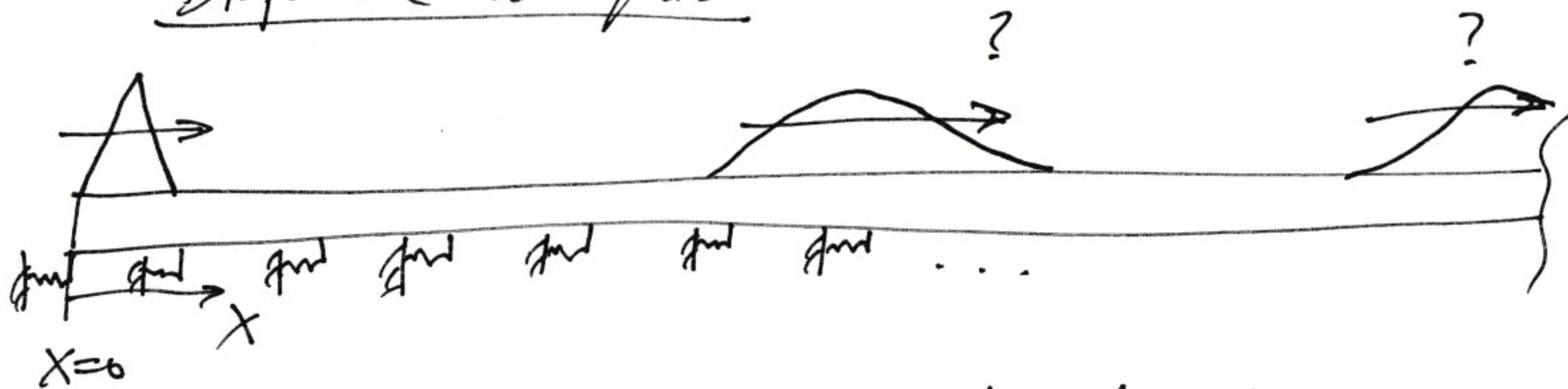
Substitute into ~~the~~ ^{classical} wave equation $\rightarrow -\omega^2 = c^2 k^2 \Rightarrow c^2 = \frac{\omega^2}{k^2} \Rightarrow c = \frac{\omega}{k}$

Represents a
non-dispersive
waveguide

Non-dispersive waveguide: E.g., governed by wave equation
classic

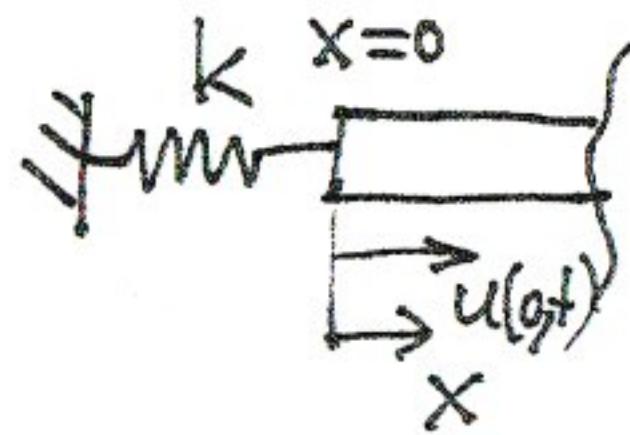


Dispersive waveguides



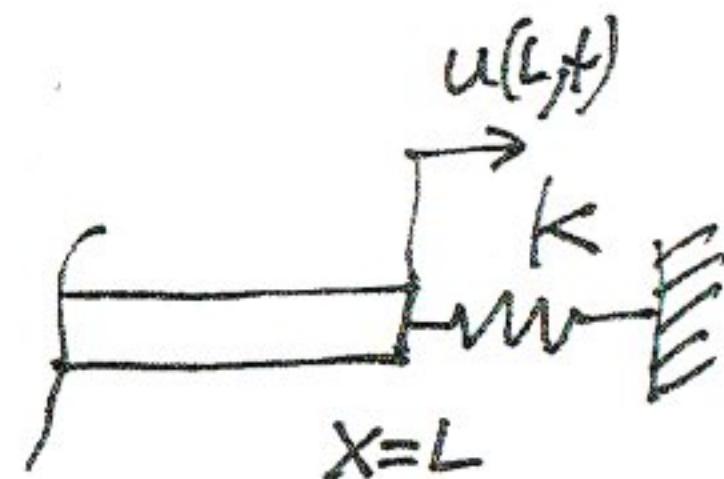
$c \neq \text{const}$ b/c depends on wavenumber
or frequency

Stiffness at the boundary



Performing balance of axial force at $x=0 \Rightarrow N(0,t) - ku(0,t) = 0 \Rightarrow$

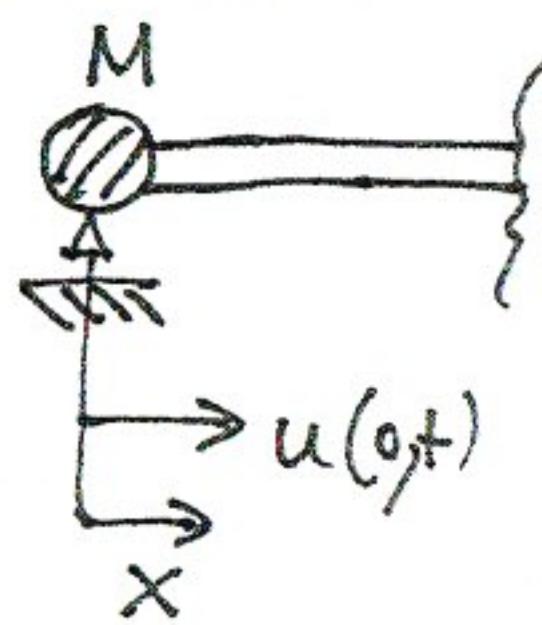
$$\Rightarrow EA(0) \frac{\partial u(0,t)}{\partial x} - ku(0,t) = 0$$



At the other end we can show that

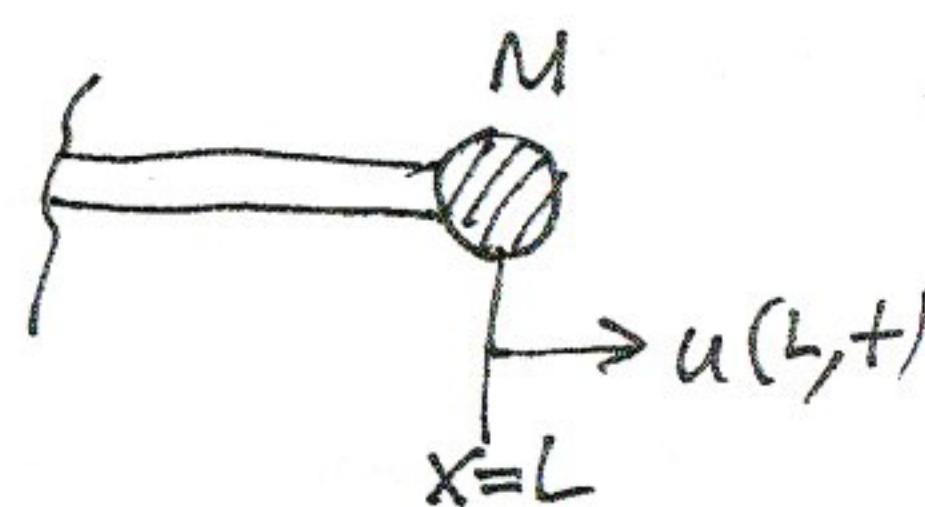
$$EA(L) \frac{\partial u(L,t)}{\partial x} + ku(L,t) = 0$$

Inertia at the boundary



Perform again balance of axial force at $x=0 \Rightarrow$

$$\Rightarrow EA(0) \frac{\partial u(0,t)}{\partial x} - M \frac{\partial^2 u(0,t)}{\partial t^2} = 0$$

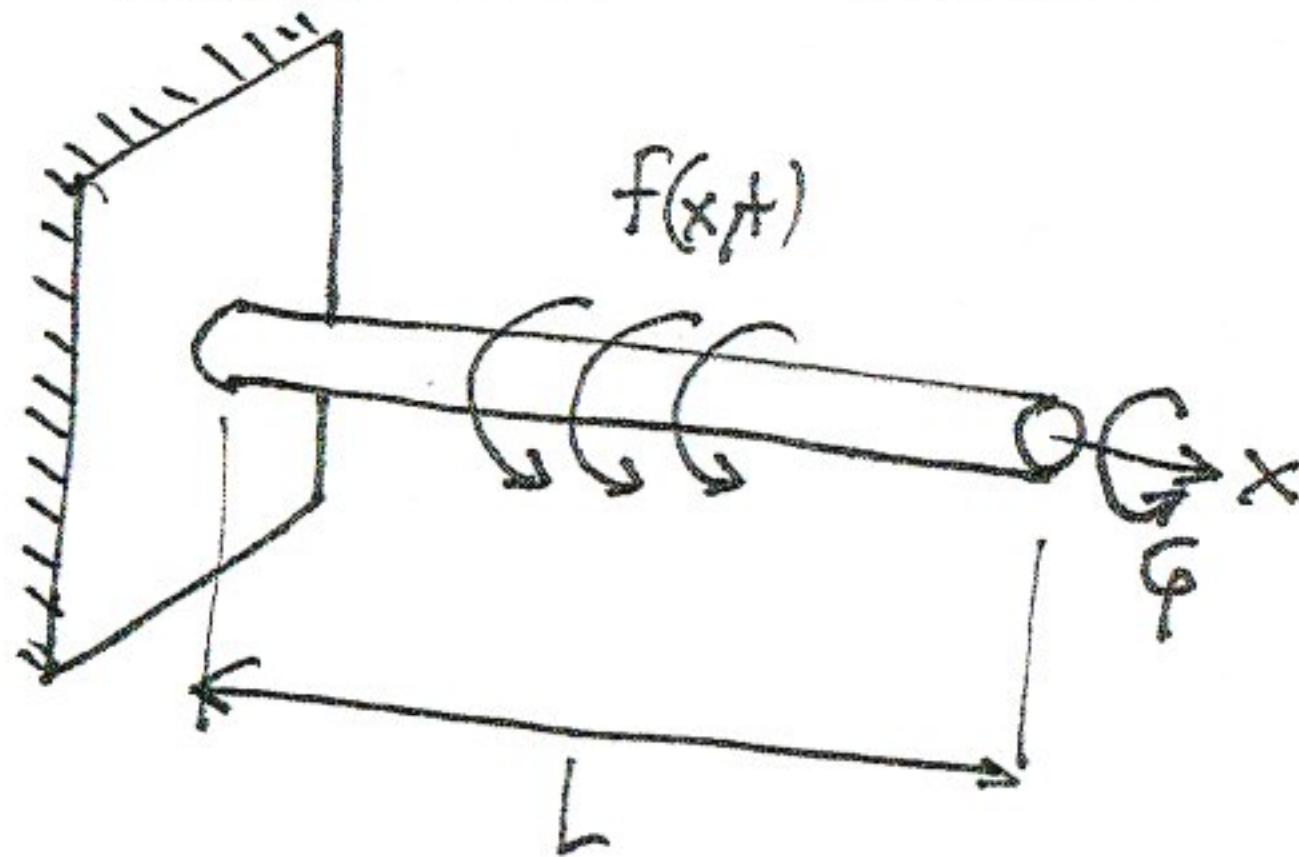


Then the BC becomes

$$EA(L) \frac{\partial u(L,t)}{\partial x} + M \frac{\partial^2 u(L,t)}{\partial t^2} = 0$$

Suggestion: Please try to recover these boundary conditions!

C. Torsional vibrations of circular shafts



By performing balance of moments on a differential element of this system we can show that the torsional oscillations are governed by the generalized wave equation in the form:

$$\rho J_p(x) \frac{\partial^2 \phi(x,t)}{\partial t^2} = \frac{\partial}{\partial x} [GJ_p(x) \frac{\partial \phi(x,t)}{\partial x}] + f(x,t)$$

Polar moment
of inertia of the
cross section at x

Modulus of
torsional
rigidity

Assuming a shaft with constant properties $\Rightarrow \rho J_p(x) = \rho J_p$ \Rightarrow Equation becomes
the classic wave equation

$$\frac{\partial^2 \phi(x,t)}{\partial x^2} = \frac{1}{c^2} \frac{\partial^2 \phi(x,t)}{\partial t^2}$$

$c = \sqrt{\frac{G}{\rho}}$ speed of sound in
this medium

Brief overview of boundary conditions:

fixed boundary: $\phi(0,t) = 0$ or $\dot{\phi}(L,t) = 0$

free boundary: $\frac{\partial \phi(0,t)}{\partial x} = 0$ or $\frac{\partial \phi(L,t)}{\partial x} = 0$