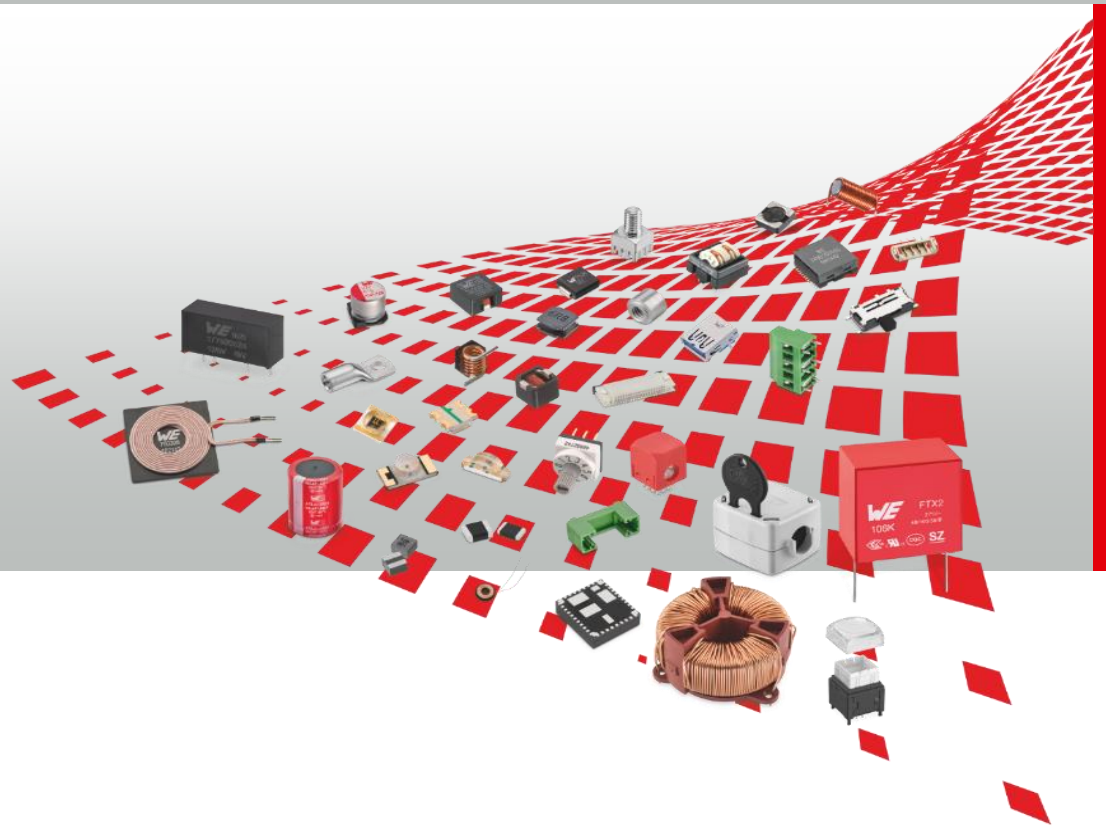
TECHNICAL ACADEMY

WÜRTH ELEKTRONIK

Anticipate EMC with LTSPICE

more than you expect



Sylvain Le Bras

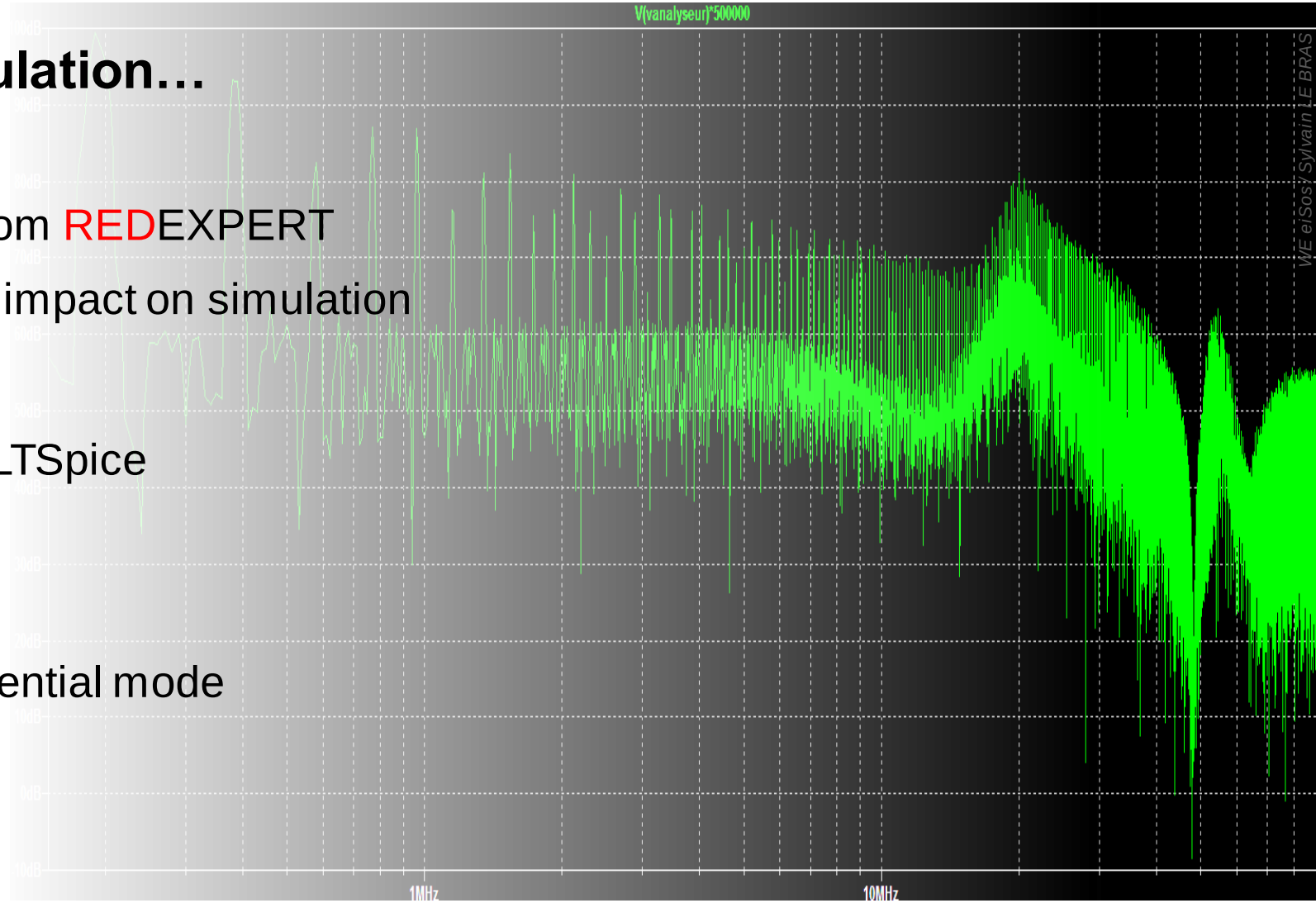
Field Application Engineer

Sylvain.LeBras@we-online.com

Anticipate EMC with LTSpice

Using LTSPICE and Redexpert to check power supply designs

- **Intro : From functional simulation…**
  - Output ripple of a Buck
  - Extracting EMC accurate data from REDEXPERT
  - Example of (non) EMC accurate impact on simulation
- **…To EMC simulation**
  - Enabling EMC measurement in LTSpice
  - Getting Seriously Accurate ?
  - Going further with simulation
    - Splitting Common and Differential mode
    - Making simulation look real
  - Examples

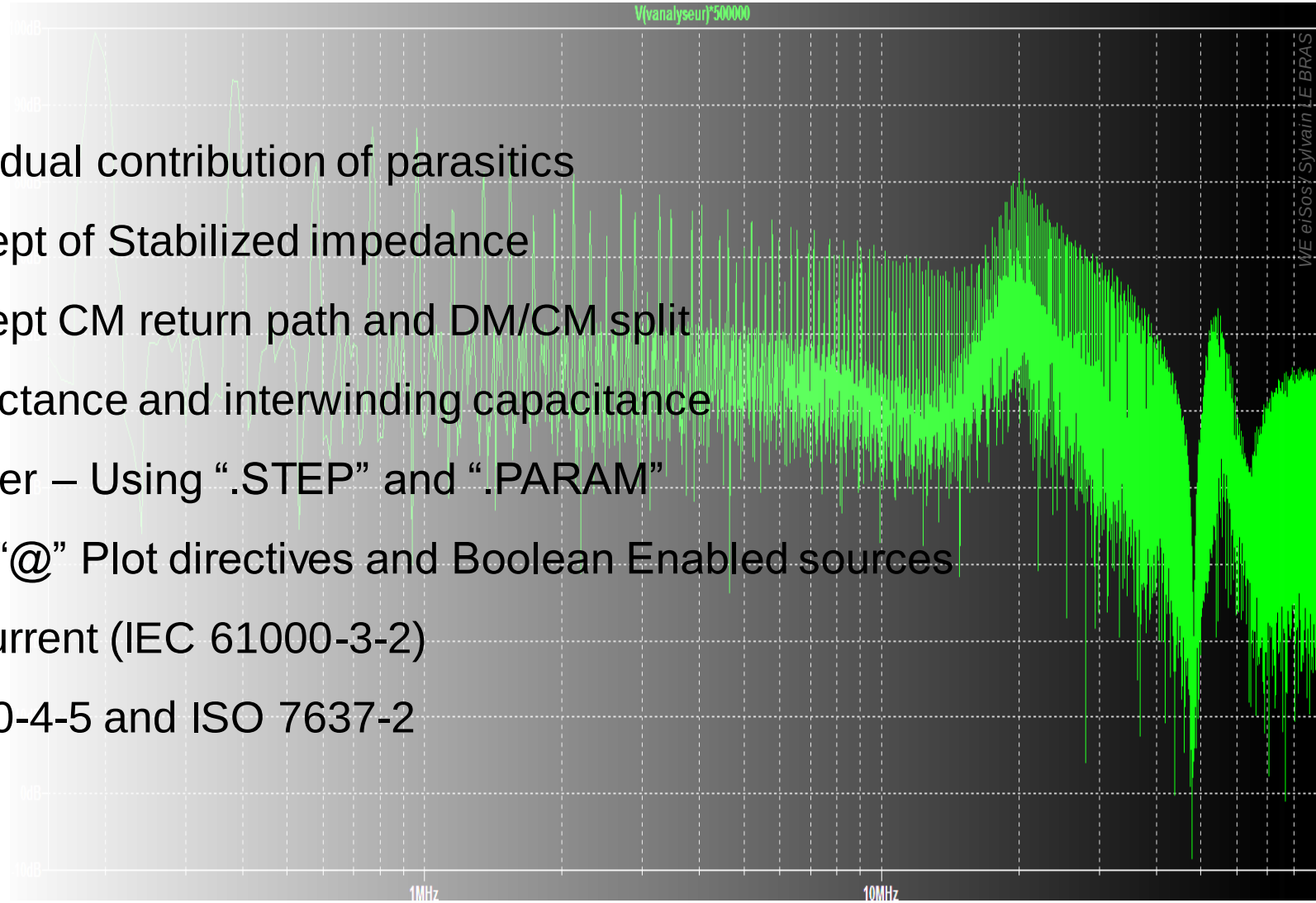


Anticipate EMC with LTSpice

Using LTSPICE and Redexpert to check power supply designs

- **Available examples**

1. Output ripple of a Buck – Individual contribution of parasitics
2. Noise at Input of Buck – Concept of Stabilized impedance
3. Noise at Input of Buck – Concept CM return path and DM/CM split
4. Flyback converter – Stray inductance and interwinding capacitance
5. Brushless DC motor and inverter – Using “.STEP” and “.PARAM”
6. Evaluation of filter response – “@” Plot directives and Boolean Enabled sources
7. Power Factor and Harmonic current (IEC 61000-3-2)
8. Surges according to IEC 61000-4-5 and ISO 7637-2



Setup

Getting the tools ready

LINEAR TECHNOLOGY | NOW PART OF ANALOG DEVICES

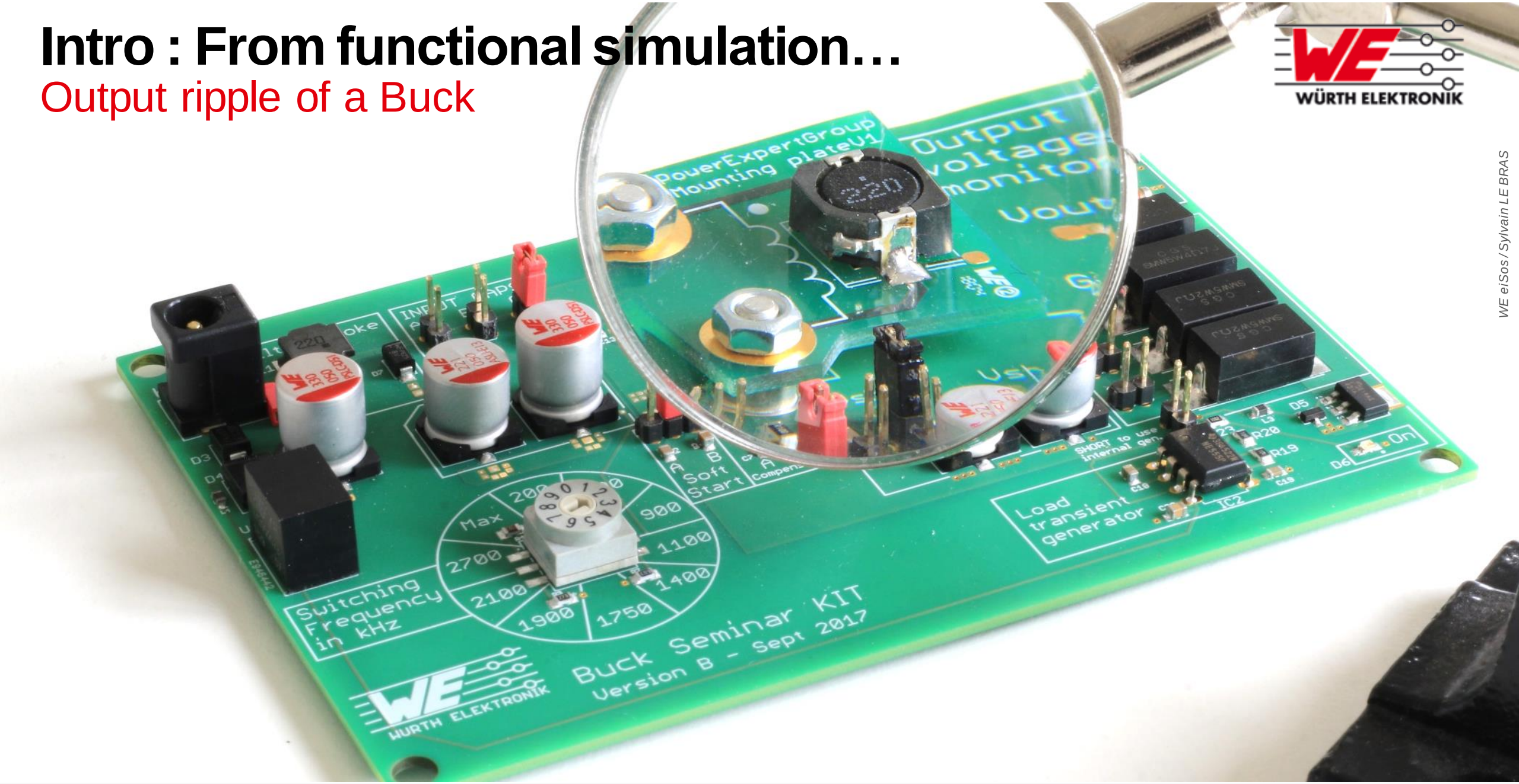
https://www.analog.com/en/design-center/design-tools-and-calculators/ltspice-simulator.html

REDEXPERT

https://www.we-online.com/redexpert

Intro : From functional simulation…

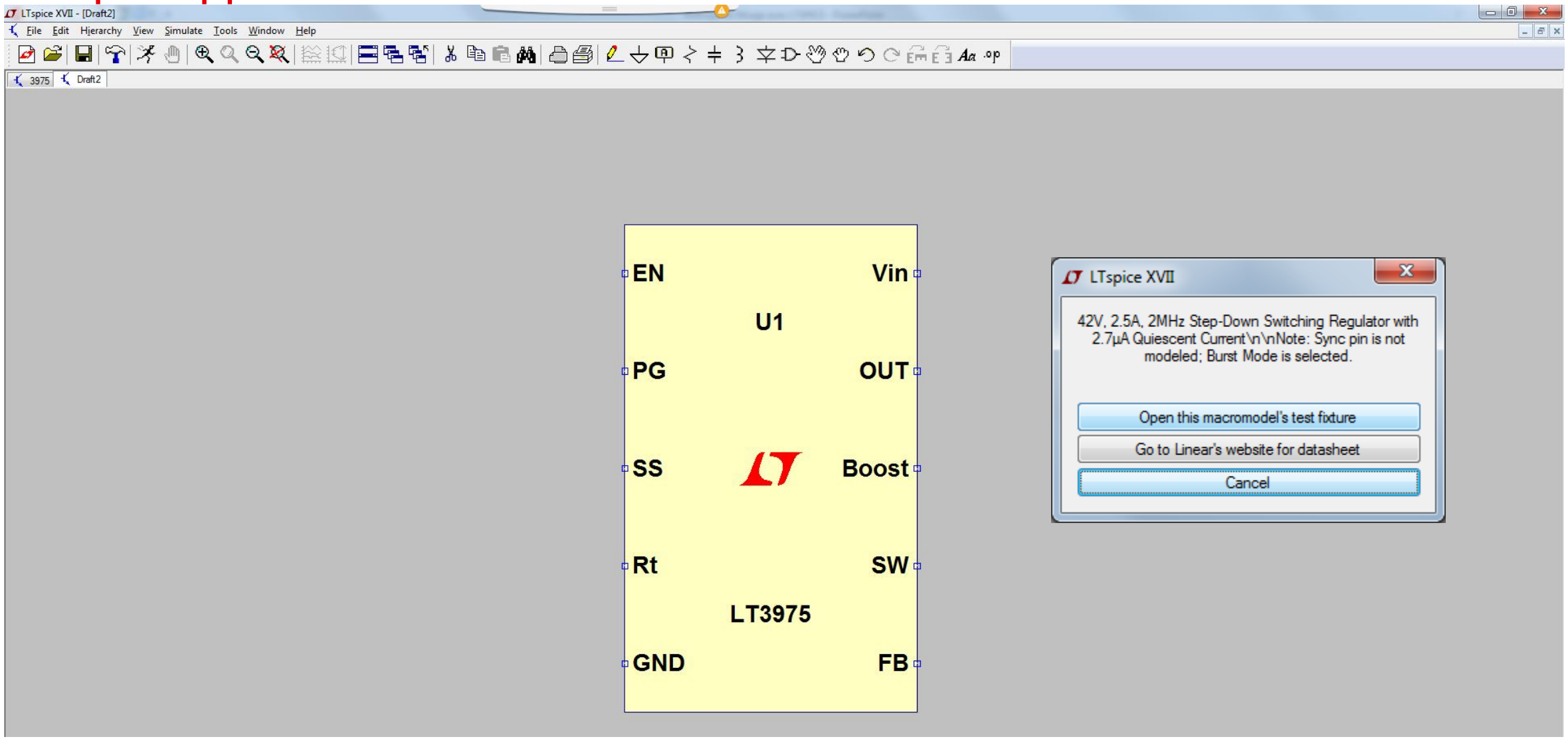
Output ripple of a Buck



WE eiSos / Sylvain LE BRAS

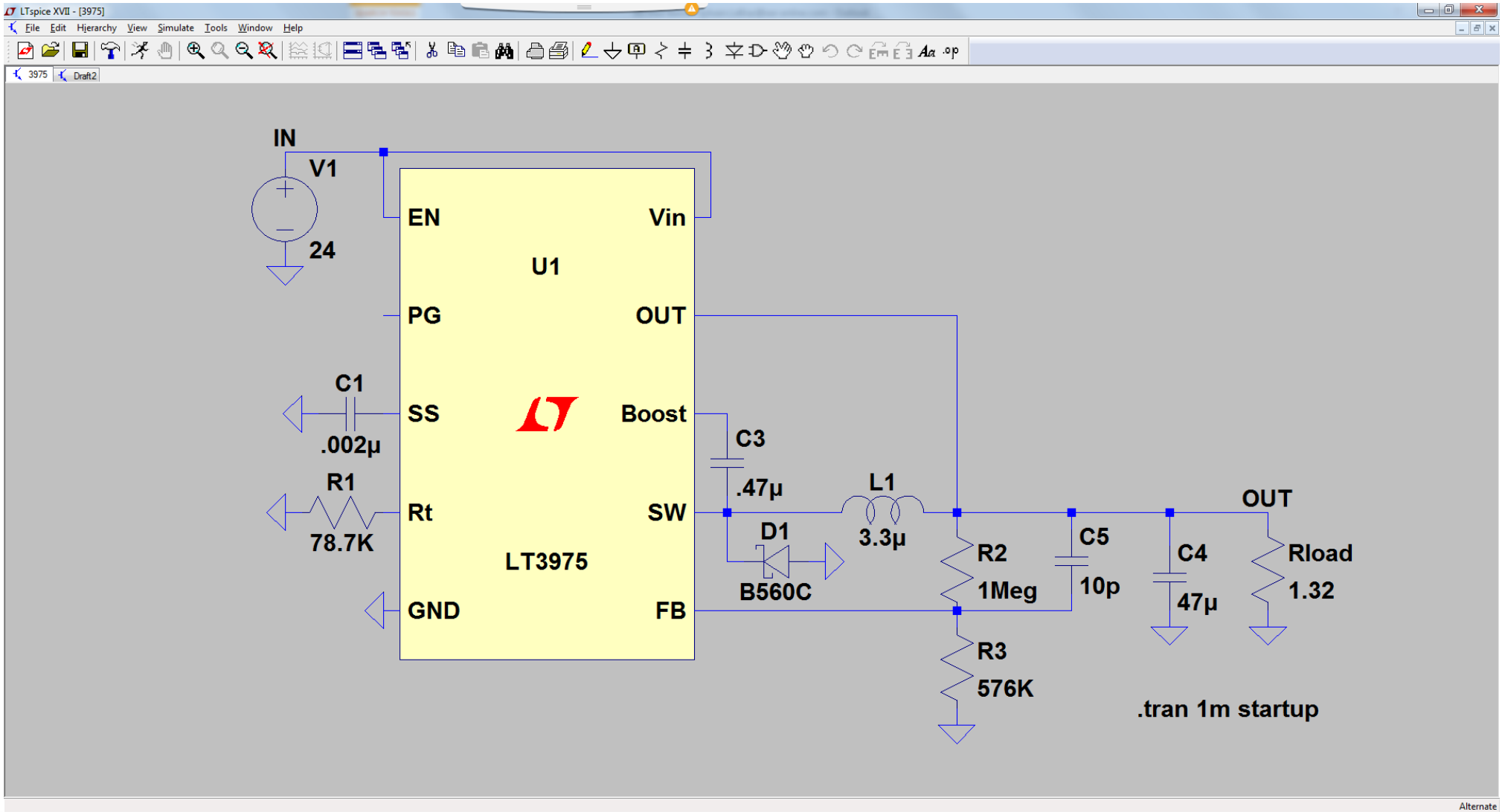
Intro : From functional simulation…

Output ripple of a Buck



Intro : From functional simulation…

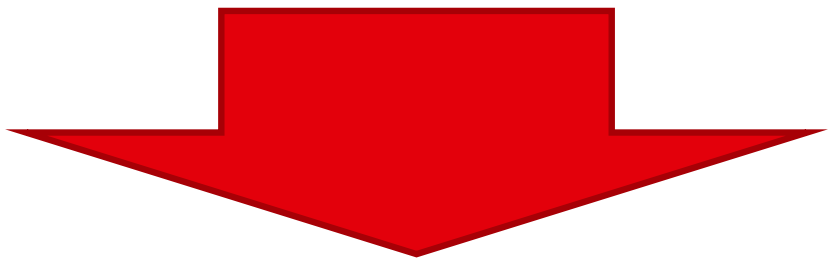
Output ripple of a Buck (without the “hardcore mathematics”)



Output ripple of a Buck

Hardcore maths ?

$$V = R \cdot I$$

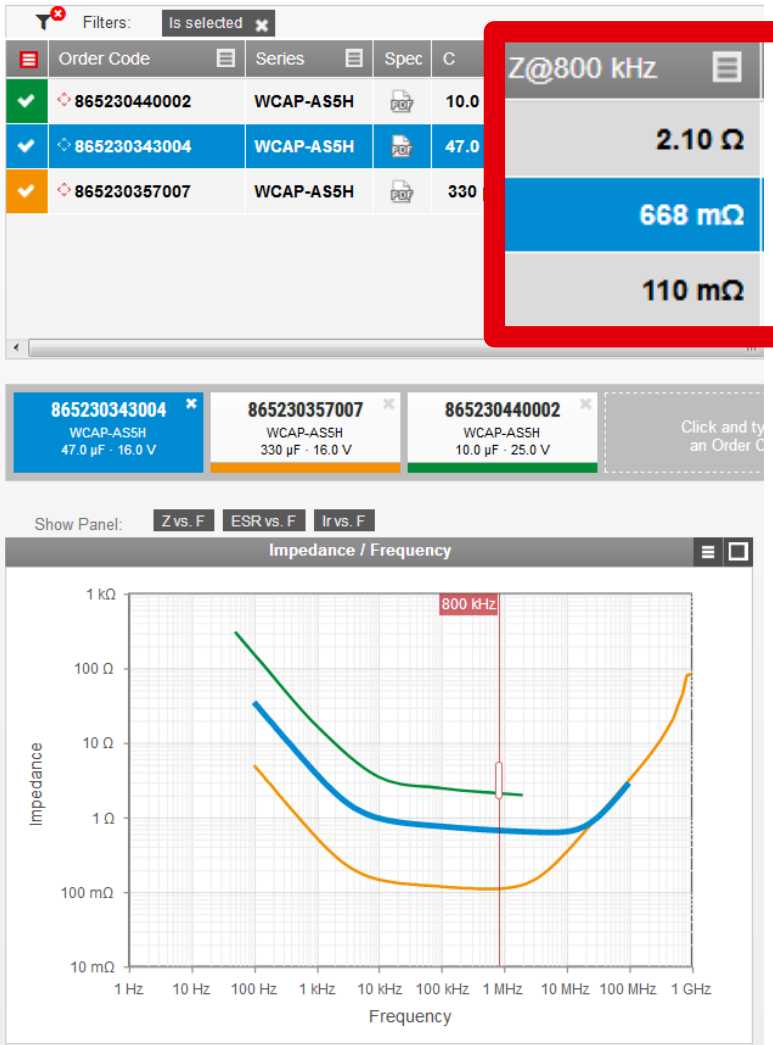


$$\Delta V = Z_C \cdot \Delta I_L$$

Output ripple of a Buck

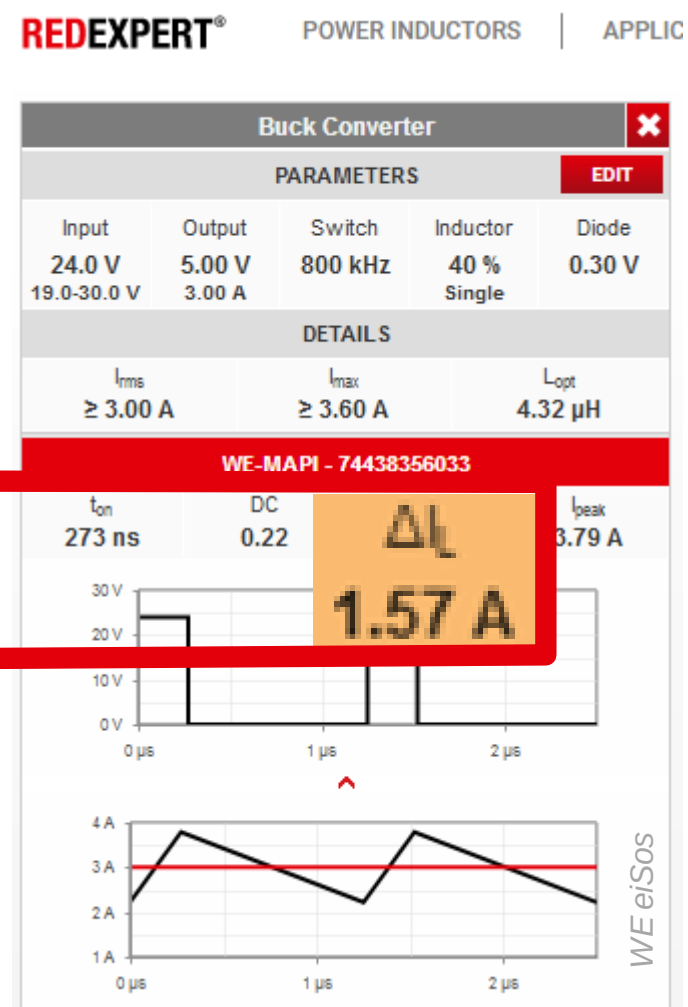
Redexpert : an ode to laziness

REDEXPERT® ALUMINIUM ELECTROLYTIC CAPACITORS | APPLICATIONS



Z_C

ΔI_L



Output ripple of a Buck

Redexpert : an ode to laziness

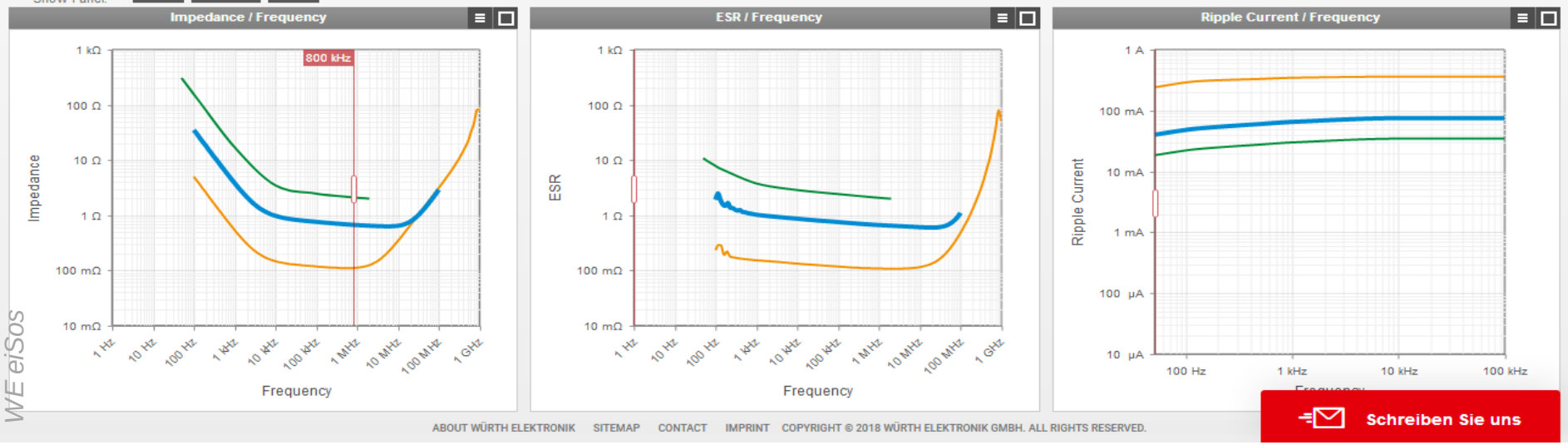
REDEXPERT® ALUMINIUM ELECTROLYTIC CAPACITORS | APPLICATIONS | HOW TO | SHARE ITEMS LE BRAS

Filters: Is selected 3 items

Order Code	Series	Sp...	C	V_R	Z@800 kHz	DF	Z_{max} @ 100kHz	I_{ripple} @Tmax°C 120Hz	I_{ripple} @T_{max} 100kHz	Description	I_{leak}
865230440002	WCAP-AS5H		10.0 µF	25.0 V	2.10 Ω	< 16 %		23.0 mA		ASDB055100M025DVCTAE000	3.00
865230343004	WCAP-AS5H		47.0 µF	16.0 V	668 mΩ	< 22 %		50.0 mA		ASDD055470M016DVCTBE000	7.52
865230357007	WCAP-AS5H		330 µF	16.0 V	110 mΩ	< 22 %		300 mA		ASDF105331M016DVCTEE000	52.8

865230343004 WCAP-AS5H 47.0 µF · 16.0 V | 865230357007 WCAP-AS5H 330 µF · 16.0 V | 865230440002 WCAP-AS5H 10.0 µF · 25.0 V | Click and type or drop an Order Code here | Add to Cart | More...

Show Panel: Z vs. F | ESR vs. F | Ir vs. F



ABOUT WÜRTH ELEKTRONIK SITEMAP CONTACT IMPRINT COPYRIGHT © 2018 WÜRTH ELEKTRONIK GMBH. ALL RIGHTS RESERVED. Schreiben Sie uns

Link

Output ripple of a Buck

Redexpert : an ode to laziness

REDEXPERT® POWER INDUCTORS | APPLICATIONS | HOW TO | SHARE ITEMS LE BRAS

Buck Converter

PARAMETERS EDIT

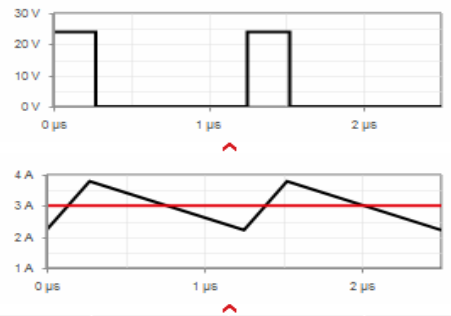
Input	Output	Switch	Inductor	Diode
24.0 V 19.0-30.0 V	5.00 V 3.00 A	800 kHz	40 % Single	0.30 V

DETAILS

I_{rms}	I_{max}	L_{opt}
≥ 3.00 A	≥ 3.60 A	4.32 µH

WE-MAPI - 74438356033

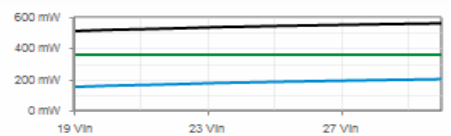
t_{on}	DC	ΔI_L	I_{peak}
273 ns	0.22	1.57 A	3.79 A



AC Losses	DC Losses	Total Losses	ΔT_{TOT}
179 mW	359 mW	538 mW	42.0 K

P vs. V_{in} | P vs. f_{sw} | P vs. I_{out}

P vs. V_{in}



Filters: Type = Single | I_R ≥ 3.00 A | I_{sat} ≥ 3.60 A | 3.02 µH ≤ L_0 ≤ 5.62 µH — 100 / 160 items

Order Code	Series	Size	Sp...	Type	L_0	$R_{DC,typ}$	I_R	I_{sat}	P_{AC}	P_{DC}	P_T
74438356033	WE-MAPI	4020		Single	3.30 µH	39.9 mΩ	3.60 A	5.50 A	179 mW	359 mW	5
74438357047	WE-MAPI	4030		Single	4.70 µH	39.9 mΩ	3.90 A	6.40 A	102 mW	359 mW	4
74438357056	WE-MAPI	4030		Single	5.60 µH	46.5 mΩ	3.60 A	6.00 A	94.9 mW	418 mW	5
744071039	WE-TPC	8043		Single	3.90 µH	13.0 mΩ	4.90 A	4.50 A	241 mW	117 mW	3
744071047	WE-TPC	8043		Single	4.70 µH	17.0 mΩ	4.80 A	4.30 A	200 mW	153 mW	3
744071056	WE-TPC	8043		Single	5.60 µH	20.0 mΩ	4.00 A	4.00 A	168 mW	180 mW	3

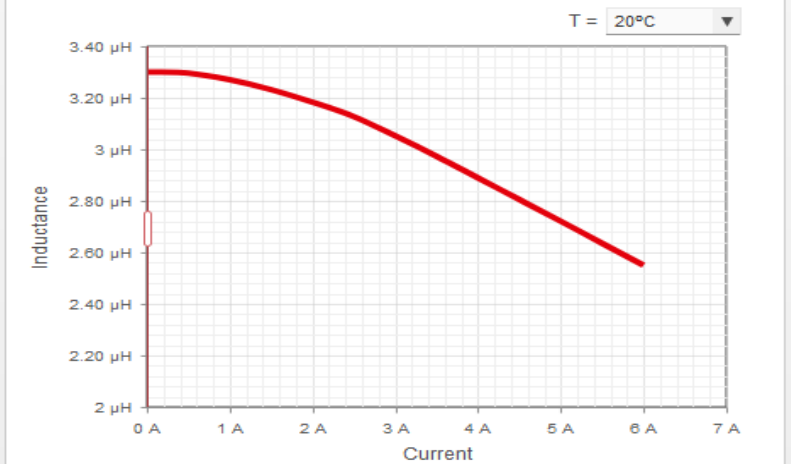
Click and type or drop an Order Code here

Add to Cart

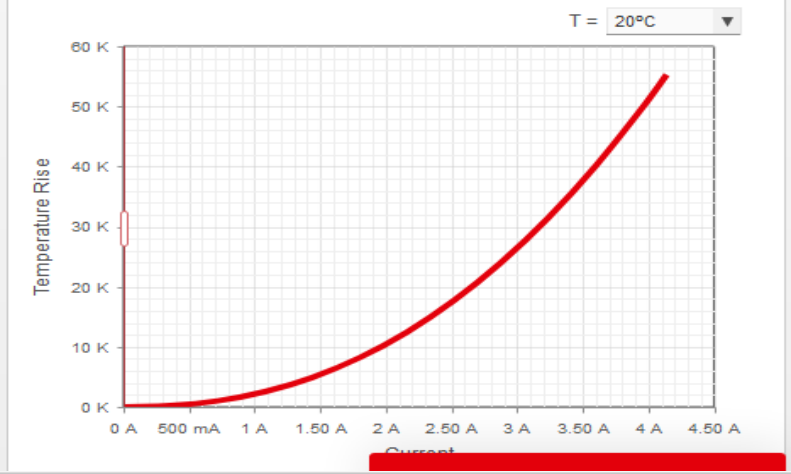
More...

Show Panel: L vs. I(T) | K vs. I(T)

Inductance / DC Current (Ambient Temperature)



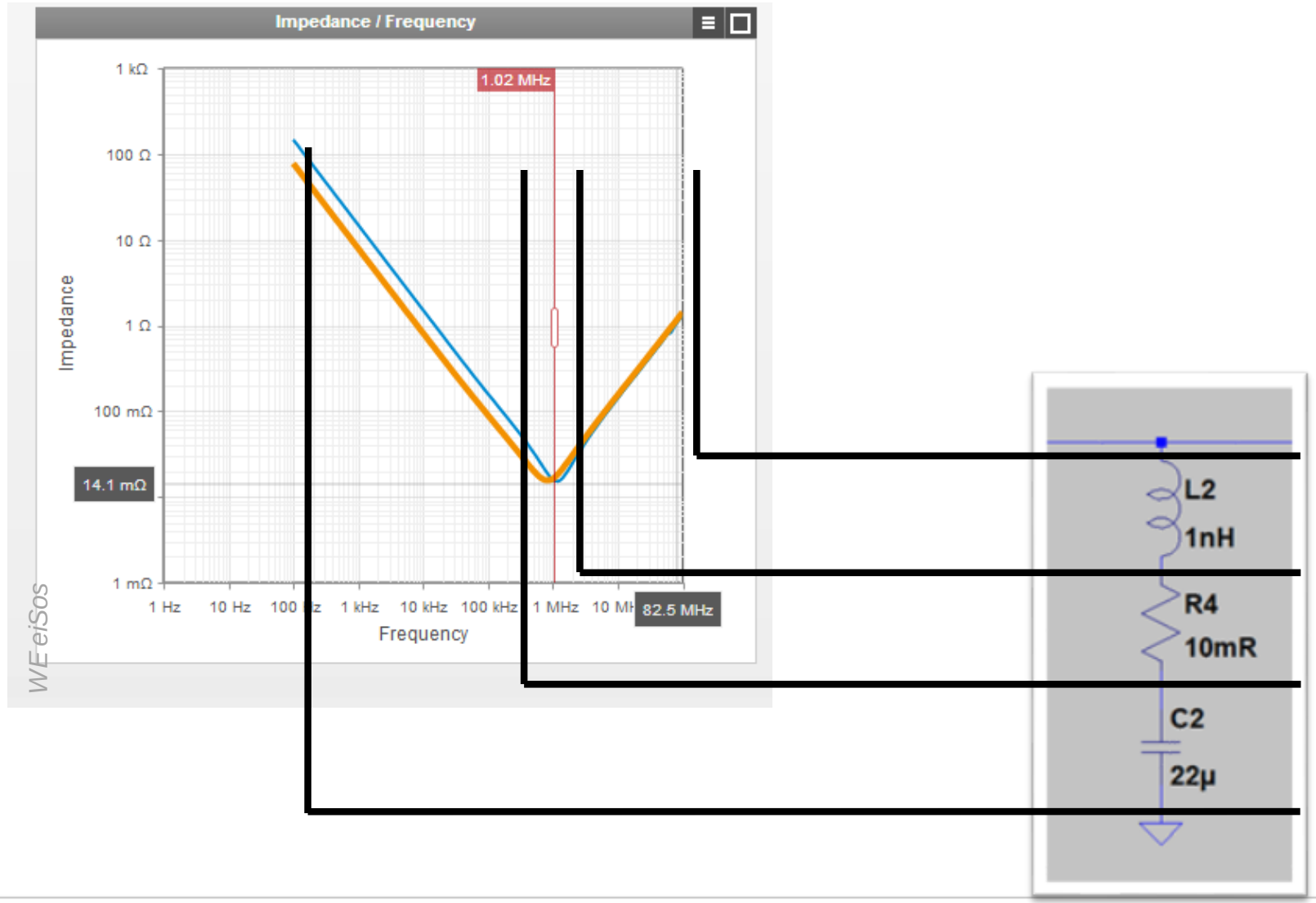
Temperature Rise / DC Current (Ambient Temperature)



- Link

Output ripple of a Buck

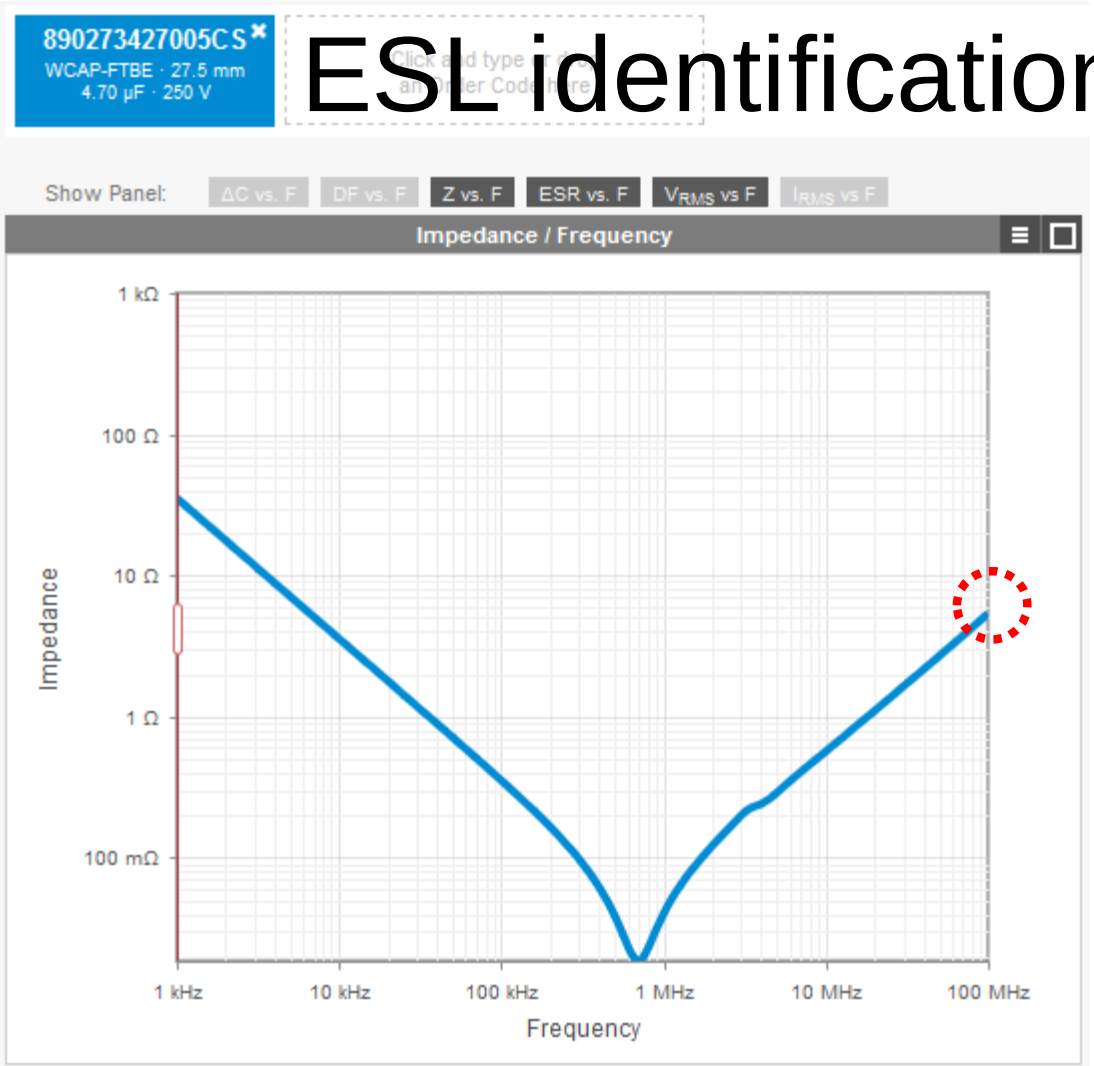
Extracting EMC accurate data from REDEXPERT

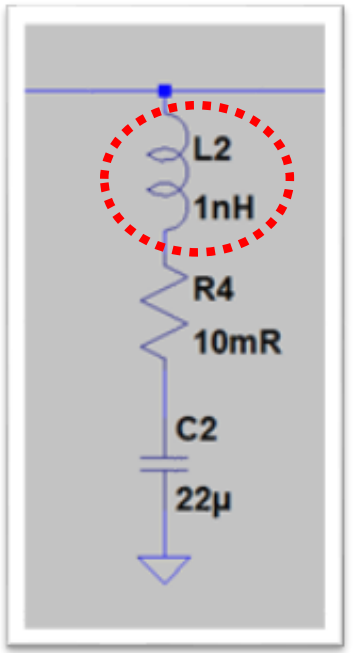


Output ripple of a Buck

Extracting EMC accurate data from REDEXPERT

ESL identification





$$|Z_L| = L\omega$$

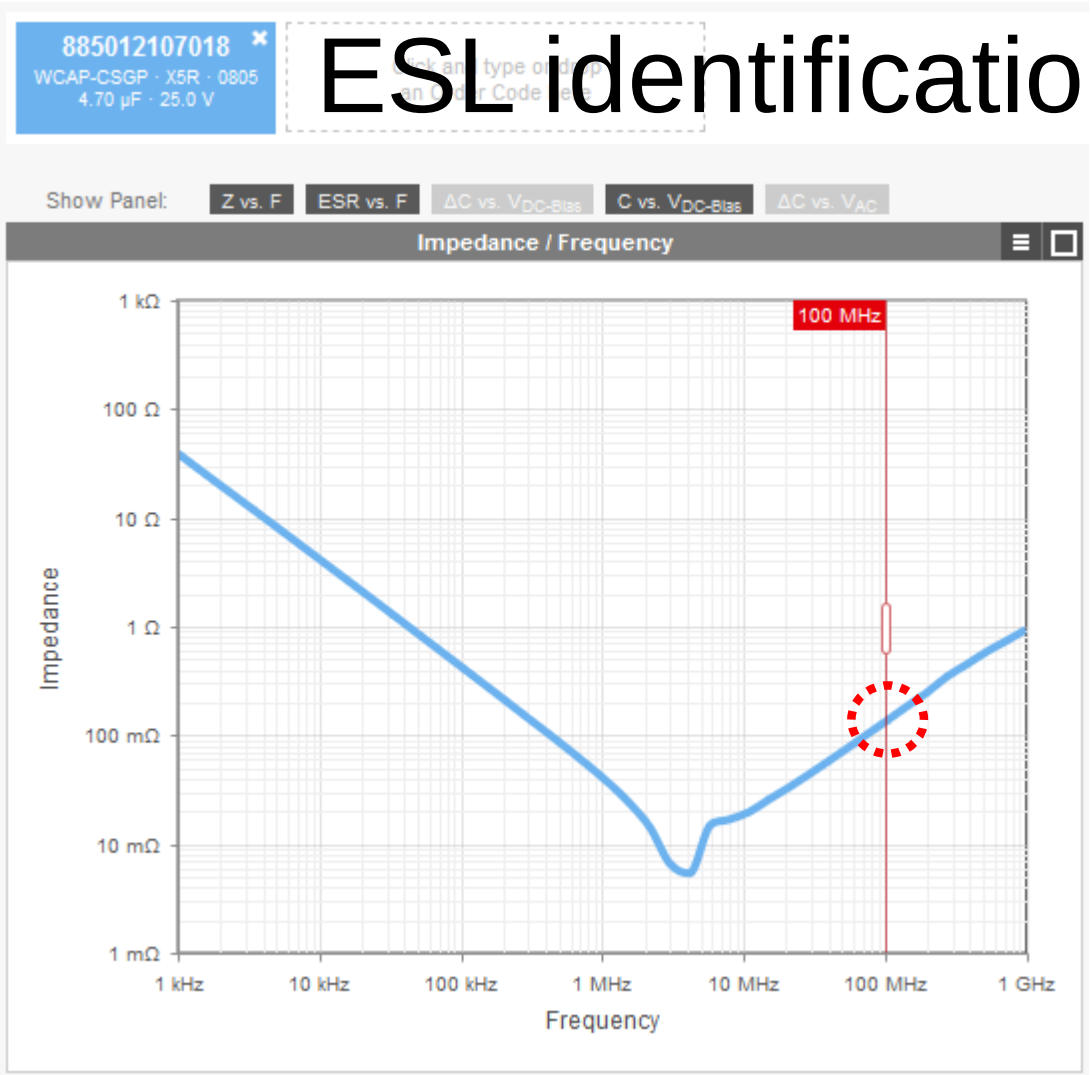
$$\frac{Z_L}{\omega} = L$$

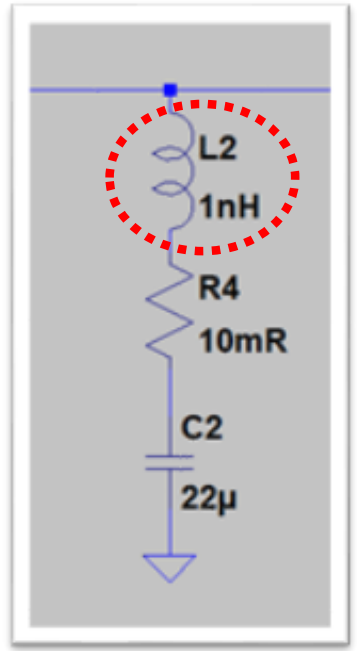
$$L = \frac{|Z_L|}{2\pi F} = \frac{5}{100 \times 10^6 \times 2\pi} \cong 8\ nH$$

Output ripple of a Buck

Extracting EMC accurate data from REDEXPERT

ESL identification





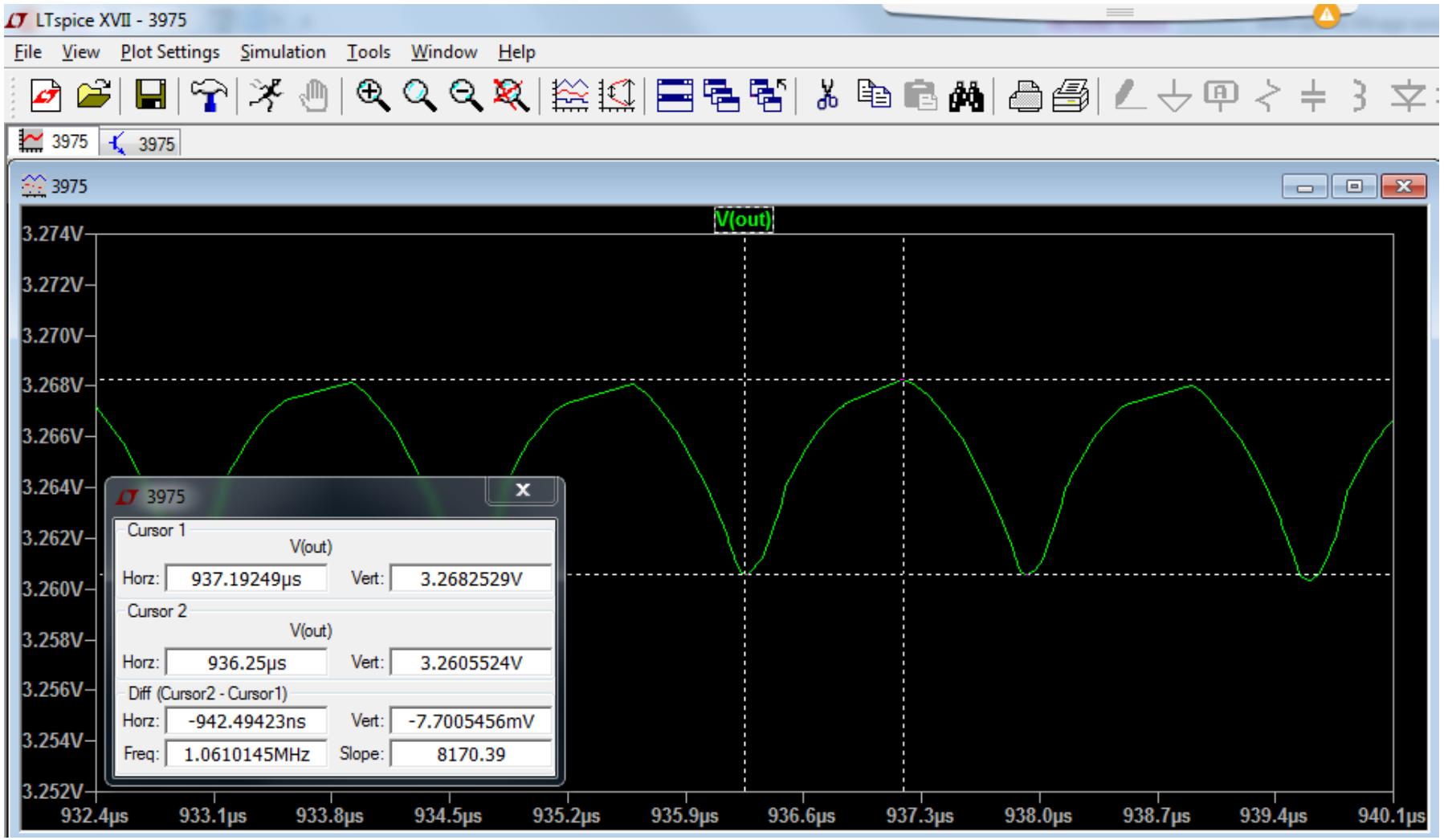
$$|Z_L| = L\omega$$

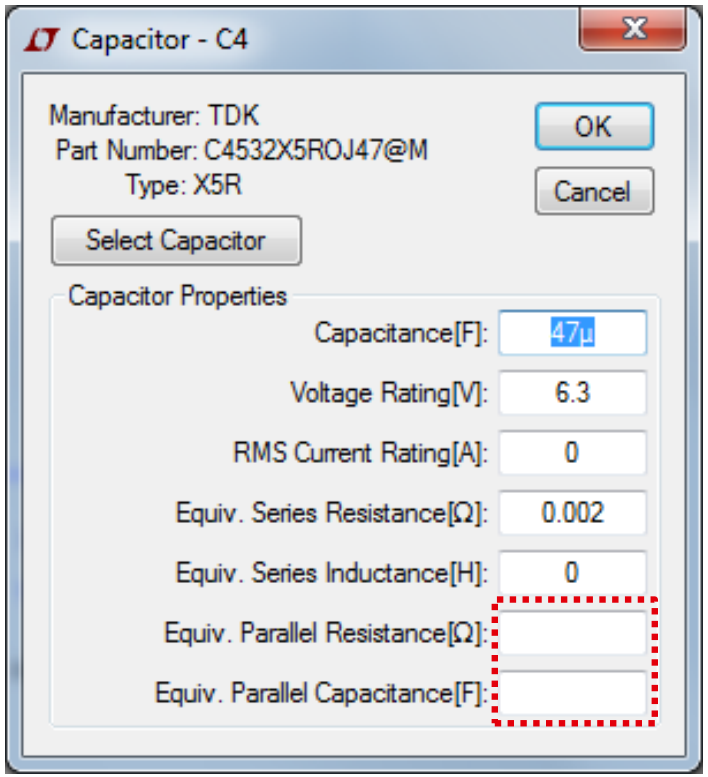
$$\frac{Z_L}{\omega} = L$$

$$L = \frac{|Z_L|}{2\pi F} = \frac{0{,}132}{100 \times 10^6 \times 2\pi} \cong 0.2\ nH$$

Output ripple of a Buck

Example of (non) EMC accurate impact on simulation



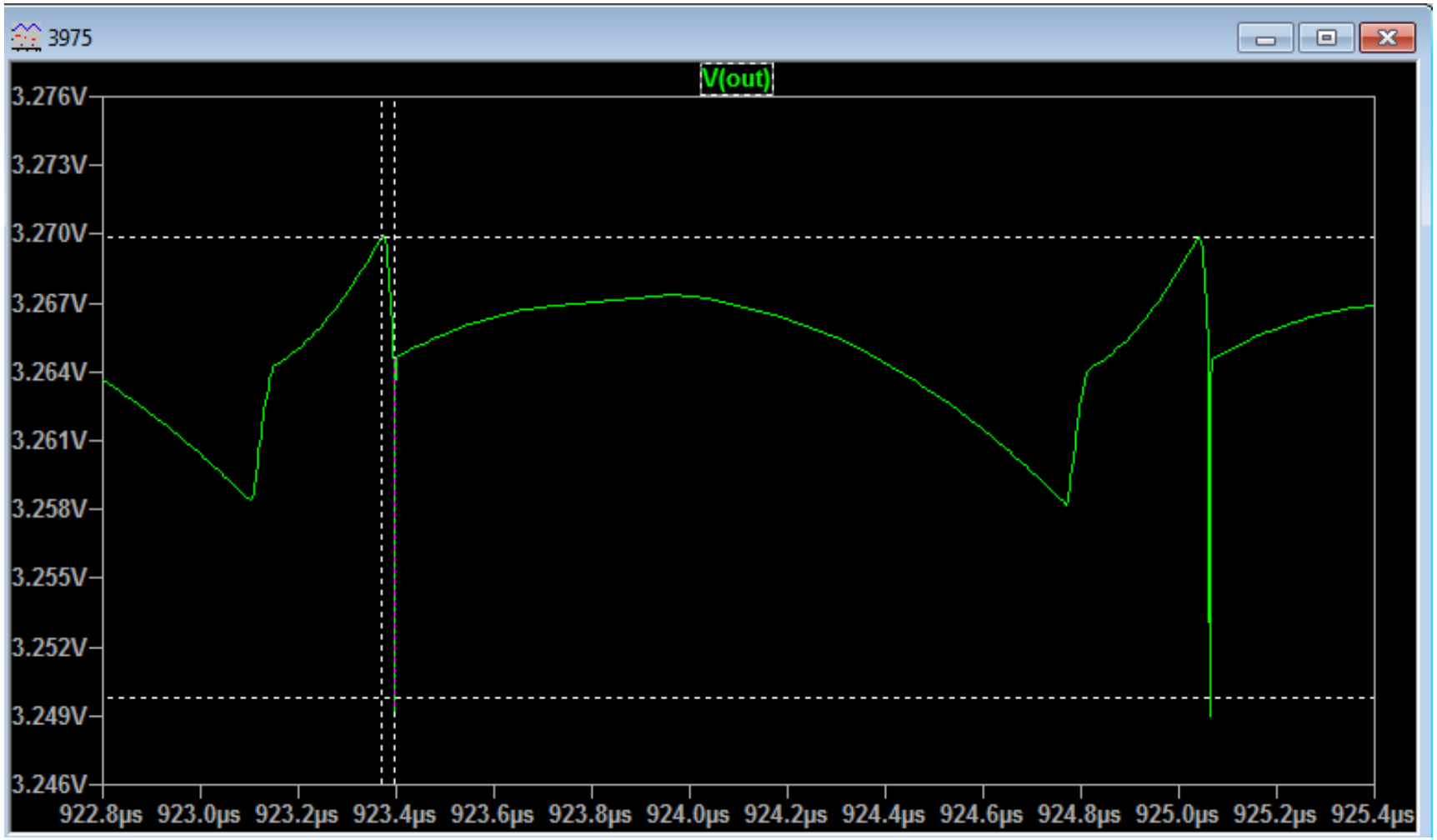


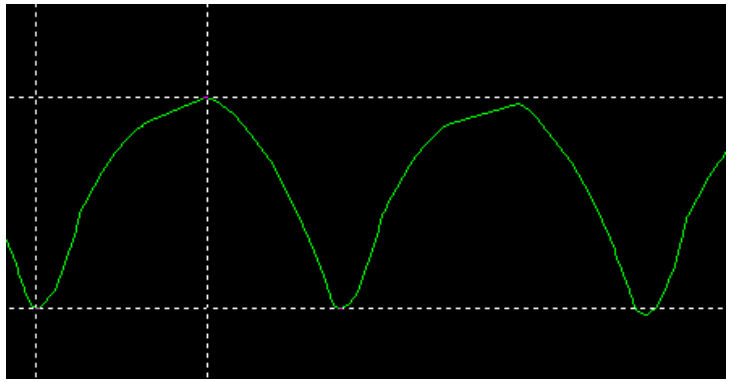
- ESR = 2 mOhms
- ESL = 0 nH
- DC bias

(DC ? Like don’t care ?)

Output ripple of a Buck

Example of (non) EMC accurate impact on simulation





Output ripple of a Buck

Example of EMC accurate simulation

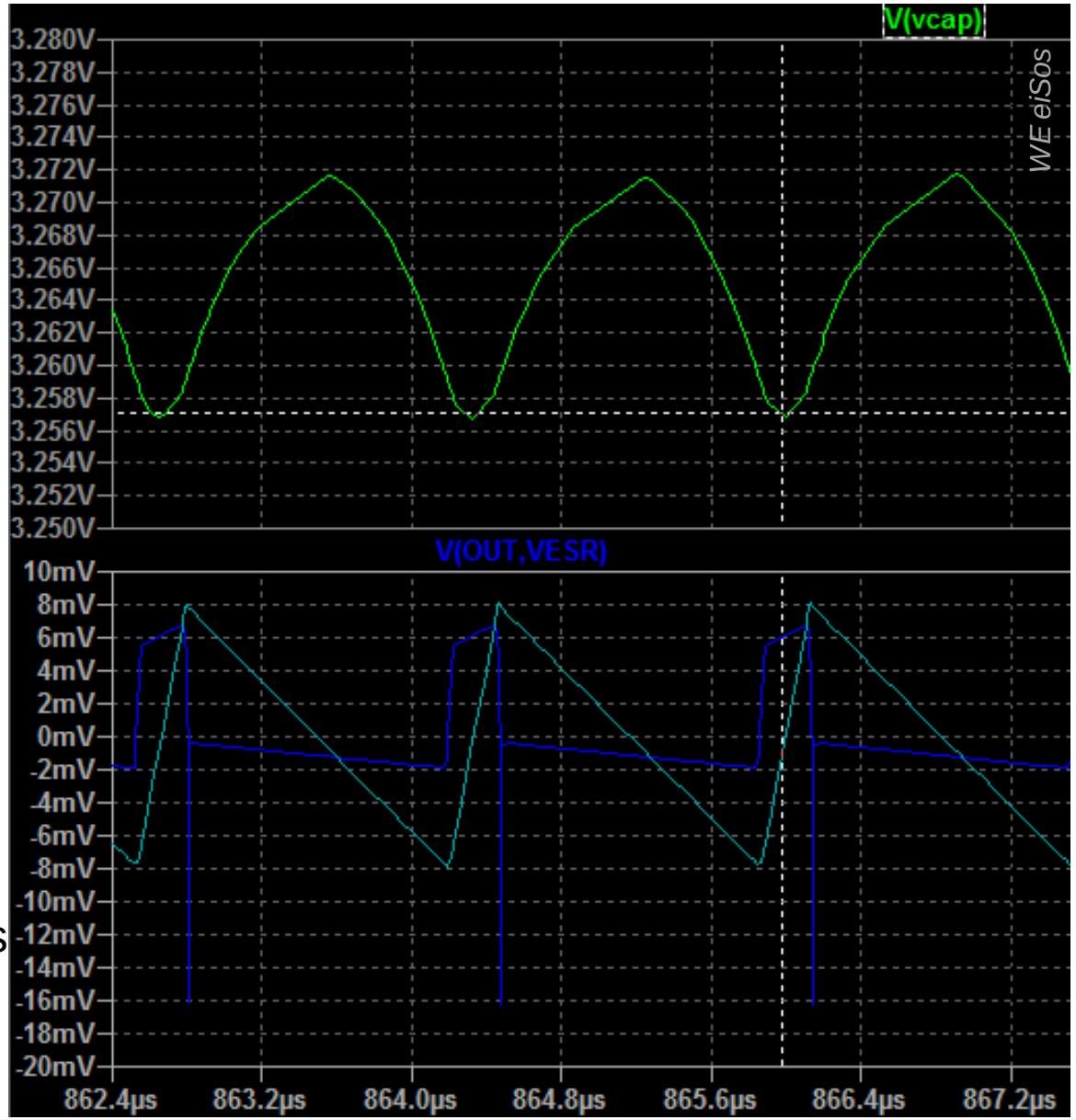
Charge and discharge of cap

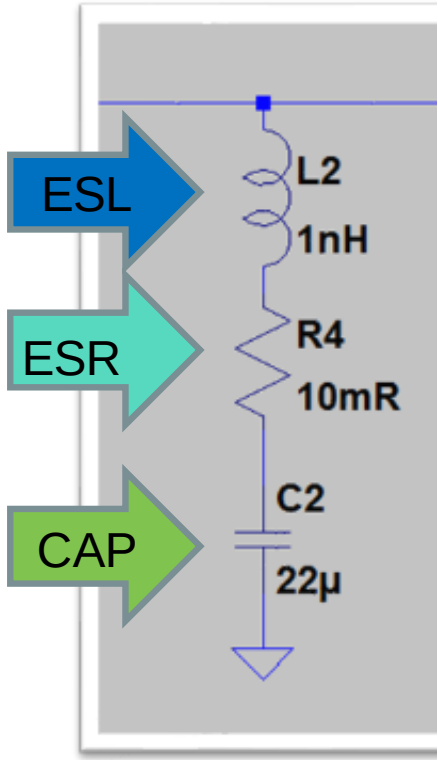
CAP $14\ mV_{p-p}$

ESR $16\ mV_{p-p}$

ESL $10\ mV_{p-p}$ at low frequencies

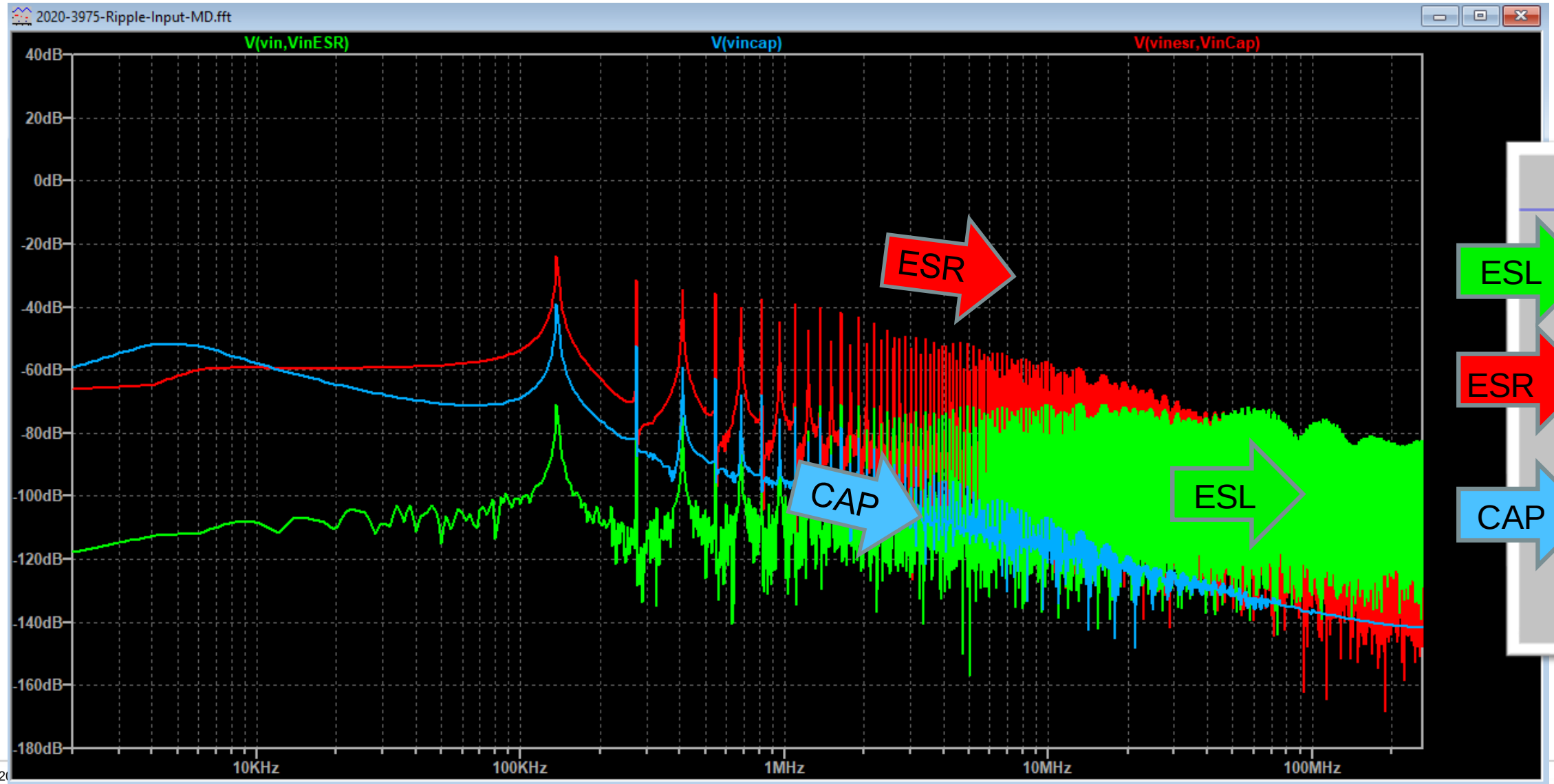
$25\ mV_{p-p}$ at high frequencies

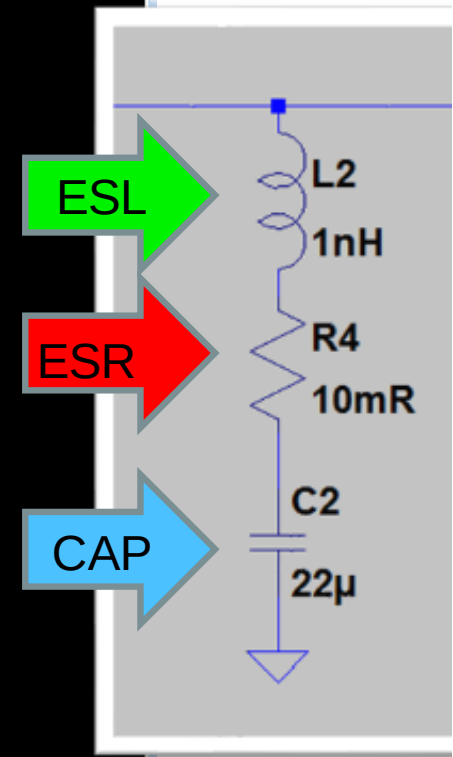




Capacitor ripple voltage example

ESR / ESL / CAP breakdown in frequency





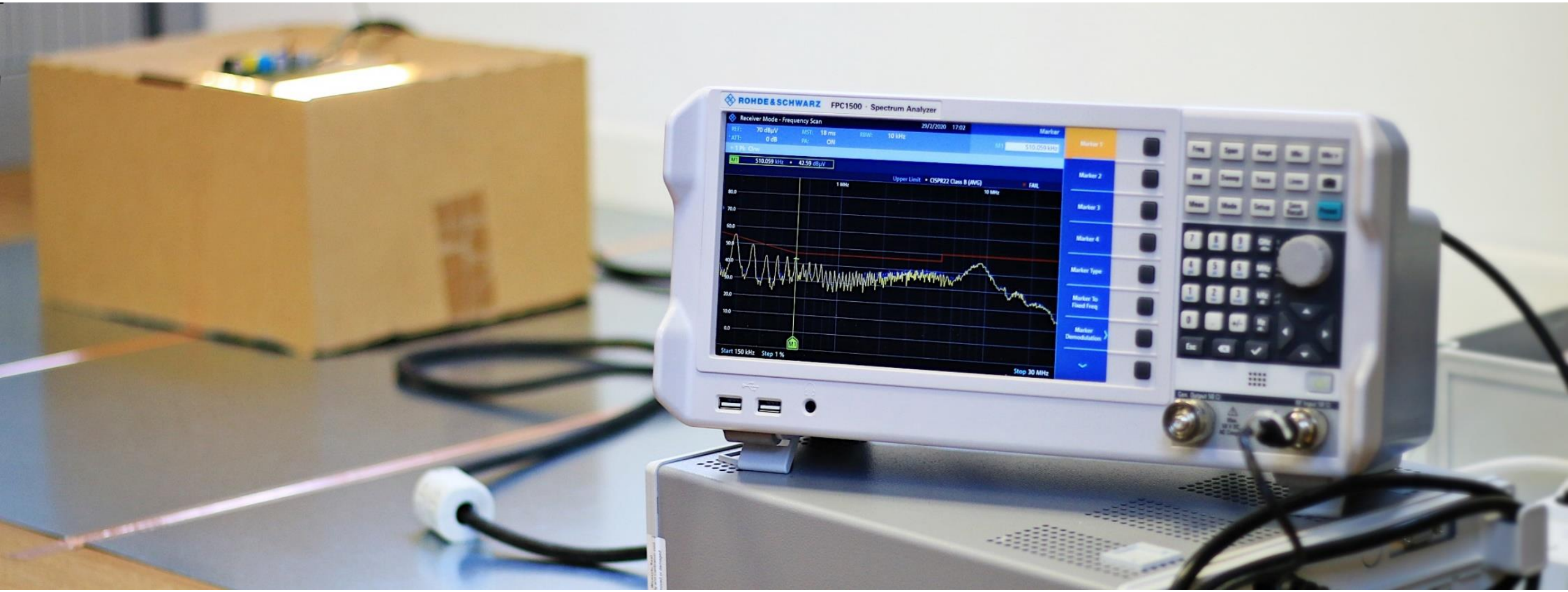
… To EMC simulation

The missing link

WE eiSos / Sylvain LE BRAS

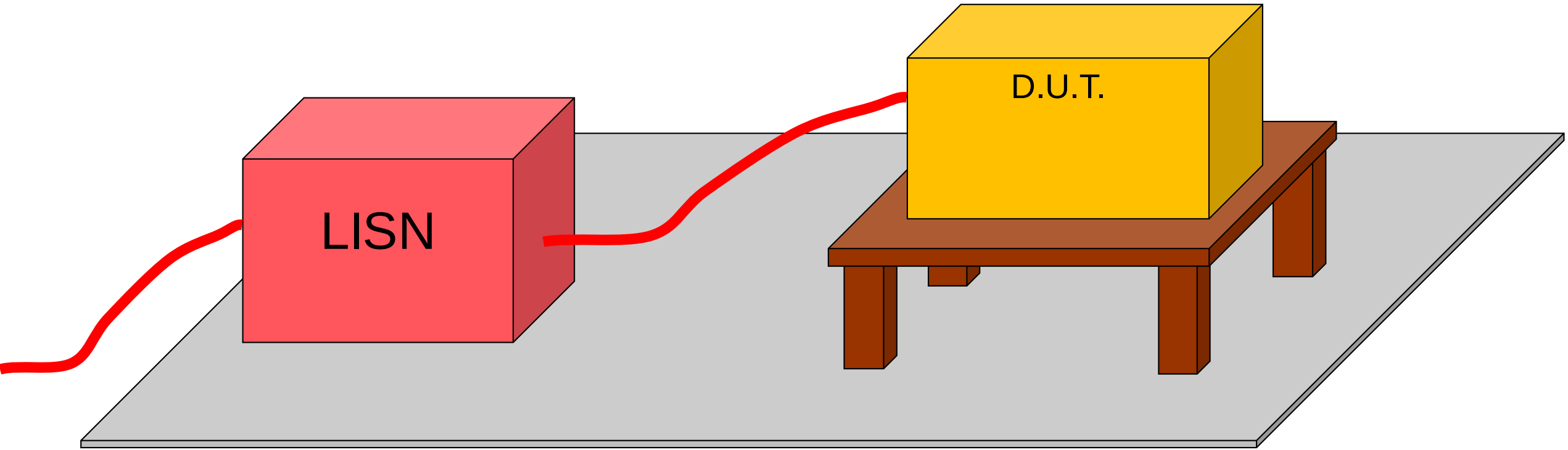
Enabling EMC accurate measurement in LTSpice

What is the keystone of conducted emissions ?



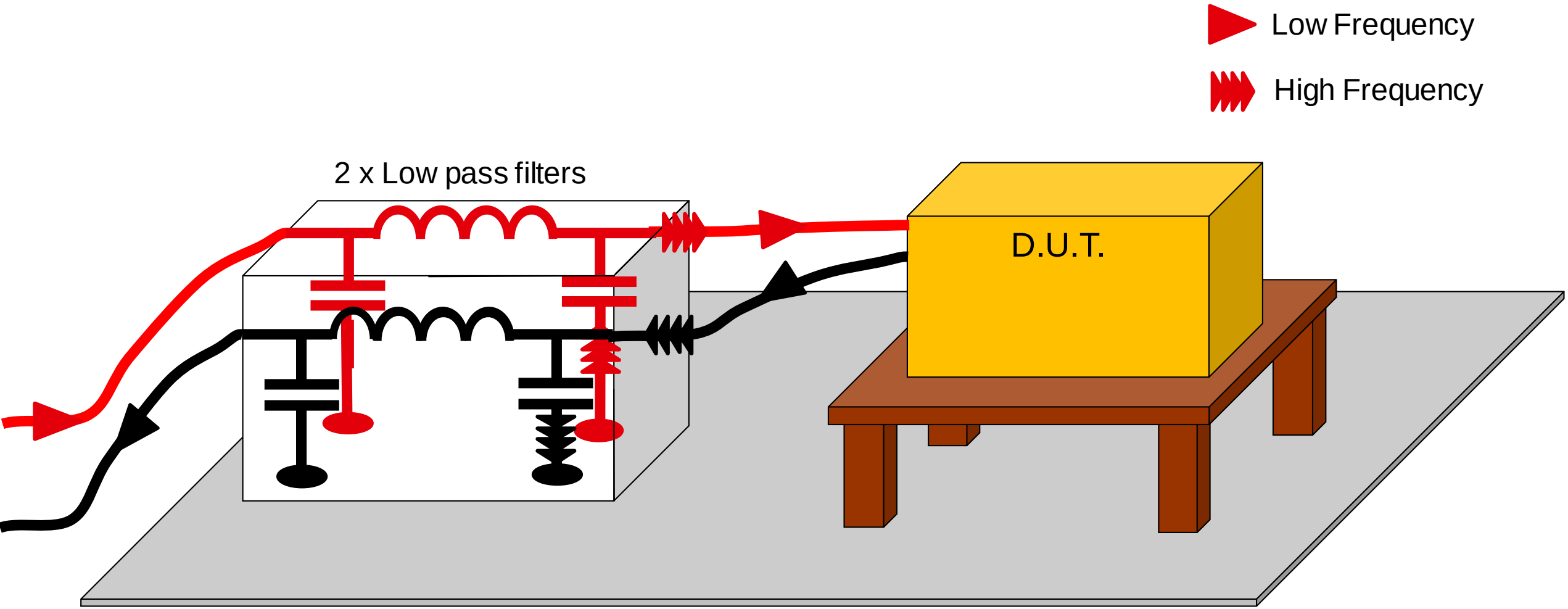
Enabling EMC accurate measurement in LTSpice

What is the keystone of conducted emissions ?



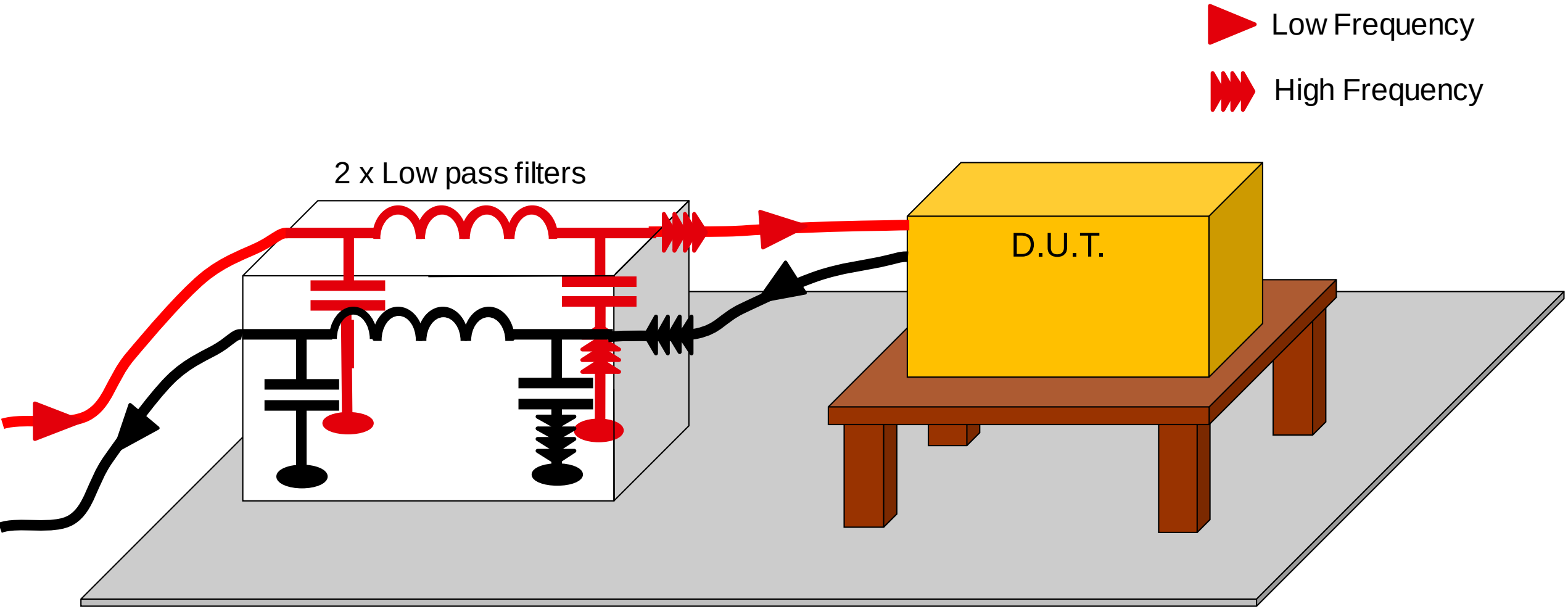
Enabling EMC accurate measurement in LTSpice

What is the keystone of conducted emissions ?



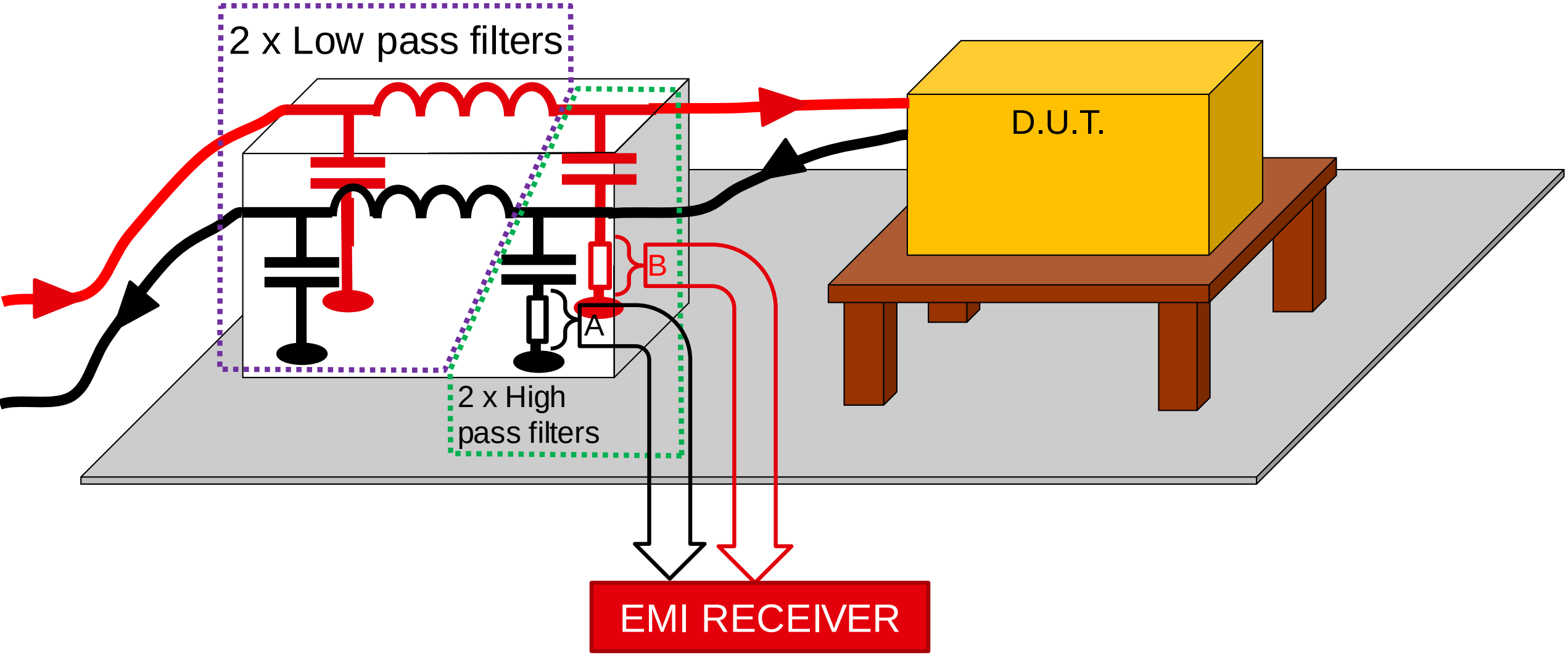
Enabling EMC accurate measurement in LTSpice

What is the keystone of conducted emissions ?



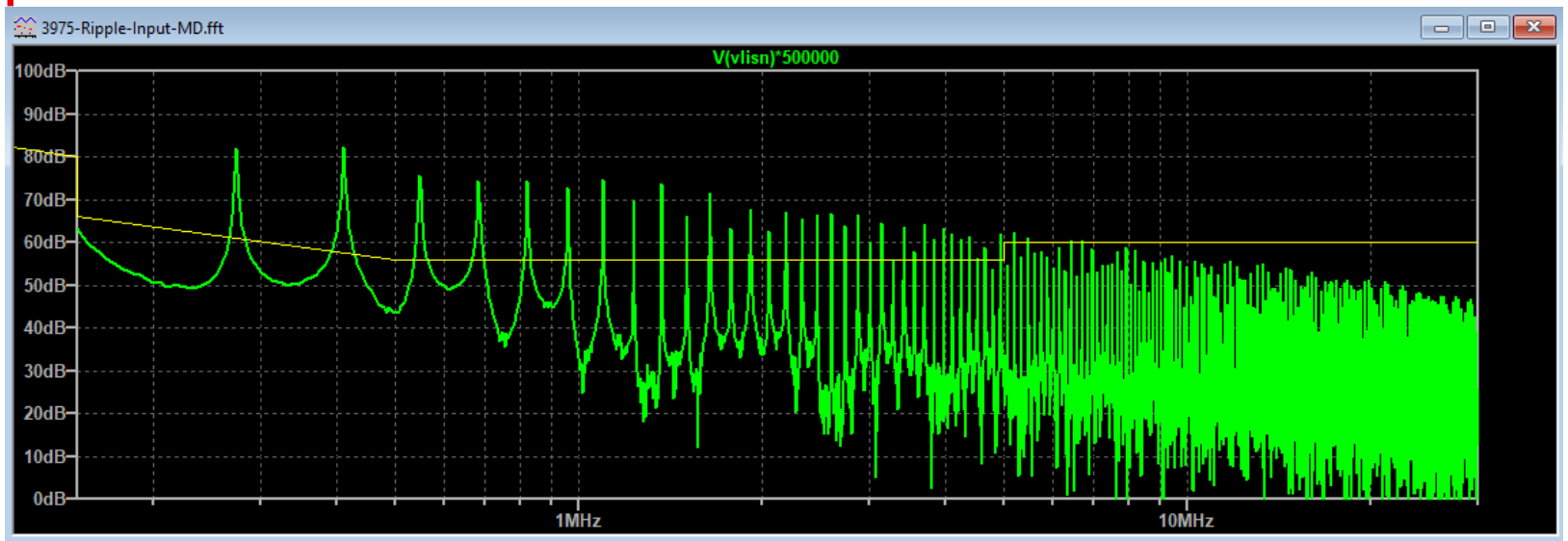
Enabling EMC accurate measurement in LTSpice

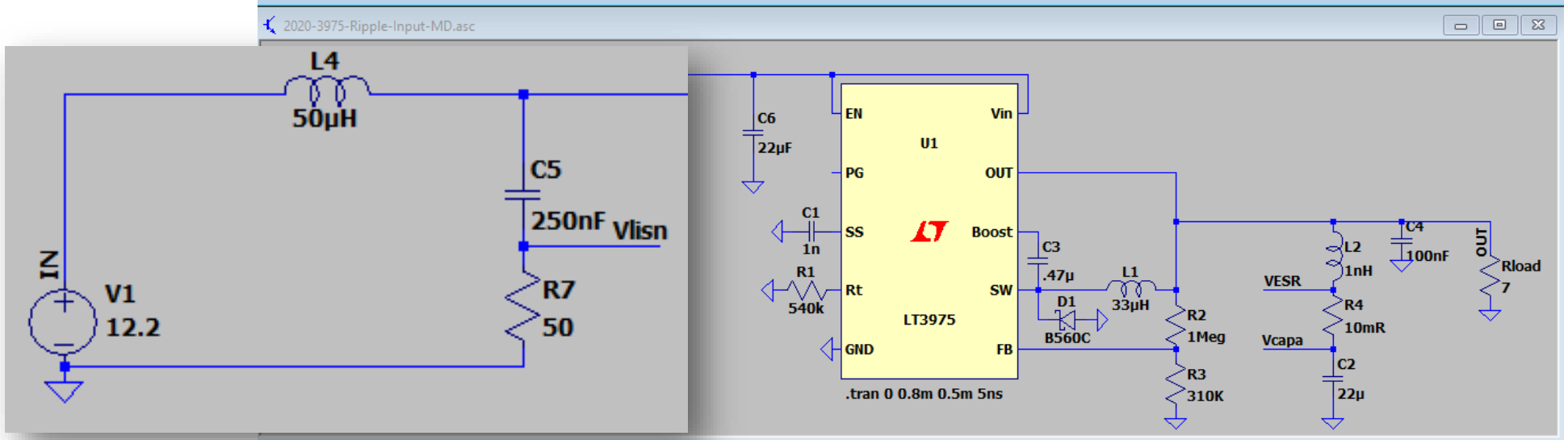
What is the keystone of conducted emissions ?



Enabling EMC accurate measurement in LTSpice

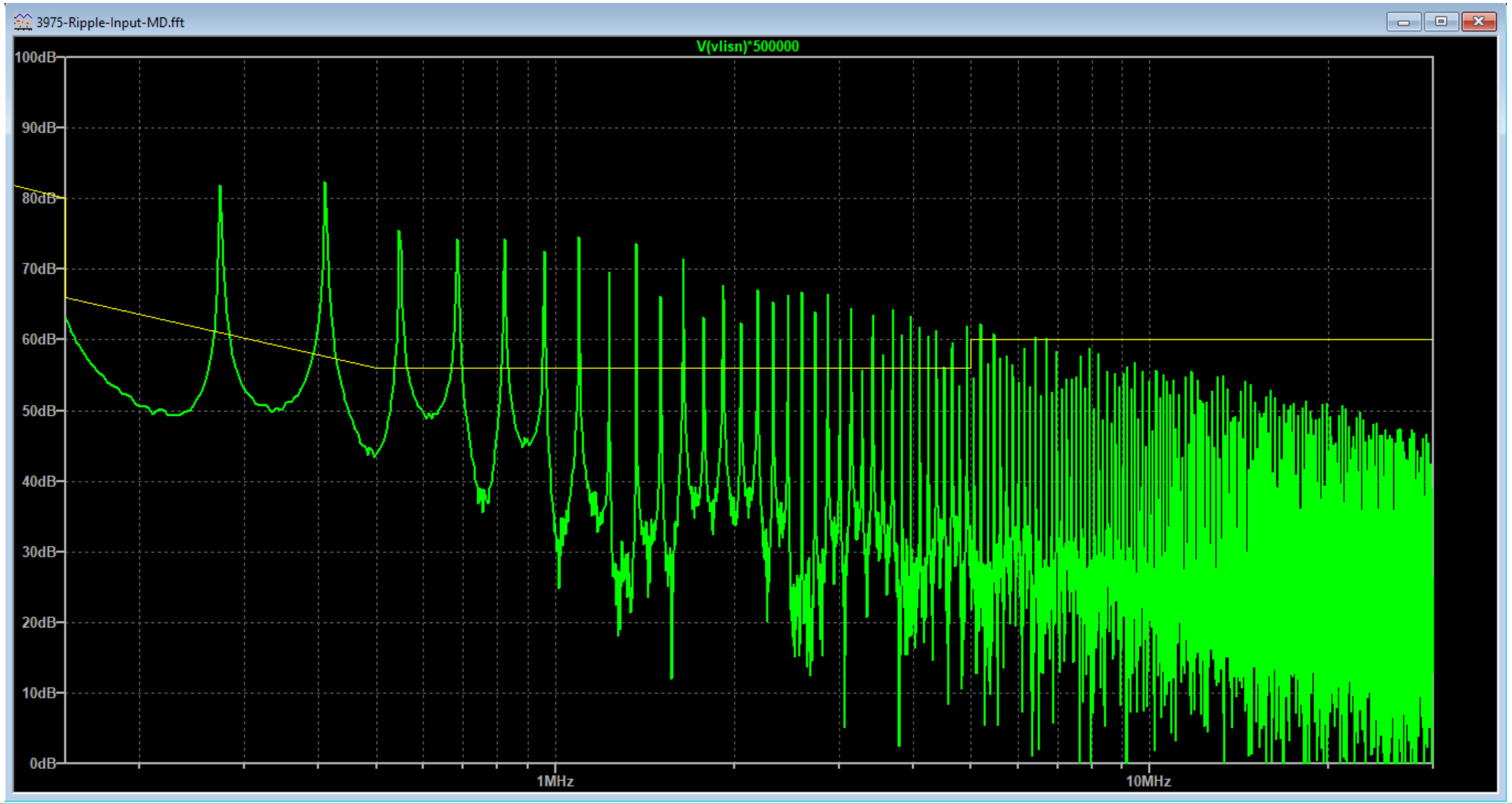
FFT with simplified LISN





Reality VS Simulation

FFT with simplified LISN



Reality VS Simulation

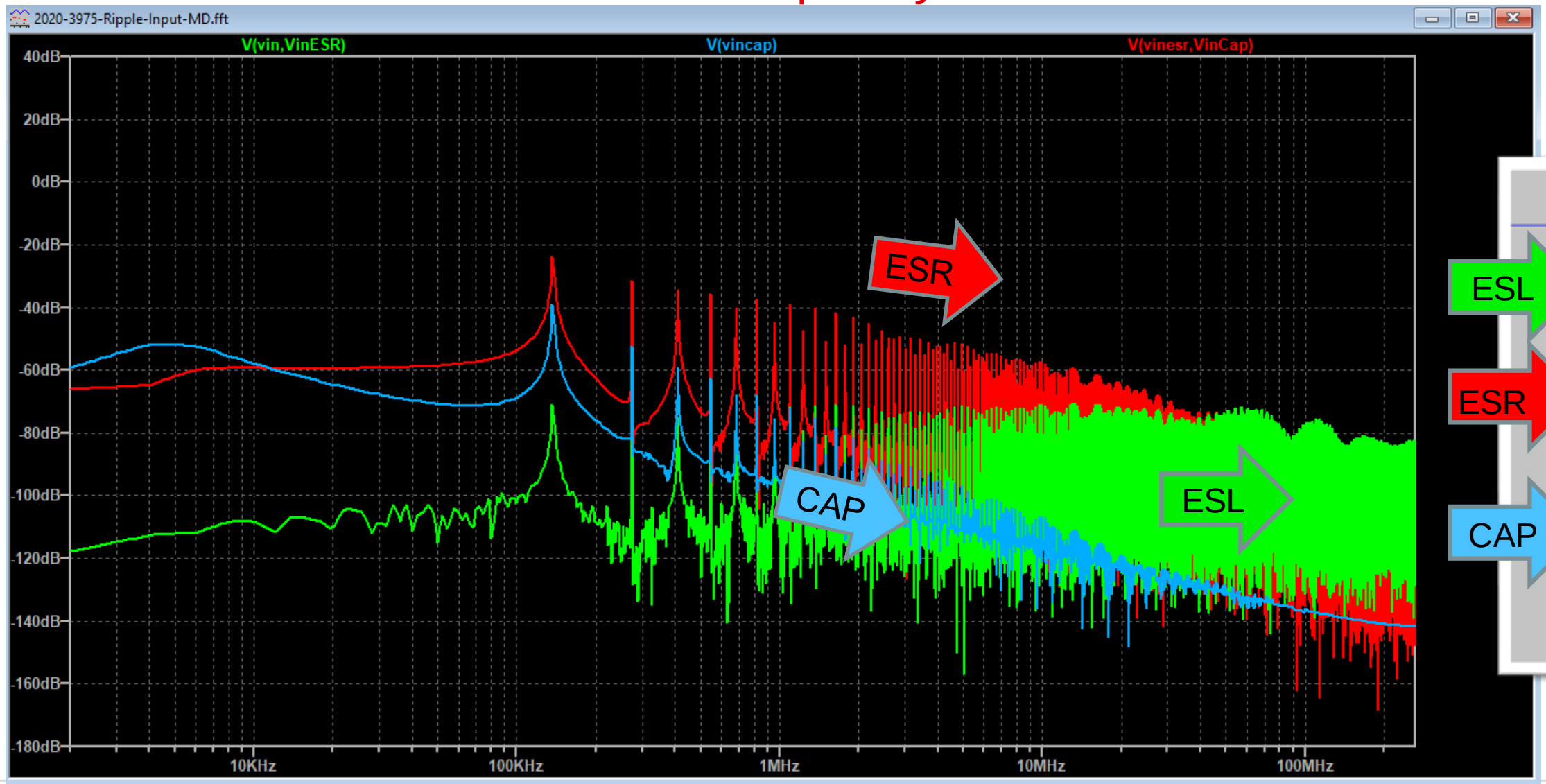
Conducted Emissions measurement

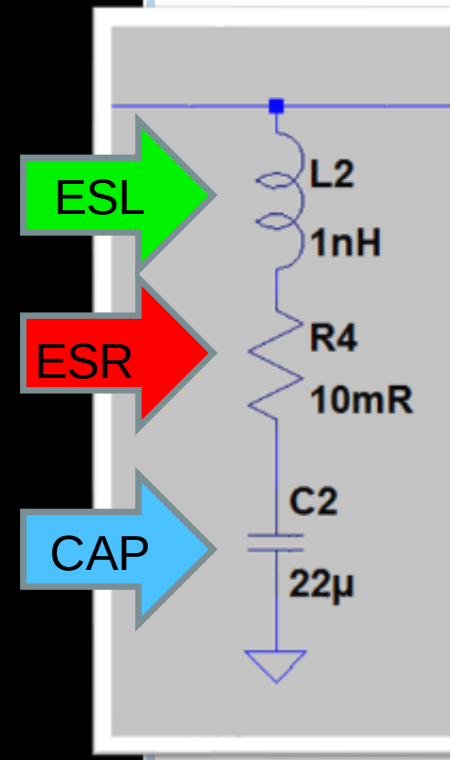
Reality VS Simulation

Conducted Emissions measurement

Reality VS Simulation

ESR / ESL / CAP breakdown in frequency



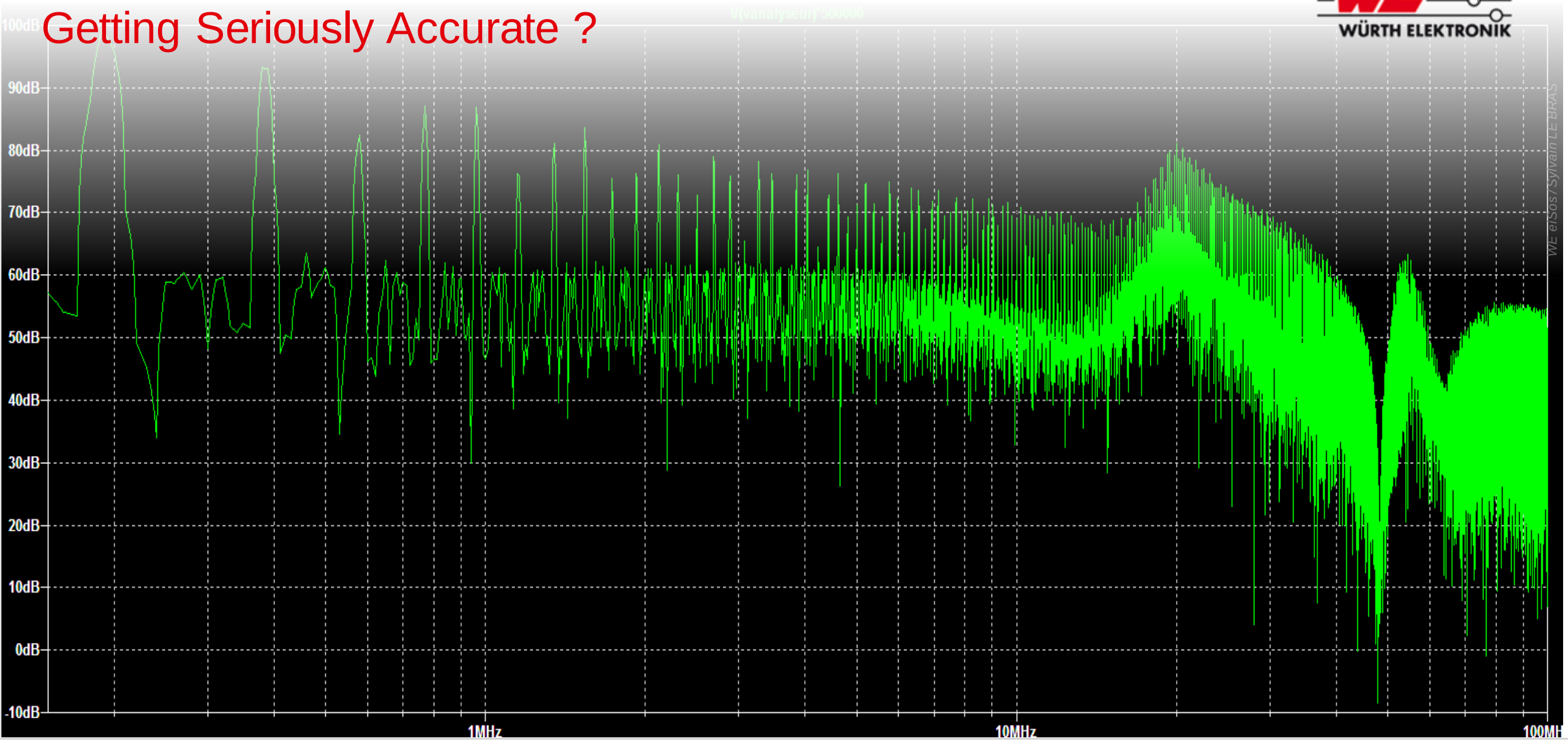


Reality VS Simulation

EMI measurement = ∑ (Common Mode + Differential Mode)

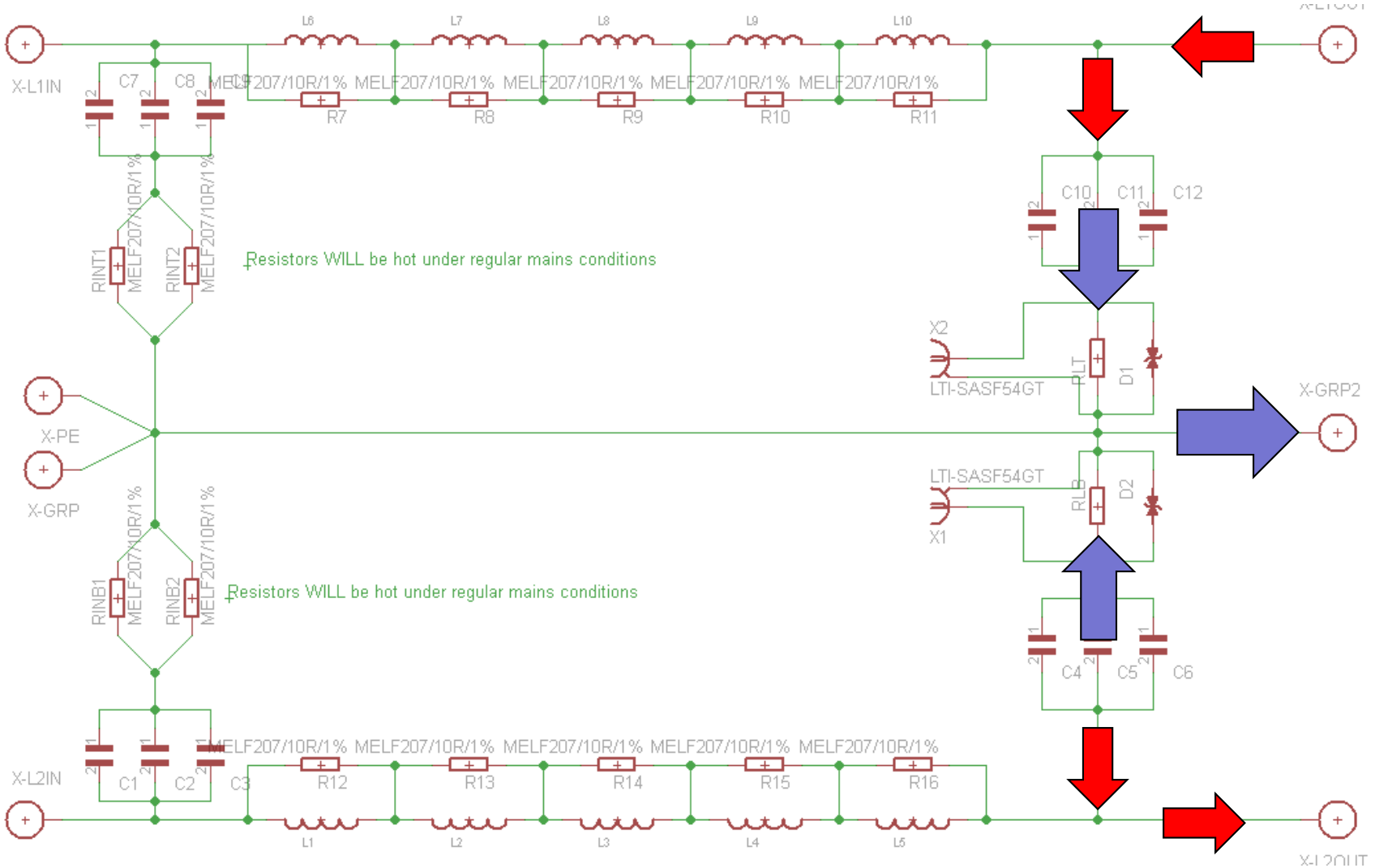
… To EMC simulation

Getting Seriously Accurate ?



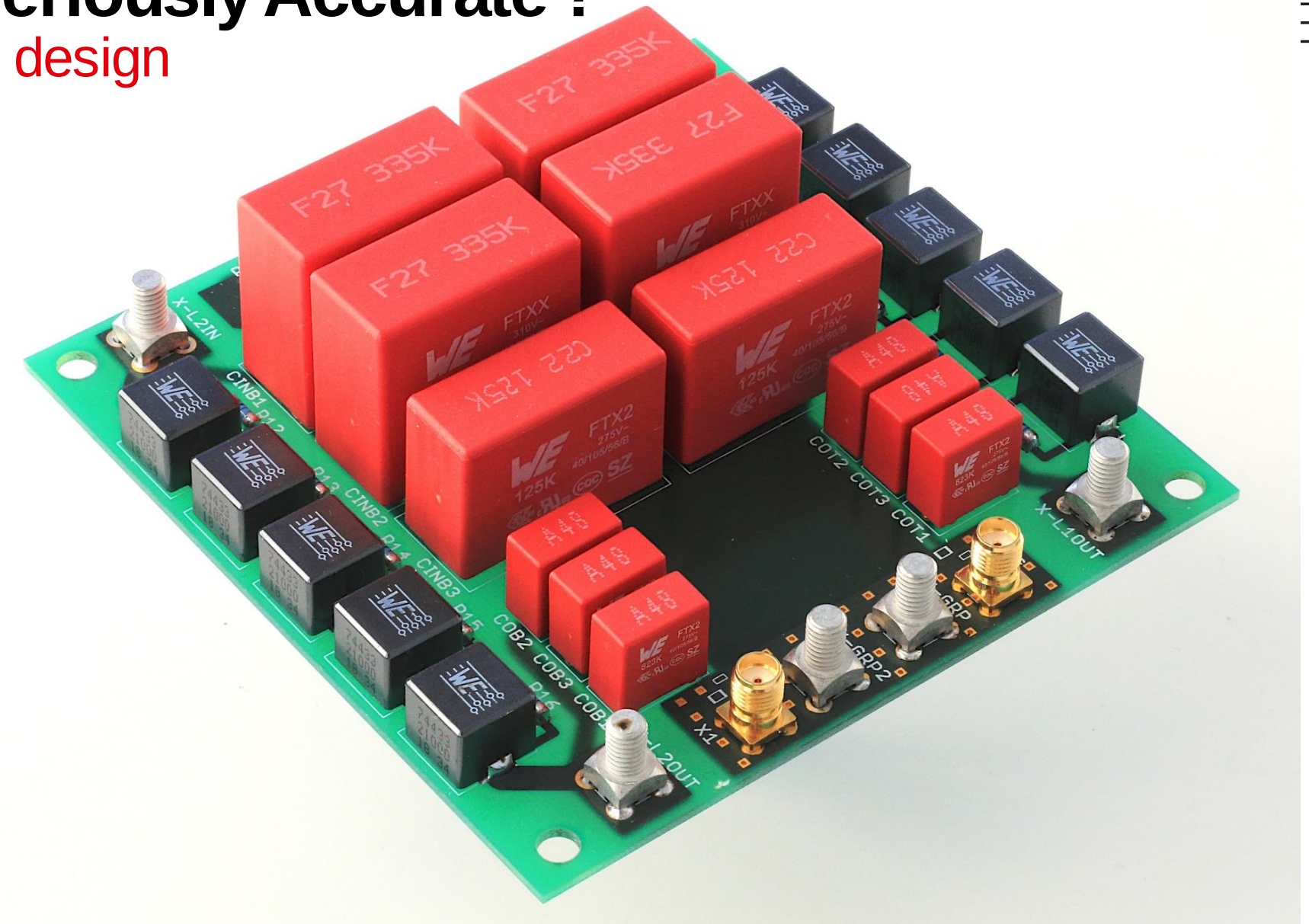
Getting Seriously Accurate ?

Actual LISN design



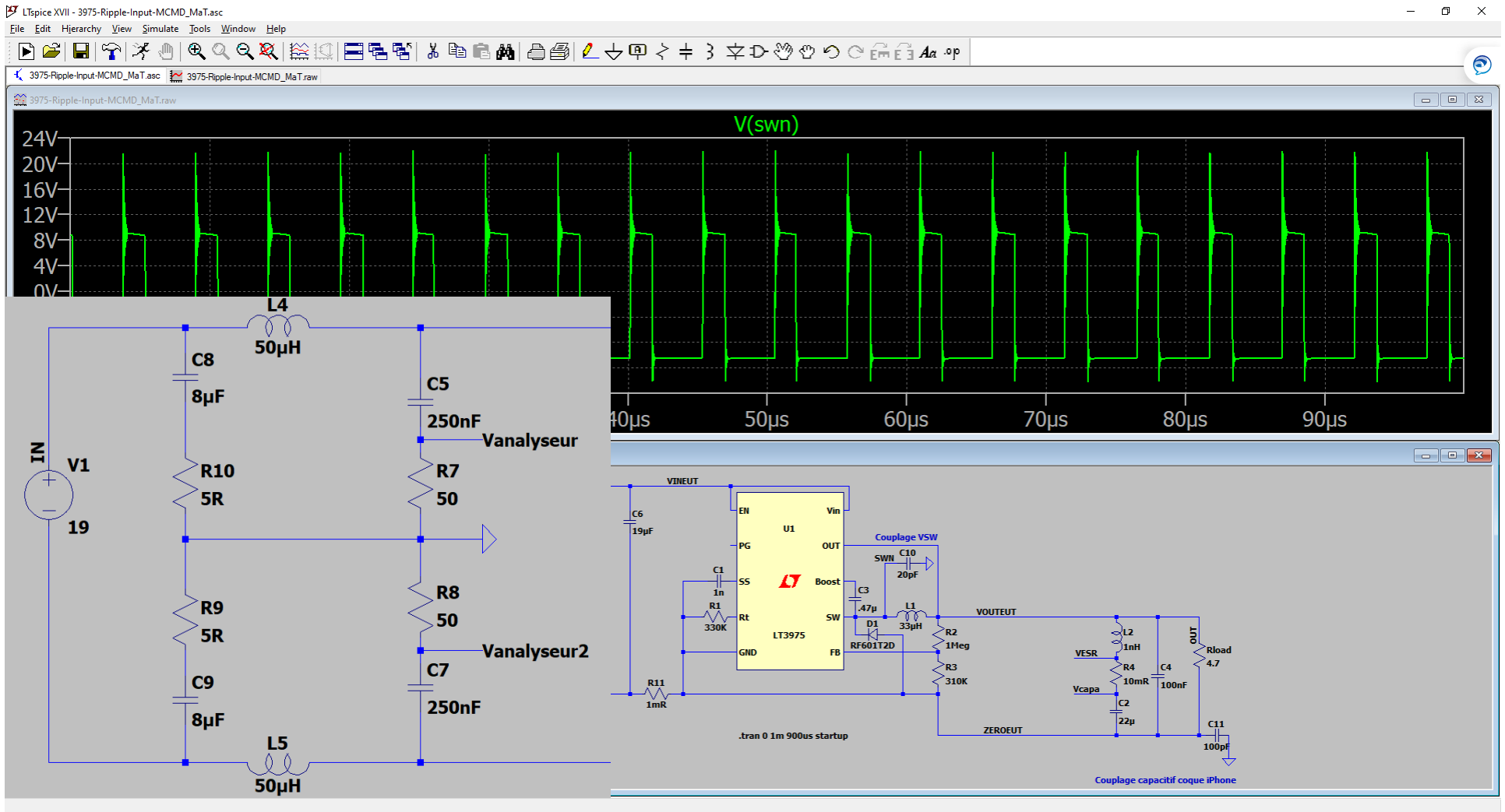
Getting Seriously Accurate ?

Actual LISN design



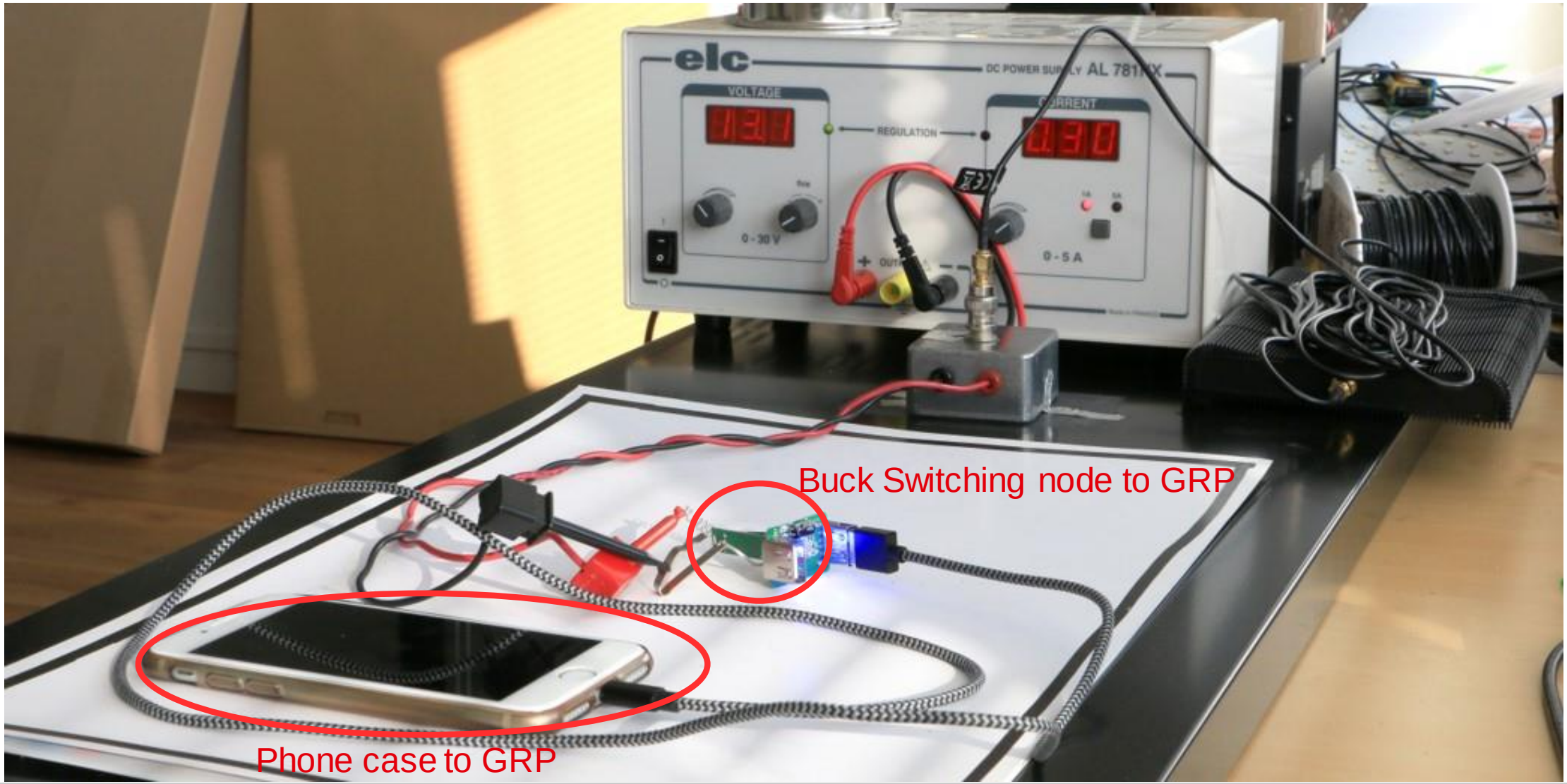
Getting Seriously Accurate ?

Simulation Ready LISN design



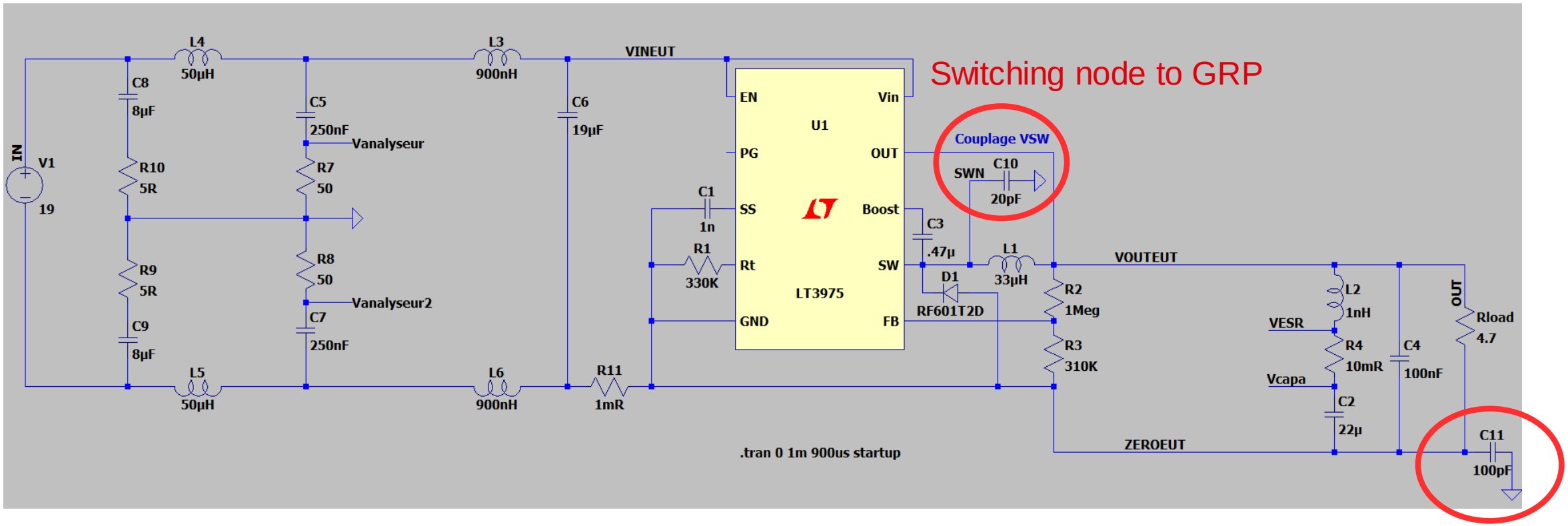
Getting Seriously Accurate ?

Adding E-Field parasitic coupling



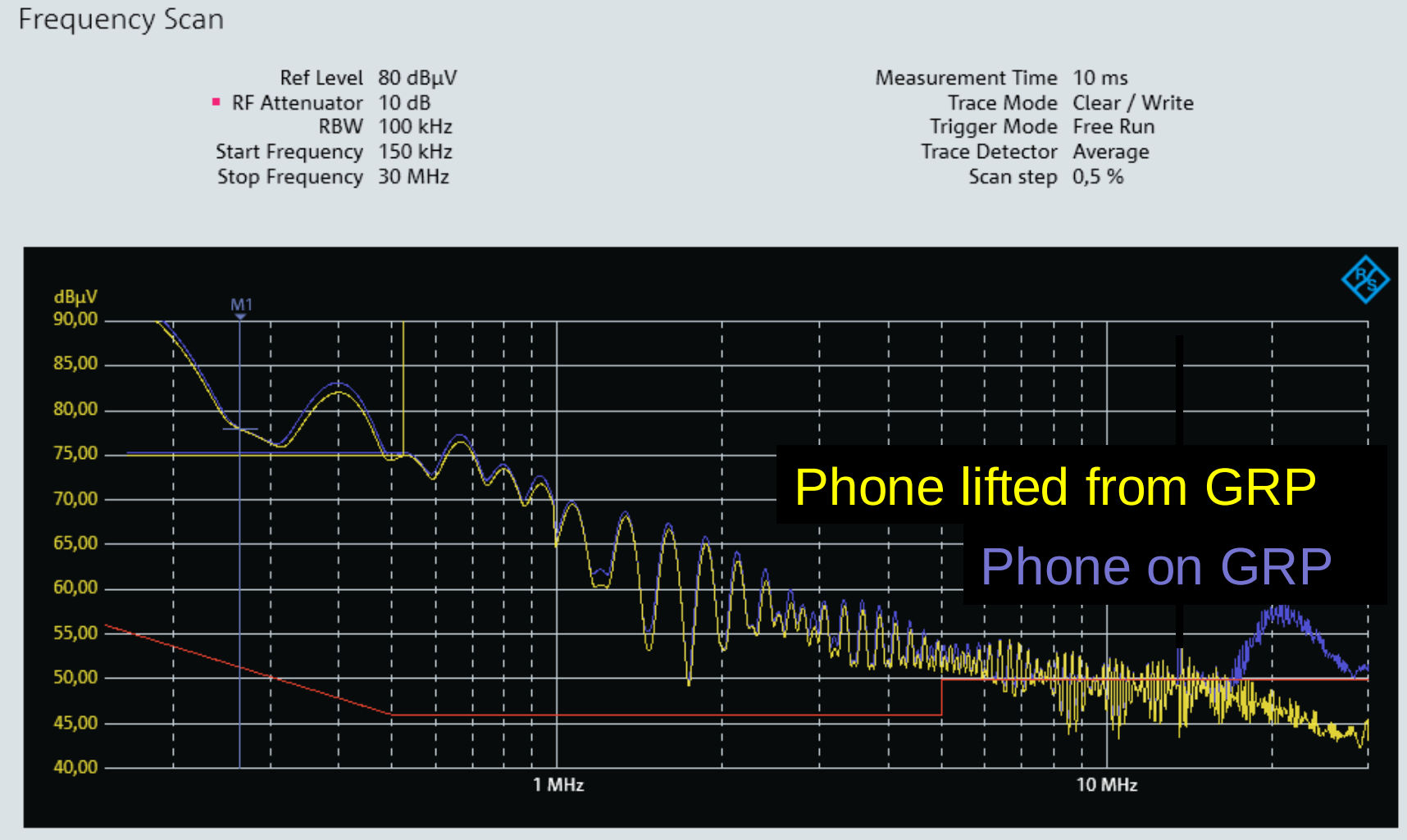
Getting Seriously Accurate ?

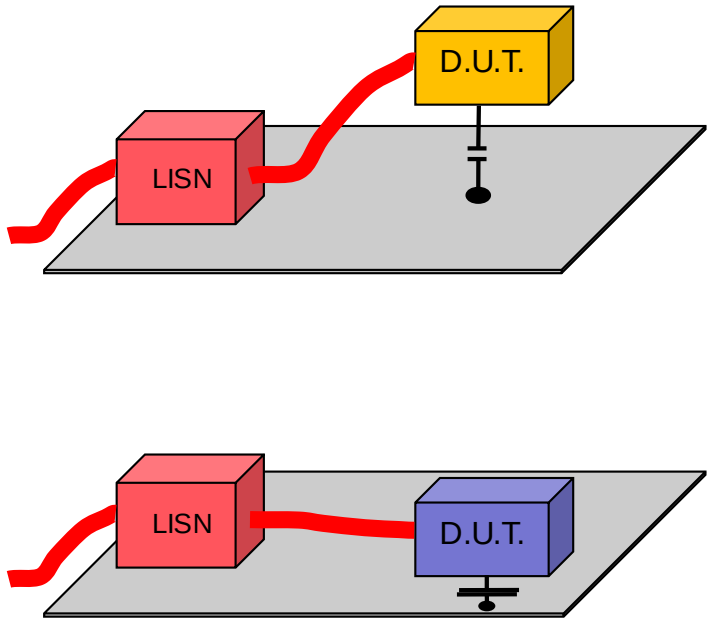
Adding E-Field parasitic coupling



Getting Seriously Accurate ?

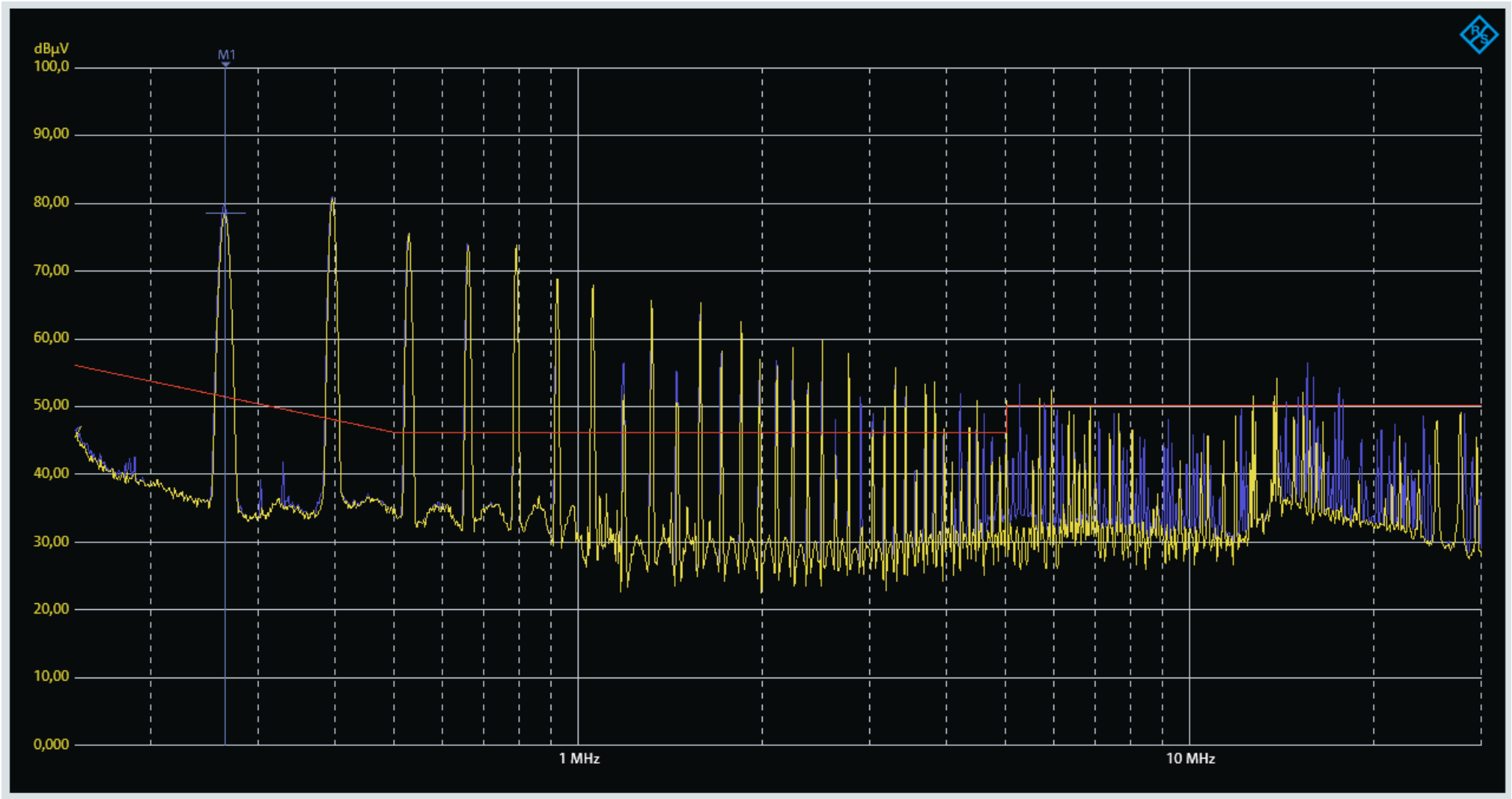
Reality VS Simulation





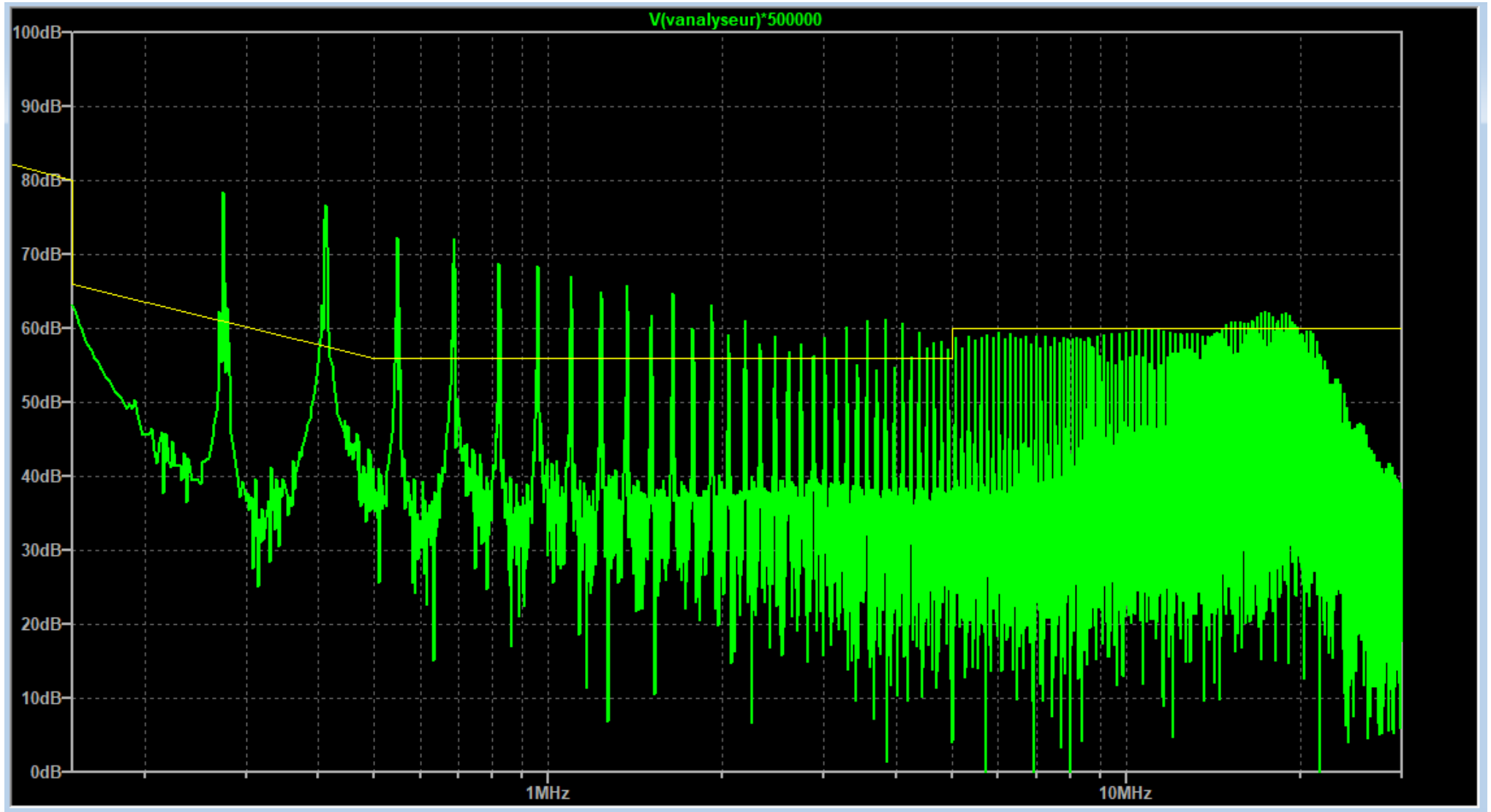
Getting Seriously Accurate ?

Reality VS Simulation



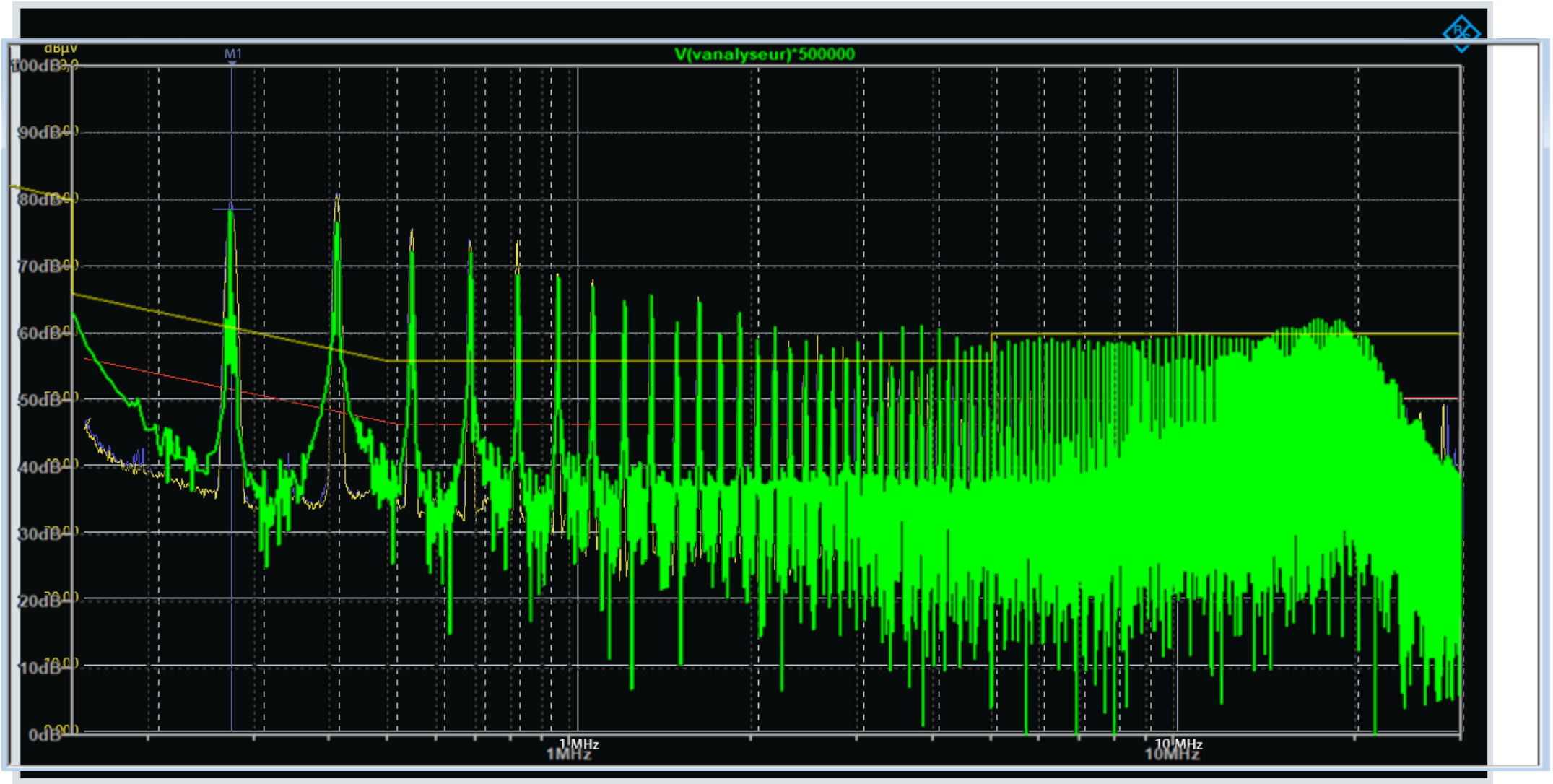
Getting Seriously Accurate ?

Reality VS Simulation



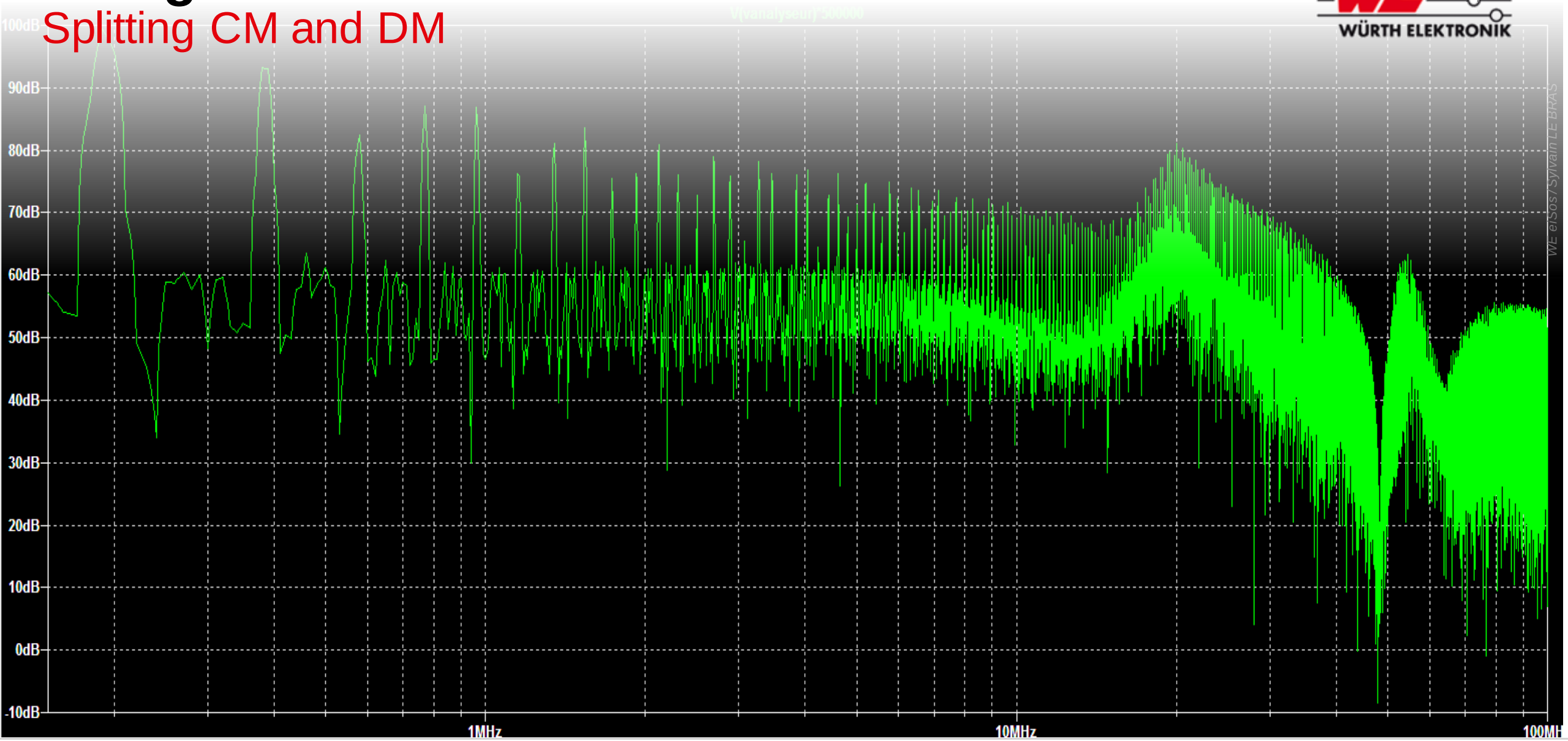
Getting Seriously Accurate ?

Reality VS Simulation



Going further with simulation

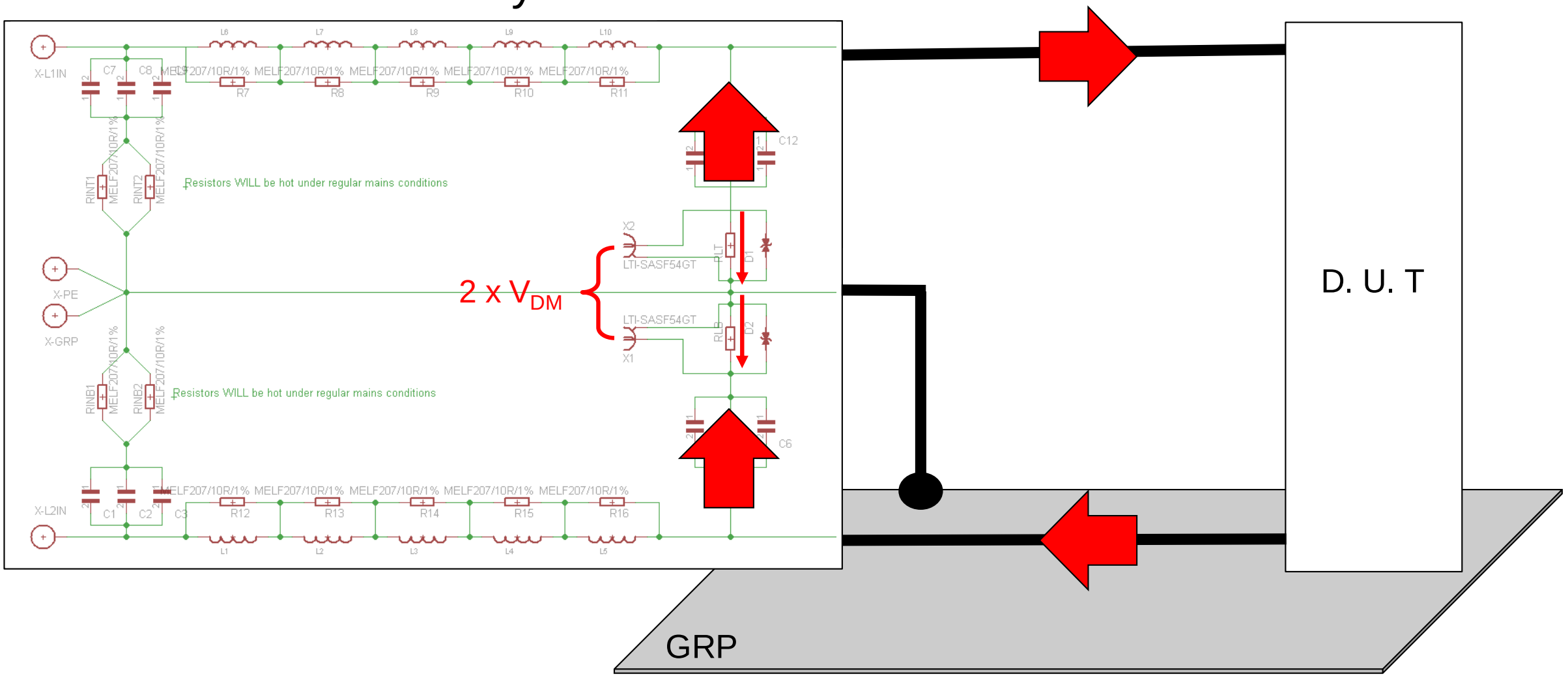
Splitting CM and DM



Going further with simulation

Splitting CM and DM

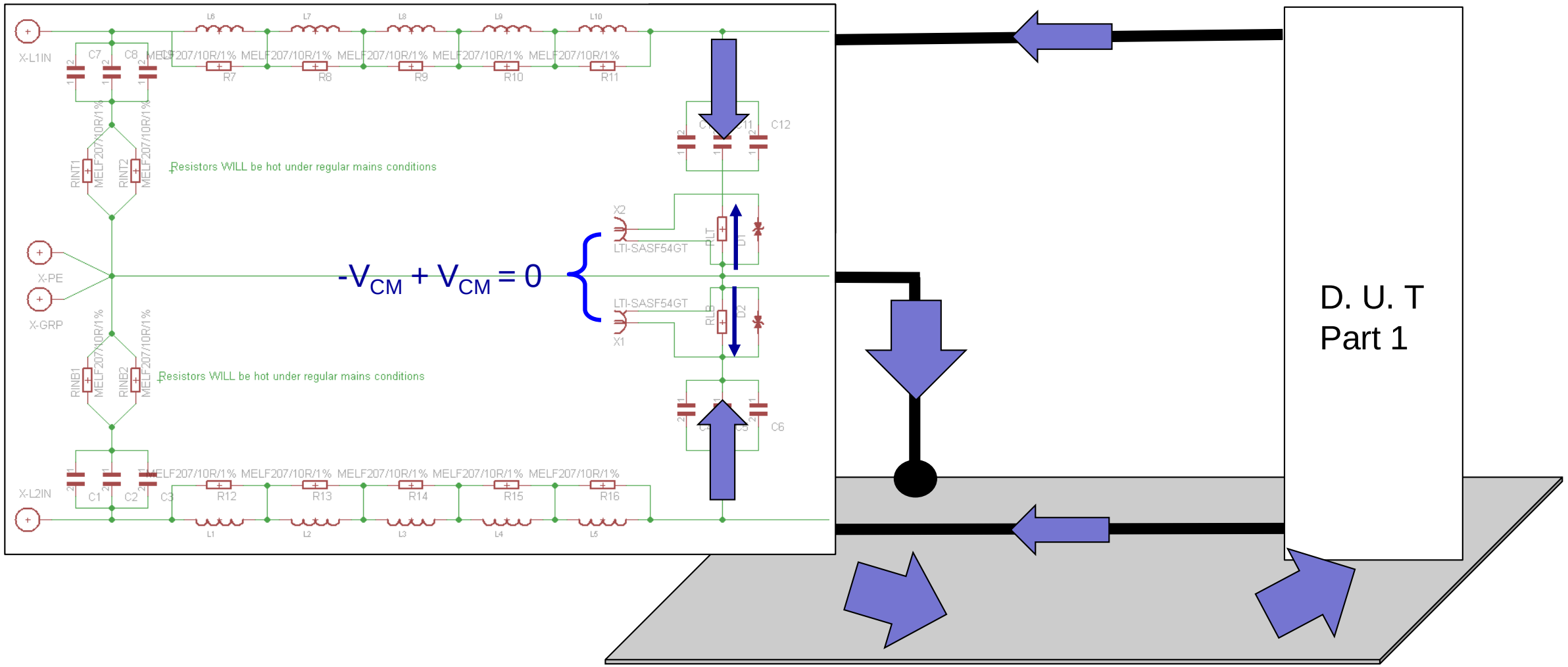
- Symetrical interference ?



Going further with simulation

Splitting CM and DM

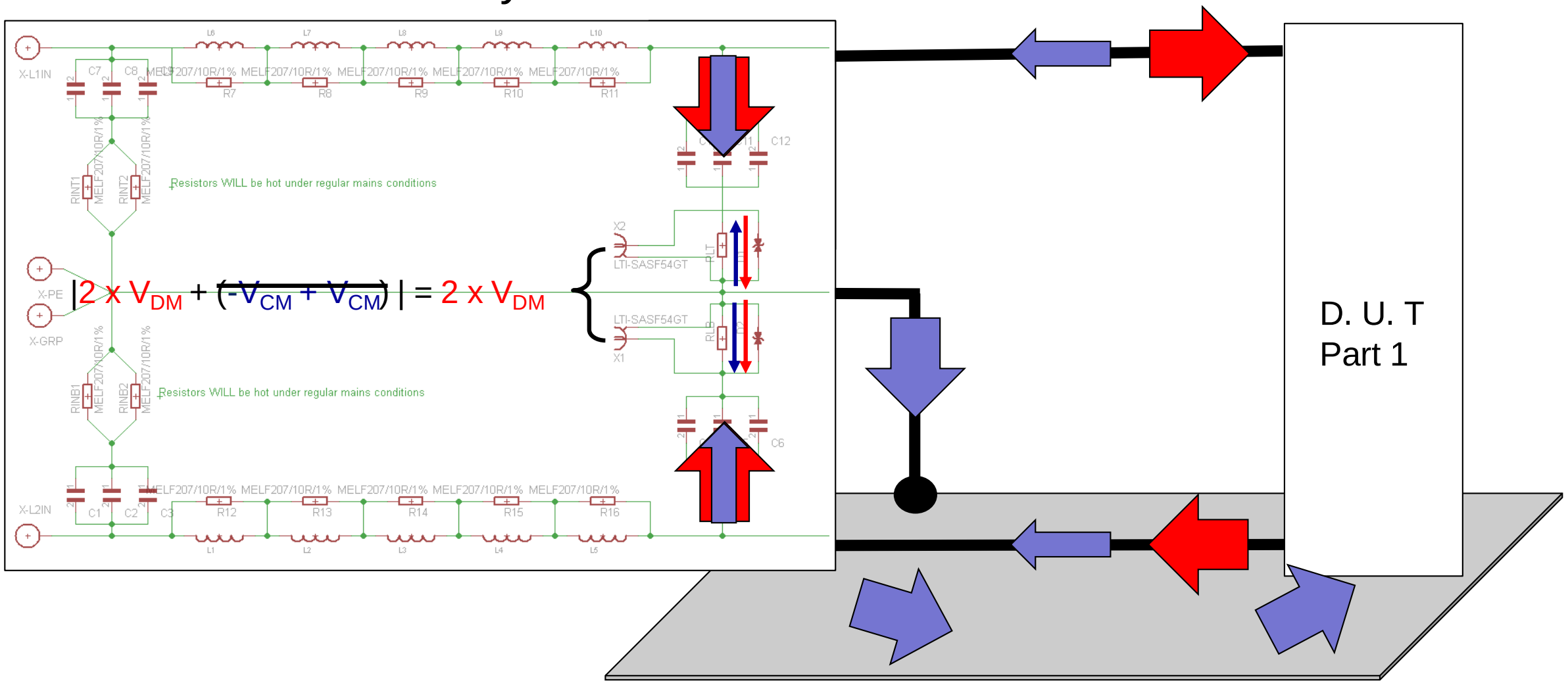
- Asymetrical interference ?



Going further with simulation

Splitting CM and DM

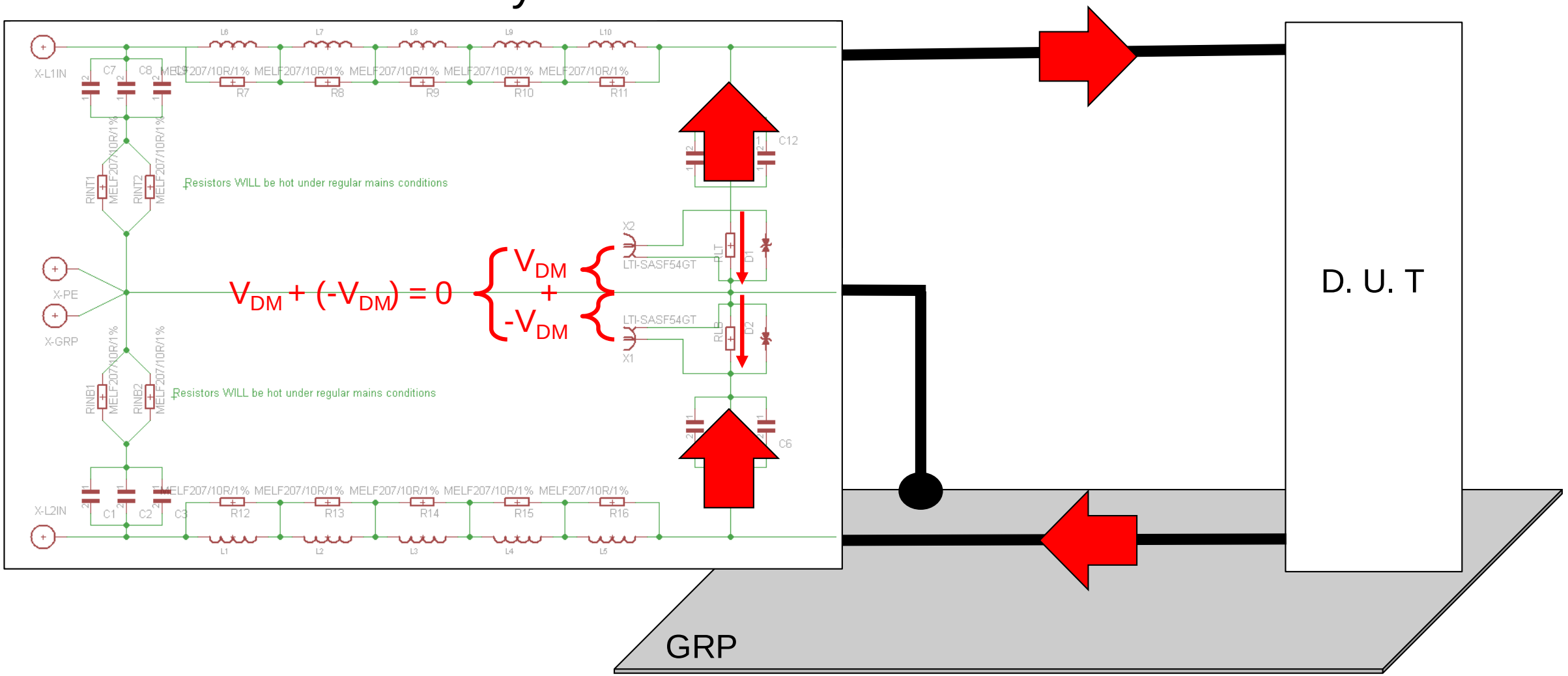
- Asymetrical interference ?



Going further with simulation

Splitting CM and DM

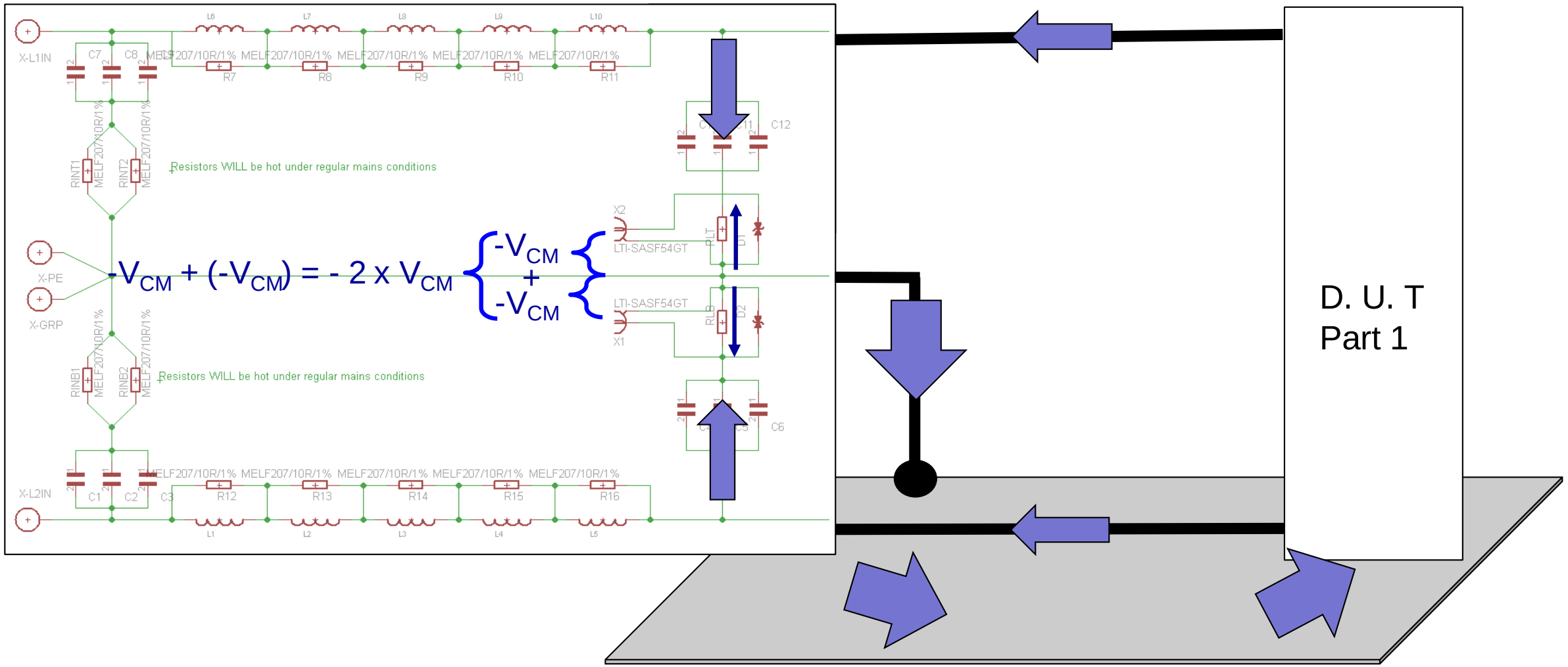
- Symetrical interference ?



Going further with simulation

Splitting CM and DM

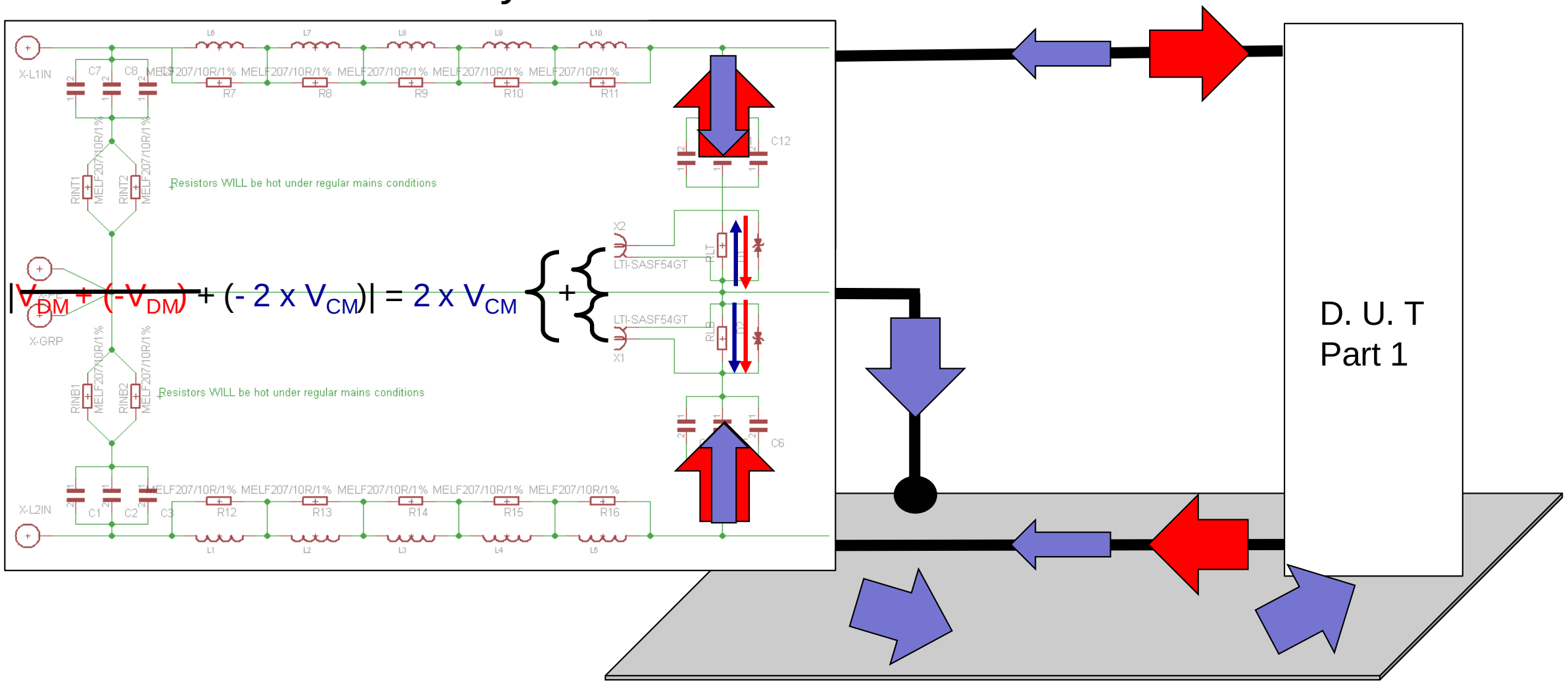
- Asymetrical interference ?



Going further with simulation

Splitting CM and DM

- Asymetrical interference ?



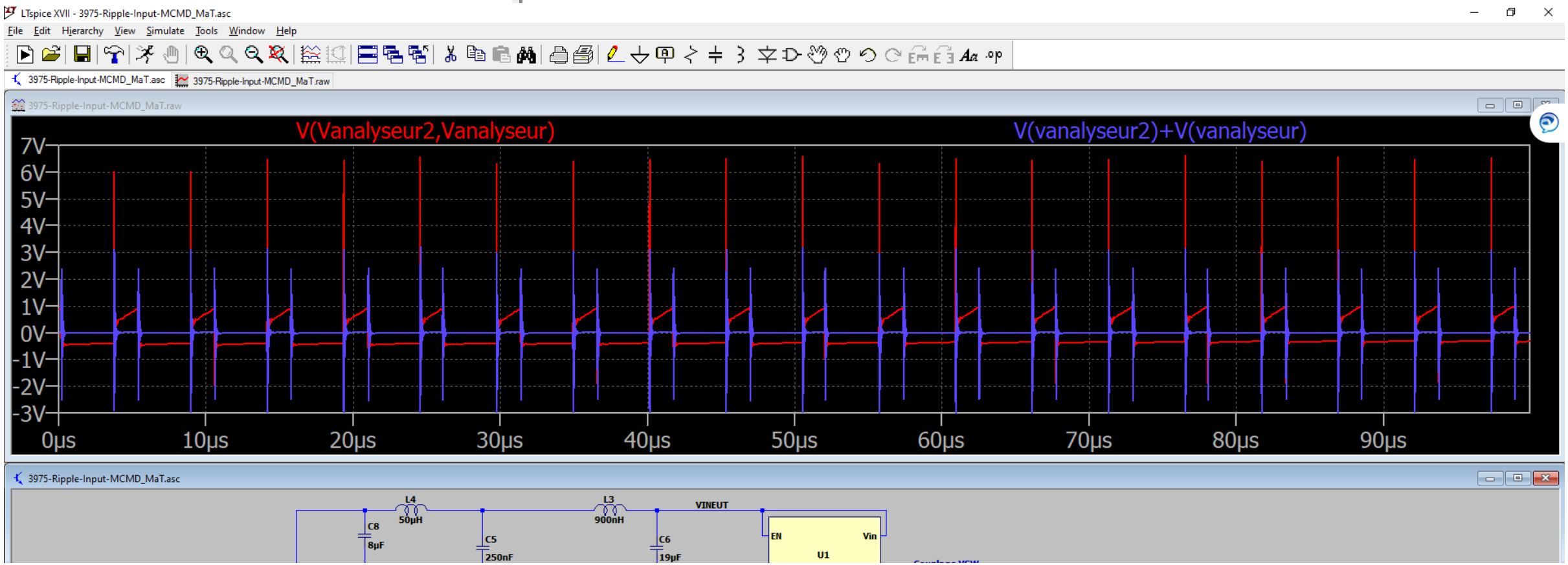
Going further with simulation

Splitting CM and DM

V(vanalyseur,vanalyseur2)
V(vanalyseur2)+V(vanalyseur)

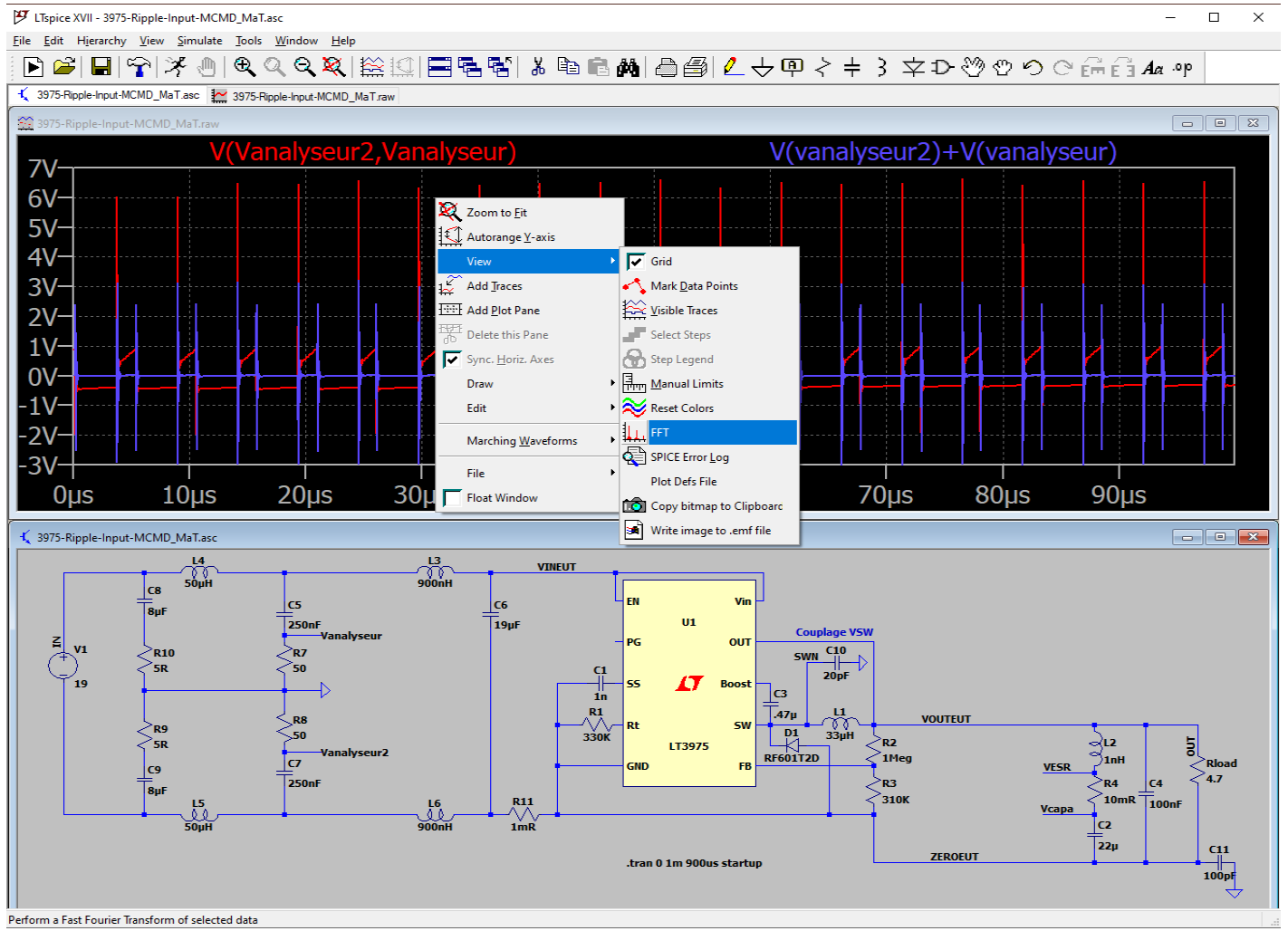
2 * DM noise

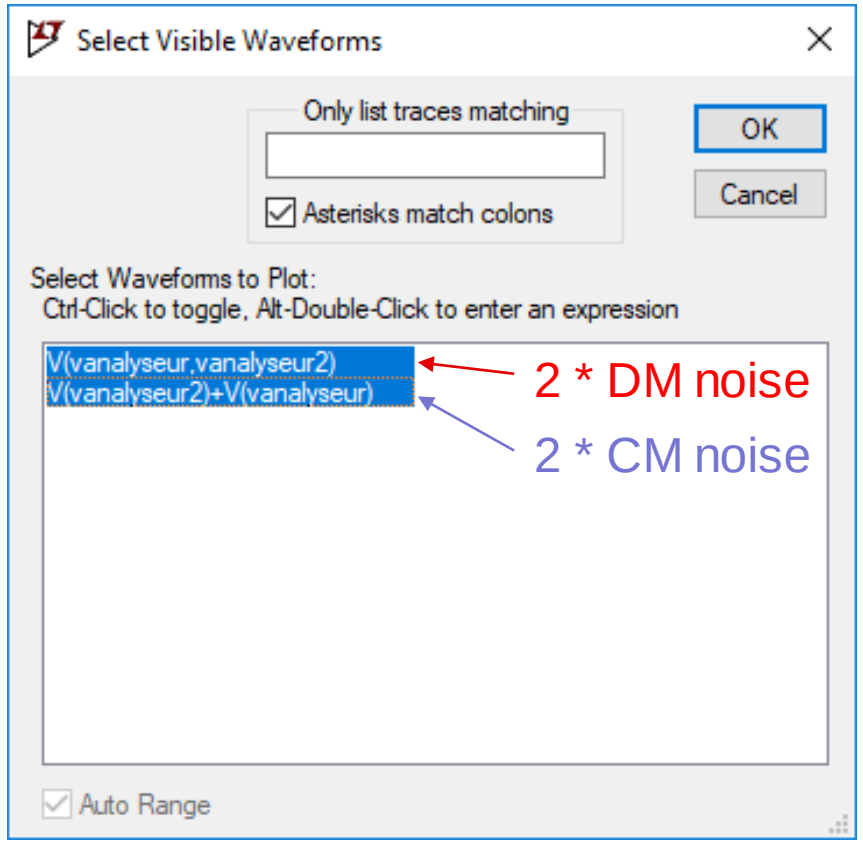
2 * CM noise



Going further with simulation

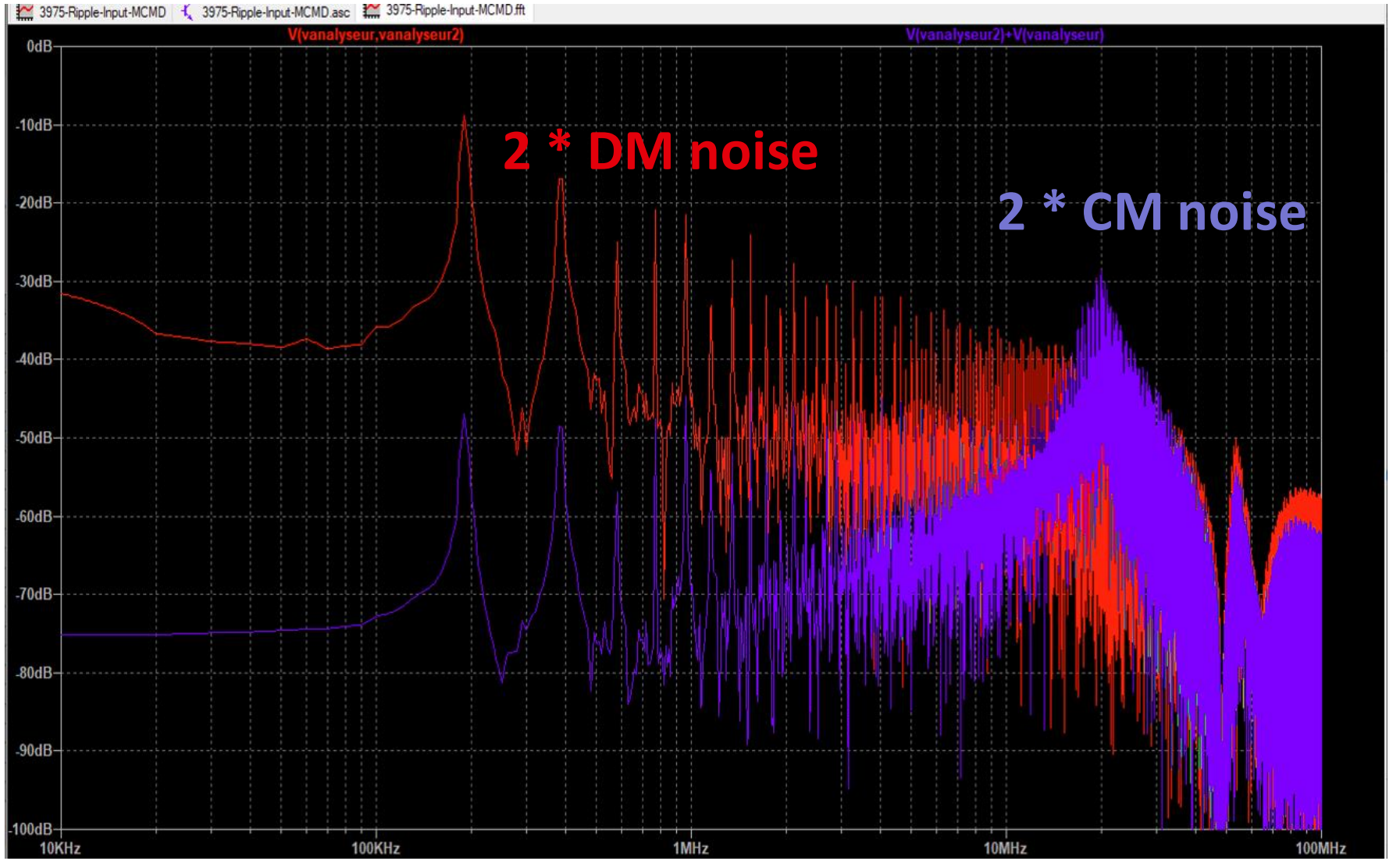
Splitting CM and DM





Going further with simulation

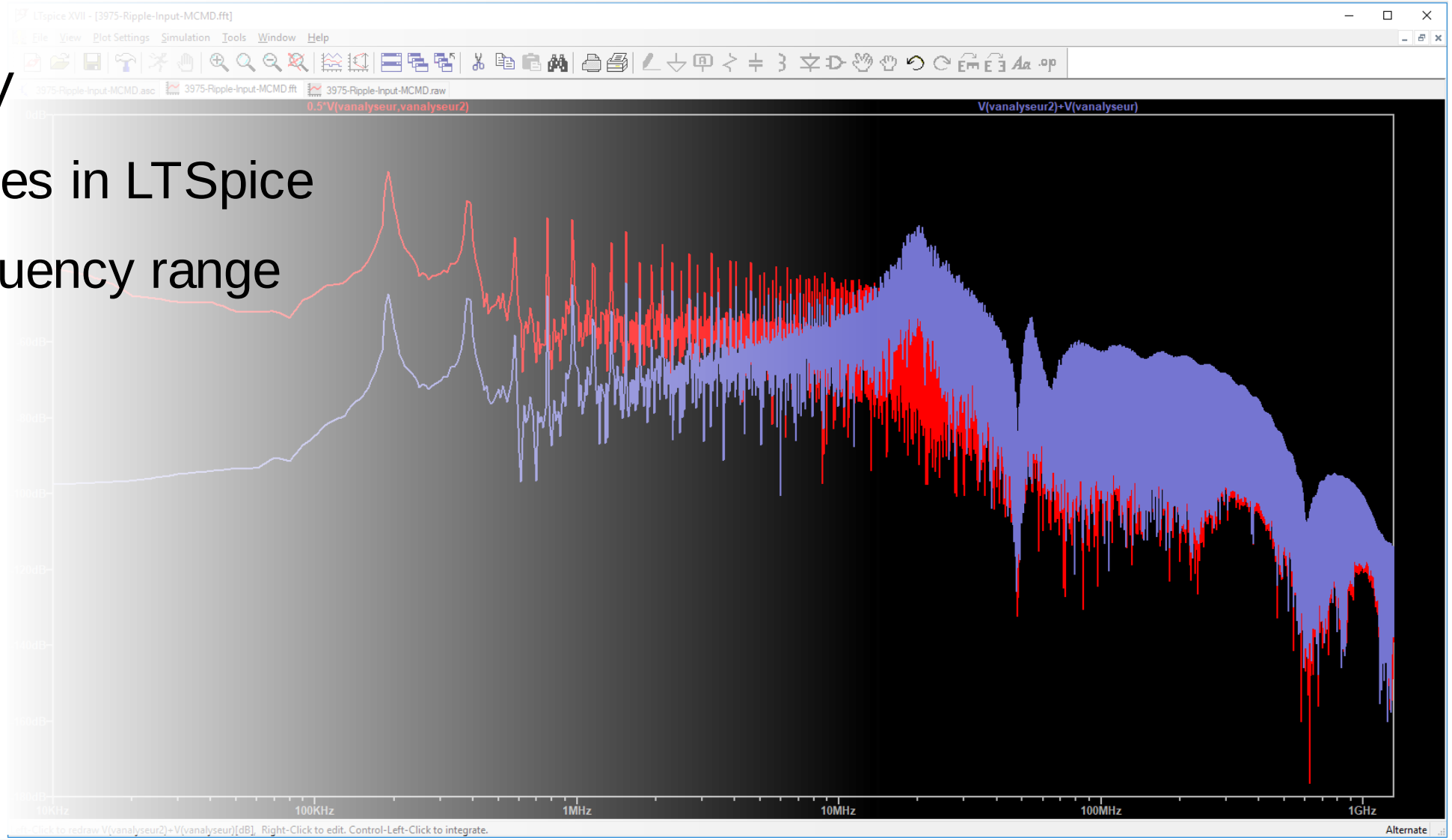
Splitting CM and DM



Going further with simulation

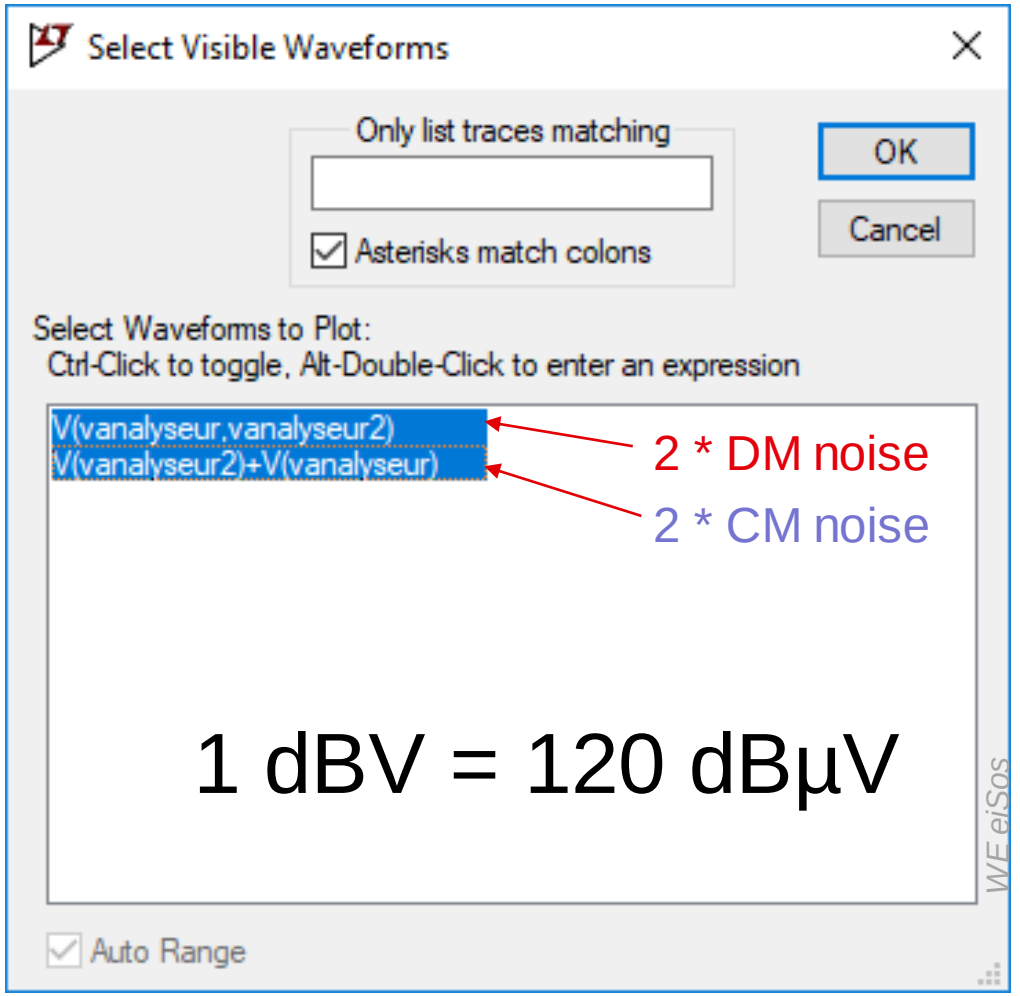
Making simulation look real

- Scaling to dBµV
- Loading limit lines in LTSpice
- Defining a Frequency range



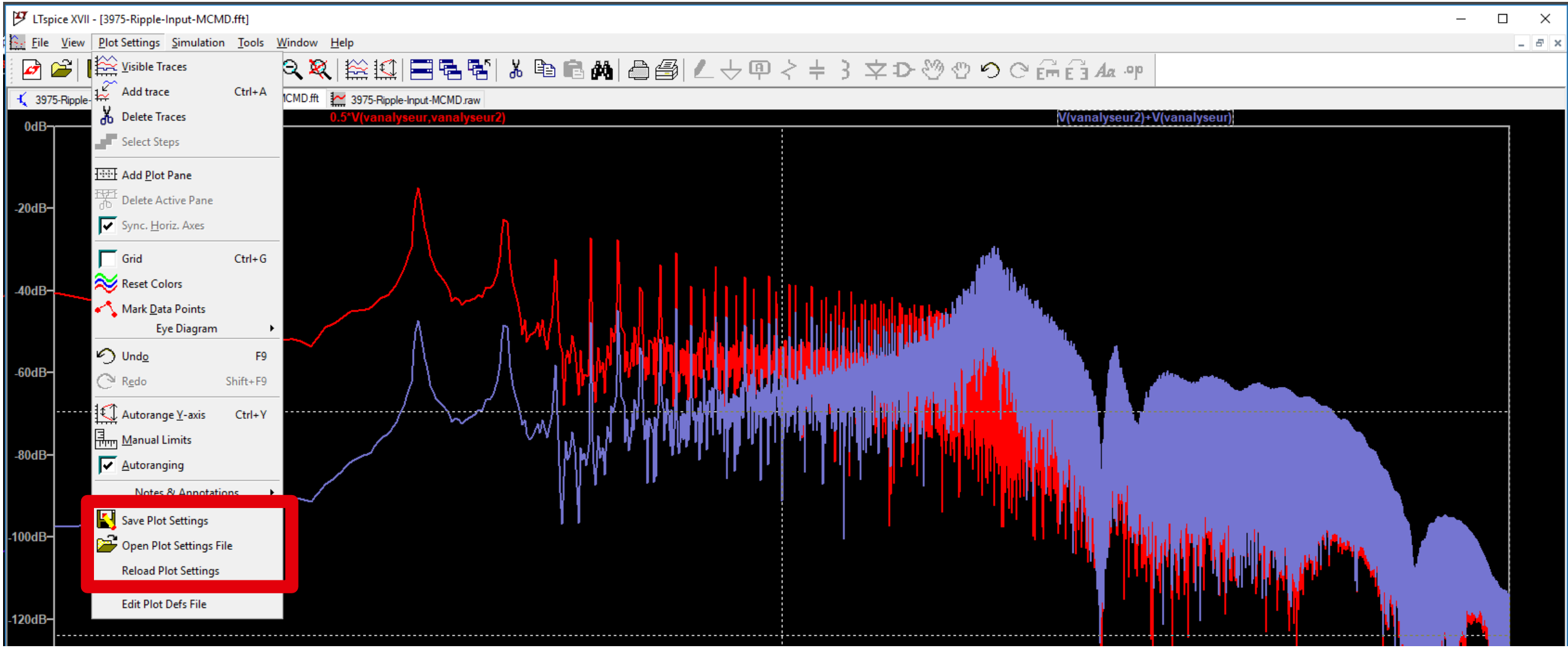
Going further with simulation

Making simulation look real



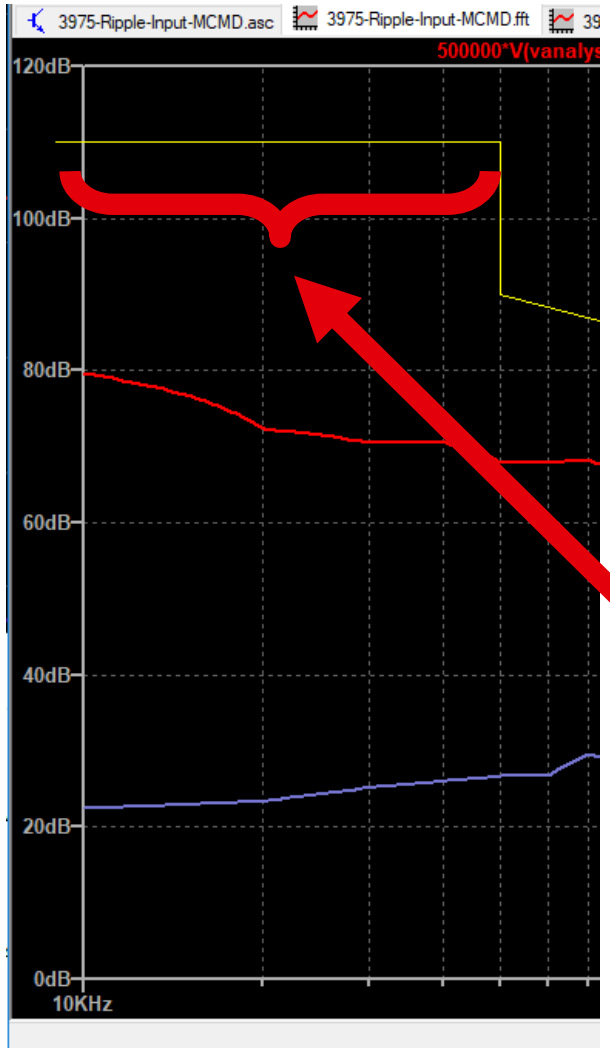
Going further with simulation

Making simulation look real



Going further with simulation

Making simulation look real – Adding limit lines



		Start	End	Amp dBµV start	Amp dBµV stop	Line def for LTSPICE
Line	1	9000	50000	110	110	(9000,0.316227766016838) (50000,0.316227766016838)
Line	2	50000	150000	90	80	(50000,0.0316227766016838) (150000,0.01)
Line	3	150000	500000	66	56	(150000,0.00199526231496888) (500000,0.000630957344480192)
Line	4	500000	5000000	56	56	(500000,0.000630957344480192) (5000000,0.000630957344480192)
Line	5	5000000	30000000	60	60	(5000000,0.001) (30000000,0.001)

Fill according to EMC standards

Copy the result

Flyback-example-2-base - Bloc-notes

Fichier Edition Format Affichage Aide

```
[FFT of time domain data]
{
   Npanes: 1
   {
      traces: 1 {2,0,"V(vanalyseur2)+V(vanalyseur)"}
      X: ('M',0,9000,0,30000000)
      Y[0]: (' ',0,1e-006,10,1)
      Y[1]: (' ',0,-200,40,200)
      Log: 1 2 0
      PltMag: 1
      Line: "dB" 4 0 (9000,0.3162277660168) (50000,0.316227766)
      Line: "dB" 4 0 (50049.8435712172,0.0317065818612387) (150407.110289202,0.0100397786508485)
      Line: "dB" 4 0 (150000,0.00199526231496888) (500000,0.000630957344480192)
      Line: "dB" 4 0 (500000,0.000630957344480192) (5000000,0.000630957344480192)
      Line: "dB" 4 0 (5000000,0.001) (30000000,0.001)
   }
}
```

Paste it here

Windows (CRLF) Ln 10, Col 16 100%

Going further with simulation

Making simulation look real – Defining a range

10kHz to 30 MHz

0 to 120dBµV

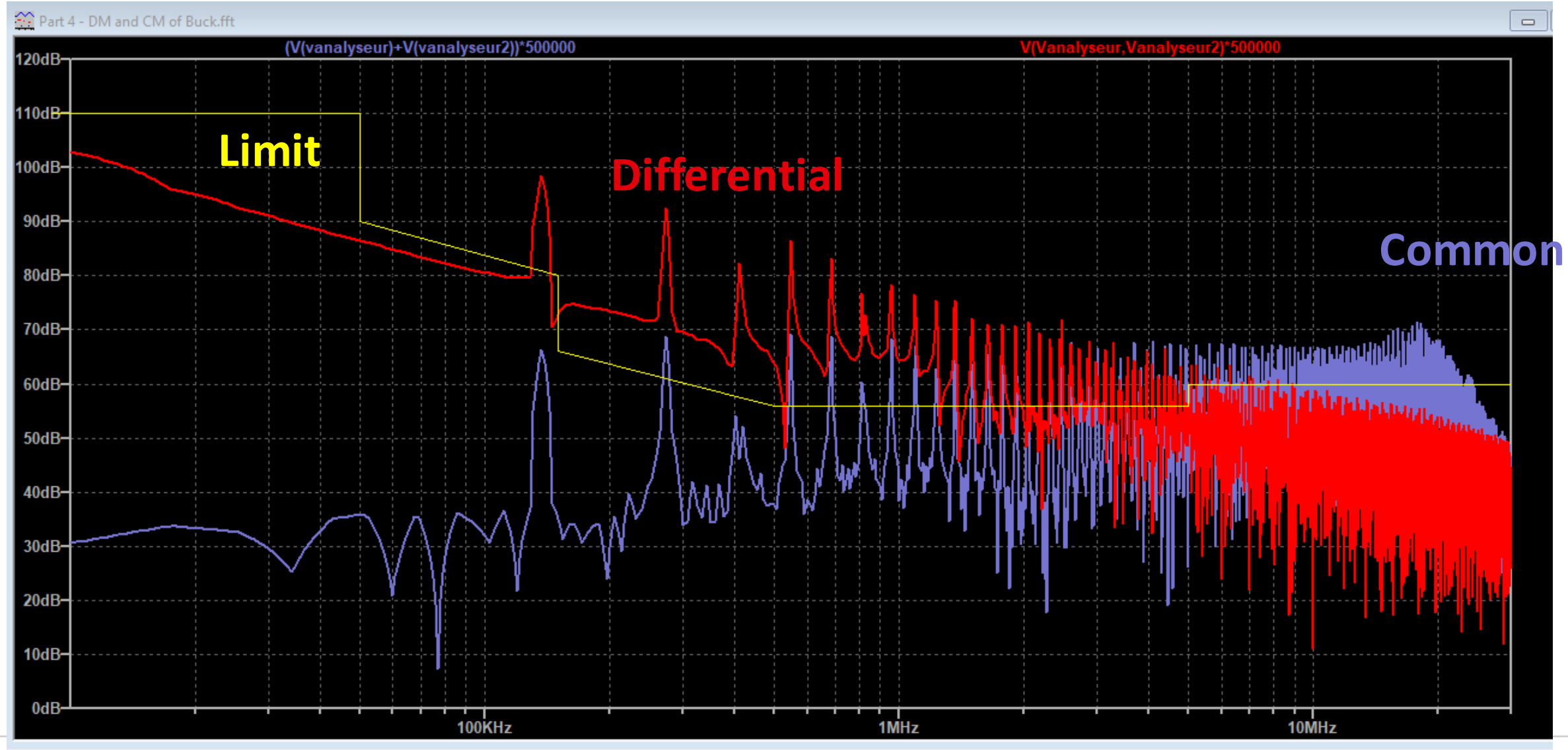
3975-Ripple-Input-MCMD-dbuv.plt - Bloc-notes

Fichier Edition Format Affichage ?

```
[FFT of time domain data]
{
   Npanes: 1
   {
      traces: 2 {65540,0,"500000*V(vanalyseur,vanalyseur2)"} {65547,0,"1000000*(V(vanalyseur2)+V(vanalyseur))"}
      X: ('M',0,10000,0,3e+007)
      Y[0]: (' ',0,1,20,1e+006)
      Log: 1 2 0
      GridStyle: 1
      PltMag: 1
      Line: "dB" 13 0 (8983.92329505352,319040.747263751) (49889.5367382049,319040.747263751)
      Line: "dB" 13 0 (50000,316227.766016838) (50000,31622.7766016838)
      Line: "dB" 13 0 (50000,31622.7766016838) (150000,10000)
      Line: "dB" 13 0 (150000,10000) (150000,1995.26231496888)
      Line: "dB" 13 0 (150000,1995.26231496888) (500000,630.957344480193)
      Line: "dB" 13 0 (500000,630.957344480193) (5000000,630.957344480193)
      Line: "dB" 13 0 (5000000,630.957344480193) (5000000,1000)
      Line: "dB" 13 0 (5000000,1000) (30000000,1000)
   }
}
```

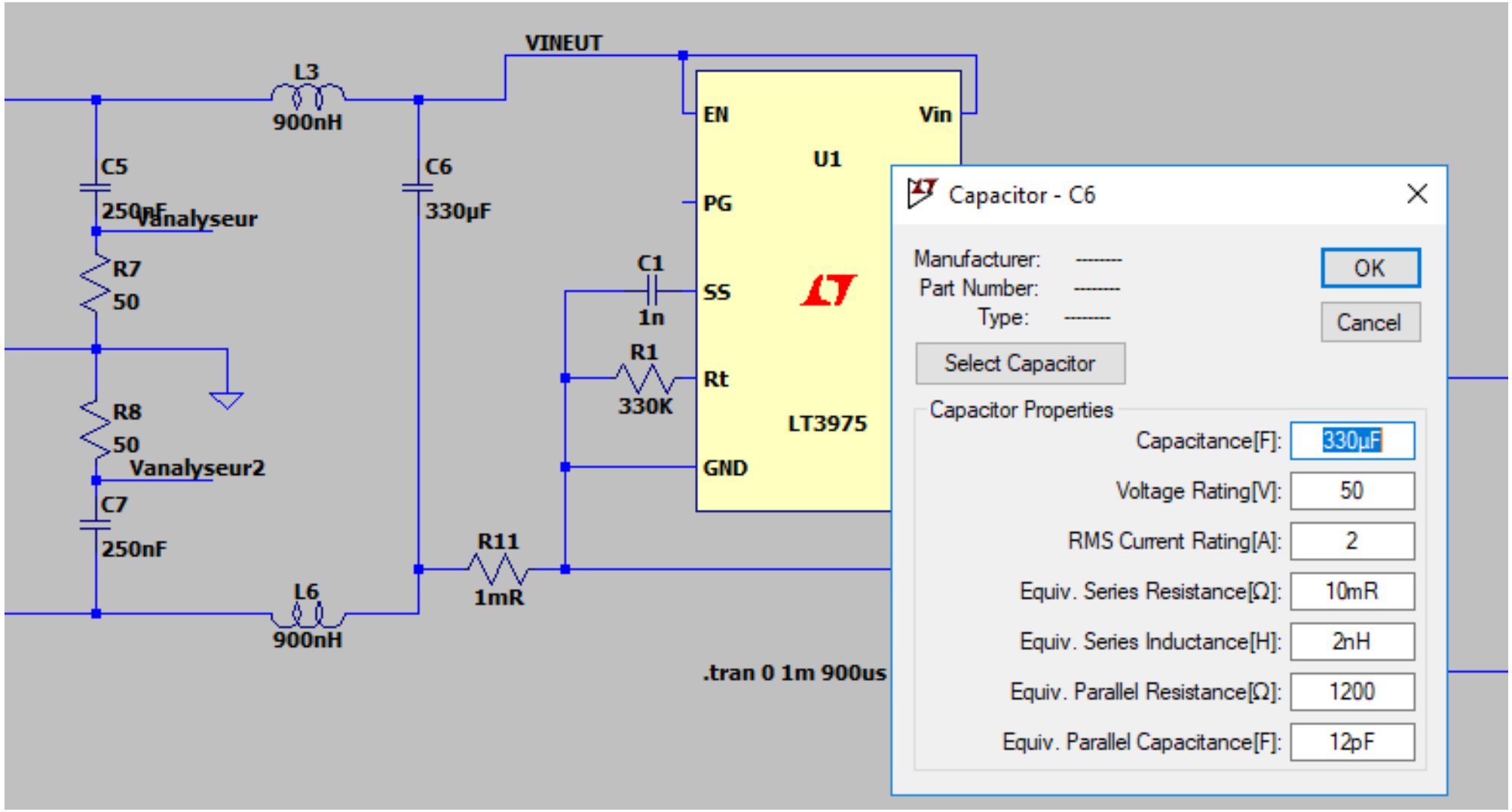
Going further with simulation

Making simulation look real – Result ☺



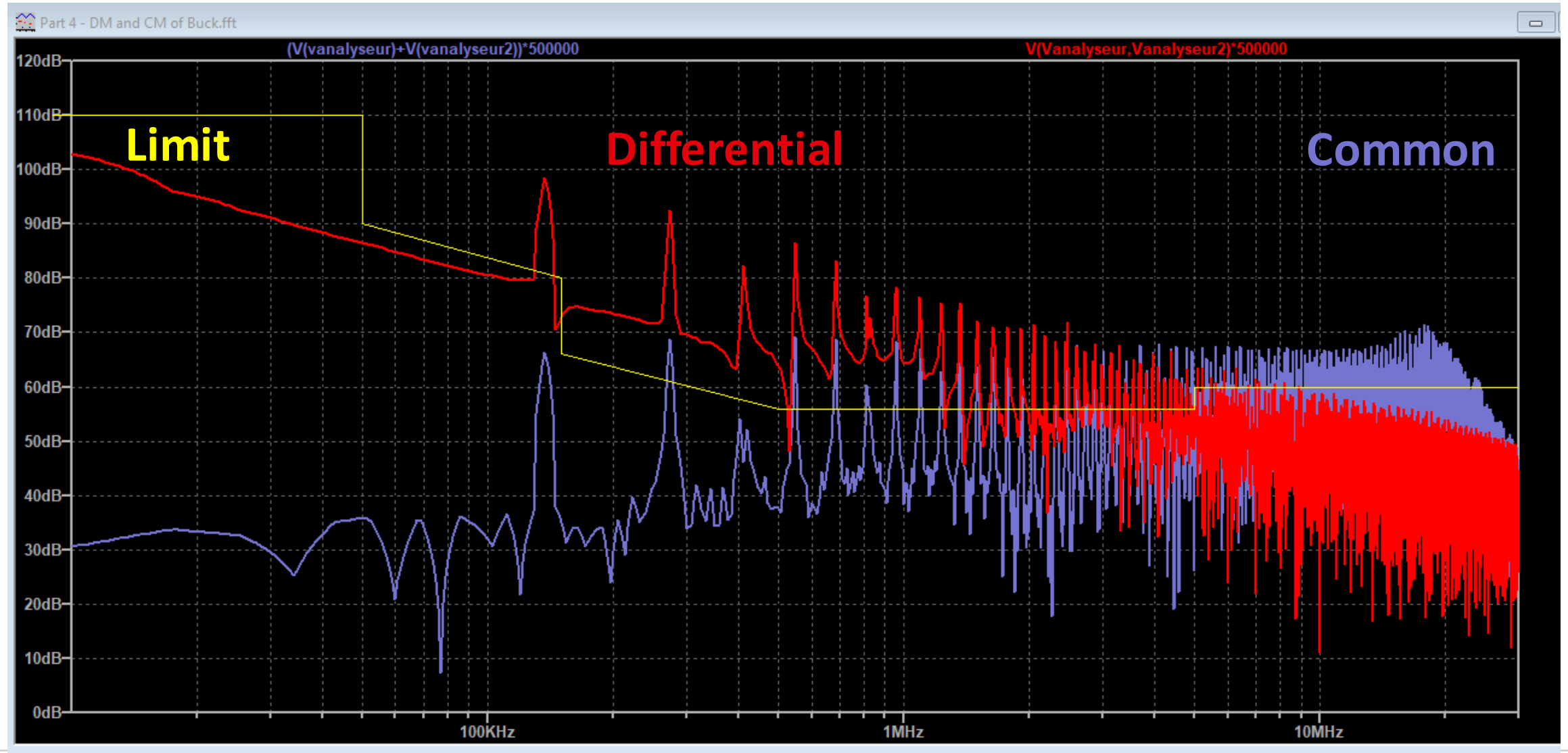
Going further with simulation

Fixing that buck in the simulation – Polymer input cap



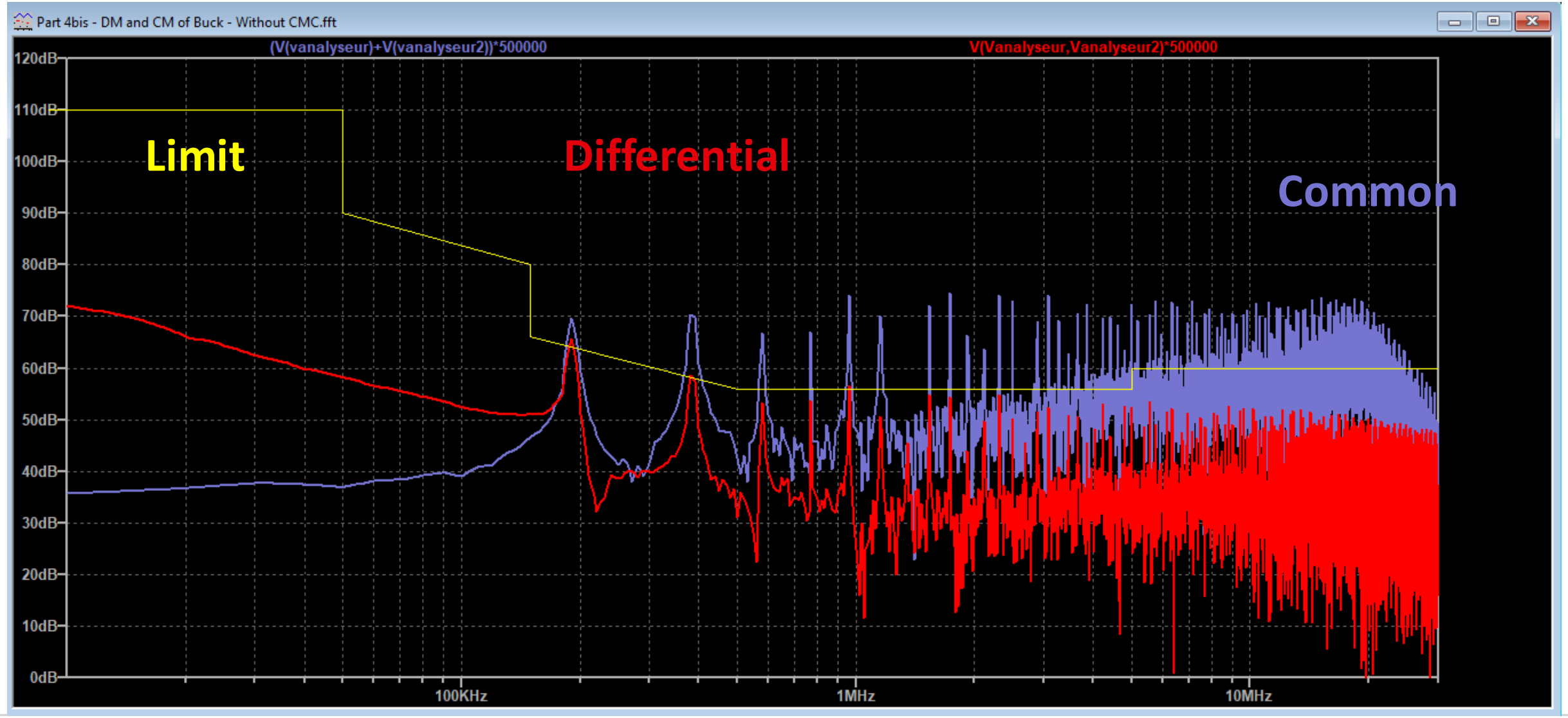
Going further with simulation

Fixing that buck in the simulation – **Before** Polymer Cap



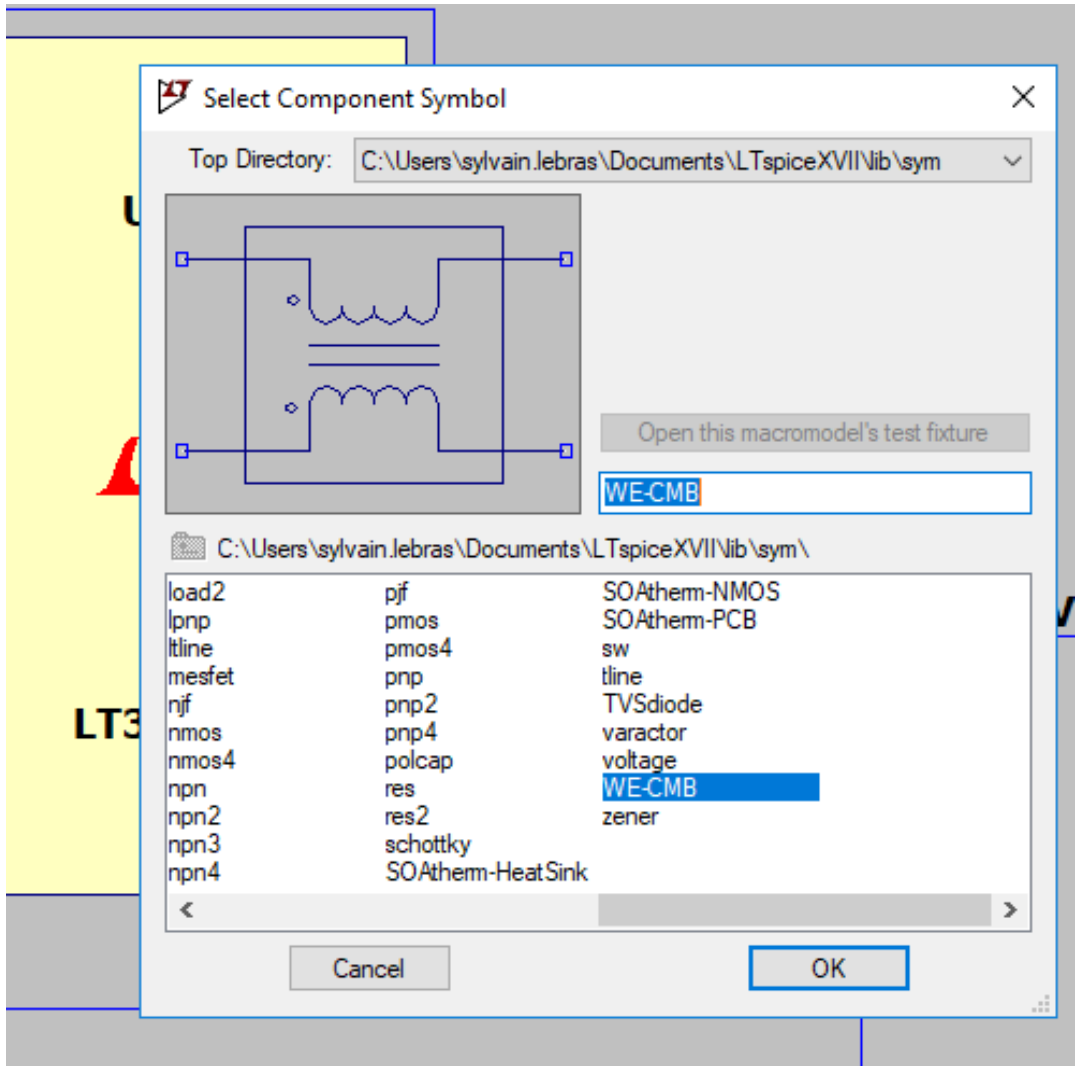
Going further with simulation

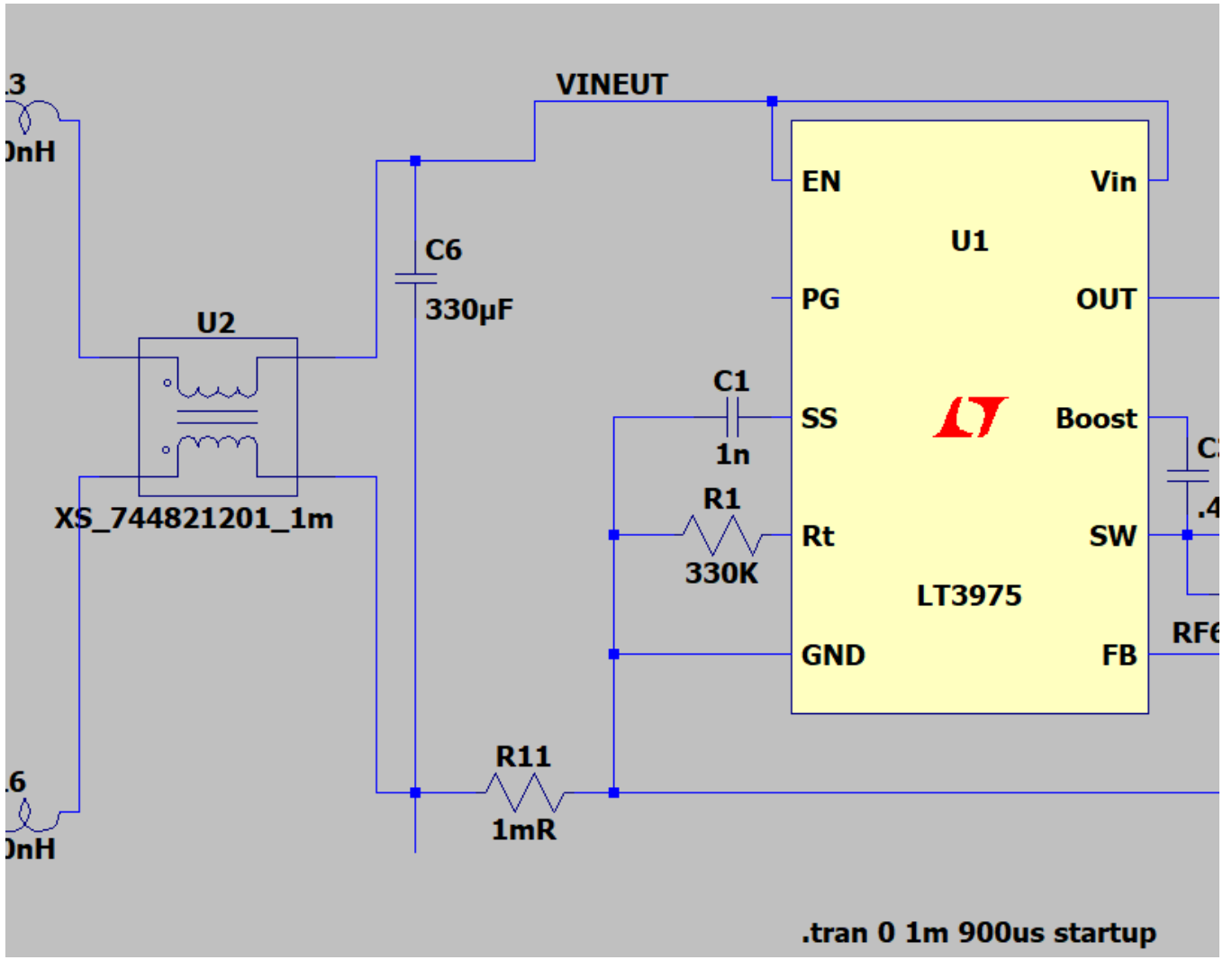
Fixing that buck in the simulation – **After** Polymer Cap



Going further with simulation

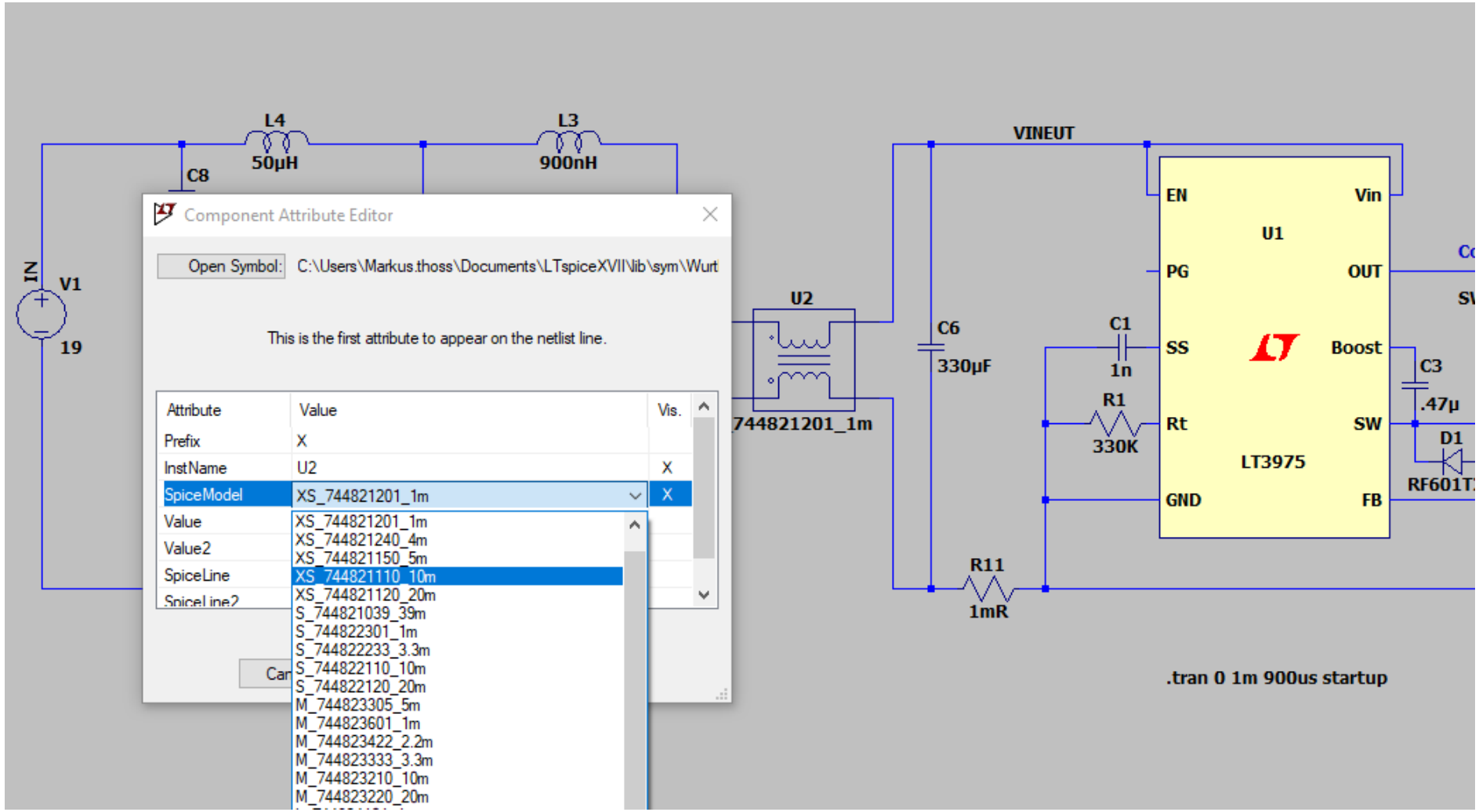
Fixing that buck in the simulation – Common mode choke





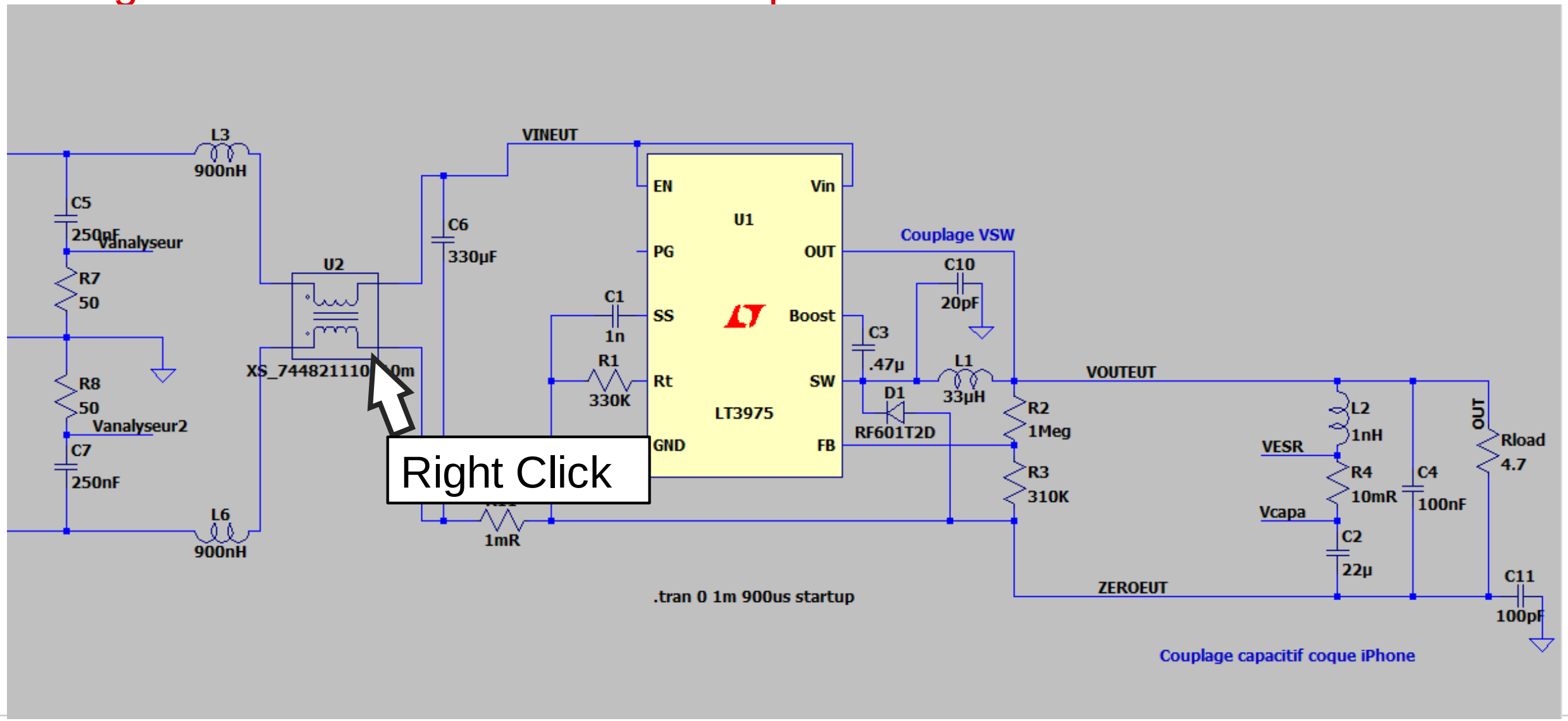
Going further with simulation

Fixing that buck in the simulation – Input Common mode choke



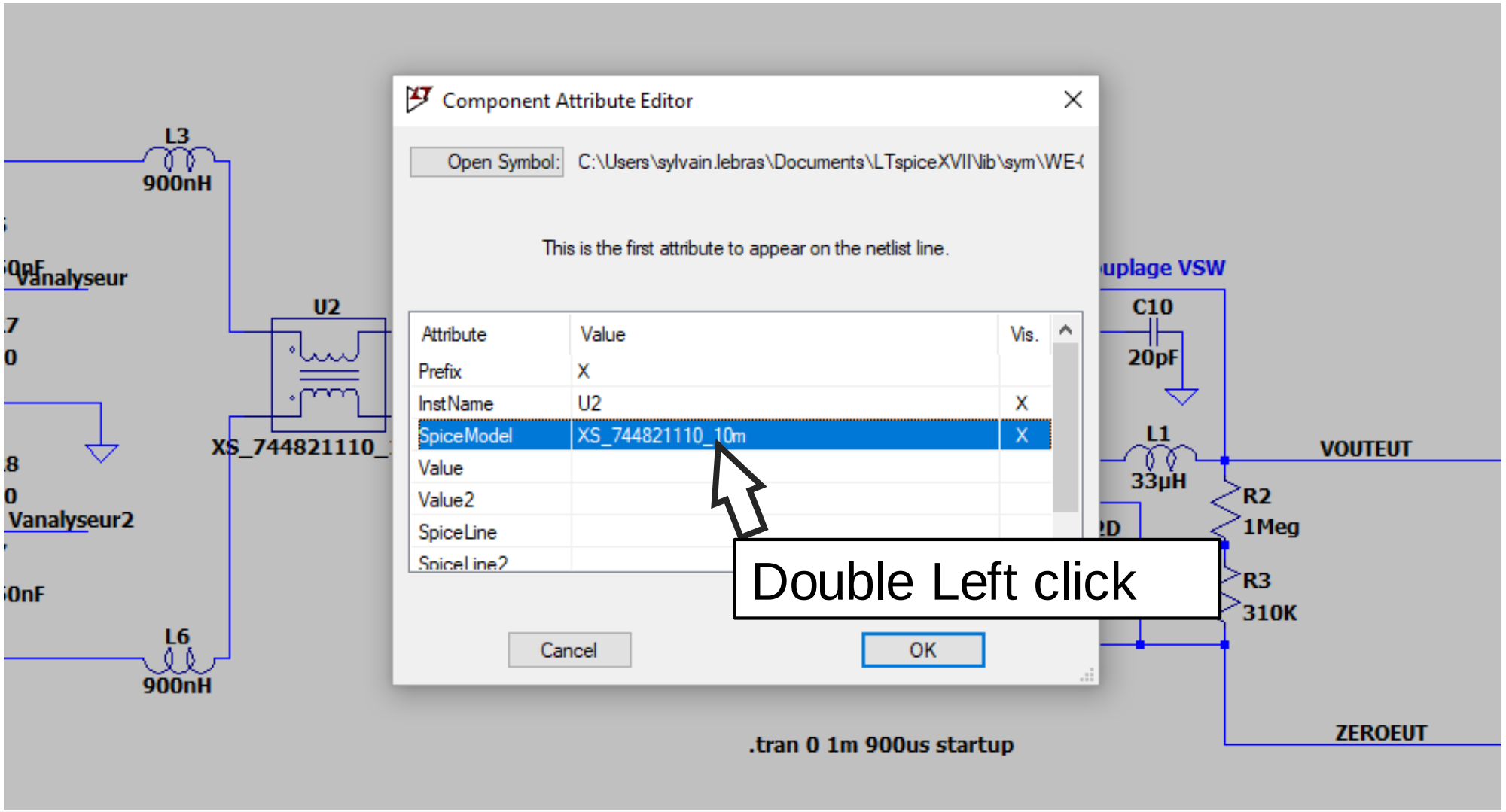
Going further with simulation

Fixing that buck in the simulation – Input Common mode choke



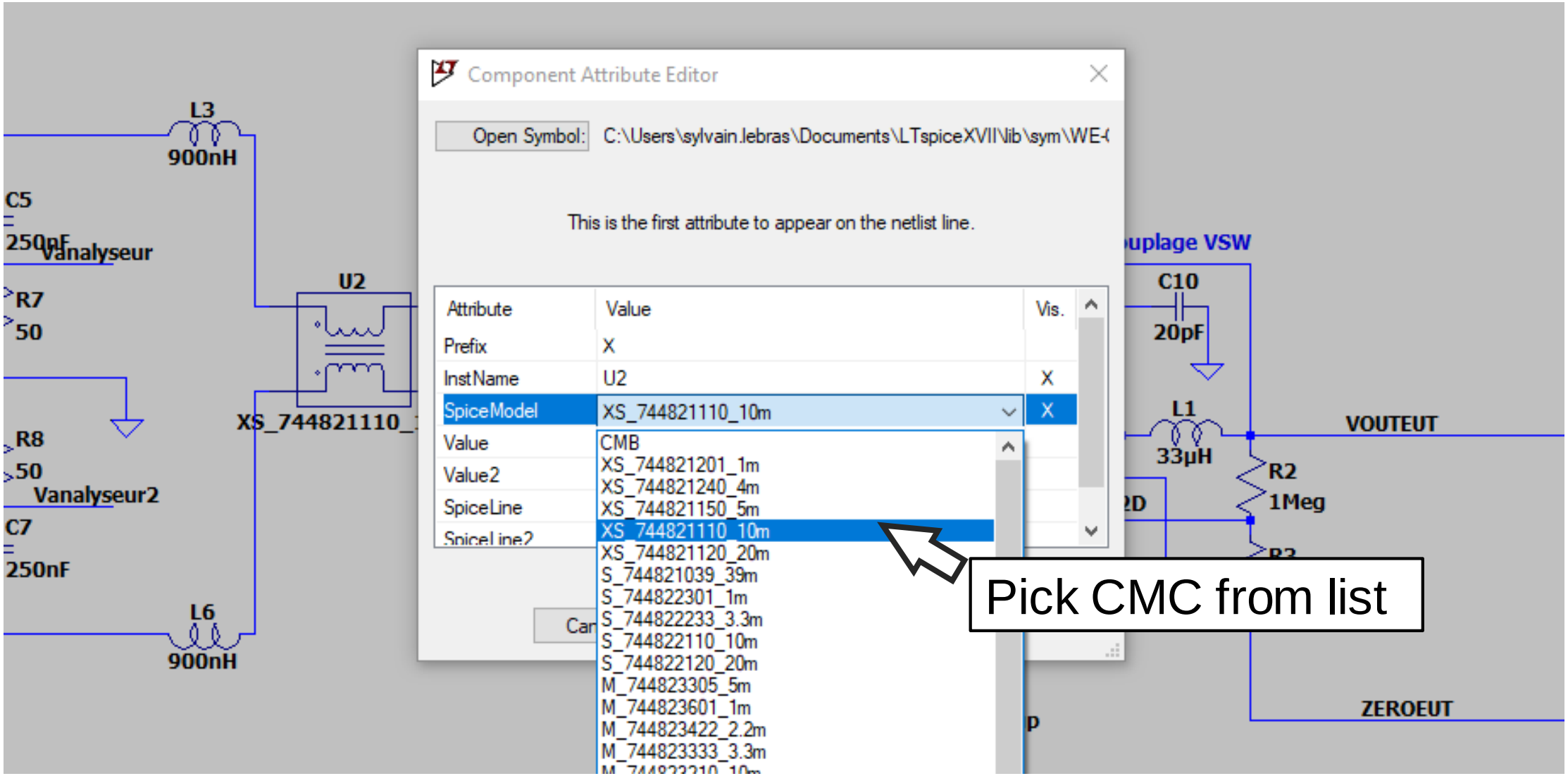
Going further with simulation

Fixing that buck in the simulation – Input Common mode choke



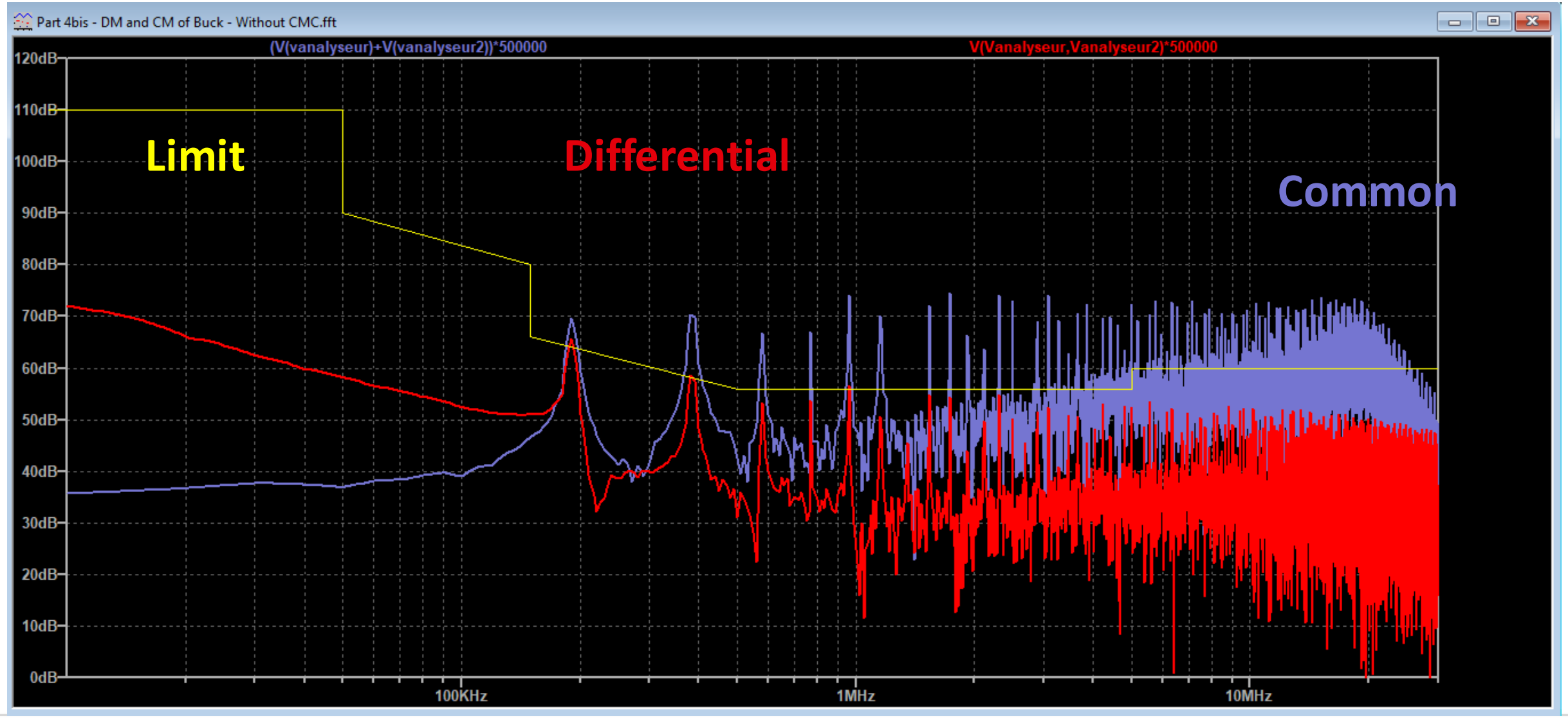
Going further with simulation

Fixing that buck in the simulation – Input Common mode choke



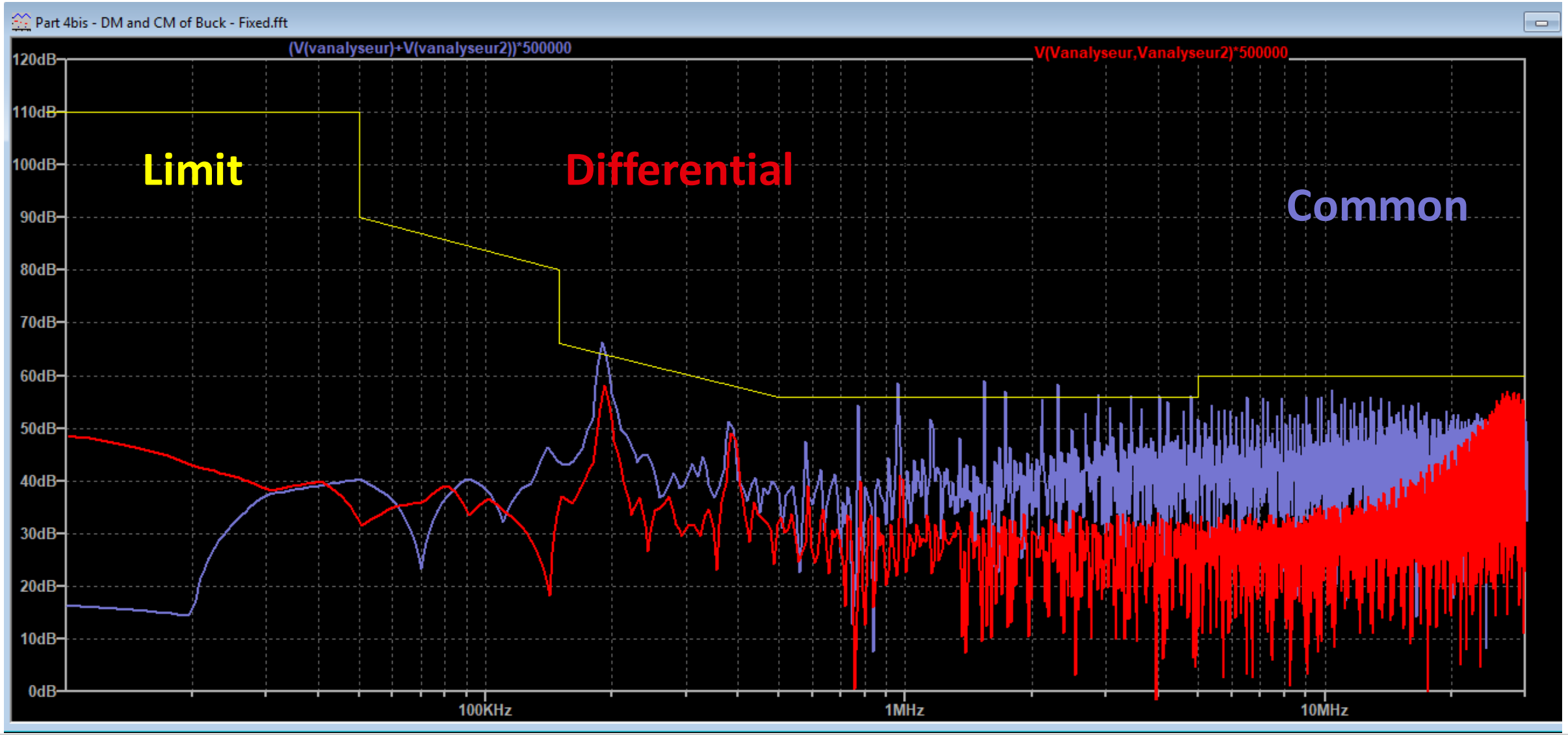
Going further with simulation

Fixing that buck in the simulation – **Without** Common mode choke



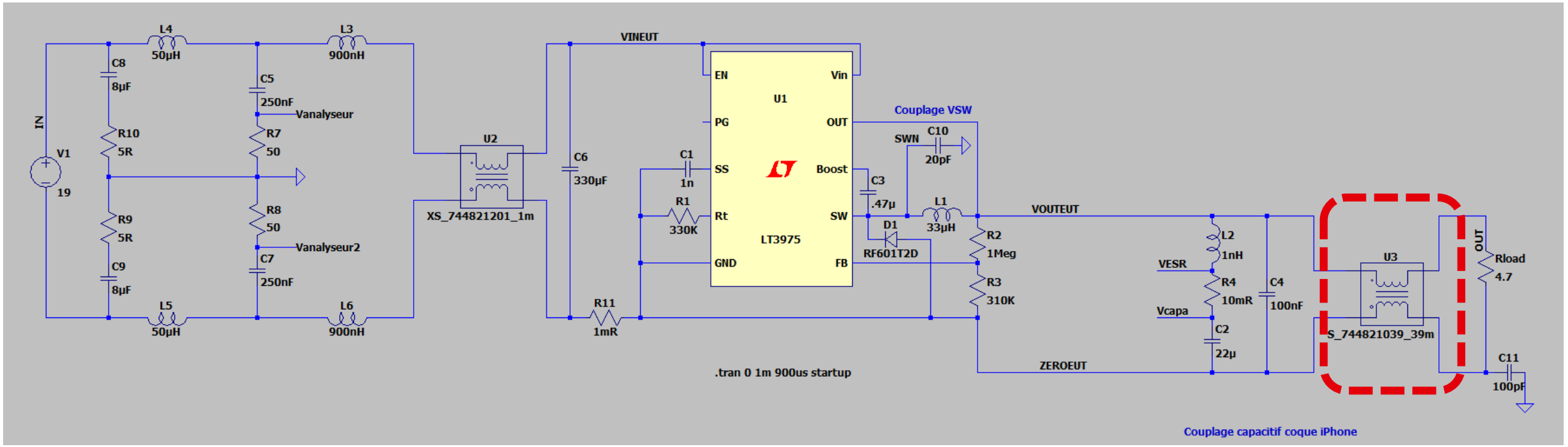
Going further with simulation

Fixing that buck in the simulation – **With** input Common mode choke



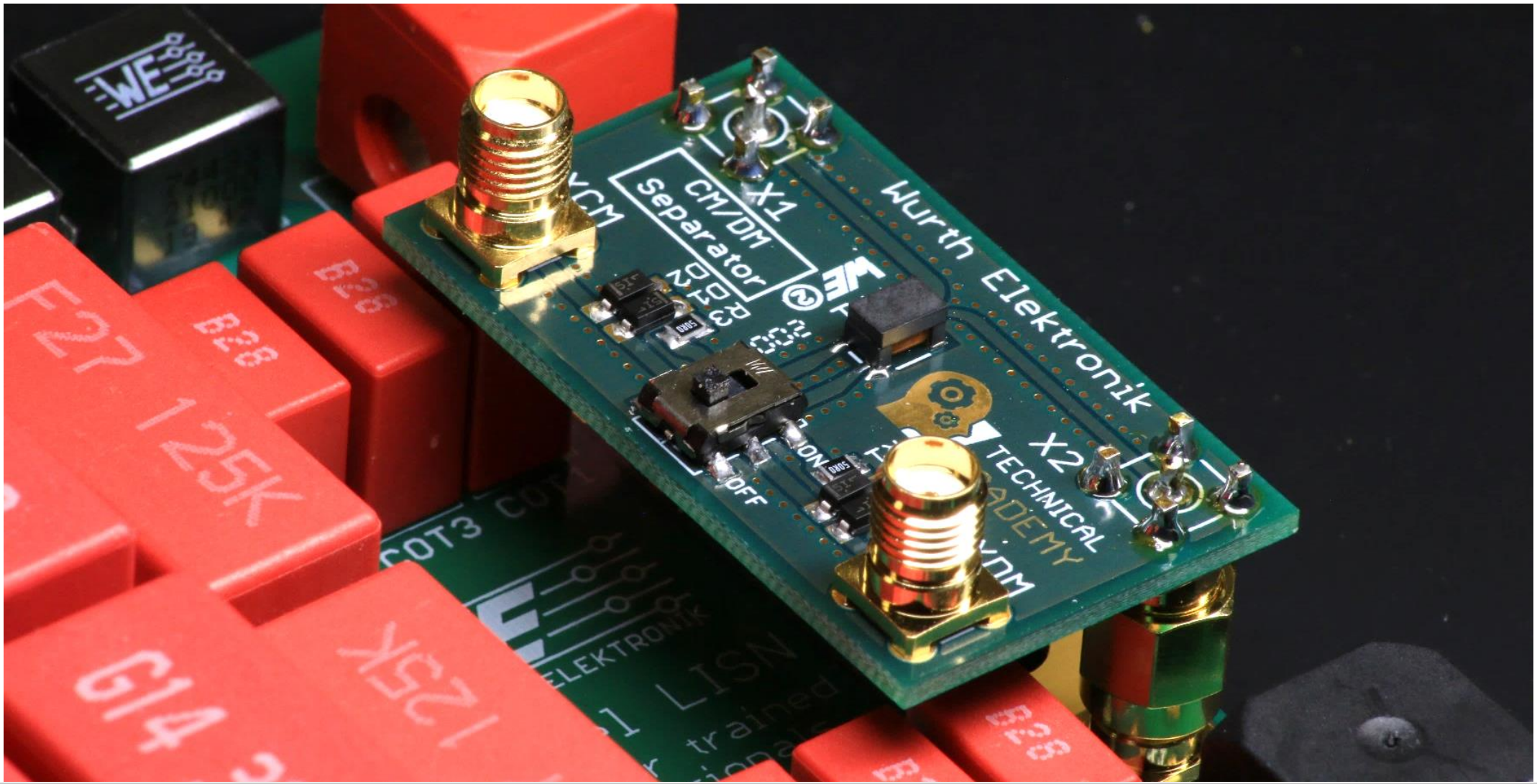
Going further with simulation

Fixing that buck in the simulation – **With** output CMC



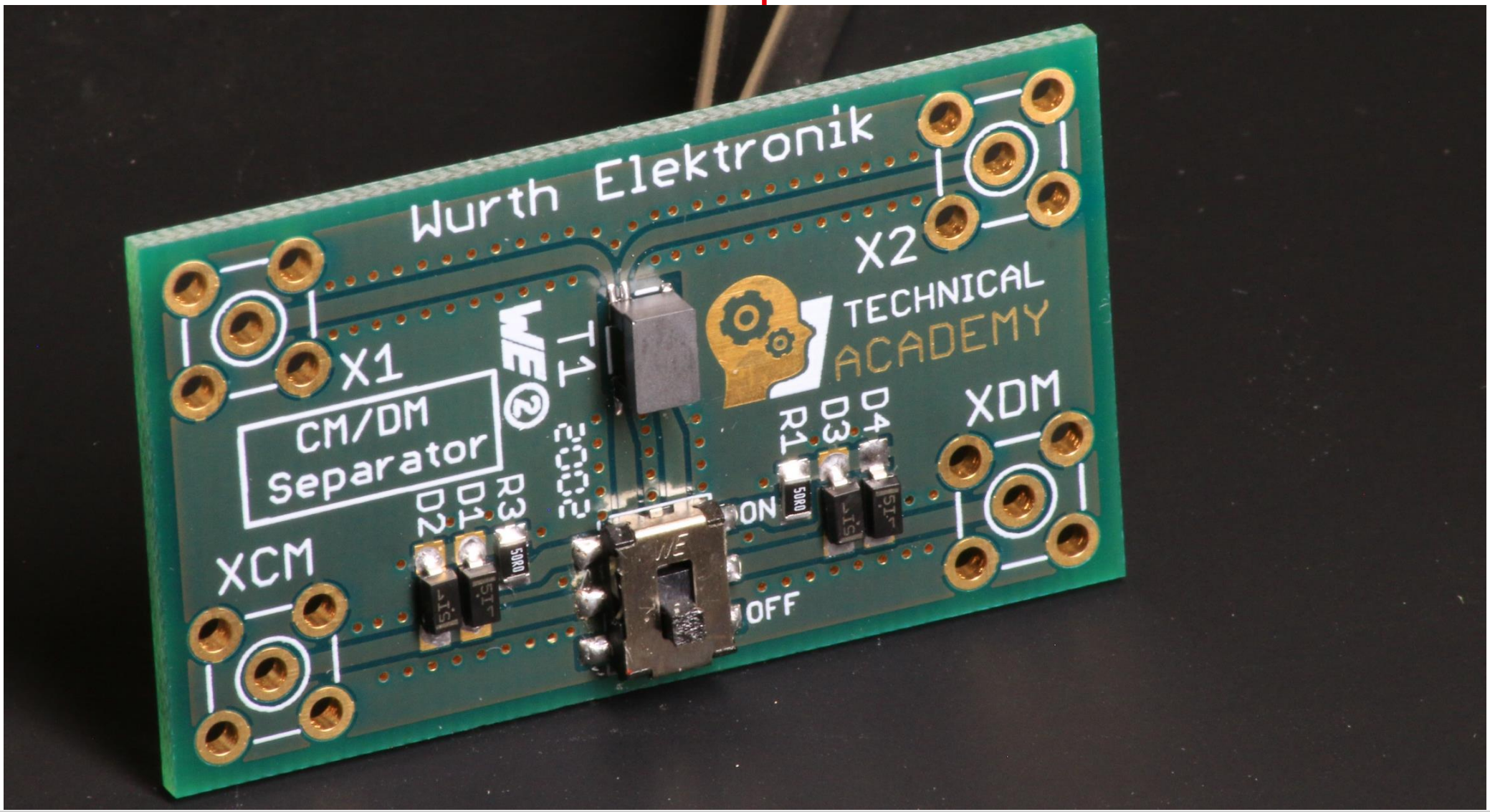
Going further ?

Common mode / Differential Mode separator in real life



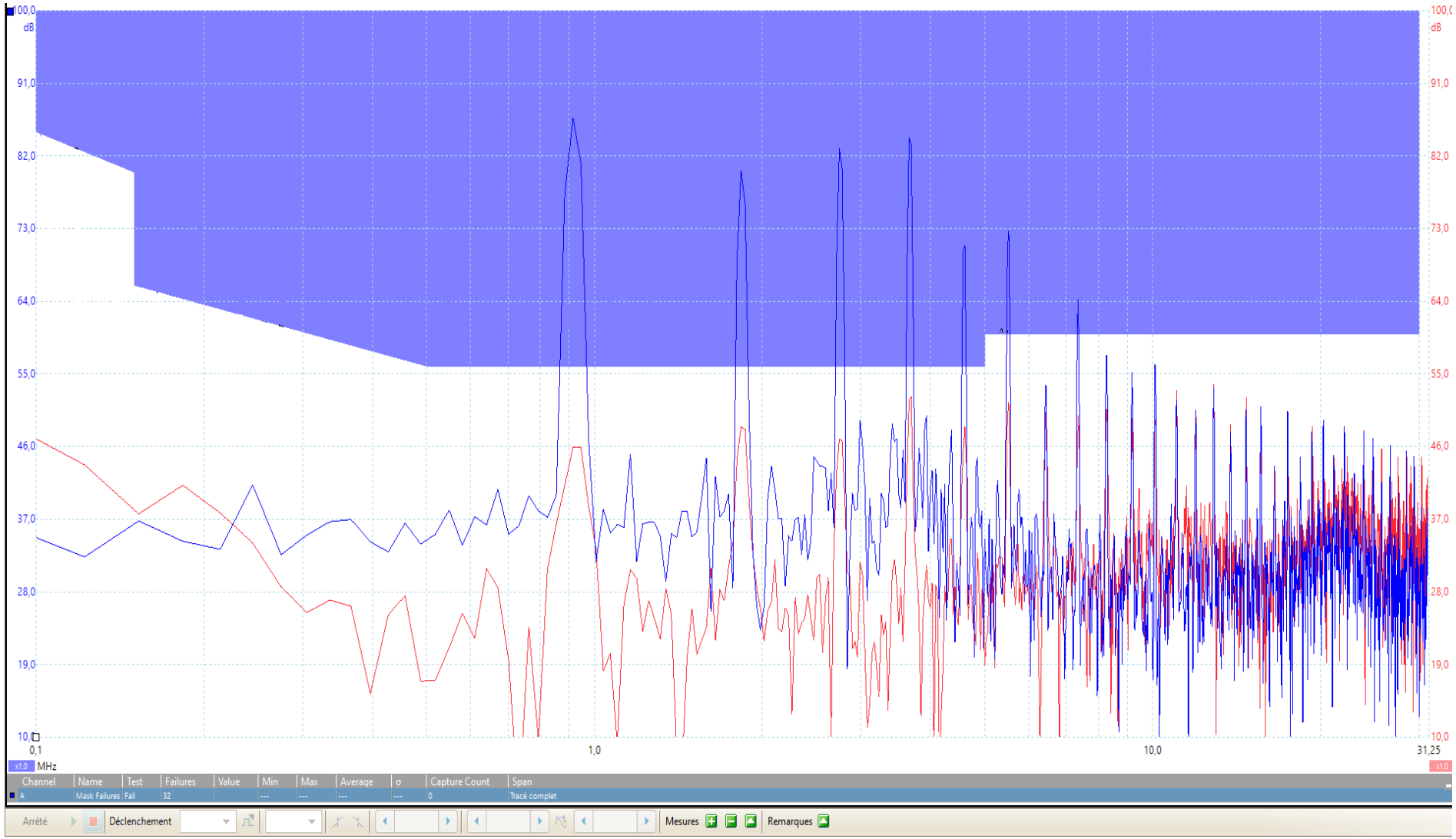
Going further ?

Common mode / Differential Mode separator in real life



Going further ?

Common mode / Differential Mode separator in real life



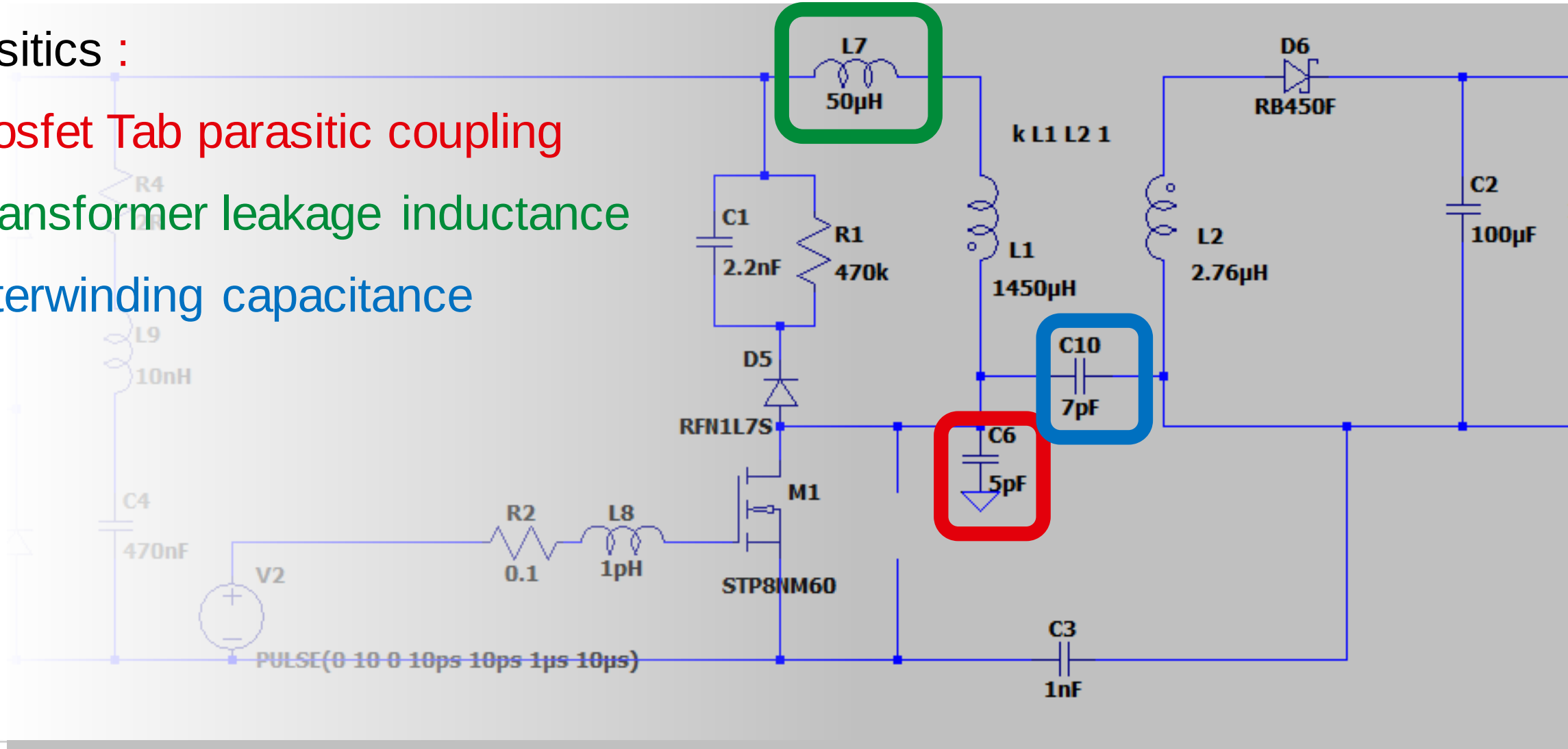
Modeling Real life examples

Flyback converter for lighting applications

Modeling Real life examples

Flyback converter for lighting applications

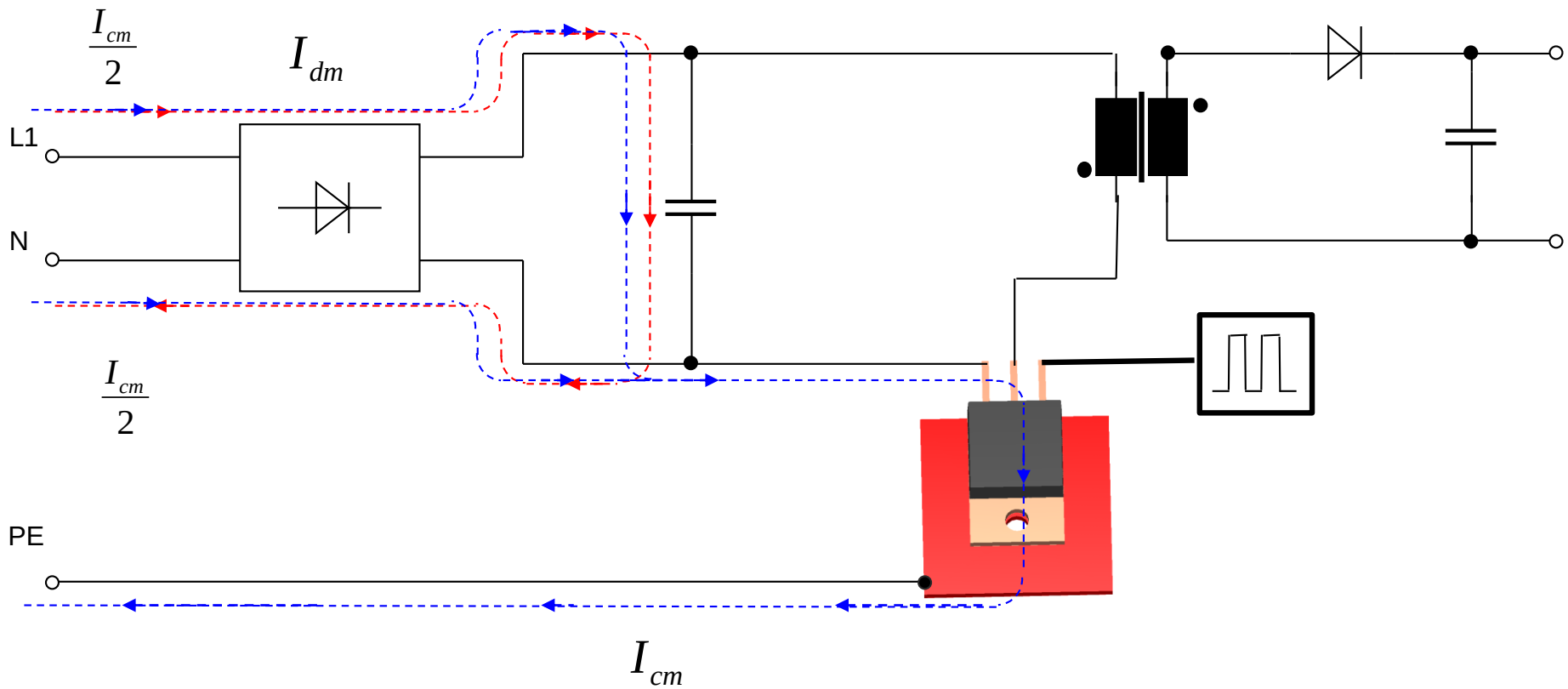
- Parasitics :
  - Mosfet Tab parasitic coupling
  - Transformer leakage inductance
  - Interwinding capacitance



Real life examples

Flyback converter for lighting applications

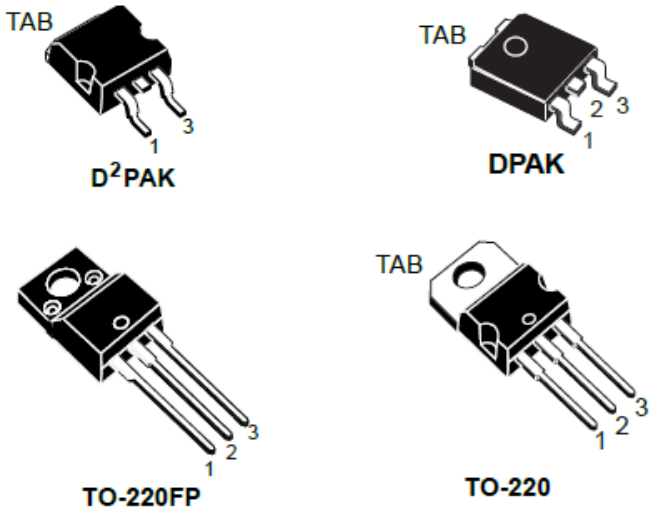
Mosfet Tab parasitic coupling

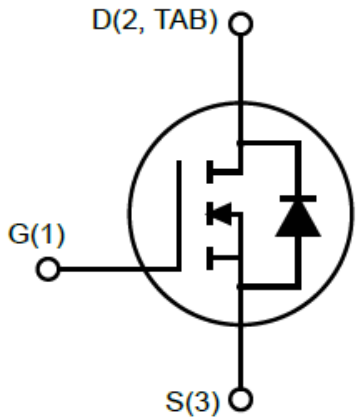


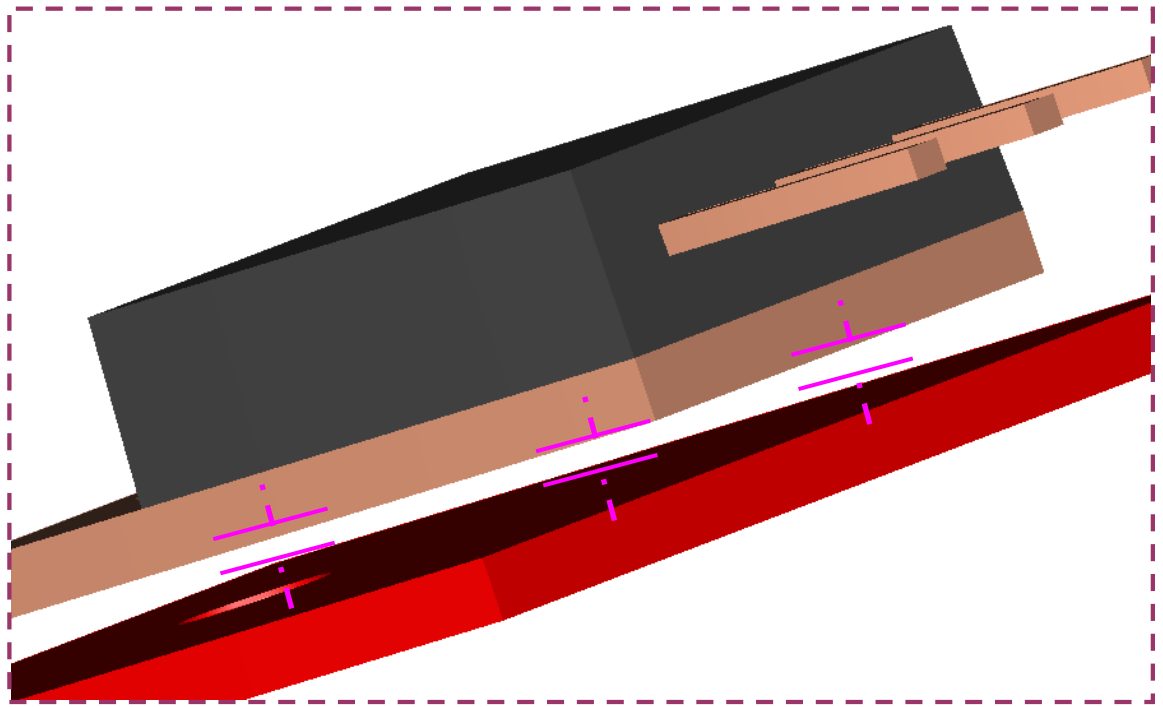
Real life examples

Flyback converter for lighting applications

Mosfet Tab parasitic coupling



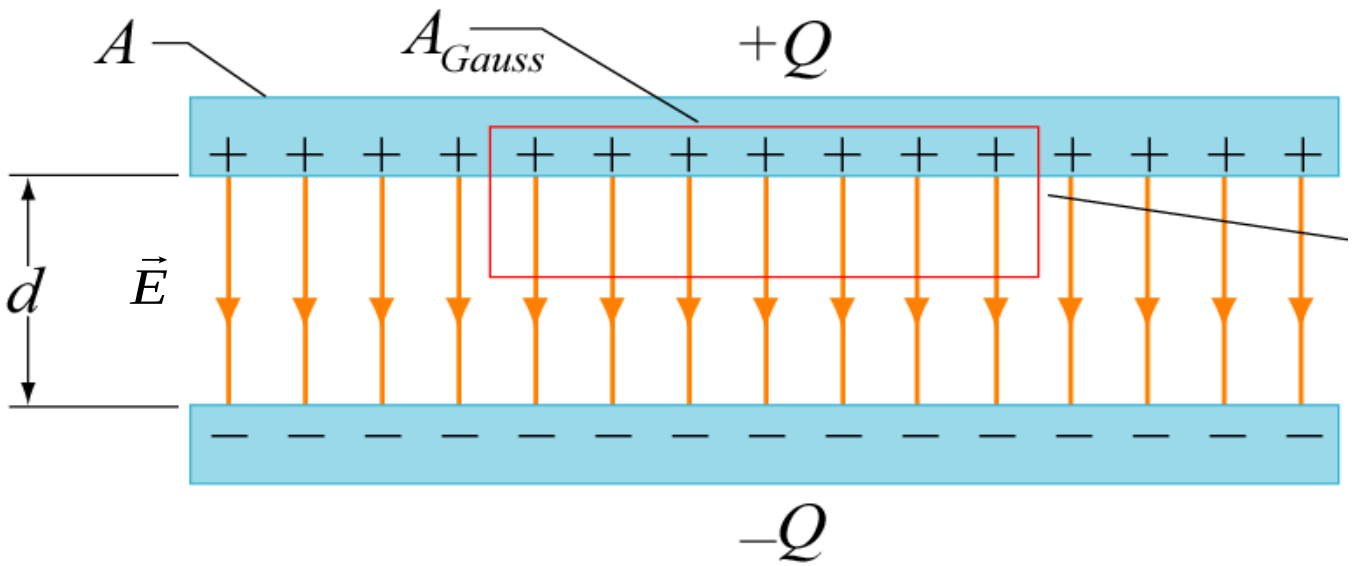




Real life examples

Flyback converter for lighting applications

Mosfet Tab parasitic coupling



$$C = \frac{\varepsilon_0 A}{d}$$

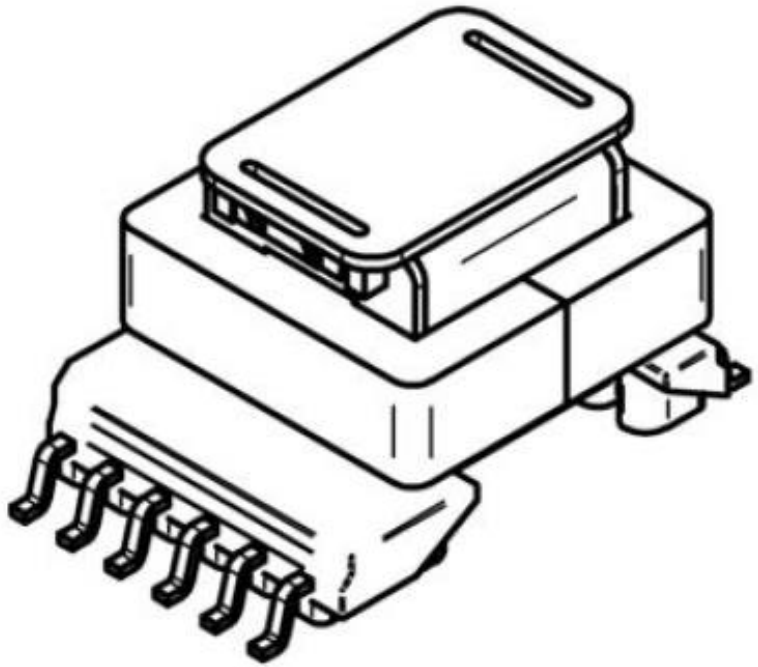
Real life examples

Flyback converter for lighting applications

Primary leakage inductance

D Electrical Properties:

Properties	Test conditions		Value	Unit	Tol.
Inductance	100 kHz/ 100 mV	L	1310	µH	±10%
Turns ratio		n	140 : 6 : 6 : 16		±3%
Saturation current	|ΔL/L| < 20%	I_{sat}	0.8	A	typ.
DC Resistance 1	@ 20°C	R_{DC1}	3000.0	mΩ	max.
DC Resistance 2	@ 20°C	R_{DC2}	25.0	mΩ	max.
DC Resistance 3	@ 20°C	R_{DC3}	25.0	mΩ	max.
DC Resistance 4	@ 20°C	R_{DC4}	450.0	mΩ	max.
Leakage inductance	100 kHz/ 100 mV	L_S	40.0	µH	max.
Insulation test voltage	W1,4 => W2,3	U_T	4000	V (AC)	



WE-UOST

Real life examples

Turn ratio to inductance ?

Transformers : from datasheet to LTSpice model

Primary inductance

1310	µH	Lp

Leakage inductance

50	µH	L1

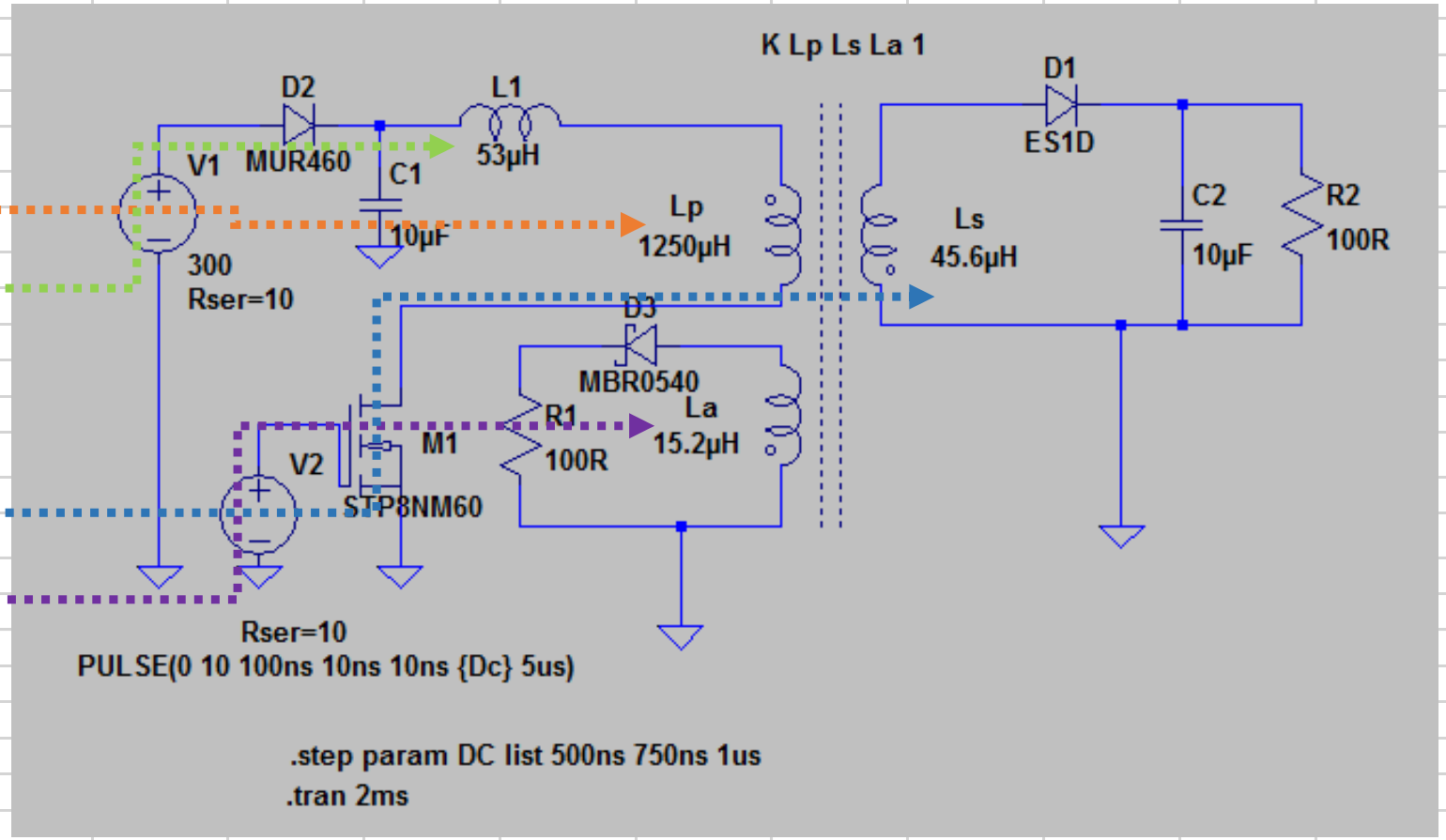
	Primary	Secondary	Aux
Ratio	130	6	16

Secondary inductance

2.79	µH	Ls

Auxiliary inductance

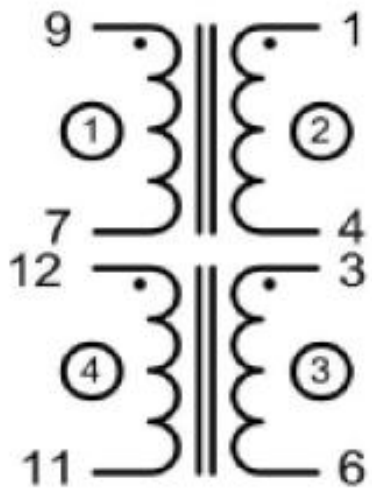
19.84	µH	La

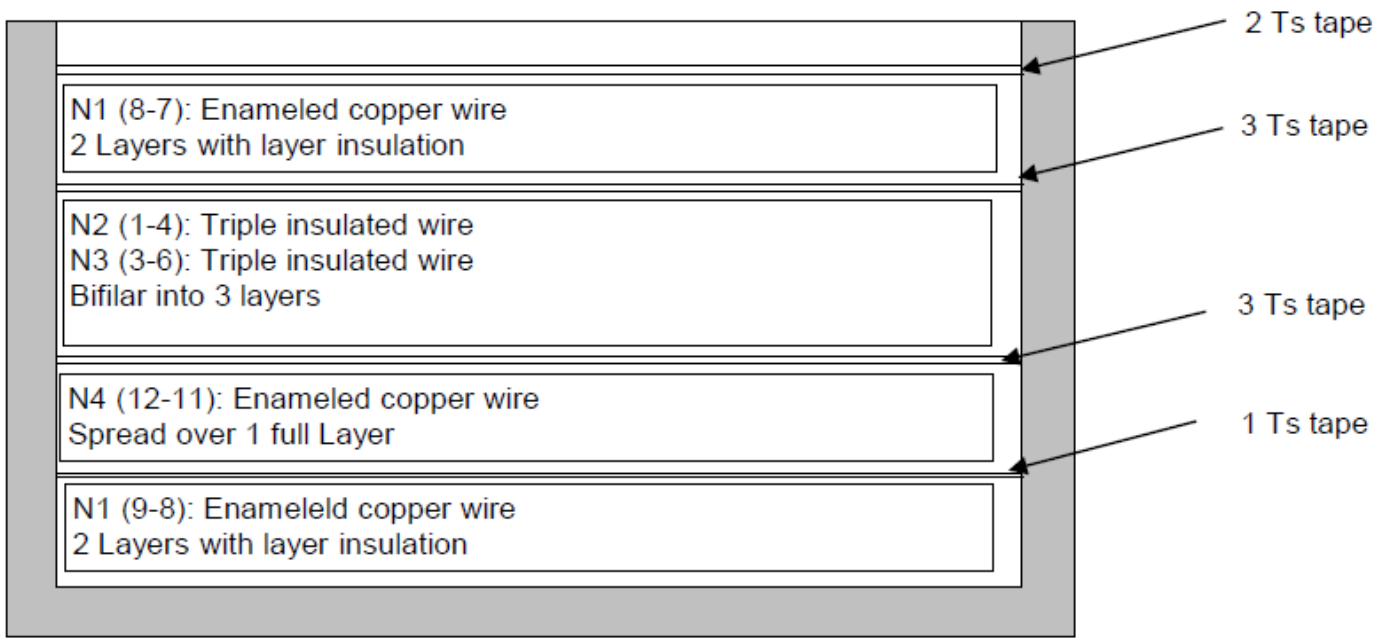


Real life examples

Flyback converter for lighting applications

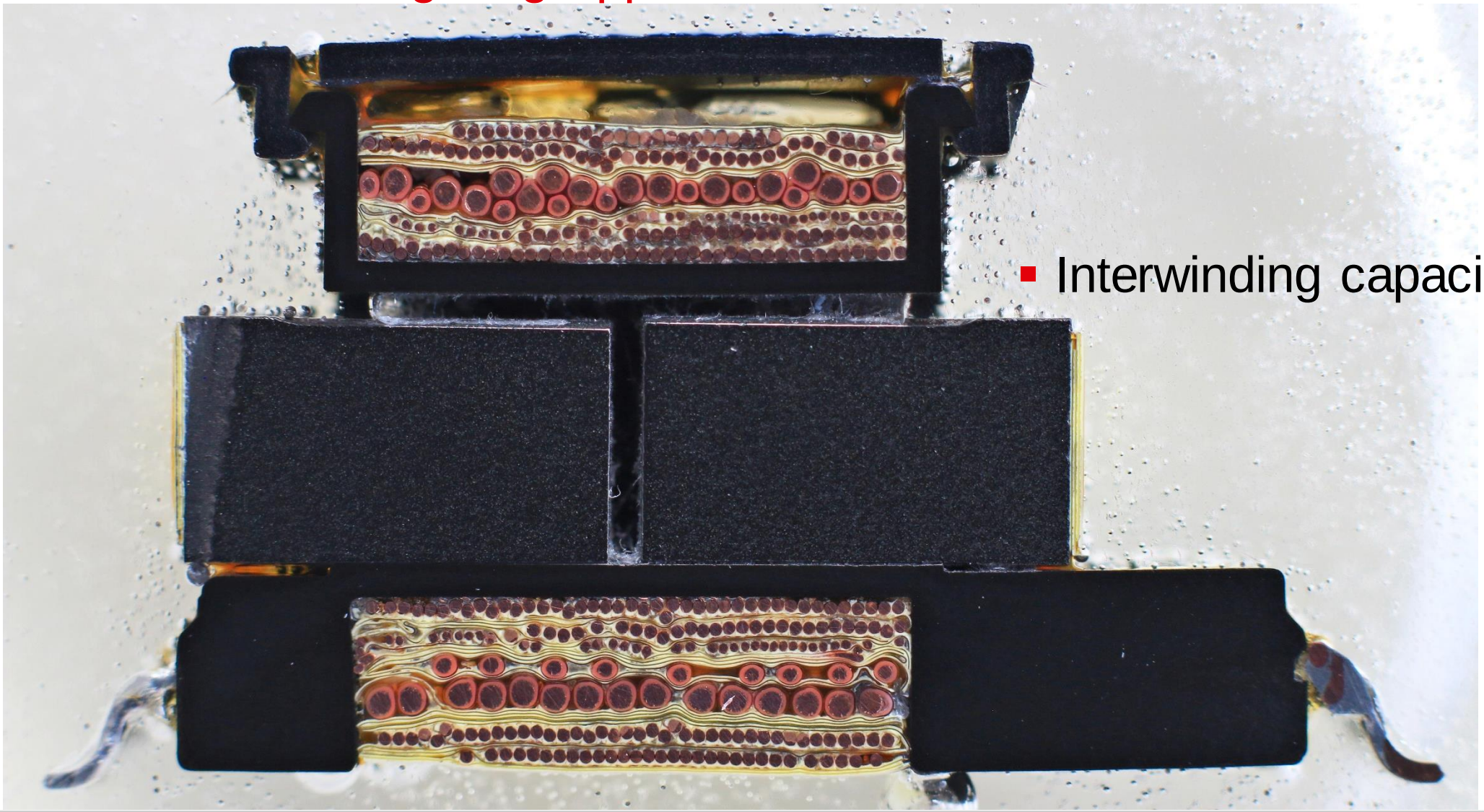
- Interwinding capacitance ?





Real life examples

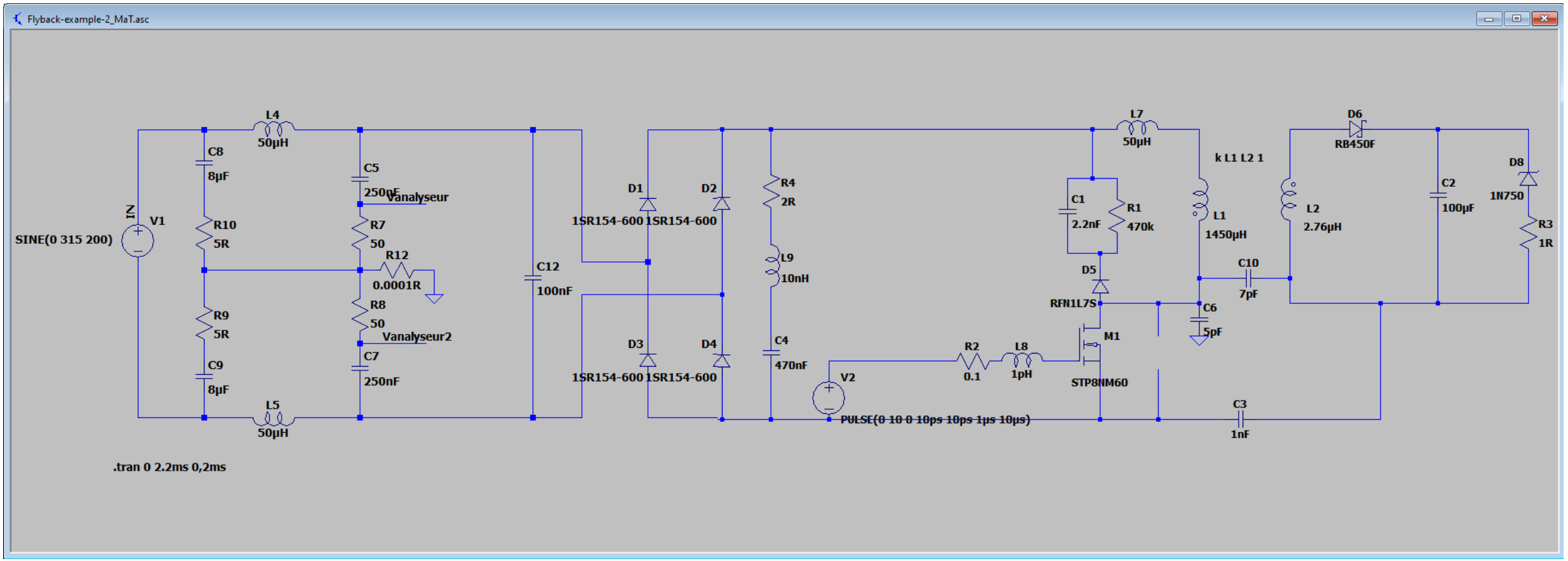
Flyback converter for lighting applications



- Interwinding capacitance ?

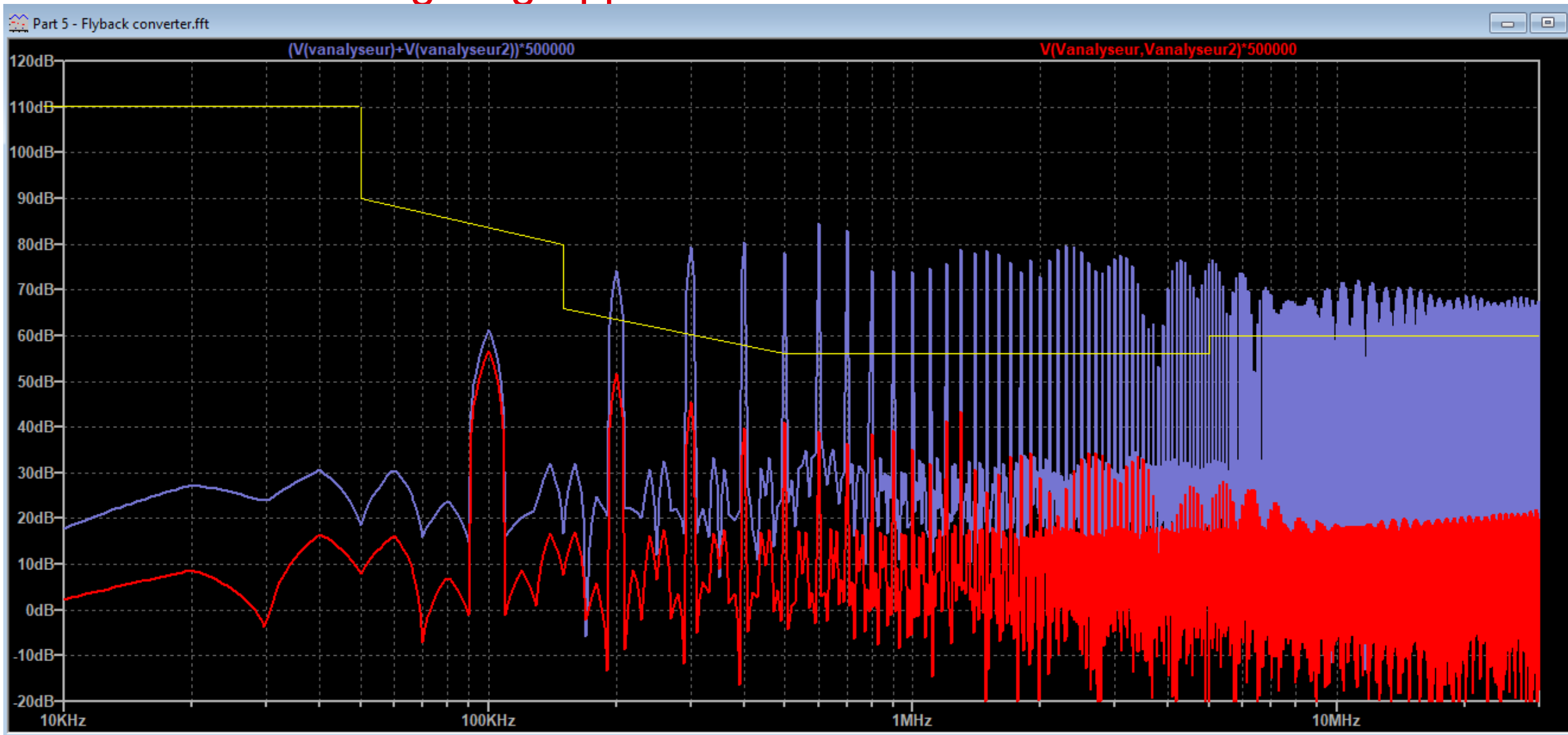
Real life examples

Flyback converter for lighting applications



Real life examples

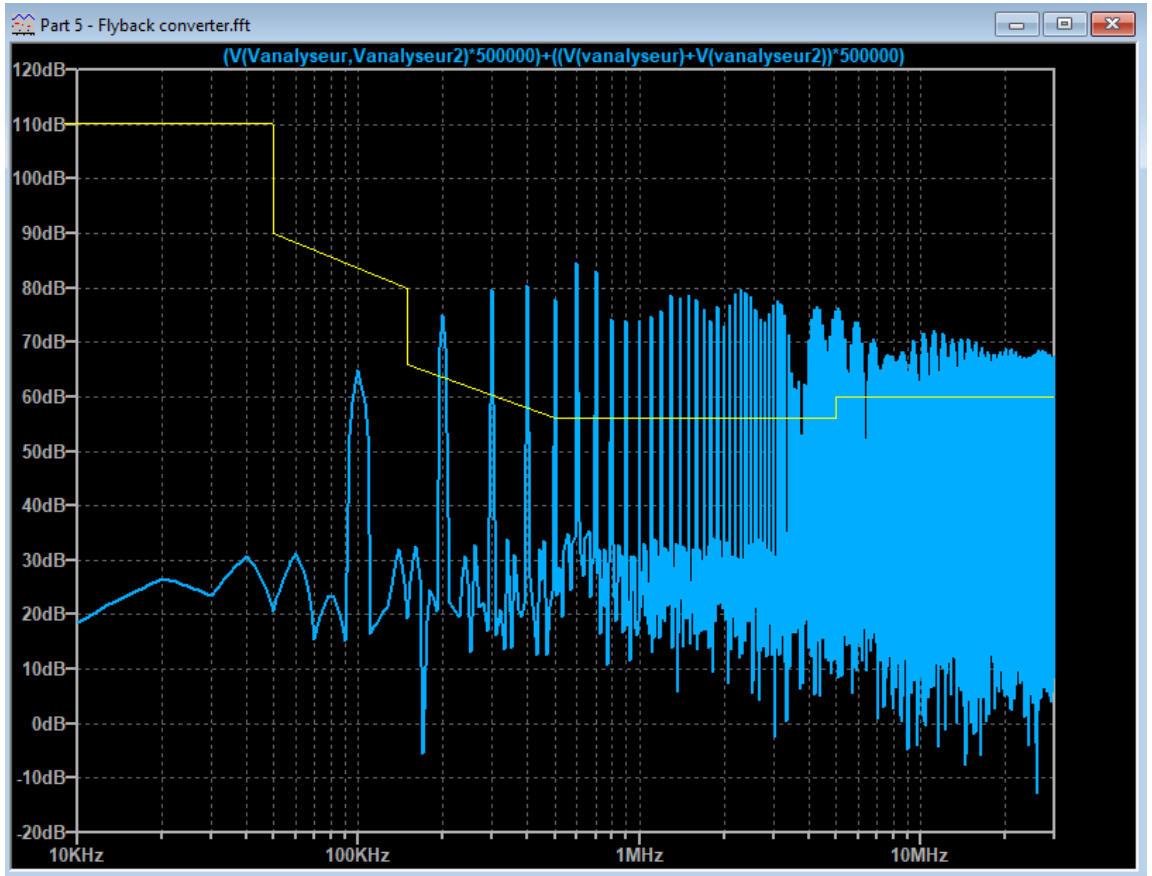
Flyback converter for lighting applications



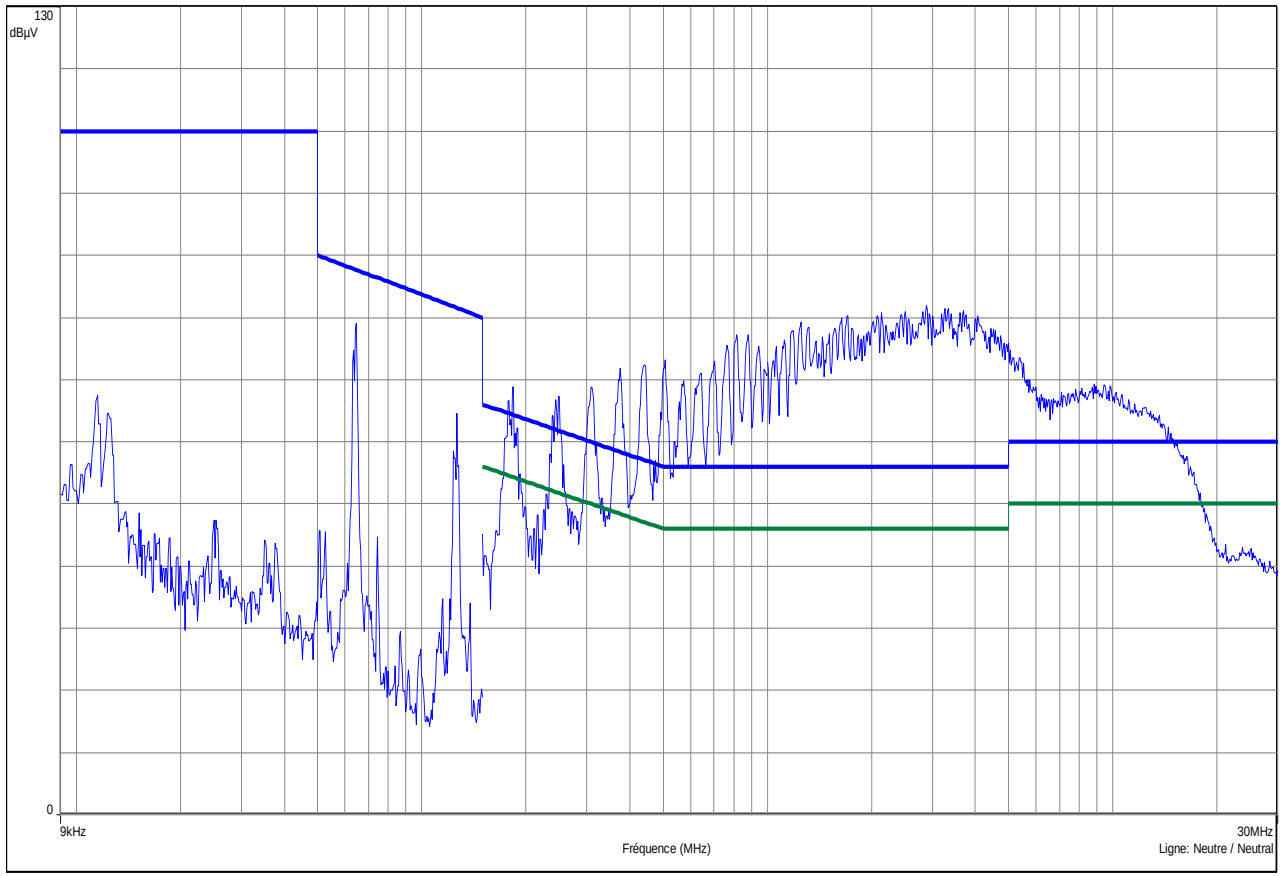
Real life examples

Flyback converter for lighting applications

Simulation



Example of actual measurement



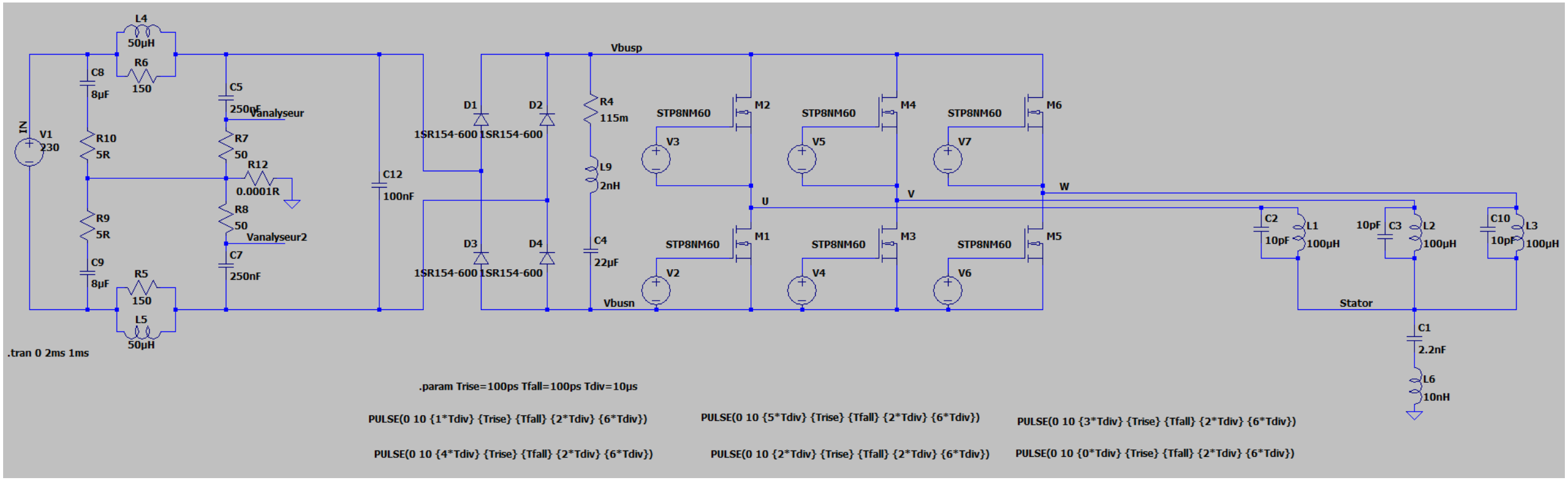
Real life examples

Mains voltage BLDC driver + motor

Real life examples

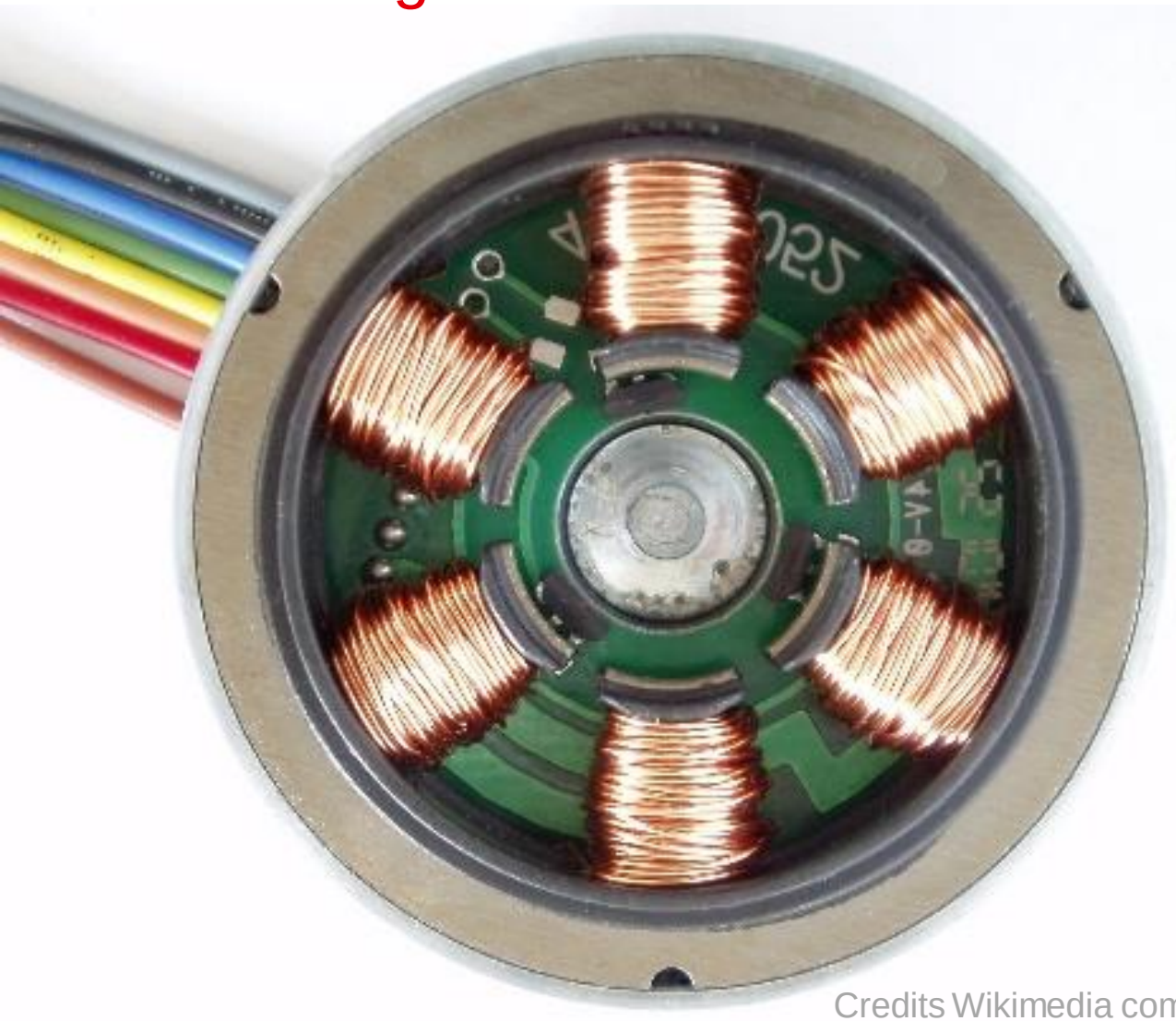
Mains voltage BLDC driver + motor

- Parasitic coupling to and through stator
- Influence of grounding
- Slew rate of driver
- Dead time impact



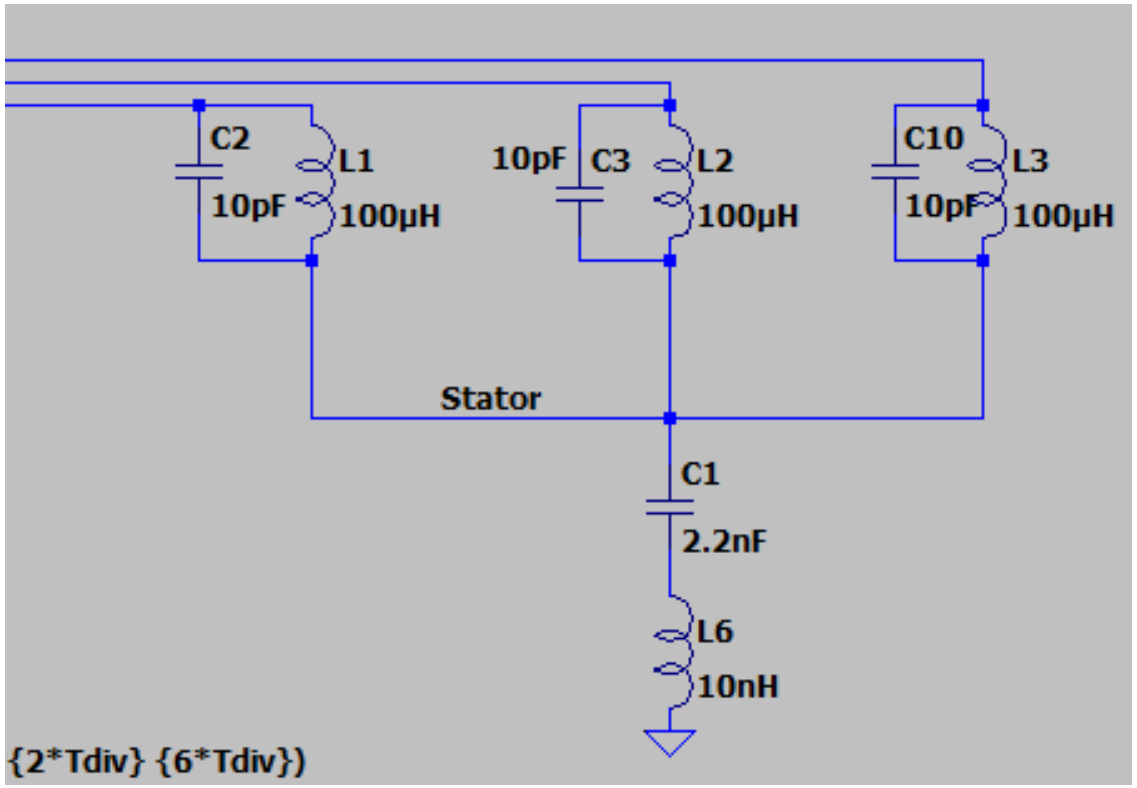
Real life examples

Mains voltage BLDC driver + motor



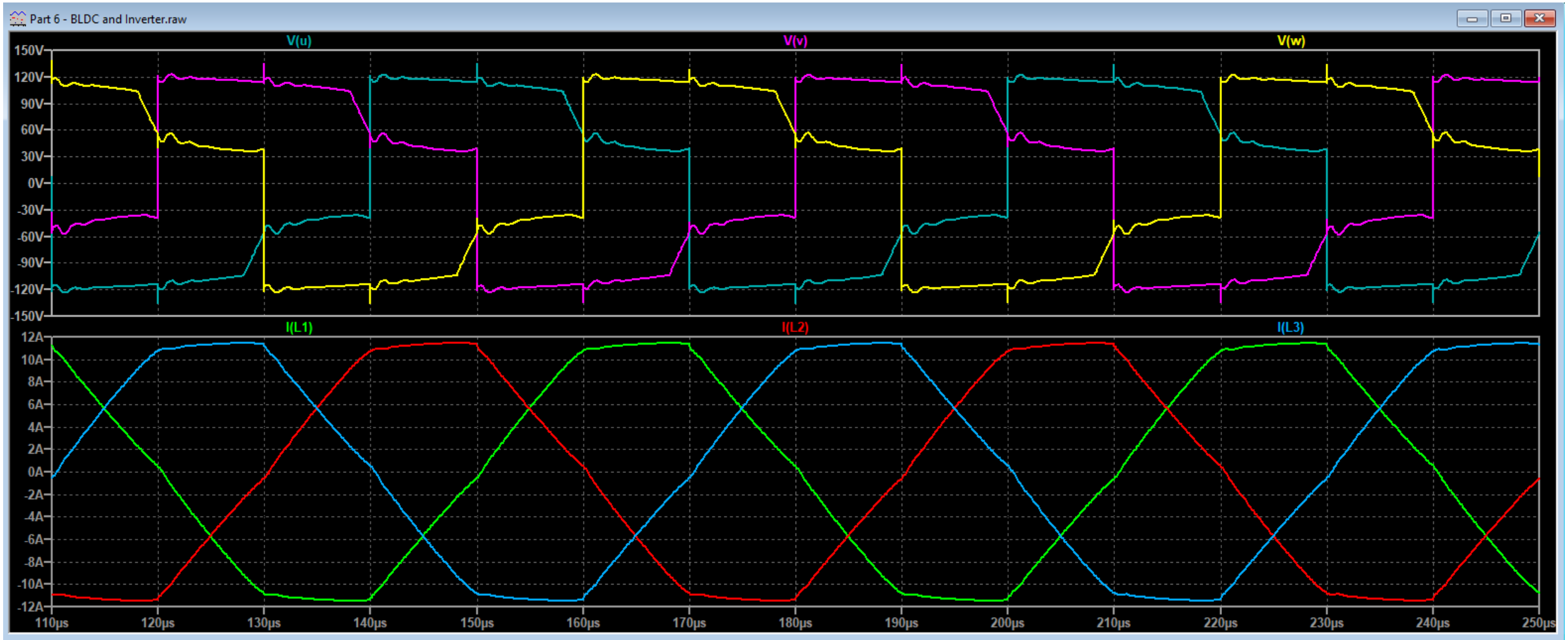
Credits Wikimedia commons

- Parasitic coupling to and through stator
- Influence of grounding (of stator)



Real life examples

Mains voltage BLDC driver + motor



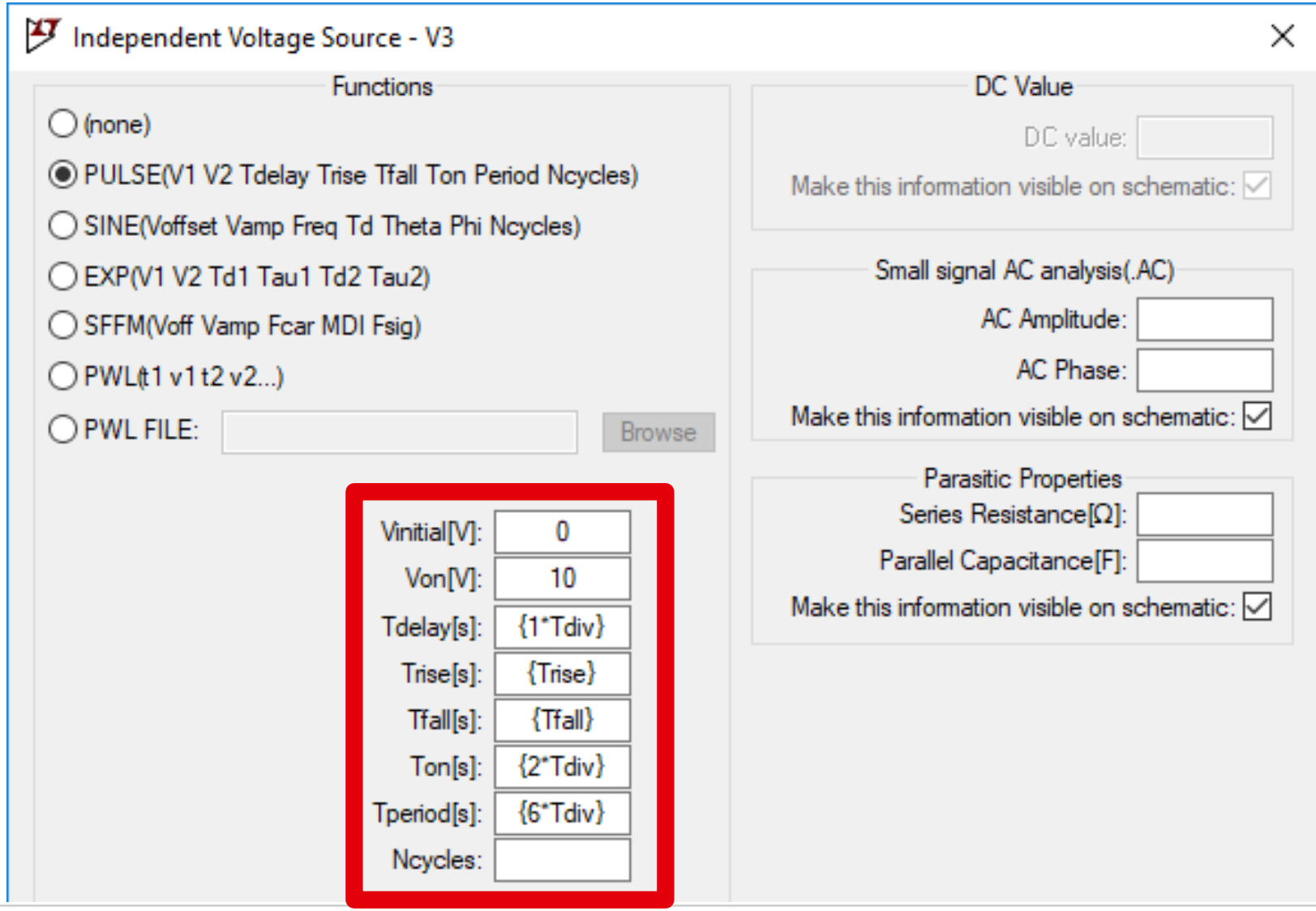
Real life examples

Mains voltage BLDC driver + motor

- Parametric simulation

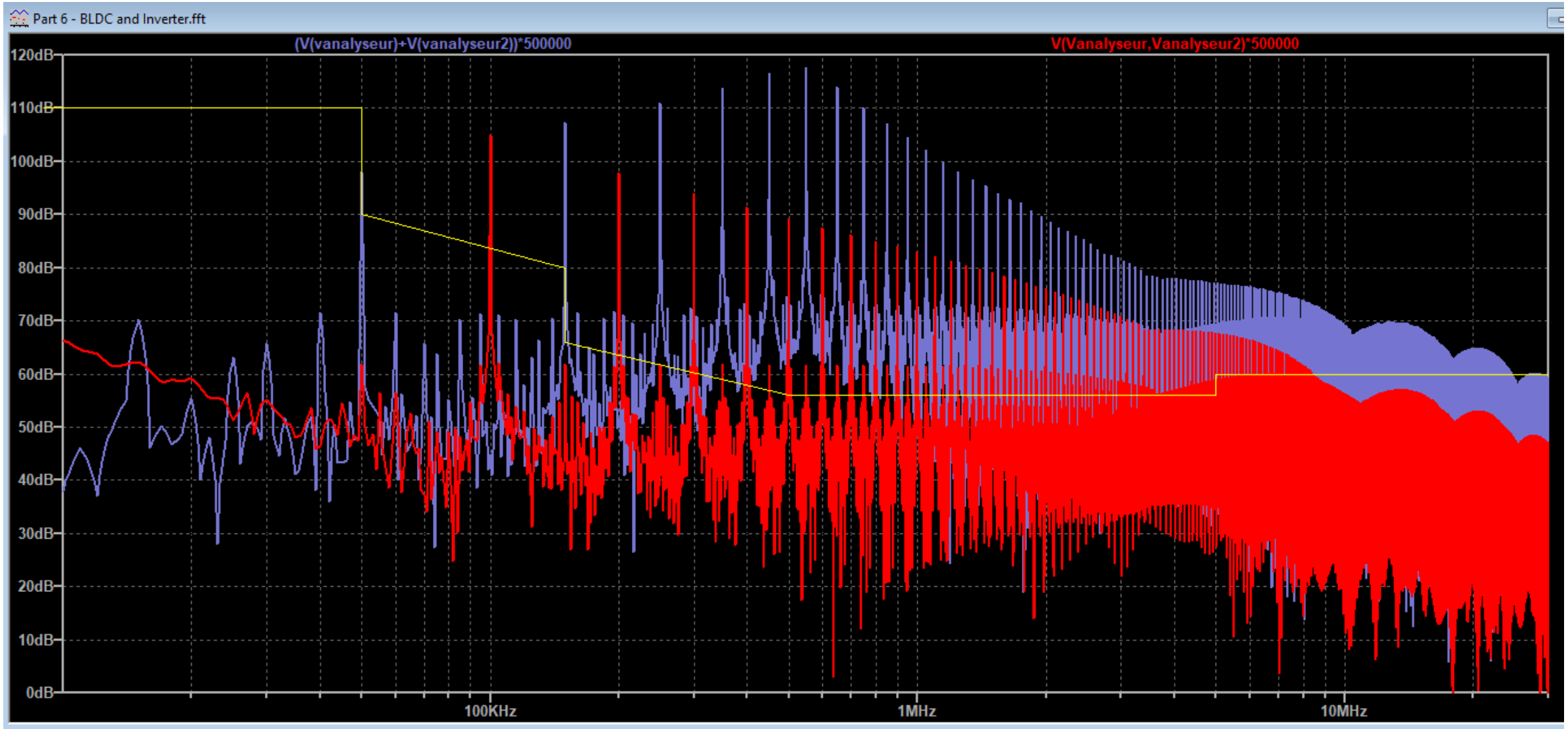
```
.param Trise=100ps Tfall=100ps Tdiv=10µs
```

- .STEP is possible to see impact of slew rate and dead time on EMC signature



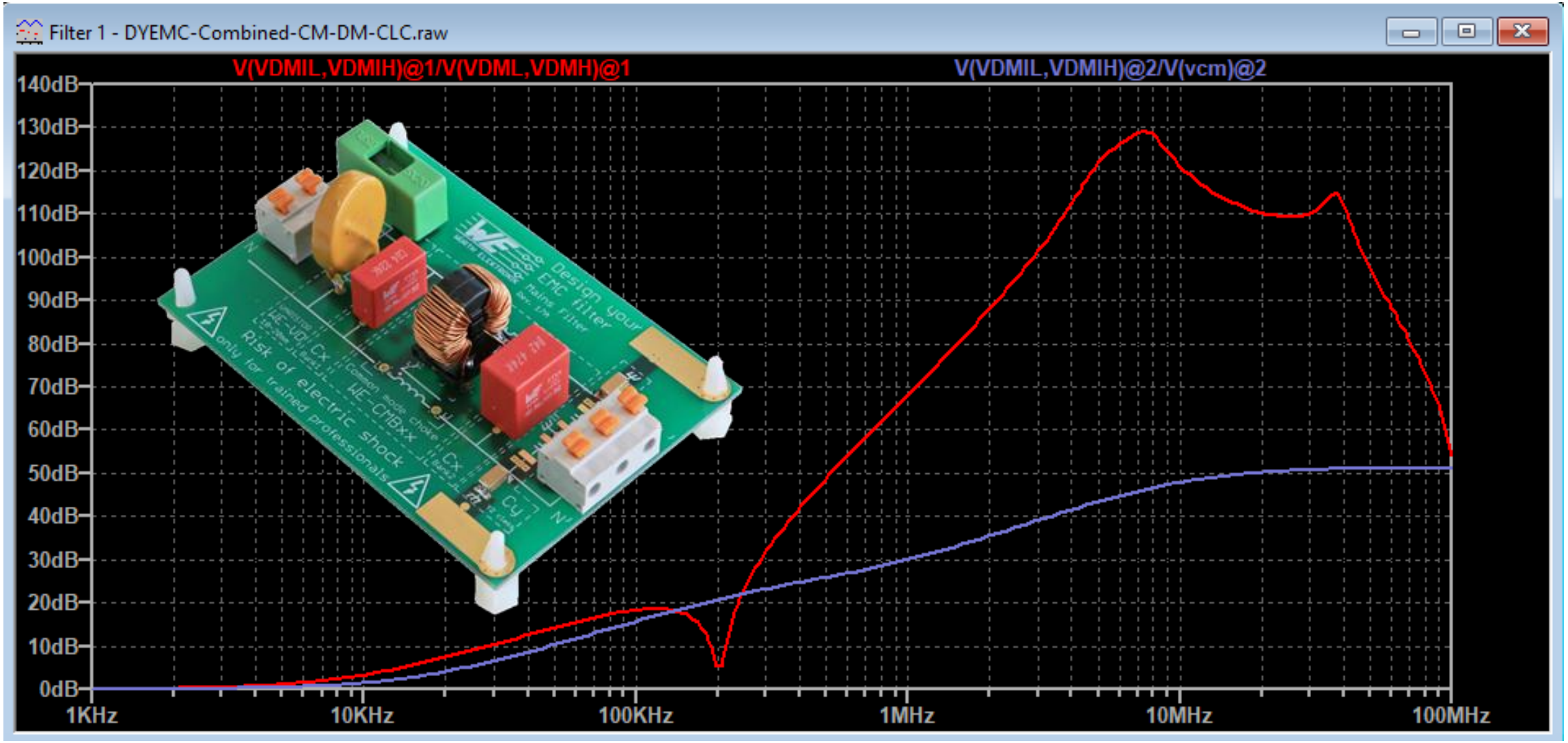
Real life examples

Mains voltage BLDC driver + motor



Evaluation of Filter Insertion losses

Design your EMC filter in LTspice

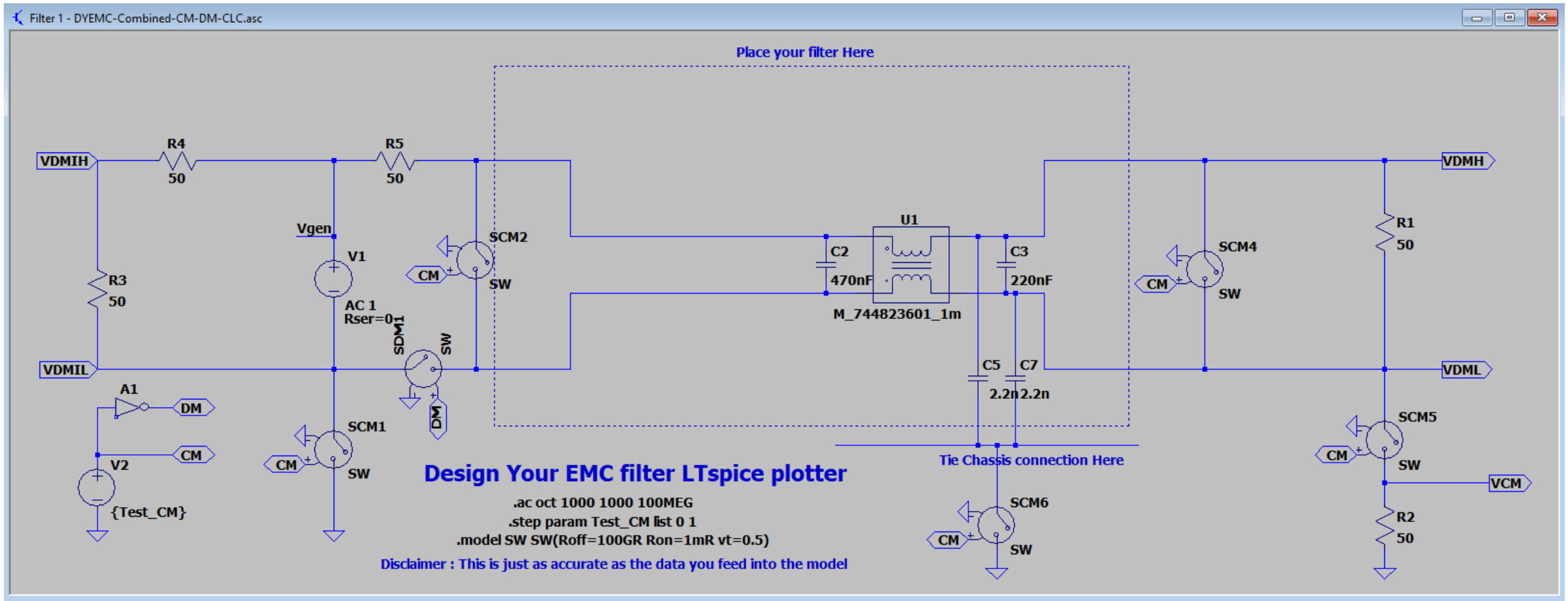


Evaluation of Filter Insertion losses

Design your EMC filter in LTspice

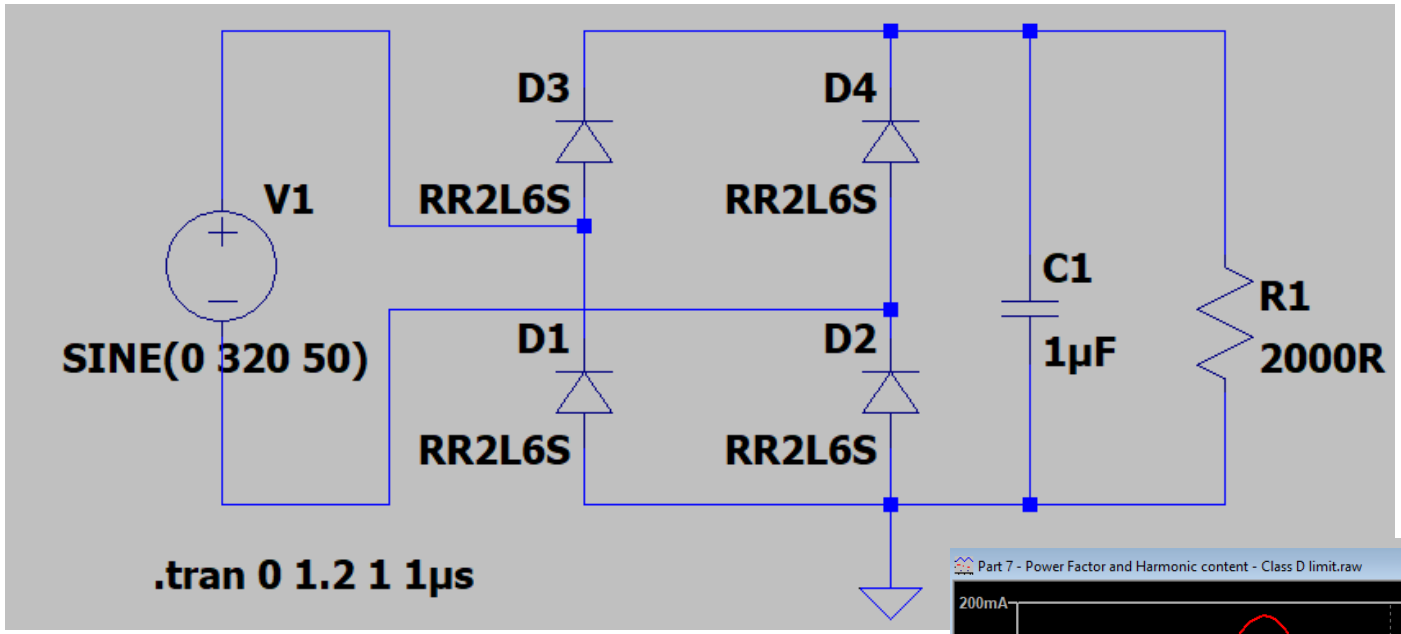
V(VDMIL,VDMIH)@1/V(VDML,VDMH)@1

V(VDMIL,VDMIH)@2/V(vcm)@2

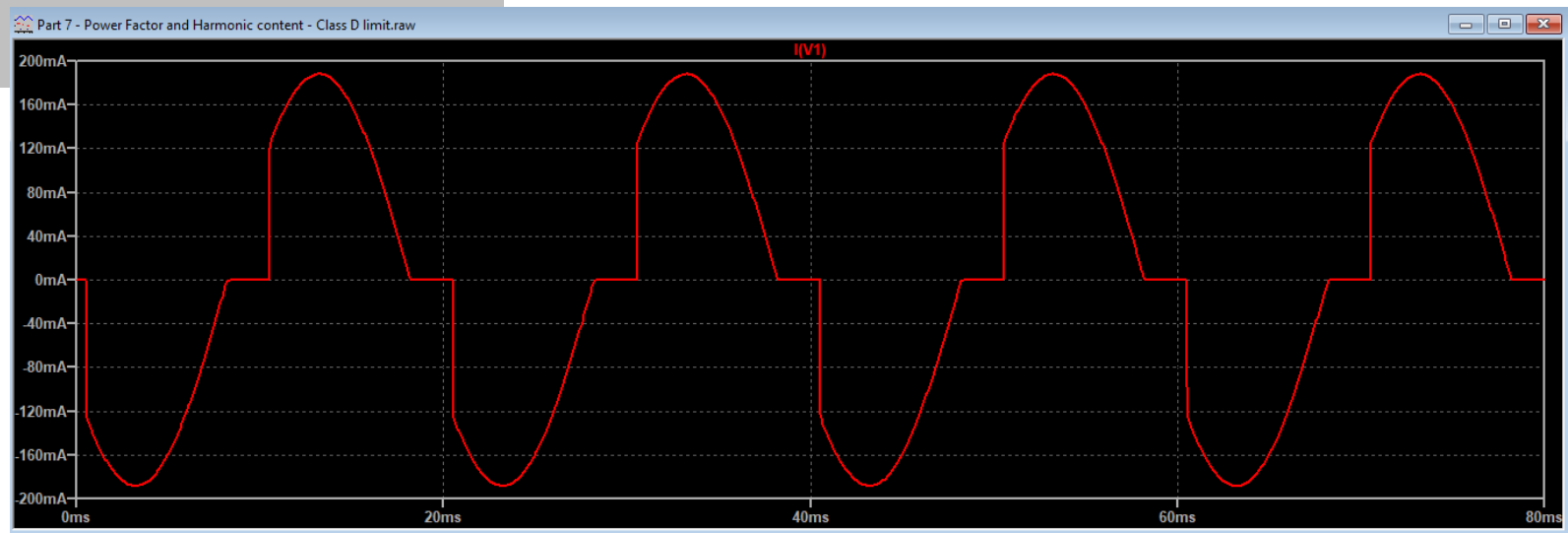


Power Factor and Harmonic current

Anticipate IEC 61000-3-2

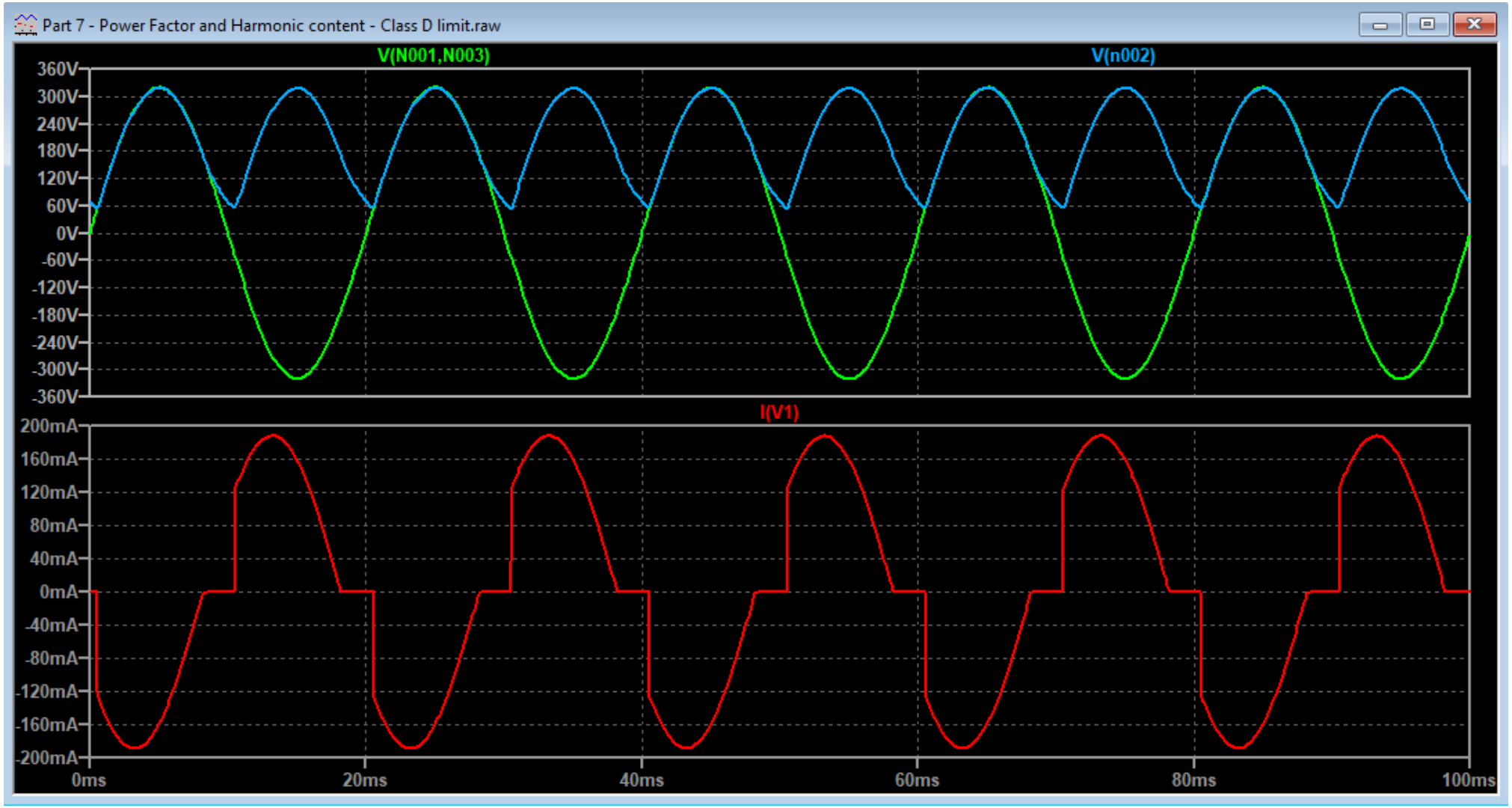


Harmonic order (n)	Maximum permissible harmonic current per watt (mA/W)
3	3.4
5	1.9
7	1.0
9	0.5
11	0.35
13	0.3
$15 \leq n \leq 39$ (odd harmonics only)	3.85/n



Power Factor and Harmonic current

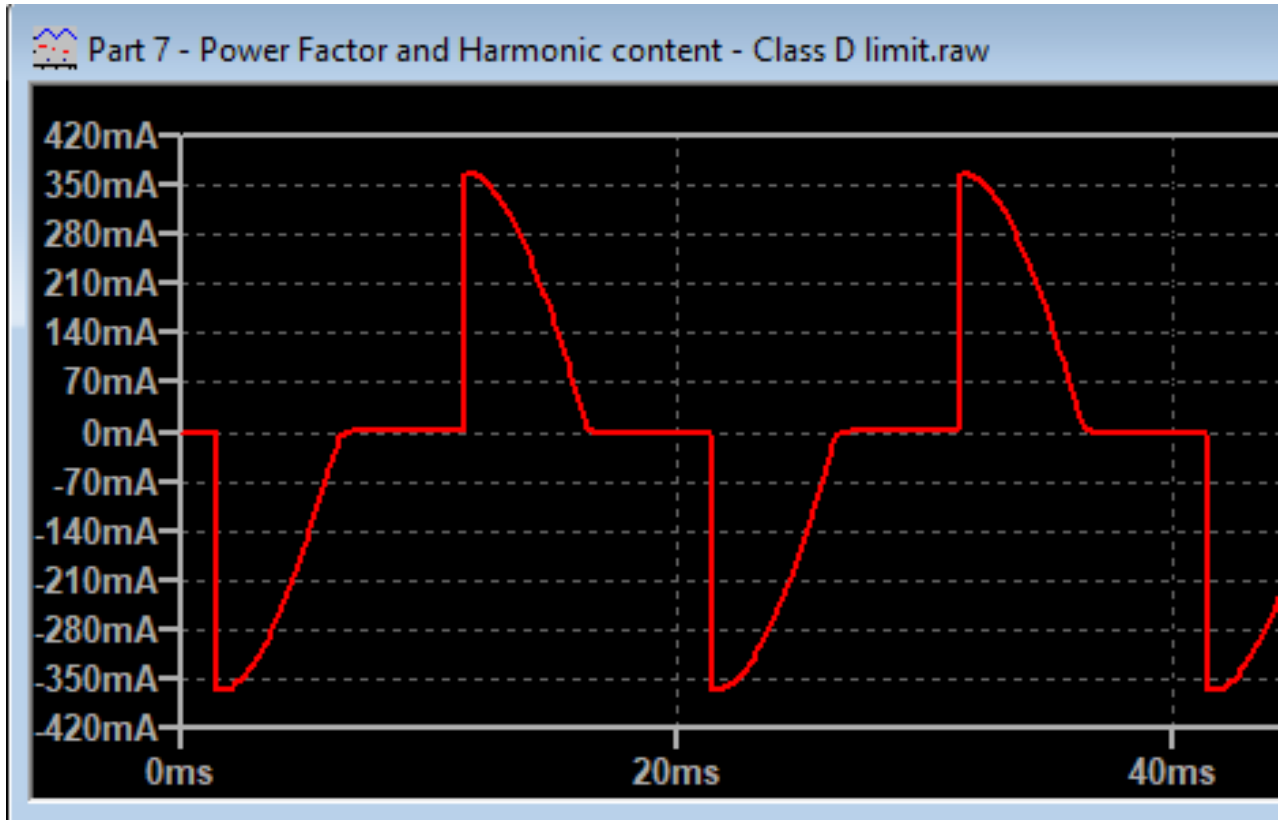
Anticipate IEC 61000-3-2



Power Factor and Harmonic current

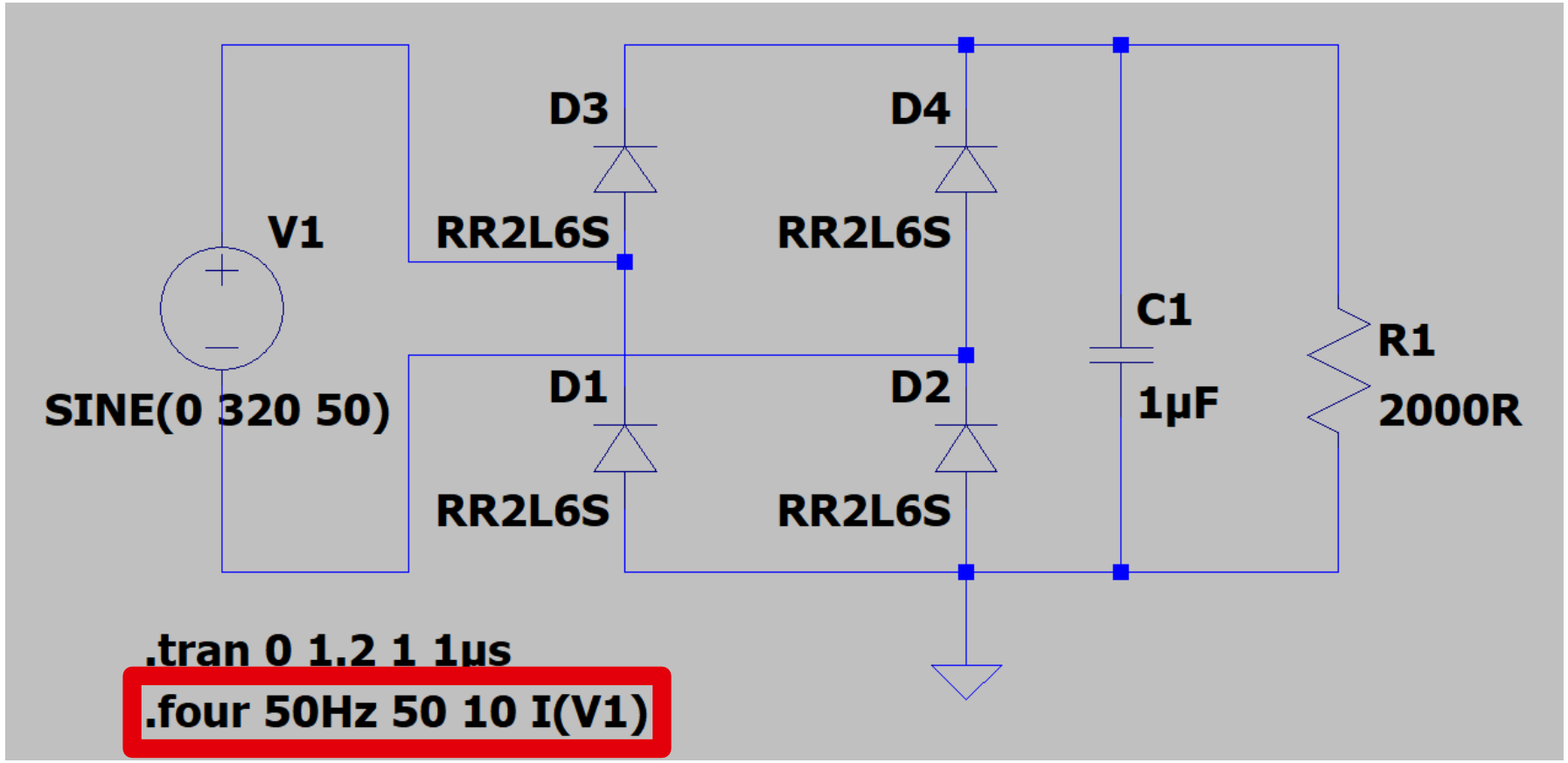
Anticipate IEC 61000-3-2

Harmonic order (n)	Maximum permissible harmonic current per watt (mA/W)
3	3.4
5	1.9
7	1.0
9	0.5
11	0.35
13	0.3
$15 \leq n \leq 39$ (odd harmonics only)	3.85/n



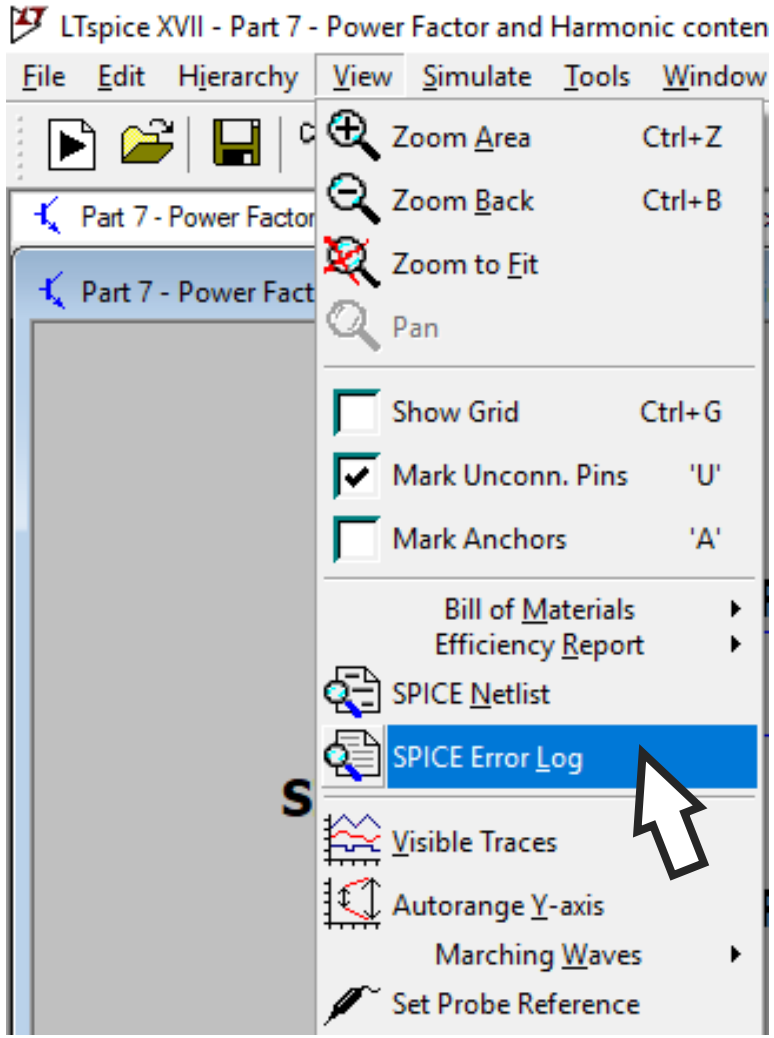
Power Factor and Harmonic current

.FOUR directive to Anticipate IEC 61000-3-2



Power Factor and Harmonic current

.FOUR directive to Anticipate IEC 61000-3-2



SPICE Error Log: C:\Users\sylvain.lebras\Docu

Ampera

Fraction of fundamental

nonic content - Class D limit.log

```
Fourier components of I(v1)
DC component:5.23172e-007

Harmonic      Frequency      Fourier       Normalized      Phase        Normalized
 Number         [Hz]        Component      Component     [degree]     Phase [deg]
    1        5.000e+01      1.760e-01      1.000e+00     -156.56°        0.00°
    2        1.000e+02      3.265e-07      1.855e-06       57.75°      214.31°
    3        1.500e+02      2.687e-02      1.526e-01      102.46°      259.01°
    4        2.000e+02      1.123e-06      6.379e-06        2.94°      159.50°
    5        2.500e+02      2.074e-02      1.178e-01      108.42°      264.98°
    6        3.000e+02      2.040e-07      1.159e-06     -164.89°       -8.33°
    7        3.500e+02      1.391e-02      7.904e-02      108.04°      264.59°
    8        4.000e+02      9.960e-07      5.658e-06      -63.52°       93.04°
    9        4.500e+02      8.532e-03      4.847e-02       93.80°      250.36°
   10        5.000e+02      9.480e-07      5.386e-06      125.74°      282.30°
   11        5.500e+02      6.452e-03      3.665e-02       64.05°      220.61°
   12        6.000e+02      7.110e-07      4.039e-06     -101.44°       55.12°
   13        6.500e+02      6.362e-03      3.614e-02       41.96°      198.52°
   14        7.000e+02      1.526e-06      8.671e-06       51.93°      208.48°
   15        7.500e+02      5.865e-03      3.332e-02       29.38°      185.94°
   16        8.000e+02      4.225e-07      2.401e-06      -89.14°       67.42°
   17        8.500e+02      4.761e-03      2.705e-02       14.64°      171.20°
   18        9.000e+02      1.168e-06      6.634e-06      -50.15°      106.41°
   19        9.500e+02      3.923e-03      2.229e-02       -8.40°      148.16°
   20        1.000e+03      8.830e-07      5.016e-06     -105.51°       51.05°
   21        1.050e+03      3.752e-03      2.131e-02      -31.96°      124.60°

   45        2.250e+03      1.732e-03      9.838e-03       98.91°      255.46°
   46        2.300e+03      7.944e-07      4.513e-06      -44.86°      111.70°
   47        2.350e+03      1.685e-03      9.573e-03       77.95°      234.51°
   48        2.400e+03      1.657e-07      9.416e-07      -81.86°       74.69°
   49        2.450e+03      1.657e-03      9.412e-03       59.24°      215.79°
   50        2.500e+03      7.697e-07      4.373e-06     -107.70°       48.86°
Total Harmonic Distortion: 23.211629%(23.614123%) PF=0.893698(0.8929)
```

Power Factor and Harmonic current

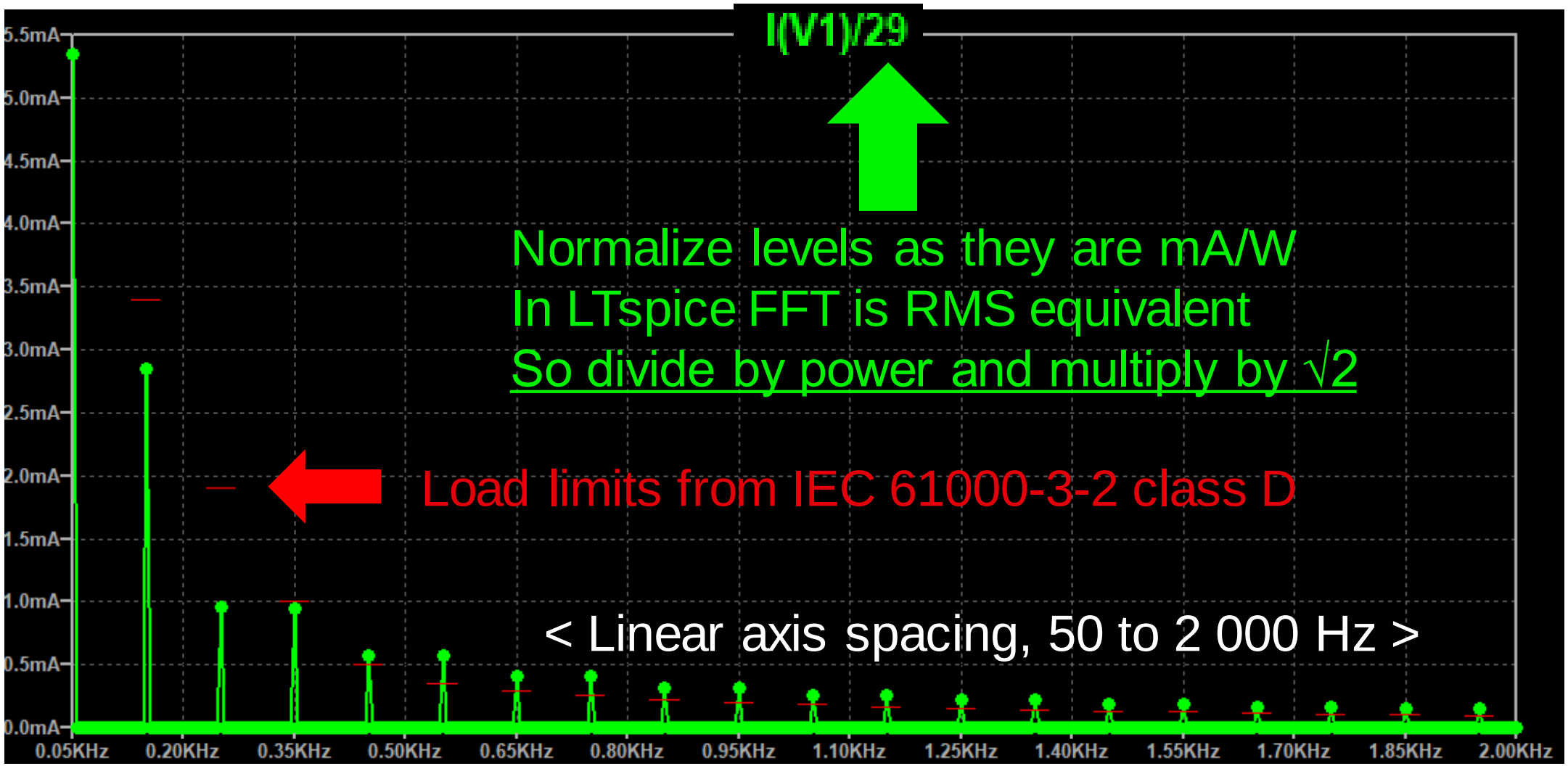
Graphical method to anticipate IEC 61000-3-2

IEC 61000-3-2 Class D - LTSpice limit line calculator

in 50Hz base		Start Freq	End Freq	mA/W start	Line def for LTSPICE plot settings file	
Line	3	130	170	3.4	Line: "A" 4 0	(130,0.0034) (170,0.0034)
Line	5	230	270	1.9	Line: "A" 4 0	(230,0.0019) (270,0.0019)
Line	7	330	370	1	Line: "A" 4 0	(330,0.001) (370,0.001)
Line	9	430	470	0.5	Line: "A" 4 0	(430,0.0005) (470,0.0005)
Line	11	530	570	0.35	Line: "A" 4 0	(530,0.00035) (570,0.00035)
Line	13	630	670	0.296153846	Line: "A" 4 0	(630,0.000296153846153846) (670,0.000296153846153846)
Line	15	730	770	0.256666667	Line: "A" 4 0	(730,0.000256666666666667) (770,0.000256666666666667)
Line	17	830	870	0.226470588	Line: "A" 4 0	(830,0.000226470588235294) (870,0.000226470588235294)
Line	19	930	970	0.202631579	Line: "A" 4 0	(930,0.000202631578947368) (970,0.000202631578947368)
Line	21	1030	1070	0.183333333	Line: "A" 4 0	(1030,0.000183333333333333) (1070,0.000183333333333333)
Line	23	1130	1170	0.167391304	Line: "A" 4 0	(1130,0.000167391304347826) (1170,0.000167391304347826)
Line	25	1230	1270	0.154	Line: "A" 4 0	(1230,0.000154) (1270,0.000154)
Line	27	1330	1370	0.142592593	Line: "A" 4 0	(1330,0.000142592592592593) (1370,0.000142592592592593)
Line	29	1430	1470	0.132758621	Line: "A" 4 0	(1430,0.000132758620689655) (1470,0.000132758620689655)
Line	31	1530	1570	0.124193548	Line: "A" 4 0	(1530,0.000124193548387097) (1570,0.000124193548387097)
Line	33	1630	1670	0.116666667	Line: "A" 4 0	(1630,0.000116666666666667) (1670,0.000116666666666667)
Line	35	1730	1770	0.11	Line: "A" 4 0	(1730,0.00011) (1770,0.00011)
Line	37	1830	1870	0.104054054	Line: "A" 4 0	(1830,0.000104054054054054) (1870,0.000104054054054054)
Line	39	1930	1970	0.098717949	Line: "A" 4 0	(1930,9.87179487179487E-05) (1970,9.87179487179487E-05)

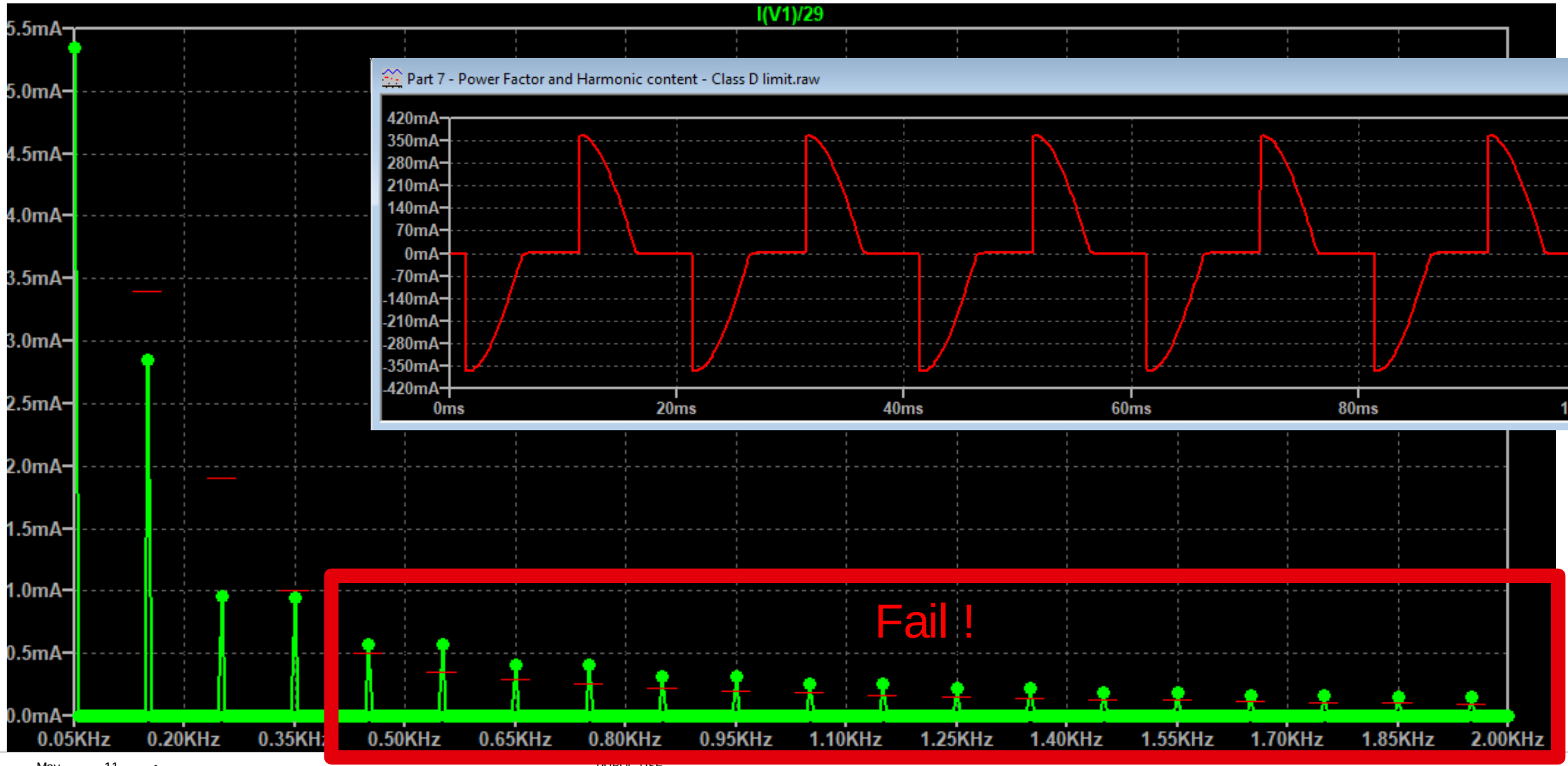
Power Factor and Harmonic current

Graphical method to anticipate IEC 61000-3-2



Power Factor and Harmonic current

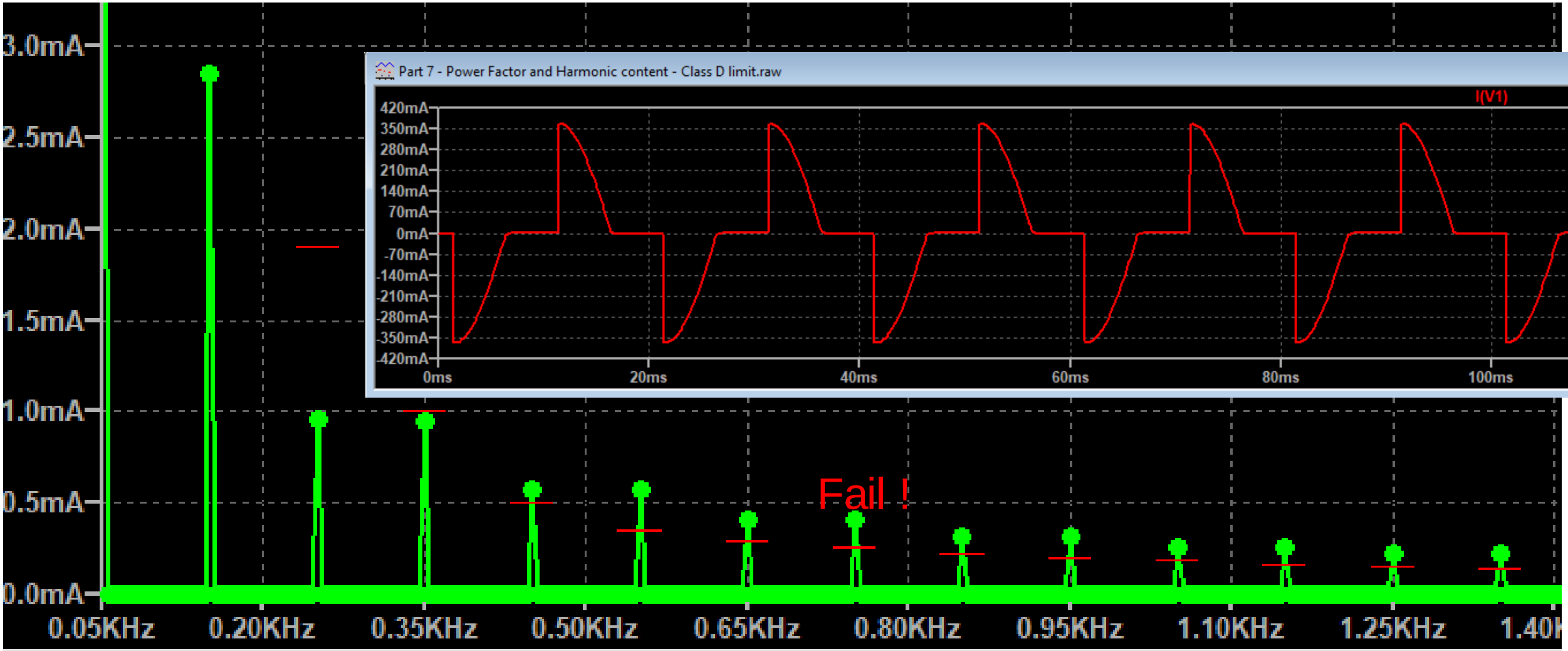
Graphical method to anticipate IEC 61000-3-2



Power Factor and Harmonic current

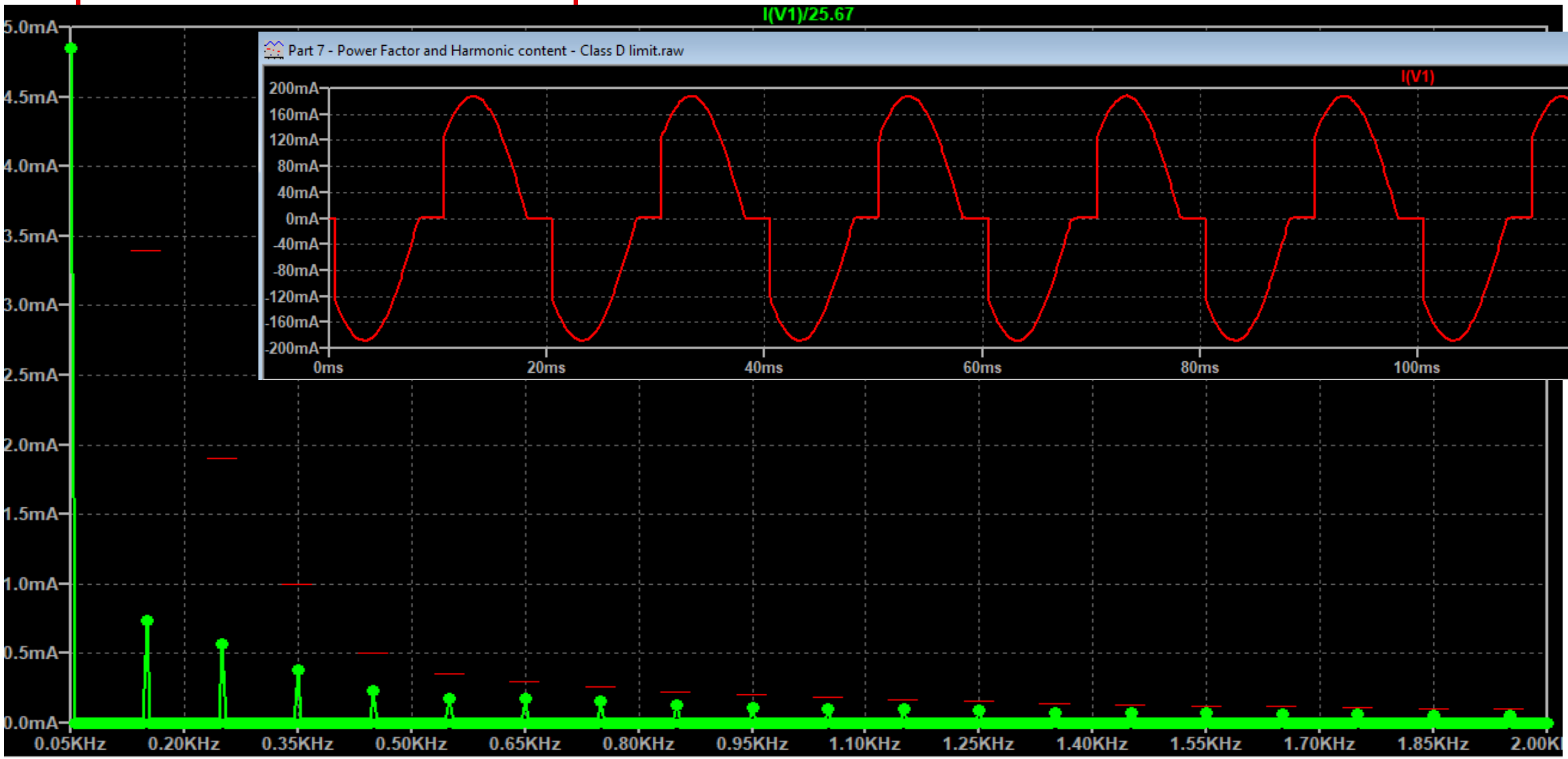
Graphical method to anticipate IEC 61000-3-2

WÜRTH ELEKTRONIK



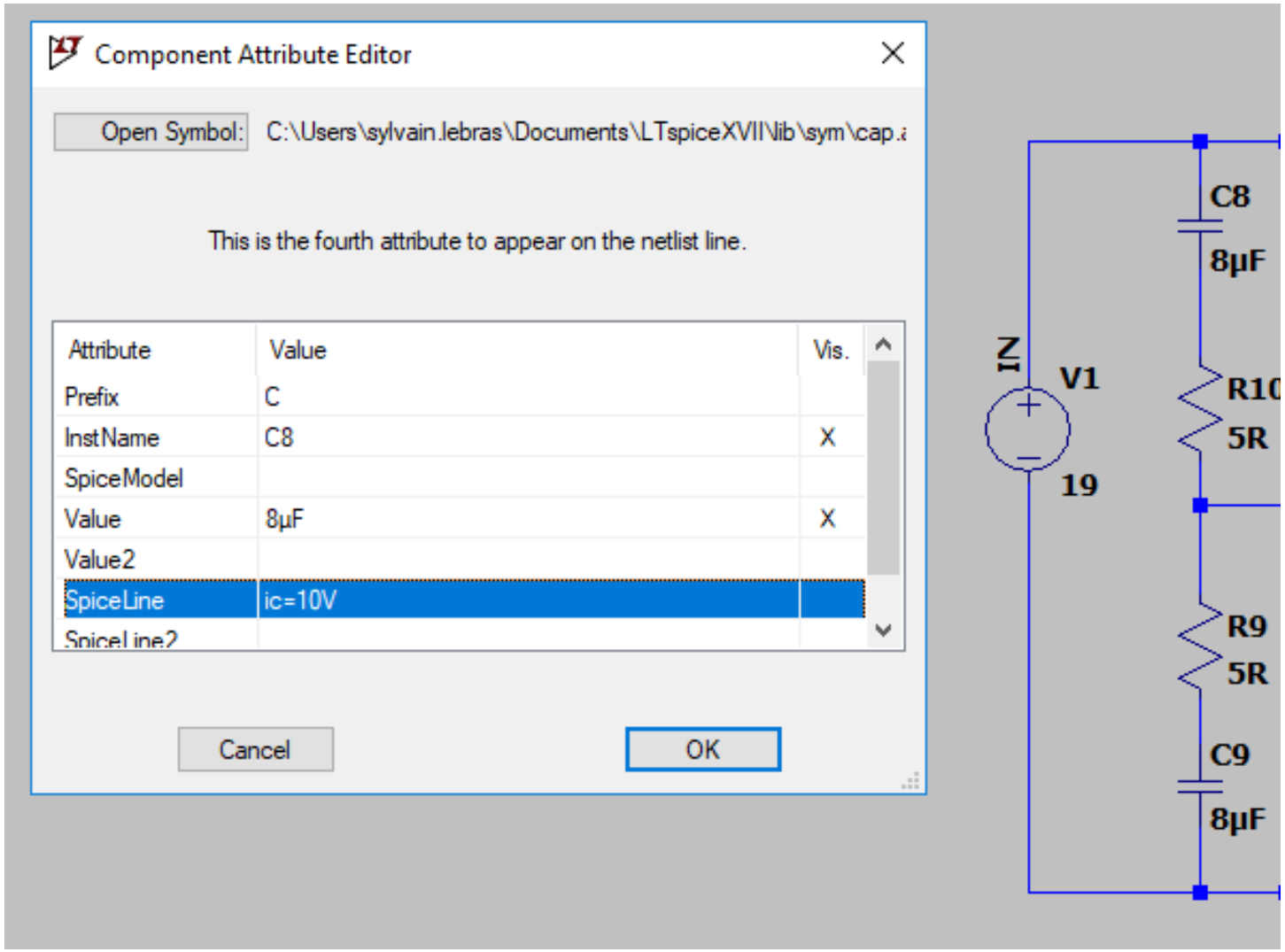
Power Factor and Harmonic current

Graphical method to anticipate IEC 61000-3-2



Good to know

Speed up simulations



Setting initial condition

- Ctrl + Right Click
- SpiceLine
  - ic=10V